

**National Aeronautics and
Space Administration**

YAV-8B Simulation and Modeling Volume II: Program Listing

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McDonnell Aircraft Company
St. Louis, Missouri 63166

Prepared for
Ames Research Center
Dryden Flight Research Facility
under Contract NAS4-2839

1983



National Aeronautics and
Space Administration

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1. INTRODUCTION AND SUMMARY

As part of its V/STOL research program, NASA intends to conduct flight investigations of the stability, control and handling qualities of highly augmented V/STOL aircraft. Specific plans include the flight tests of a YAV-8B aircraft modified to include an advanced avionics and flight control system for improving flying qualities and performance.

As an initial phase to this program, NASA will conduct flight tests of the YAV-8B vehicle in order to extract aerodynamic and propulsion characteristics, update existing simulation models, validate handling qualities and design criteria, and to improve V/STOL flight test techniques. This program will also include tests using a static test stand located at the Dryden Flight Research Center, where flight tests of the YAV-8B will take place.

In order to perform high quality parameter estimation and analysis of the YAV-8B characteristics, it is necessary to construct mathematical models of varying complexity and linearity from existing wind tunnel and flight test data.

The McDonnell Aircraft Company (MCAIR) recently completed a V/STOL simulation and modeling study under contract to NASA Dryden. This study defined and documented detailed mathematical models of varying complexity representative of the YAV-8B aircraft. These models will be used by NASA in parameter estimation and in linear analysis computer programs while investigating YAV-8B aircraft handling qualities. Both a six degree of freedom nonlinear model and a linearized three degree of freedom longitudinal and lateral directional model were developed.

The nonlinear model is based on the mathematical model used on the MCAIR YAV-8B manned flight simulator. This simulator model has undergone periodic updating based on the results of approximately 360 YAV-8B flights and 8000 hours of wind tunnel testing. Qualified YAV-8B flight test pilots have commented that the handling qualities characteristics of the simulator are quite representative of the real aircraft. These comments are validated herein by comparing data from both static and dynamic flight test maneuvers to the same obtained using the nonlinear program.

The linearized mathematical model uses stability derivatives and is formatted exactly as the models traditionally used in conventional flight dynamic analysis. Aircraft characteristics were predicted using this linearized model and compared to both the flight data and the nonlinear predictions. To document the aircraft characteristics throughout the flight envelope trim conditions and stability derivatives are provided for 24 flight conditions.

A FORTRAN batch simulation of the nonlinear model has been produced. Documentation for this simulation consists of a description of the software including top level flow charts, program structure, subroutine interfaces, modeling equations, data format, a user's guide, source listings and plots of the over 17,000 aerodynamic and propulsion data points used in the model.

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Volume II

This report is divided into two volumes. Volume I contains the description of the aircraft, documentation of the nonlinear and linear mathematical models, stability derivatives, the comparisons of predicted and actual flight test data which validate the nonlinear model and a discussion of models appropriate for use in parameter estimation programs. Volume II contains the source listings for the nonlinear program and plots of the aerodynamic and propulsion data used in the nonlinear program.

APPENDIX A
YAV-8B NONLINEAR
PROGRAM LISTING

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PAGE 2

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FTN 4,9+53M

PROGRAM YAVHR 74/174 001=2

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60      *
        * 1000 CONTINUE
        * CALL STNDAY
        *
        * CDT = EDT
        * NPASS = 0
        * RUNTIME = 0.0
        * INITIAL = 1
        * IRESF = 1
        *
70      *
        * CALL I500HCF
        * INITIAL = 0
        *
        *
        *
75      *
        *
        * RESF
        *
        *
        *
80      *
        * 1100 CONTINUE
        * CDT = EDT
        * NPASS = NPASS + 1
        *
        * CALL I500H
        *
        * IF (NPASS .LT. NPASS0) GO TO 1100
        *
        * IRESF = 0
        * CALL IRTDPA
        *
        *
        *
85      *
        *
        * OPERATE
        *
        *
        *
90      *
        * 9510 FORMAT(4, START RUN NO., 15, 5X, A10)
        *
        * 1700 CONTINUE
        * CDT = EDT
        * CALL IRTDPA
        * CALL I500H
        *
        * RUNTIME = RUNTIME + EDT
        * IF (RUNTIME .GT. (15000-.0001)) GO TO 1700
        * CALL IRTDPA
        *
        *
        *
100     *
        * CALL CAPDS
        * IF (NCARDS .NE. 0) GO TO 2600
        *
        * RUN = RUN + 1
        * GO TO 1000
        *
105     *
        * 2600 CONTINUE
        *
        * END

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*****
* THIS SUBROUTINE MUST BE USED IN A 0.02 SECOND UPDATE LOOP, AND
* PROVIDES ONE 0.02 SECOND UPDATE SECTION.
* ALSO, THIS SUBROUTINE PROVIDES ALL THE ENTRY POINTS REQUIRED IN
* INTERFACE WITH PROGRAM YAWB. ONE ADDITIONAL ENTRY POINT (T60NCE)
* IS INCLUDED IN THIS SUBROUTINE FOR ONE PASS (INITIAL=1)
* INITIALIZATION.
* F-ARRAY INPUT DEFINITIONS
C FOT    BASIC UPDATE TIME INCREMENT IN SECONDS
* INITIAL INITIAL FLAG
* RESET RESET FLAG
C
* F-ARRAY OUTPUT DEFINITIONS
C COT    CURRENT UPDATE TIME INCREMENT IN SECONDS
C
*****
* COMMON STATEMENTS
*      COMMON / FARRAY / F(1001)
* EQUIVALENCE STATEMENTS
*      EQUIVALENCE
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7-175 021-2

A-6

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SUBROUTINE	ISONS	74/175	02T=2	FTN 4.0+534	07/10/77, 15.12.77	PAGE	3
115	+				15015	115	
	+				15045	116	
	+				15045	117	
120					15045	118	
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					15045	162	
					15045	163	
					15045	164	

SYMBOLIC REFERENCE MAP (R-2)

A-8

ORIGINAL PAGE 1
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5

PAGE

92/10/22, 15,12,34

FTM 4.8+538

SUBROUTINE ISOMS		74/175	OUT=2	
EXTERNALS	TYPE	ARGS	REFERENCES	140
AC07		0	134	
FSRCH		5	129	
FIB	REAL	4	130	
COMMON BLOCKS	LENGTH			
FARRAY	2000			
STATISTICS				
PROGRAM LENGTH		37318	89	
CM LABELED COMMON LENGTH		37208	2000	
CM LABELED COMMON CM USED				

SUBROUTINE AERQAT
74/1173 1101-2

A-10

07.21.1912

FILE 4.44632

SUBROUTINE AFRONT 74/175 1017=?

[illegible]

741175 DP1=2

A-12

12/10/22. 14.12.40

FORM 4-44-33

SUBROUTINE AERODAT 74/175 OPI-2

[illegible]

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SURFDEPTH	4CRD04T	74/175	00T=2	CTM 4, 44+34	07/10/2, 14, 12, 40
230	DATA (CRP0MT111)=0.11301/	-0.100, -0.245, -0.340, -0.311, -0.285, -0.245, -0.190, -0.131, -0.060, -0.020, -0.010, -0.000, -0.000/	-0.245, -0.203, -0.158, -0.100, -0.060, -0.030, -0.010, -0.000, -0.000/	-0.340, -0.245, -0.170, -0.110, -0.060, -0.040, -0.010, -0.020, -0.020/	YAF09 229 YAF09 230 YAF09 231 YAF09 232 YAF09 233 YAF09 234 YAF09 235 YAF09 236 YAF09 237 YAF09 238 YAF09 239 YAF09 240 YAF09 241 YAF09 242 YAF09 243 YAF09 244 YAF09 245 YAF09 246 YAF09 247 YAF09 248 YAF09 249 YAF09 250 YAF09 251 YAF09 252 YAF09 253 YAF09 254 YAF09 255 YAF09 256 YAF09 257 YAF09 258 YAF09 259 YAF09 260 YAF09 261 YAF09 262 YAF09 263 YAF09 264 YAF09 265 YAF09 266 YAF09 267 YAF09 268 YAF09 269 YAF09 270 YAF09 271 YAF09 272 YAF09 273 YAF09 274 YAF09 275 YAF09 276 YAF09 277 YAF09 278 YAF09 279 YAF09 280 YAF09 281 YAF09 282 YAF09 283 YAF09 284 YAF09 285
235	DATA (CRP0MT111)=0.11301/	-0.170, -0.400, -0.570, -0.530, -0.440, -0.320, -0.240, -0.170, -0.110, -0.060, -0.030, -0.010, -0.000/	-0.400, -0.385, -0.350, -0.320, -0.280, -0.240, -0.200, -0.170, -0.140, -0.110, -0.080, -0.060, -0.040/	-0.570, -0.440, -0.320, -0.240, -0.170, -0.110, -0.060, -0.030, -0.020, -0.020, -0.020, -0.020, -0.020/	YAF09 230 YAF09 231 YAF09 232 YAF09 233 YAF09 234 YAF09 235 YAF09 236 YAF09 237 YAF09 238 YAF09 239 YAF09 240 YAF09 241 YAF09 242 YAF09 243 YAF09 244 YAF09 245 YAF09 246 YAF09 247 YAF09 248 YAF09 249 YAF09 250 YAF09 251 YAF09 252 YAF09 253 YAF09 254 YAF09 255 YAF09 256 YAF09 257 YAF09 258 YAF09 259 YAF09 260 YAF09 261 YAF09 262 YAF09 263 YAF09 264 YAF09 265 YAF09 266 YAF09 267 YAF09 268 YAF09 269 YAF09 270 YAF09 271 YAF09 272 YAF09 273 YAF09 274 YAF09 275 YAF09 276 YAF09 277 YAF09 278 YAF09 279 YAF09 280 YAF09 281 YAF09 282 YAF09 283 YAF09 284 YAF09 285
240	DATA (CRP0MT111)=0.11301/	-0.310, -0.540, -0.710, -0.670, -0.580, -0.460, -0.380, -0.310, -0.240, -0.170, -0.110, -0.060, -0.030, -0.010, -0.000/	-0.540, -0.525, -0.500, -0.470, -0.440, -0.410, -0.380, -0.350, -0.320, -0.290, -0.260, -0.230, -0.200, -0.170, -0.140/	-0.710, -0.580, -0.460, -0.380, -0.310, -0.240, -0.170, -0.110, -0.060, -0.030, -0.020, -0.020, -0.020, -0.020, -0.020/	YAF09 236 YAF09 237 YAF09 238 YAF09 239 YAF09 240 YAF09 241 YAF09 242 YAF09 243 YAF09 244 YAF09 245 YAF09 246 YAF09 247 YAF09 248 YAF09 249 YAF09 250 YAF09 251 YAF09 252 YAF09 253 YAF09 254 YAF09 255 YAF09 256 YAF09 257 YAF09 258 YAF09 259 YAF09 260 YAF09 261 YAF09 262 YAF09 263 YAF09 264 YAF09 265 YAF09 266 YAF09 267 YAF09 268 YAF09 269 YAF09 270 YAF09 271 YAF09 272 YAF09 273 YAF09 274 YAF09 275 YAF09 276 YAF09 277 YAF09 278 YAF09 279 YAF09 280 YAF09 281 YAF09 282 YAF09 283 YAF09 284 YAF09 285
245	DATA (CRP0MT111)=0.11301/	-0.470, -0.700, -0.870, -0.830, -0.740, -0.620, -0.540, -0.470, -0.400, -0.330, -0.260, -0.190, -0.120, -0.060, -0.030, -0.010, -0.000/	-0.700, -0.685, -0.660, -0.630, -0.600, -0.570, -0.540, -0.510, -0.480, -0.450, -0.420, -0.390, -0.360, -0.330, -0.300, -0.270, -0.240/	-0.870, -0.740, -0.620, -0.540, -0.470, -0.400, -0.330, -0.260, -0.190, -0.120, -0.060, -0.030, -0.020, -0.020, -0.020, -0.020, -0.020/	YAF09 240 YAF09 241 YAF09 242 YAF09 243 YAF09 244 YAF09 245 YAF09 246 YAF09 247 YAF09 248 YAF09 249 YAF09 250 YAF09 251 YAF09 252 YAF09 253 YAF09 254 YAF09 255 YAF09 256 YAF09 257 YAF09 258 YAF09 259 YAF09 260 YAF09 261 YAF09 262 YAF09 263 YAF09 264 YAF09 265 YAF09 266 YAF09 267 YAF09 268 YAF09 269 YAF09 270 YAF09 271 YAF09 272 YAF09 273 YAF09 274 YAF09 275 YAF09 276 YAF09 277 YAF09 278 YAF09 279 YAF09 280 YAF09 281 YAF09 282 YAF09 283 YAF09 284 YAF09 285
250	DATA (CRP0MT111)=0.11301/	-0.630, -0.860, -1.030, -0.990, -0.900, -0.780, -0.700, -0.630, -0.560, -0.490, -0.420, -0.350, -0.280, -0.210, -0.140, -0.070, -0.030, -0.010, -0.000/	-0.860, -0.845, -0.820, -0.790, -0.760, -0.730, -0.700, -0.670, -0.640, -0.610, -0.580, -0.550, -0.520, -0.490, -0.460, -0.430, -0.400, -0.370, -0.340/	-1.030, -0.900, -0.780, -0.700, -0.630, -0.560, -0.490, -0.420, -0.350, -0.280, -0.210, -0.140, -0.070, -0.030, -0.020, -0.020, -0.020, -0.020, -0.020/	YAF09 246 YAF09 247 YAF09 248 YAF09 249 YAF09 250 YAF09 251 YAF09 252 YAF09 253 YAF09 25

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PAGE

82/10/22, 15.12.40

FTN 4.44438

SUBROUTINE ACRDAD 74/175 DPT=2

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290      .0.160, .0.340, .0.120, .0.545, .0.680, .0.770,
      .0.025, .0.240, .0.220, .0.310, .0.380, .0.470,
      .0.030, .0.180, .0.200, .0.270, .0.350, .0.440,
      .0.035, .0.170, .0.190, .0.260, .0.340, .0.430,
      .0.020, .0.080, .0.100, .0.170, .0.250, .0.340,
      .0.020, .0.080, .0.100, .0.170, .0.250, .0.340,
      .0.020, .0.080, .0.100, .0.170, .0.250, .0.340,
      .0.020, .0.080, .0.100, .0.170, .0.250, .0.340,
      DATA (CMPIAT(I), I=197, 462)
      .0.150, .0.450, .0.880, .1.320, .1.300, .1.320,
      .0.050, .0.250, .0.370, .0.470, .0.540, .0.610,
      .0.040, .0.150, .0.250, .0.350, .0.420, .0.490,
      .0.035, .0.140, .0.240, .0.340, .0.410, .0.480,
      .0.030, .0.130, .0.230, .0.330, .0.400, .0.470,
      .0.020, .0.080, .0.100, .0.170, .0.250, .0.340,
      .0.010, .0.050, .0.050, .0.100, .0.150, .0.200,
      .0.010, .0.050, .0.050, .0.100, .0.150, .0.200,
      .0.010, .0.050, .0.050, .0.100, .0.150, .0.200,
      DATA (CMPIAT(I), I=463, 581)
      .0.050, .0.470, .0.700, .1.140, .1.40, .1.40,
      .0.050, .0.250, .0.370, .0.470, .0.540, .0.610,
      .0.040, .0.150, .0.250, .0.350, .0.420, .0.490,
      .0.035, .0.140, .0.240, .0.340, .0.410, .0.480,
      .0.030, .0.130, .0.230, .0.330, .0.400, .0.470,
      .0.020, .0.080, .0.100, .0.170, .0.250, .0.340,
      .0.010, .0.050, .0.050, .0.100, .0.150, .0.200,
      .0.010, .0.050, .0.050, .0.100, .0.150, .0.200,
      .0.010, .0.050, .0.050, .0.100, .0.150, .0.200,
      BASELINE PM (LOW SPEED), ALP=10.30, IN 2 DEG INCREMENTS
      .0.025, .0.070, .0.047, .0.026, .0.004, .0.015, .0.035,
      .0.032, .0.081, .0.106, .0.131, .0.160, .0.190, .0.225,
      .0.259, .0.294, .0.320, .0.340, .0.360, .0.420, .0.450,
      BASELINE PM (LOW SPEED), ALP=180.100, IN 10 DEG INCREMENTS
      .0.000, .0.000, .0.000, .0.000, .0.000, .0.000,
      DATA CMPIAT/
      .0.000, .0.100, .0.330, .0.450, .0.520, .0.619, .0.622,
      .0.697, .0.710, .0.725, .0.719, .0.697, .0.622, .0.619,
      .0.525, .0.440, .0.350, .0.250, .0.150, .0.050, .0.025,
      .0.019, .0.000, .0.000, .0.000, .0.000, .0.000, .0.000,
      .0.140, .0.000, .0.000, .0.000, .0.000, .0.000, .0.000,
      INCREMENTAL PM DUE TO FLAP DEFLECTION, PER FLAP (LOW SPEED)
      ALP=4.28 IN 4 DEG INCR AND DELAP=0.40, IN 20 DEG INCR
      DATA CMPIAT/
      .000.0,
  
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02/10/22. 15.12.40

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761875 1107 = ?

SUBROUTINE AERUDAT

[illegible]

4218.1122. 16.12.41

015 4040 40

SUBROUTINE AFKDDAT 740175 :01=2

[illegible]

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[illegible]

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07.1.51. 221012H

74/17, 101-2

AXIAL FORCE DUE TO POWER EFFECTS; $\Delta P = -4.24$ IN 4 DEG INCR; $VFO = -0.570$ IN -0.5 INCR FOR THEIAJ.25 DEG

[illegible]

DATA CRYSTAL	BASELINE STD. FORCE DUE TO H ₂ O (LOW RTAS), 2--4, 24 IN 4 DEG INCR AND DELTA=0.25, DEG
-0.01801	-0.01833, -0.01468, -0.01473, -0.01657,
-0.01801	-0.01504, -0.01440, -0.01440, -0.01700,
-0.01777	-0.02040, -0.02140, -0.02090, -0.01700,
-0.01572	-0.01440, -0.01440, -0.01440, -0.01700,

BASELINE SIDE FORCE DUE TO BETA (H) BETAS) 2=-4.24 IN 4 DEG INCR
DATA DCYHIT/
.. 0.0076, 0.00965, 0.00980, 0.01050, 0.01220, 0.01260,
.. 0.01290, 0.01303/
POWER EFFECTS ON CY9, VEQ=0.4 IN .05 INCR AND ALP=-4.24.

[illegible]

DATA CYCLES:
0.0370, 0.0345, 0.0333, 0.0233, 0.0142, 0.0055, -0.0003, -0.0177,
-0.0300 IN 4, OFC INCR
SIDE FORCE DUE TO AIRFRON DEF., ALP = 4.24 IN 4, OFC INCR AND DAE

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PAGE 13

8/10/22, 1-12-40

FIN 4.4+538

74/175, 001-2

SUMROUTINE ALRODAY

695	.0440, .0418, .0402, .0314, .0234, .0173, .0115, .0044,	VAF01	695
	.0477, .0460, .0453, .0362, .0297, .0243, .0195, .0140,	VAF02	696
	.0451, .0457, .0450, .0360, .0323, .0275, .0233, .0165,	VAF03	697
	.0400, .0380, .0370, .0300, .0270, .0230, .0200, .0130,	VAF04	698
	.0200, .0190, .0185, .0150, .0135, .0115, .0100, .0065,	VAF05	699
690	.0190, .0185, .0180, .0150, .0135, .0115, .0100, .0065,	VAF06	700
	.0190, .0185, .0180, .0150, .0135, .0115, .0100, .0065,	VAF07	701
	.0190, .0185, .0180, .0150, .0135, .0115, .0100, .0065,	VAF08	702
	.0190, .0185, .0180, .0150, .0135, .0115, .0100, .0065,	VAF09	703
695	.0190, .0185, .0180, .0150, .0135, .0115, .0100, .0065,	VAF10	704
	.0190, .0185, .0180, .0150, .0135, .0115, .0100, .0065,	VAF11	705
	.0190, .0185, .0180, .0150, .0135, .0115, .0100, .0065,	VAF12	706
	.0190, .0185, .0180, .0150, .0135, .0115, .0100, .0065,	VAF13	707
700	.0190, .0185, .0180, .0150, .0135, .0115, .0100, .0065,	VAF14	708
	.0190, .0185, .0180, .0150, .0135, .0115, .0100, .0065,	VAF15	709
	.0190, .0185, .0180, .0150, .0135, .0115, .0100, .0065,	VAF16	710
	.0190, .0185, .0180, .0150, .0135, .0115, .0100, .0065,	VAF17	711
705	.0190, .0185, .0180, .0150, .0135, .0115, .0100, .0065,	VAF18	712
	.0190, .0185, .0180, .0150, .0135, .0115, .0100, .0065,	VAF19	713
	.0190, .0185, .0180, .0150, .0135, .0115, .0100, .0065,	VAF20	714
	.0190, .0185, .0180, .0150, .0135, .0115, .0100, .0065,	VAF21	715
710	.0190, .0185, .0180, .0150, .0135, .0115, .0100, .0065,	VAF22	716
	.0190, .0185, .0180, .0150, .0135, .0115, .0100, .0065,	VAF23	717
	.0190, .0185, .0180, .0150, .0135, .0115, .0100, .0065,	VAF24	718
	.0190, .0185, .0180, .0150, .0135, .0115, .0100, .0065,	VAF25	719
715	.0190, .0185, .0180, .0150, .0135, .0115, .0100, .0065,	VAF26	720
	.0190, .0185, .0180, .0150, .0135, .0115, .0100, .0065,	VAF27	721
	.0190, .0185, .0180, .0150, .0135, .0115, .0100, .0065,	VAF28	722
	.0190, .0185, .0180, .0150, .0135, .0115, .0100, .0065,	VAF29	723
720	.0190, .0185, .0180, .0150, .0135, .0115, .0100, .0065,	VAF30	724
	.0190, .0185, .0180, .0150, .0135, .0115, .0100, .0065,	VAF31	725
	.0190, .0185, .0180, .0150, .0135, .0115, .0100, .0065,	VAF32	726
	.0190, .0185, .0180, .0150, .0135, .0115, .0100, .0065,	VAF33	727
725	.0190, .0185, .0180, .0150, .0135, .0115, .0100, .0065,	VAF34	728
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730	.0190, .0185, .0180, .0150, .0135, .0115, .0100, .0065,	VAF38	732
	.0190, .0185, .0180, .0150, .0135, .0115, .0100, .0065,	VAF39	733
	.0190, .0185, .0180, .0150, .0135, .0115, .0100, .0065,	VAF40	734
	.0190, .0185, .0180, .0150, .0135, .0115, .0100, .0065,	VAF41	735
735	.0190, .0185, .0180, .0150, .0135, .0115, .0100, .0065,	VAF42	736
	.0190, .0185, .0180, .0150, .0135, .0115, .0100, .0065,	VAF43	737
	.0190, .0185, .0180, .0150, .0135, .0115, .0100, .0065,	VAF44	738
	.0190, .0185, .0180, .0150, .0135, .0115, .0100, .0065,	VAF45	739
740	.0190, .0185, .0180, .0150, .0135, .0115, .0100, .0065,	VAF46	740
	.0190, .0185, .0180, .0150, .0135, .0115, .0100, .0065,	VAF47	741

APR 10 1955. 14.12.50

ملفوظات

741175 10152

SHARDYNE AFRONT

[illegible]

SUBJECT: THE AFRO

A-25

07-01-15, 15:20

05.04.5. 113

SUBROUTINE AFQ00AT 74/11/5 QPI=2

INCREASING NOZZLE EQUIVALENT NOZZLE EXIT DIAMETER IN 4 DEG INCR, HT=0.12 IN 1 FT INCR AND 2.154 IN 10 FT INCR	DATA(CNCF55) I=1.001/	DATA(CNCF55) I=1.001/
0.0500	0.0300	0.0500
0.0150	0.0400	0.0150
0.0155	0.0155	0.0155
0.0125	0.0095	0.0125
0.0120	0.0090	0.0120
0.0050	0.0095	0.0050
0.0055	0.0175	0.0055
0.0090	0.0090	0.0090
0.0150	0.0070	0.0150
0.0155	0.0170	0.0155
0.0125	0.0090	0.0125
0.0120	0.0090	0.0120
0.0050	0.0150	0.0050
0.0055	0.0150	0.0055
0.0090	0.0150	0.0090
0.0150	0.0150	0.0150
0.0155	0.0150	0.0155
0.0125	0.0150	0.0125
0.0120	0.0150	0.0120
0.0050	0.0150	0.0050
0.0055	0.0150	0.0055
0.0090	0.0150	0.0090
0.0150	0.0150	0.0150
0.0155	0.0150	0.0155
0.0125	0.0150	0.0125
0.0120	0.0150	0.0120
0.0050	0.0150	0.0050
0.0055	0.0150	0.0055
0.0090	0.0150	0.0090
0.0150	0.0150	0.0150
0.0155	0.0150	0.0155
0.0125	0.0150	0.0125
0.0120	0.0150	0.0120
0.0050	0.0150	0.0050
0.0055	0.0150	0.0055
0.0090	0.0150	0.0090
0.0150	0.0150	0.0150
0.0155	0.0150	0.0155
0.0125	0.0150	0.0125
0.0120	0.0150	0.0120
0.0050	0.0150	0.0050
0.0055	0.0150	0.0055
0.0090	0.0150	0.0090
0.0150	0.0150	0.0150
0.0155	0.0150	0.0155
0.0125	0.0150	0.0125
0.0120	0.0150	0.0120
0.0050	0.0150	0.0050
0.0055	0.0150	0.0055
0.0090	0.0150	0.0090
0.0150	0.0150	0.0150
0.0155	0.0150	0.0155
0.0125	0.0150	0.0125
0.0120	0.0150	0.0120
0.0050	0.0150	0.0050
0.0055	0.0150	0.0055
0.0090	0.0150	0.0090
0.0150	0.0150	0.0150
0.0155	0.0150	0.0155
0.0125	0.0150	0.0125
0.0120	0.0150	0.0120
0.0050	0.0150	0.0050
0.0055	0.0150	0.0055
0.0090	0.0150	0.0090
0.0150	0.0150	0.0150
0.0155	0.0150	0.0155
0.0125	0.0150	0.0125
0.0120	0.0150	0.0120
0.0050	0.0150	0.0050
0.0055	0.0150	0.0055
0.0090	0.0150	0.0090
0.0150	0.0150	0.0150
0.0155	0.0150	0.0155
0.0125	0.0150	0.0125
0.0120	0.0150	0.0120
0.0050	0.0150	0.0050
0.0055	0.0150	0.0055
0.0090	0.0150	0.0090
0.0150	0.0150	0.0150
0.0155	0.0150	0.0155
0.0125	0.0150	0.0125
0.0120	0.0150	0.0120
0.0050	0.0150	0.0050
0.0055	0.0150	0.0055
0.0090	0.0150	0.0090
0.0150	0.0150	0.0150
0.0155	0.0150	0.0155
0.0125	0.0150	0.0125
0.0120	0.0150	0.0120
0.0050	0.0150	0.0050
0.0055	0.0150	0.0055
0.0090	0.0150	0.0090
0.0150	0	

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SUBROUTINE AERODAT	74/175	04T=2	FTN 4,04534	P2/10/22, 15.15.40	PAGE	14
970	.0624	.0445	.0740	.0480	VAE00	970
	.0595	.0400	.0710	.0460	VAE01	971
	.0425	.0530	.0610	.0410	VAE02	972
975	.0435	.0440	.0515	.0420	VAE03	973
	.0352	.0335	.0410	.0320	VAE04	974
	.0275	.0230	.0300	.0255	VAE05	975
	.0197	.0125	.0190	.0220	VAE06	976
	.0155	.0062	.0130	.0140	VAE07	977
	.0060	.0010	.0030	.0070	VAE08	978
980	.0010	0.	.0002	.0035	VAE09	979
	.0007	.0000	.0000	.0020	VAE10	980
	.0000	.0000	.0000	.0000	VAE11	981
985	.0000	.0000	.0000	.0000	VAE12	982
	.0000	.0000	.0000	.0000	VAE13	983
	.0000	.0000	.0000	.0000	VAE14	984
	.0000	.0000	.0000	.0000	VAE15	985
	.0000	.0000	.0000	.0000	VAE16	986
	.0000	.0000	.0000	.0000	VAE17	987
	.0000	.0000	.0000	.0000	VAE18	988
	.0000	.0000	.0000	.0000	VAE19	989
990	.0000	.0000	.0000	.0000	VAE20	990
	.0000	.0000	.0000	.0000	VAE21	991
	.0000	.0000	.0000	.0000	VAE22	992
	.0000	.0000	.0000	.0000	VAE23	993
	.0000	.0000	.0000	.0000	VAE24	994
995	.0000	.0000	.0000	.0000	VAE25	995
	.0000	.0000	.0000	.0000	VAE26	996
	.0000	.0000	.0000	.0000	VAE27	997
	.0000	.0000	.0000	.0000	VAE28	998
	.0000	.0000	.0000	.0000	VAE29	999
1000	.0000	.0000	.0000	.0000	VAE30	1000
	.0000	.0000	.0000	.0000	VAE31	1001
	.0000	.0000	.0000	.0000	VAE32	1002
1005	.0000	.0000	.0000	.0000	VAE33	1003
	.0000	.0000	.0000	.0000	VAE34	1004
	.0000	.0000	.0000	.0000	VAE35	1005
	.0000	.0000	.0000	.0000	VAE36	1006
	.0000	.0000	.0000	.0000	VAE37	1007
1010	.0000	.0000	.0000	.0000	VAE38	1008
	.0000	.0000	.0000	.0000	VAE39	1009
	.0000	.0000	.0000	.0000	VAE40	1010
	.0000	.0000	.0000	.0000	VAE41	1011
	.0000	.0000	.0000	.0000	VAE42	1012
1015	.0000	.0000	.0000	.0000	VAE43	1013
	.0000	.0000	.0000	.0000	VAE44	1014
	.0000	.0000	.0000	.0000	VAE45	1015
	.0000	.0000	.0000	.0000	VAE46	1016
	.0000	.0000	.0000	.0000	VAE47	1017
1020	.0000	.0000	.0000	.0000	VAE48	1018
	.0000	.0000	.0000	.0000	VAE49	1019
	.0000	.0000	.0000	.0000	VAE50	1020
	.0000	.0000	.0000	.0000	VAE51	1021
	.0000	.0000	.0000	.0000	VAE52	1022
1025	.0000	.0000	.0000	.0000	VAE53	1023
	.0000	.0000	.0000	.0000	VAE54	1024
	.0000	.0000	.0000	.0000	VAE55	1025
	.0000	.0000	.0000	.0000	VAE56	1026

AXIAL FORCE COEFFICIENT INCREMENT IN GROUND EFFECT
IN 1 FT INCR AND 0.22 IN 2 FT
INCR. VFA=0.15, 0.2, 0.25

10e5	10e6	10e7	10e8	10e9	10e10	10e11	10e12	10e13	10e14	10e15	10e16	10e17	10e18	10e19	10e20	10e21	10e22	10e23	10e24	10e25	10e26	10e27	10e28	10e29	10e30	10e31	10e32	10e33	10e34	10e35	10e36	10e37	10e38	10e39	10e40	10e41	10e42	10e43	10e44	10e45	10e46	10e47	10e48	10e49	10e50	10e51	10e52	10e53	10e54	10e55	10e56	10e57	10e58	10e59	10e60	10e61	10e62	10e63	10e64	10e65	10e66	10e67	10e68	10e69	10e70	10e71	10e72	10e73	10e74	10e75	10e76	10e77	10e78	10e79	10e80	10e81	10e82	10e83	10e84	10e85	10e86	10e87	10e88	10e89	10e90	10e91	10e92	10e93	10e94	10e95	10e96	10e97	10e98	10e99	10e100	10e101	10e102	10e103	10e104	10e105	10e106	10e107	10e108	10e109	10e110	10e111	10e112	10e113	10e114	10e115	10e116	10e117	10e118	10e119	10e120	10e121	10e122	10e123	10e124	10e125	10e126	10e127	10e128	10e129	10e130	10e131	10e132	10e133	10e134	10e135	10e136	10e137	10e138	10e139	10e140	10e141	10e142	10e143	10e144	10e145	10e146	10e147	10e148	10e149	10e150	10e151	10e152	10e153	10e154	10e155	10e156	10e157	10e158	10e159	10e160	10e161	10e162	10e163	10e164	10e165	10e166	10e167	10e168	10e169	10e170	10e171	10e172	10e173	10e174	10e175	10e176	10e177	10e178	10e179	10e180	10e181	10e182	10e183	10e184	10e185	10e186	10e187	10e188	10e189	10e190	10e191	10e192	10e193	10e194	10e195	10e196	10e197	10e198	10e199	10e200	10e201	10e202	10e203	10e204	10e205	10e206	10e207	10e208	10e209	10e210	10e211	10e212	10e213	10e214	10e215	10e216	10e217	10e218	10e219	10e220	10e221	10e222	10e223	10e224	10e225	10e226	10e227	10e228	10e229	10e230	10e231	10e232	10e233	10e234	10e235	10e236	10e237	10e238	10e239	10e240	10e241	10e242	10e243	10e244	10e245	10e246	10e247	10e248	10e249	10e250	10e251	10e252	10e253	10e254	10e255	10e256	10e257	10e258	10e259	10e260	10e261	10e262	10e263	10e264	10e265	10e266	10e267	10e268	10e269	10e270	10e271	10e272	10e273	10e274	10e275	10e276	10e277	10e278	10e279	10e280	10e281	10e282	10e283	10e284	10e285	10e286	10e287	10e288	10e289	10e290	10e291	10e292	10e293	10e294	10e295	10e296	10e297	10e298	10e299	10e300	10e301	10e302	10e303	10e304	10e305	10e306	10e307	10e308	10e309	10e310	10e311	10e312	10e313	10e314	10e315	10e316	10e317	10e318	10e319	10e320	10e321	10e322	10e323	10e324	10e325	10e326	10e327	10e328	10e329	10e330	10e331	10e332	10e333	10e334	10e335	10e336	10e337	10e338	10e339	10e340	10e341	10e342	10e343	10e344	10e345	10e346	10e347	10e348	10e349	10e350	10e351	10e352	10e353
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SUBROUTINE AERD04T 74/175 021=2

A-31

09-01-01 2011/09

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SUBROUTINE AFPOOAT
75/17% 10Y=2

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SUBROUTINE AIRRNDAT 74/175 MPI=2          FPN 4.8+138          22/10/72, 16.12.49          26
*
*  RFTA - 0 TO 24, 2 DEGREE INCREMENTS
*  DATA(PM2=470(1),1-1,911) /
*  1430  1.000, -.027, -.345, -.110, -.132, -.163, -.150, -.217,
*        1.245, -.275, -.300, -.325, -.160, -.210, -.250, -.333,
*        1.000, -.042, -.085, -.125, -.160, -.200, -.240, -.333,
*        1.375, -.415, -.460, -.500, -.540, -.580, -.620, -.700,
*        1.000, -.055, -.110, -.165, -.220, -.277, -.330, -.385, -.440,
*        1.495, -.550, -.605, -.660, -.715, -.770, -.825, -.880,
*        1.000, -.060, -.120, -.180, -.240, -.295, -.355, -.417, -.472,
*        1.532, -.570, -.610, -.650, -.690, -.735, -.785, -.835,
*        1.000, -.070, -.140, -.210, -.280, -.345, -.413, -.480, -.540,
*        1.620, -.690, -.760, -.830, -.895, -.965, -.100, -.165,
*        1.000, -.077, -.150, -.223, -.295, -.368, -.442, -.513, -.585,
*        1.660, -.737, -.805, -.880, -.950, -.100, -.165,
*        1.000, -.075, -.140, -.210, -.282, -.350, -.420, -.490, -.560,
*        1.700, -.700, -.765, -.835,
*        1.625, -.700, -.765, -.835,
*
*  *****
*  *  YAMING MOMENT - (ON SPEED)
*  *****
*
*  YMTDF/RFTA AT NOZZLES = 00 (DEG) AS A FUNCTION OF :
*  1450  ALPHA (DEG)  -4 TO 24, 2 DEGREE INCREMENTS
*        ALT (FT)    70.0
*        VELOC       .05(1A), .095(1B), .247(1C)
*
*  DATA(YMTDFRFTA(1),1-1,451) /
*  1455  A 1.00114, +.00170, +.00162, +.00155, +.00152, +.00135, +.00122,
*        A 1.00110, +.00094, +.00080, +.00068, +.00054, +.00039, +.00020,
*        A 1.00000, +.00065, +.00048, +.00032, +.00018, +.00005, +.00000,
*        B 1.00310, +.00165, +.00278, +.00512, +.00408, +.00705, +.00770,
*        B 1.00415, +.00285, +.00570, +.00440, +.00308, +.00195, +.00095,
*        C 1.02315, +.02460, +.02940, +.03255, +.03450, +.03300, +.02980,
*        C 1.02645, +.02360, +.02225, +.02170, +.02125, +.02090, +.02067,
*        C 1.02050 /
*
*  YMTDF/RFTA AT NOZZLES = 60 (DEG) AS A FUNCTION OF :
*  1465  ALPHA (DEG)  -4 TO 24, 2 DEGREE STEPS
*        ALT (FT)    70.0
*        VELOC       .03(1A), .095(1B), .247(1C)
*
*  DATA(YMTDFRFTA(1),1-1,451) /
*  1470  A 1.00130, +.00140, +.00130, +.00118, +.00107, +.00102, +.00099,
*        A 1.00130, +.00084, +.00076, +.00068, +.00060, +.00050, +.00040,
*        A 1.00030, +.00020, +.00020, +.00020, +.00020, +.00020, +.00020,
*        B 1.00220, +.00242, +.00292, +.00340, +.00440, +.00510, +.00550,
*        B 1.00560, +.00535, +.00485, +.00438, +.00338, +.00270, +.00180,
*        C 1.03000,
*        C 1.01370, +.01800, +.02200, +.02617, +.02965, +.03288, +.03480,
*        C 1.03575, +.03112, +.02950, +.02538, +.02022, +.01400, +.00960,
*        C 1.00330 /
*
*  YMTDF/RFTA AT NOZZLES = 91 (DEG) AS A FUNCTION OF :

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PAGE

1770 1775 1780 1785 1790 1795 1800 1805 1810 1815 1820

FTN 4, 9, 13, 14

SUBROUTINE AFRONT 74/175 DAT=2

* DELTA(YM/TDE)/DELTA(G) AT NOZZLES = H1 (DEG) AS A FUNCTION OF :
* ALPHA(100) = 1.20(1), 4.12(2), 7.05(3)
* ALT (FT) .05(4), .05(8), .07(16), .09(32)
* VFE

DATA(YMGE01H1), 1.1(5) /
1 1 .00060, .00054, .00001, .00017, .00020, .00013, .00009,
1 1 .00018, .00024, .00018, .00018, .00019, .00018, .00018,
1 1 .00018, .00019, .00019, .00019, .00019, .00019, .00019,
2 1 .00012, .00012, .00012, .00012, .00012, .00012, .00012,
2 1 .00012, .00012, .00012, .00012, .00012, .00012, .00012,
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3 1 .00012, .00012, .00012, .00012, .00012, .00012, .00012,

DATA(YMGE01H1), 1.1(5) /
1 1 .00012, .00012, .00012, .00012, .00012, .00012, .00012,
1 1 .00012, .00012, .00012, .00012, .00012, .00012, .00012,
1 1 .00012, .00012, .00012, .00012, .00012, .00012, .00012,
2 1 .00012, .00012, .00012, .00012, .00012, .00012, .00012,
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3 1 .00012, .00012, .00012, .00012, .00012, .00012, .00012,

DATA(YMGE01H1), 1.1(5) /
1 1 .00012, .00012, .00012, .00012, .00012, .00012, .00012,
1 1 .00012, .00012, .00012, .00012, .00012, .00012, .00012,
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2 1 .00012, .00012, .00012, .00012, .00012, .00012, .00012,
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3 1 .00012, .00012, .00012, .00012, .00012, .00012, .00012,
3 1 .00012, .00012, .00012, .00012, .00012, .00012, .00012,

DATA(YMGE01H1), 1.1(5) /
1 1 .00012, .00012, .00012, .00012, .00012, .00012, .00012,
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2 1 .00012, .00012, .00012, .00012, .00012, .00012, .00012,
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3 1 .00012, .00012, .00012, .00012, .00012, .00012, .00012,

DATA(YMGE01H1), 1.1(5) /
1 1 .00012, .00012, .00012, .00012, .00012, .00012, .00012,
1 1 .00012, .00012, .00012, .00012, .00012, .00012, .00012,
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2 1 .00012, .00012, .00012, .00012, .00012, .00012, .00012,
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3 1 .00012, .00012, .00012, .00012, .00012, .00012, .00012,

DATA(YMGE01H1), 1.1(5) /
1 1 .00012, .00012, .00012, .00012, .00012, .00012, .00012,
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2 1 .00012, .00012, .00012, .00012, .00012, .00012, .00012,
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3 1 .00012, .00012, .00012, .00012, .00012, .00012, .00012,
3 1 .00012, .00012, .00012, .00012, .00012, .00012, .00012,

DATA(YMGE01H1), 1.1(5) /
1 1 .00012, .00012, .00012, .00012, .00012, .00012, .00012,
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2 1 .00012, .00012, .00012, .00012, .00012, .00012, .00012,
2 1 .00012, .00012, .00012, .00012, .00012, .00012, .00012,
3 1 .00012, .00012, .00012, .00012, .00012, .00012, .00012,
3 1 .00012, .00012, .00012, .00012, .00012, .00012, .00012,

* SIDE FORCE AND YAWING MOMENT (IN) TO PSI BREAK LINES AS A FUNCTION OF

* NOZZLES

* ALTITUDE

* K

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SUBROUTINE AERODAT		74/175	001=2	FTW 4, H, S, T, D		02/10/77, 17, 12, 60	0601	75
1940	1	+0.0000	-0.0124	-0.0000	-0.0000	-0.0000	-0.0000	1940
	2	+0.0000	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	1941
	3	+0.0000	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	1942
1945	4	+0.0000	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	1943
	5	+0.0000	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	1944
	6	+0.0000	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	1945
	7	+0.0000	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	1946
	8	+0.0000	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	1947
1950	9	+0.0000	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	1948
	10	+0.0000	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	1949
	11	+0.0000	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	1950
1955	12	+0.0000	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	1951
	13	+0.0000	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	1952
	14	+0.0000	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	1953
	15	+0.0000	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	1954
	16	+0.0000	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	1955
1960	17	+0.0000	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	1956
	18	+0.0000	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	1957
	19	+0.0000	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	1958
	20	+0.0000	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	1959
1965	21	+0.0000	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	1960
	22	+0.0000	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	1961
	23	+0.0000	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	1962
	24	+0.0000	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	1963
	25	+0.0000	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	1964
1970	26	+0.0000	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	1965
	27	+0.0000	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	1966
	28	+0.0000	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	1967
	29	+0.0000	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	1968
	30	+0.0000	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	1969
1975	31	+0.0000	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	1970
	32	+0.0000	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	1971
	33	+0.0000	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	1972
	34	+0.0000	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	1973
	35	+0.0000	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	1974
1980	36	+0.0000	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	1975
	37	+0.0000	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	1976
	38	+0.0000	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	1977
	39	+0.0000	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	1978
	40	+0.0000	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	1979
1985	41	+0.0000	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	1980
	42	+0.0000	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	1981
	43	+0.0000	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	1982
	44	+0.0000	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	1983
	45	+0.0000	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	1984
1990	46	+0.0000	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	1985
	47	+0.0000	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	1986
	48	+0.0000	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	1987
	49	+0.0000	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	1988
	50	+0.0000	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	1989
1995	51	+0.0000	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	1990
	52	+0.0000	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	1991
	53	+0.0000	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	1992
	54	+0.0000	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	1993
	55	+0.0000	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	1994
	56	+0.0000	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	1995

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SUBROUTINE AERODAT 74/175 001-2

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SUBROUTINE: AERODAT

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SUBROUTINE	AFM004	74/175	UPF=2	FIN 4.8+533	-2710722, 15.12.40	PAGE	40
2640	.133	.102	.100	.046	.305	.260	.191
	.140	.135	.133	.311	.345	.275	.222
2685	.145	.155	.145	.075	.136	.080	.072
	.0414	.111	.110	.123	.226	.130	.111
	.150	.185	.146	.215	.273	.200	.154
2690	.145	.175	.175	.040	.326	.225	.200
	.140	.165	.165	.119	.366	.261	.222
2695	.145	.138	.135	.160	.127	.083	.077
	.145	.135	.135	.160	.226	.115	.120
2700	.145	.135	.135	.160	.293	.179	.170
	.145	.135	.135	.160	.326	.220	.200
2705	.145	.135	.135	.160	.344	.240	.223
	.145	.135	.135	.160	.090	.091	.085
2710	.145	.135	.135	.160	.147	.150	.125
	.145	.135	.135	.160	.205	.145	.174
2715	.145	.135	.135	.160	.257	.236	.210
	.145	.135	.135	.160	.305	.275	.240
2720	.145	.135	.135	.160	.166	.166	.110
	.145	.135	.135	.160	.200	.160	.148
2725	.145	.135	.135	.160	.240	.210	.210
	.145	.135	.135	.160	.280	.250	.240
2730	.145	.135	.135	.160	.300	.265	.260
	.145	.135	.135	.160	.090	.102	.125
2735	.145	.135	.135	.160	.140	.152	.130
	.145	.135	.135	.160	.167	.215	.216
	.145	.135	.135	.160	.215	.248	.270

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SUBROUTINE	AFROBAT	74/175	OPT-2	FTN 4,00038	02/10/22, 15.17.40	PAGE 40
2740	+	+.330, .207, .100, .171, .155, .132, .130, .230, .200,			YAF00	2773
	+	+.050, .230, .200, .100, .155, .130, .130, .230, .200,			YAF00	2773
	+	+.050, .230, .200, .100, .155, .130, .130, .230, .200,			YAF00	2773
2745	+	DATA UCMODAT/			YAF00	2773
	+	+.120, -.061, 0.0, .000, .177,			YAF00	2773
	+	+.135, -.068, 0.0, .000, .177,			YAF00	2773
	+	+.107, -.054, 0.0, .000, .120,			YAF00	2773
	+	+.010, -.015, 0.0, .000, .120,			YAF00	2773
2750	+	PITCHING MOMENT INCREMENT DUE TO ADA RATE			YAF00	2773
	+	MAC 4-30.30 IN 15 DEG INCR, M=5.65, 8.0, 1.2			YAF00	2773
	+	DATA UCMODAT/			YAF00	2773
	+	+.120, -.061, 0.0, .000, .177,			YAF00	2773
	+	+.135, -.068, 0.0, .000, .177,			YAF00	2773
	+	+.107, -.054, 0.0, .000, .120,			YAF00	2773
	+	+.010, -.015, 0.0, .000, .120,			YAF00	2773
2755	+	PITCHING MOMENT INCREMENT DUE TO AILERONS			YAF00	2773
	+	MAC 4-30.30 IN 10 DEG INCR, ALPHA=4.25 IN 4 DEG INCR			YAF00	2773
	+	DATA UCMODAT/			YAF00	2773
	+	+.120, -.061, 0.0, .000, .177,			YAF00	2773
	+	+.135, -.068, 0.0, .000, .177,			YAF00	2773
	+	+.107, -.054, 0.0, .000, .120,			YAF00	2773
	+	+.010, -.015, 0.0, .000, .120,			YAF00	2773
2760	+	PITCHING MOMENT INCREMENT DUE TO ADA RATE			YAF00	2773
	+	MAC 4-30.30 IN 15 DEG INCR, M=5.65, 8.0, 1.2			YAF00	2773
	+	DATA UCMODAT/			YAF00	2773
	+	+.120, -.061, 0.0, .000, .177,			YAF00	2773
	+	+.135, -.068, 0.0, .000, .177,			YAF00	2773
	+	+.107, -.054, 0.0, .000, .120,			YAF00	2773
	+	+.010, -.015, 0.0, .000, .120,			YAF00	2773
2765	+	PITCHING MOMENT INCREMENT DUE TO AILERONS			YAF00	2773
	+	MAC 4-30.30 IN 10 DEG INCR, ALPHA=4.25 IN 4 DEG INCR			YAF00	2773
	+	DATA UCMODAT/			YAF00	2773
	+	+.120, -.061, 0.0, .000, .177,			YAF00	2773
	+	+.135, -.068, 0.0, .000, .177,			YAF00	2773
	+	+.107, -.054, 0.0, .000, .120,			YAF00	2773
	+	+.010, -.015, 0.0, .000, .120,			YAF00	2773
2770	+	PITCHING MOMENT INCREMENT DUE TO ADA RATE			YAF00	2773
	+	MAC 4-30.30 IN 15 DEG INCR, M=5.65, 8.0, 1.2			YAF00	2773
	+	DATA UCMODAT/			YAF00	2773
	+	+.120, -.061, 0.0, .000, .177,			YAF00	2773
	+	+.135, -.068, 0.0, .000, .177,			YAF00	2773
	+	+.107, -.054, 0.0, .000, .120,			YAF00	2773
	+	+.010, -.015, 0.0, .000, .120,			YAF00	2773
2775	+	PITCHING MOMENT INCREMENT DUE TO AILERONS			YAF00	2773
	+	MAC 4-30.30 IN 10 DEG INCR, ALPHA=4.25 IN 4 DEG INCR			YAF00	2773
	+	DATA UCMODAT/			YAF00	2773
	+	+.120, -.061, 0.0, .000, .177,			YAF00	2773
	+	+.135, -.068, 0.0, .000, .177,			YAF00	2773
	+	+.107, -.054, 0.0, .000, .120,			YAF00	2773
	+	+.010, -.015, 0.0, .000, .120,			YAF00	2773
2780	+	PITCHING MOMENT INCREMENT DUE TO ADA RATE			YAF00	2773
	+	MAC 4-30.30 IN 15 DEG INCR, M=5.65, 8.0, 1.2			YAF00	2773
	+	DATA UCMODAT/			YAF00	2773
	+	+.120, -.061, 0.0, .000, .177,			YAF00	2773
	+	+.135, -.068, 0.0, .000, .177,			YAF00	2773
	+	+.107, -.054, 0.0, .000, .120,			YAF00	2773
	+	+.010, -.015, 0.0, .000, .120,			YAF00	2773
2785	+	PITCHING MOMENT INCREMENT DUE TO AILERONS			YAF00	2773
	+	MAC 4-30.30 IN 10 DEG INCR, ALPHA=4.25 IN 4 DEG INCR			YAF00	2773
	+	DATA UCMODAT/			YAF00	2773
	+	+.120, -.061, 0.0, .000, .177,			YAF00	2773
	+	+.135, -.068, 0.0, .000, .177,			YAF00	2773
	+	+.107, -.054, 0.0, .000, .120,			YAF00	2773
	+	+.010, -.015, 0.0, .000, .120,			YAF00	2773
2790	+	PITCHING MOMENT INCREMENT DUE TO ADA RATE			YAF00	2773
	+	MAC 4-30.30 IN 15 DEG INCR, M=5.65, 8.0, 1.2			YAF00	2773
	+	DATA UCMODAT/			YAF00	2773
	+	+.120, -.061, 0.0, .000, .177,			YAF00	2773
	+	+.135, -.068, 0.0, .000, .177,			YAF00	2773
	+	+.107, -.054, 0.0, .000, .120,			YAF00	2773
	+	+.010, -.015, 0.0, .000, .120,			YAF00	2773

07.01.61 15.12.22. 02/10/20

SUBROUTINE AERODAT 74/175 (PT=2)

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67-2171-22/08/28

UFG 4115 MIF

SUBROUTINE AFQOAT 74/175 (051=2

3025	.025	.097	.094	.126	.222	.152	.180	.205	3025
3026	.026	.098	.095	.127	.223	.153	.181	.206	3026
3027	.027	.099	.096	.128	.224	.154	.182	.207	3027
3028	.028	.100	.097	.129	.225	.155	.183	.208	3028
3029	.029	.101	.098	.130	.226	.156	.184	.209	3029
3030	.030	.102	.099	.131	.227	.157	.185	.210	3030
3031	.031	.103	.100	.132	.228	.158	.186	.211	3031
3032	.032	.104	.101	.133	.229	.159	.187	.212	3032
3033	.033	.105	.102	.134	.230	.160	.188	.213	3033
3034	.034	.106	.103	.135	.231	.161	.189	.214	3034
3035	.035	.107	.104	.136	.232	.162	.190	.215	3035
3036	.036	.108	.105	.137	.233	.163	.191	.216	3036
3037	.037	.109	.106	.138	.234	.164	.192	.217	3037
3038	.038	.110	.107	.139	.235	.165	.193	.218	3038
3039	.039	.111	.108	.140	.236	.166	.194	.219	3039
3040	.040	.112	.109	.141	.237	.167	.195	.220	3040
3041	.041	.113	.110	.142	.238	.168	.196	.221	3041
3042	.042	.114	.111	.143	.239	.169	.197	.222	3042
3043	.043	.115	.112	.144	.240	.170	.198	.223	3043
3044	.044	.116	.113	.145	.241	.171	.199	.224	3044
3045	.045	.117	.114	.146	.242	.172	.200	.225	3045
3046	.046	.118	.115	.147	.243	.173	.201	.226	3046
3047	.047	.119	.116	.148	.244	.174	.202	.227	3047
3048	.048	.120	.117	.149	.245	.175	.203	.228	3048
3049	.049	.121	.118	.150	.246	.176	.204	.229	3049
3050	.050	.122	.119	.151	.247	.177	.205	.230	3050
3051	.051	.123	.120	.152	.248	.178	.206	.231	3051
3052	.052	.124	.121	.153	.249	.179	.207	.232	3052
3053	.053	.125	.122	.154	.250	.180	.208	.233	3053
3054	.054	.126	.123	.155	.251	.181	.209	.234	3054
3055	.055	.127	.124	.156	.252	.182	.210	.235	3055
3056	.056	.128	.125	.157	.253	.183	.211	.236	3056
3057	.057	.129	.126	.158	.254	.184	.212	.237	3057
3058	.058	.130	.127	.159	.255	.185	.213	.238	3058
3059	.059	.131	.128	.160	.256	.186	.214	.239	3059
3060	.060	.132	.129	.161	.257	.187	.215	.240	3060
3061	.061	.133	.130	.162	.258	.188	.216	.241	3061
3062	.062	.134	.131	.163	.259	.189	.217	.242	3062
3063	.063	.135	.132	.164	.260	.190	.218	.243	3063
3064	.064	.136	.133	.165	.261	.191	.219	.244	3064
3065	.065	.137	.134	.166	.262	.192	.220	.245	3065
3066	.066	.138	.135	.167	.263	.193	.221	.246	3066
3067	.067	.139	.136	.168	.264	.194	.222	.247	3067
3068	.068	.140	.137	.169	.265	.195	.223	.248	3068
3069	.069	.141	.138	.170	.266	.196	.224	.249	3069
3070	.070	.142	.139	.171	.267	.197	.225	.250	3070
3071	.071	.143	.140	.172</					

ORIGINAL PAGE 19
OF POOR QUALITY

PAGE 45

02/10/79, 15.17.40

FTN 4.4+30

SURROUNDING AERODAY 74/170 UPT-2

3080	0002	0004	0002	0002	0002	YAF00	3079
	0008	0004	0002	0002	0002	YAF00	3080
	0016	0004	0002	0002	0002	YAF00	3081
	0024	0004	0002	0002	0002	YAF00	3082
	0032	0004	0002	0002	0002	YAF00	3083
	DATA MCNDRT/	1-120.1631				YAF00	3084
3085	320.07					YAF00	3085
	DATA MCNDRT/	1-161.1921				YAF00	3086
	0019	0018	0011	0010	0010	YAF00	3087
	0027	0018	0007	0008	0008	YAF00	3088
	0035	0008	0003	0004	0004	YAF00	3089
3090	0004	0008	0013	0018	0018	YAF00	3090
	0014	0023	0031	0037	0037	YAF00	3091
	0022	0036	0050	0060	0060	YAF00	3092
	0030	0052	0071	0083	0083	YAF00	3093
3095	DATA MCNDRT/	1-193.2241				YAF00	3094
	0037	0016	0011	0010	0010	YAF00	3095
	0045	0006	0004	0004	0004	YAF00	3096
	0053	0007	0004	0004	0004	YAF00	3097
3100	0010	0010	0004	0004	0004	YAF00	3098
	0018	0007	0004	0004	0004	YAF00	3099
	0026	0007	0004	0004	0004	YAF00	3100
	0034	0007	0004	0004	0004	YAF00	3101
	0042	0007	0004	0004	0004	YAF00	3102
3105	DATA MCNDRT/	1-225.2561				YAF00	3103
	0079	0014	0018	0038	0038	YAF00	3104
	0087	0014	0018	0038	0038	YAF00	3105
	0095	0008	0013	0032	0032	YAF00	3106
	0103	0008	0013	0032	0032	YAF00	3107
3110	0066	0104	0139	0156	0156	YAF00	3108
	0074	0150	0174	0216	0216	YAF00	3109
	0082	0200	0236	0280	0280	YAF00	3110
	0090	0200	0236	0280	0280	YAF00	3111
3115	INCREMENTAL YAWING MOMENT COEFFICIENT DUE TO RUDDER					YAF00	3112
	M=65.0, 6, 0.51, 0.51, 2; ALPHA=4.24 IN 4 DEG INCR					YAF00	3113
	DATA MCNDRT/					YAF00	3114
	0235	0255	0244	0254	0254	YAF00	3115
3120	0255	0255	0231	0231	0231	YAF00	3116
	0255	0255	0231	0231	0231	YAF00	3117
	0255	0255	0231	0231	0231	YAF00	3118
3125	0255	0255	0231	0231	0231	YAF00	3119
	0255	0255	0231	0231	0231	YAF00	3120
	0255	0255	0231	0231	0231	YAF00	3121
	0255	0255	0231	0231	0231	YAF00	3122
3130	0255	0255	0231	0231	0231	YAF00	3123
	0255	0255	0231	0231	0231	YAF00	3124
	0255	0255	0231	0231	0231	YAF00	3125
	0255	0255	0231	0231	0231	YAF00	3126
3135	0255	0255	0231	0231	0231	YAF00	3127
	0255	0255	0231	0231	0231	YAF00	3128
	0255	0255	0231	0231	0231	YAF00	3129
	0255	0255	0231	0231	0231	YAF00	3130
	0255	0255	0231	0231	0231	YAF00	3131
	0255	0255	0231	0231	0231	YAF00	3132
	0255	0255	0231	0231	0231	YAF00	3133
	0255	0255	0231	0231	0231	YAF00	3134
	0255	0255	0231	0231	0231	YAF00	3135

ORIGINAL PAGE IS
OF POOR QUALITY

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PAGE

02/13/22, 1:13.40

FIN 4.8453H

SUBROUTINE AIRPDATA 74/1/5 OPT=2

* SF INCREMENT DUE TO AILERONS
* DA--33.20 IN 10 DEG INCR; ALPHA=-4.24 IN 4 DEG INCR

DATA HCVBRT/
* .0177, .0110, .0055, 0., -.0005, -.0177,
* .0153, .0118, .0065, 0., -.0047, -.0105,
* .0133, .0095, .0045, 0., -.0028, -.0078,
* .0057, .0036, .0027, 0., -.0034, -.0066,
* .0057, .0036, .0027, 0., -.0034, -.0066,
* .0057, .0036, .0027, 0., -.0034, -.0066

* SF INCREMENT DUE TO RUDDER
* M=.65, .95, .95, .05, 1.21 ALPHA=-4.24 IN 4 DEG INCR

DATA HCVBRT/
* .040, .040, .040, .042, .043, .030,
* .040, .038, .038, .042, .036, .040,
* .040, .038, .038, .042, .036, .040,
* .038, .038, .038, .040, .028, .030,
* .037, .038, .038, .040, .026, .027,
* .035, .038, .038, .042, .024, .026,
* .032, .028, .034, .042, .020, .026,
* .028, .018, .034, .042, .017, .026

* SF INCREMENT DUE TO YAW RATE (PER DEGREE)
* M=.5, .65, .7, .85, .9, 1.2

DATA HCVRT/
* .0050, .0058, .0058, .0055, .0059, .0061, .0064

* RM INCREMENT DUE TO FLAPS WITH LEVER OFF OF IS GREATER THAN OR
* EQUAL TO 10 DEG; M=.50 AND .65, 1.05 BY INCR OF 10; ALPHA=-4.24 IN
* 2 DEG INCR

DATA HCVBRT/
* .0003, -.0009, 0.0000, 0.0003, 0.0000, 0.0000,
* .0003, -.0009, .0001, 0.0000, 0.0000, 0.0000,
* .0001, -.0003, .0001, 0.0000, 0.0000, 0.0000,
* .0001, -.0001, .0001, 0.0000, 0.0000, 0.0000,
* .0002, -.0002, .0001, 0.0003, 0.0000, 0.0000,
* .0000, 0.0000, -.0007, 0.0000, 0.0000, 0.0000,
* .0001, .0001, .0001, 0.0000, 0.0000, 0.0000,
* .0002, .0000, .0003, 0.0000, 0.0000, 0.0000,
* .0003, 0.0000, .0003, 0.0000, 0.0000, 0.0000,
* .0016, -.0005, .0003, 0.0000, 0.0000, 0.0000,
* .0016, -.0005, .0003, 0.0000, 0.0000, 0.0000,
* .0012, -.0005, .0003, 0.0000, 0.0000, 0.0000,
* .0014, -.0013, .0004, 0.0000, 0.0000, 0.0000

* BASELINE YAWING MOMENT
* M=.5 AND .65, 1.05 BY INCR OF 10; ALPHA=-4.24 IN 2 DEG INCR

DATA HCVBRT/

YAE00 3307
YAE00 3308
YAE00 3309
YAE00 3310
YAE00 3311
YAE00 3312
YAE00 3313
YAE00 3314
YAE00 3315
YAE00 3316
YAE00 3317
YAE00 3318
YAE00 3319
YAE00 3320
YAE00 3321
YAE00 3322
YAE00 3323
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YAE00 3358
YAE00 3359
YAE00 3360
YAE00 3361
YAE00 3362
YAE00 3363

ORIGINAL PAGE IS
OF POOR QUALITY

SUBROUTINE	AFRODAY	74/175	OPI=	FIN 4, 8+538	92/1722, 15, 12, 40	0001	40
336	AFRODAY	74/175	OPI=	FIN 4, 8+538	92/1722, 15, 12, 40	0001	40
3370	AFRODAY	74/175	OPI=	FIN 4, 8+538	92/1722, 15, 12, 40	0001	40
3375	AFRODAY	74/175	OPI=	FIN 4, 8+538	92/1722, 15, 12, 40	0001	40
3380	AFRODAY	74/175	OPI=	FIN 4, 8+538	92/1722, 15, 12, 40	0001	40
3385	AFRODAY	74/175	OPI=	FIN 4, 8+538	92/1722, 15, 12, 40	0001	40
3390	AFRODAY	74/175	OPI=	FIN 4, 8+538	92/1722, 15, 12, 40	0001	40
3395	AFRODAY	74/175	OPI=	FIN 4, 8+538	92/1722, 15, 12, 40	0001	40
3400	AFRODAY	74/175	OPI=	FIN 4, 8+538	92/1722, 15, 12, 40	0001	40
3405	AFRODAY	74/175	OPI=	FIN 4, 8+538	92/1722, 15, 12, 40	0001	40
3410	AFRODAY	74/175	OPI=	FIN 4, 8+538	92/1722, 15, 12, 40	0001	40
3415	AFRODAY	74/175	OPI=	FIN 4, 8+538	92/1722, 15, 12, 40	0001	40
3420	AFRODAY	74/175	OPI=	FIN 4, 8+538	92/1722, 15, 12, 40	0001	40

SUBROUTINE AFROYDA 74/175 NOV-2

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ORIGINAL PAGE IS
OF POOR QUALITY

PAGE 3

02/10/72, 15,17,40

FTN 4.0+438

SUBPUNITNF AFQY8R 74/175 00F=2

115	EQUVALENCE	VAERD	1572
	..VAERD	VAERD	1573
	..VAERD	VAERD	1574
	..VAERD	VAERD	1575
120	..VAERD	VAERD	1576
	..VAERD	VAERD	1577
	..VAERD	VAERD	1578
	..VAERD	VAERD	1579
125	..VAERD	VAERD	1580
	..VAERD	VAERD	1581
	..VAERD	VAERD	1582
	..VAERD	VAERD	1583
130	..VAERD	VAERD	1584
	..VAERD	VAERD	1585
	..VAERD	VAERD	1586
	..VAERD	VAERD	1587
135	..VAERD	VAERD	1588
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	..VAERD	VAERD	1590
	..VAERD	VAERD	1591
	..VAERD	VAERD	1592
140	..VAERD	VAERD	1593
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	..VAERD	VAERD	1595
	..VAERD	VAERD	1596
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145	..VAERD	VAERD	1598
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	..VAERD	VAERD	1600
	..VAERD	VAERD	1601
	..VAERD	VAERD	1602
150	..VAERD	VAERD	1603
	..VAERD	VAERD	1604
	..VAERD	VAERD	1605
	..VAERD	VAERD	1606
	..VAERD	VAERD	1607
155	..VAERD	VAERD	1608
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	..VAERD	VAERD	1610
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	..VAERD	VAERD	1612
160	..VAERD	VAERD	1613
	..VAERD	VAERD	1614
	..VAERD	VAERD	1615
	..VAERD	VAERD	1616
	..VAERD	VAERD	1617
165	..VAERD	VAERD	1618
	..VAERD	VAERD	1619
	..VAERD	VAERD	1620
	..VAERD	VAERD	1621
	..VAERD	VAERD	1622
170	..VAERD	VAERD	1623
	..VAERD	VAERD	1624
	..VAERD	VAERD	1625
	..VAERD	VAERD	1626
	..VAERD	VAERD	1627

74/175 00123

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FACT:

U.S. 2102, 1922, 1923

4.64 ÷ 3.11

SUBROUTINE AFRV4B 74/175 00152

[illegible]

74-1175 041-2

A-84

0218512. 15.12.40

SUBROUTINE AFROYAR 74/175 OPT=2

[illegible]

SETAP=SIGN(1.0,RETA)
 Q1=EXP(-1.0/TAP+DTR)
 Q2=EXP(-1.0/TAP+DTR)
 IF (RETA.EQ. 90.) REIAP=1.0 -RETA
 IF (RETA.EQ. -90.) REIAP=-1.0 -RETA
 HP=INT(10.42+CUS((THAI* -4.4E0TOR)) -24.498-25.67+11.-(CUSHP))

LAT.,-DIR. CONSTANTS (NUF OF G.F.)

RVL0035=VTA/1.025
 RVL0040=VTA/1.025
 RVL0041=VTA/1.025
 RVL0042=VTA/1.025
 RVL0043=VTA/1.025
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 RVL0243=VTA/1.025
 RVL0244=VTA/1.025
 RVL0245=VTA/

630		*
635		* *
640		* * *
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650		
655		
660		** *
665		* *
670		
675		
680		* * *

A-86

MS. A. 9. 2. 22. 15. 12. 40

वि. सं. ११०५

74/175 001=?

[illegible]

74-175 DET-2

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A-90

ORIGINAL PAGE IS
OF POOR QUALITY

	SUBROUTINE	AFK0Y00	74/175	001=2	FTM 4.01434	02/10/22. 14.12.41	PAGE	18
970		CALL FSCCHIMP, MKK14.5, 1, PRV25.21				YAF00	4427	
		CALL FCALCIVEF, 0.0030(4), 3, 3				YAF01	4428	
		TEMP(1)=AETAP				YAF02	4429	
		TEMP(2)=NP				YAF03	4430	
		TEMP(3)=NP				YAF04	4431	
975		CALL FCALCIVEF, 0.0030(4), 3, 3				YAF05	4432	
		CALL FCALCIVEF, 0.0030(4), 3, 3				YAF06	4433	
		CALL FCALCIVEF, 0.0030(4), 3, 3				YAF07	4434	
		CALL FCALCIVEF, 0.0030(4), 3, 3				YAF08	4435	
980		TEMP(1)=AETAP				YAF09	4436	
		TEMP(2)=NP				YAF10	4437	
		TEMP(3)=NP				YAF11	4438	
		CALL FCALCIVEF, 0.0030(4), 3, 3				YAF12	4439	
985		CALL FCALCIVEF, 0.0030(4), 3, 3				YAF13	4440	
		TEMP(1)=AETAP				YAF14	4441	
		TEMP(2)=NP				YAF15	4442	
		TEMP(3)=NP				YAF16	4443	
		CALL FCALCIVEF, 0.0030(4), 3, 3				YAF17	4444	
990		TEMP(1)=AETAP				YAF18	4445	
		TEMP(2)=NP				YAF19	4446	
		TEMP(3)=NP				YAF20	4447	
		CALL FCALCIVEF, 0.0030(4), 3, 3				YAF21	4448	
995		CALL FCALCIVEF, 0.0030(4), 3, 3				YAF22	4449	
		TEMP(1)=AETAP				YAF23	4450	
		TEMP(2)=NP				YAF24	4451	
		TEMP(3)=NP				YAF25	4452	
1000		CALL FCALCIVEF, 0.0030(4), 3, 3				YAF26	4453	
		TEMP(1)=AETAP				YAF27	4454	
		TEMP(2)=NP				YAF28	4455	
		TEMP(3)=NP				YAF29	4456	
1005		CALL FCALCIVEF, 0.0030(4), 3, 3				YAF30	4457	
		TEMP(1)=AETAP				YAF31	4458	
		TEMP(2)=NP				YAF32	4459	
		TEMP(3)=NP				YAF33	4460	
1010		CALL FCALCIVEF, 0.0030(4), 3, 3				YAF34	4461	
		TEMP(1)=AETAP				YAF35	4462	
		TEMP(2)=NP				YAF36	4463	
		TEMP(3)=NP				YAF37	4464	
1015		CALL FCALCIVEF, 0.0030(4), 3, 3				YAF38	4465	
		TEMP(1)=AETAP				YAF39	4466	
		TEMP(2)=NP				YAF40	4467	
		TEMP(3)=NP				YAF41	4468	
1020		CALL FCALCIVEF, 0.0030(4), 3, 3				YAF42	4469	
		TEMP(1)=AETAP				YAF43	4470	
		TEMP(2)=NP				YAF44	4471	
		TEMP(3)=NP				YAF45	4472	
1025		CALL FCALCIVEF, 0.0030(4), 3, 3				YAF46	4473	
		TEMP(1)=AETAP				YAF47	4474	
		TEMP(2)=NP				YAF48	4475	
		TEMP(3)=NP				YAF49	4476	
		CALL FCALCIVEF, 0.0030(4), 3, 3				YAF50	4477	
		TEMP(1)=AETAP				YAF51	4478	
		TEMP(2)=NP				YAF52	4479	
		TEMP(3)=NP				YAF53	4480	
		CALL FCALCIVEF, 0.0030(4), 3, 3				YAF54	4481	
		TEMP(1)=AETAP				YAF55	4482	
		TEMP(2)=NP				YAF56	4483	
		TEMP(3)=NP				YAF57	4484	

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74-1175-101 AF-RNYUB 74-1175-101f=2

NO	NAME	UNIT	DEFINITION
1085	1085		1085
1090	1090		1090
1096	1096		1096
1100	1100		1100
1105	1105		1105
1110	1110		1110
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07/10/22. 15.12.40

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74/175 OPT=2

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FTN 4.8+578

SUBROUTINE AEROYUR 74/175 OPT=2

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1540      DCMST=F30(TEMP,NPT49,BND47,HCMST)
      * * FLAP INCREMENT
      *
1545      CALL ECALC(ALP,BND68(1),15,1)
      CALL ECALC(DELTA PL,BND69(1),1,2)
      CALL FSRCH(MACH,ARK22,8,1H5,1)
      TEMP(1)=DELTA PL
      DCMF=F32(TEMP,NPT49,BND68(1),52)
      CALL ECALC(DELTA PP,BND68(1),52)
      TEMP(2)=DELTA PP
      DCMF=F33(TEMP,NPT49,BND68(1),52)
      DCMF=DCMFL+DEL
      DCMF=DCMFL+DEL
      * * POWER INCREMENT
      *
1550      CALL ECALC(ALP,BND69(1),8,1)
      CALL ECALC(VFO,BND69(1),1,2)
      CALL FSRCH(THETAJ,ARK36,12,1H24,3)
      TEMP(3)=VFO
      TEMP(4)=THETAJ
      HCMP=F30(TEMP,NPT50,BND69,HCMPOINT)
      CALL ECALC(A0,BND69(1),1,2)
      TEMP(5)=A0
      TEMP(6)=0
      HCMP=F31(TEMP,NPT50,BND69,HCMPOINT)
      HCMPSU=HCMP1-HCM2
      *
1570      GKMP=ABS(THETAJ)-7
      GKMP=AMIN(1,1+MAX(GKMP,.15))
      HCMPOW=HCMPTW+GKMP
      *
1575      * PITCH RATE AND ALPHA DOT INCREMENTS
      *
      CALL FSRCH(MACH,ARK41,5,1H31,1)
      CMOT=FBI(MACH,2,BND67(5),HCMOT)
      CMOT=CMOT+OTD+CALR+C2V
      CALL ECALC(MACH,BND33,6,1)
      CMALPDY=FBI(MACH,6,BND33,HCMALDI)
      CMALPDY=INAI PDYAL PDYOTD+CM2V
      *
1585      * AILERON INCREMENT
      *
      CALL ECALC(DAR,BND52(1),6,1)
      TEMP(11)=DAR
      HCMDAE=FC(TEMP,NPT51,BND52,HCMDAT)
      CALL ECALC(DAL,BND52(1),6,1)
      TEMP(12)=DAL
      HCMDAL=FC(TEMP,NPT51,BND52,HCMDAL)
      HCMDAE=HCMDAE+HCMDAL
      *
1595      * STING INCREMENT
      *

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SUBROUTINE AEROYBB 74/175 001-2

```

1655 CALL FCALC(DAL,8ND70,1,5,1)
      CALL FSCHEMACH,RRK29,4,INI,2)
      TEMP(1)=RMACH
      DCAL=2C(TEMP,NP152,8ND70,HCLAILT)
1660 CALL FCALC(DAR,8ND70,1,5,1)
      TEMP(1)=DAR
      DCALP=2C(TEMP,NP152,8ND70,HCLAILT)
      * POWER INCREMENT
      *
1665 CALL FCALC(THETAJ,8ND611,NP15,1,1,1)
      CALL FSCHEMACH,RRK2,NP14,1,1,REFV,2)
      CALL FCALC(ALP,8ND451,NP14,1,1,3)
      TEMP(1)=THETAJ
      TEMP(3)=ALP
      TEMP(4)=F30(TEMP,NP14,8ND6,CNPNMT)
1670 CALL FCALC(C1,0.0,8ND6,1,1,NP14,1,1)
      CALL FCALC(C1,0.0,RRK2,NP14,1,1,3,2)
      TEMP(1)=0.0
      TEMP(3)=0.0
      TEMP(4)=F30(TEMP,NP14,8ND6,CNPNMT)
1675 ORNPN2=180
      CALP=COCALP
      TEMP(4)=0.0 CALP=0.0
      TEMP(4)=F30(TEMP,NP14,8ND6,CNPNMT)
1680 DCALP=DCALP-DCNPN2)/CALP
      *
      * TOTAL LIFT COEFFICIENT
      *
1685 HCL=CLBASE+DCFL+DCLEF+DCAL+DCALP+DCLEPW
      IFALP=GE.40.0,ALP,1E.-10.0) 60 TO 610
      *****
      *
1690 DRAG COEFFICIENT
      *****
      *
1695 BASELINE (CLEAN AIRCRAFT)
      *
      CALL FSCHEMACH,RRK29,4,INI,1,1)
      TEMP(1)=RMACH
      TEMP(3)=CLBASE
      CORAS2=F30(TEMP,NP153,8ND71,HCD21)
1700 IF(CORASE,GE.-35,A,CLBASE,1E.-1.20) 60 TO 611
      CONTINUE
      610
      CALL FSCHEMACH,RRK35,18,INI,1,1)
      CORAS1=F30(ALP,18,8ND1,HCD1)
      CORAS1=CORAS1
      TEMP(1)=CLBASE
      TEMP(3)=GE.40.0,ALP,1E.-10.0) 60 TO 612
1705 IF(ALP,LE.0.0) ALP=ALP+1.0
      IF(ALP,GT.0.0) ALP=ALP-1.0
      ALP=ALP+1.0
      CORAS2=(CORAS1+CORAS1)*ALP/CORAS1
      612
1710

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PTN 4.0+238

SUBROUTINE AEROYBR 74/175 OPT=2

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611 CONTINUE
612 CONTINUE
* *
* FLAP INCREMENT
1715 CALL ECALC(ALP,BND73(1),9,11)
    CALL ECALC(DELAPL,BND73(1),9,11)
    CALL ECALC(HRMACH,BND73(1),9,11)
    TEMP(1)=ALP
    TEMP(2)=DELAPL
    TEMP(3)=HRMACH
    OCDEF=F3DT(TEMP,NPT5,BND73,HCDFT)+0.5
    CALL ECALC(DELAPL,BND73(1),9,11)
    TEMP(2)=DELAPL
    OCDEF=F3DT(TEMP,NPT5,BND73,HCDFT)+0.5
    OCDEF=OCDEF+DEF
    OCDEF=OCDEF+DEF
* *
* AILERON INCREMENT
1730 CALL ECALC(ALP,BND73(1),9,11)
    CALL ECALC(DELAPL,BND73(1),9,11)
    CALL ECALC(HRMACH,BND73(1),9,11)
    TEMP(1)=ALP
    TEMP(2)=DELAPL
    TEMP(3)=HRMACH
    OCDEF=F3DT(TEMP,NPT5,BND73,HCDFT)
    CALL ECALC(DELAPL,BND73(1),9,11)
    TEMP(2)=DELAPL
    OCDEF=F3DT(TEMP,NPT5,BND73,HCDFT)
    OCDEF=OCDEF+DEF
    OCDEF=OCDEF+DEF
* *
* STABILATOR INCREMENT
1745 CALL ECALC(ALP,BND73(1),9,11)
    CALL ECALC(DELAPL,BND73(1),9,11)
    CALL ECALC(HRMACH,BND73(1),9,11)
    TEMP(1)=ALP
    TEMP(2)=DELAPL
    TEMP(3)=HRMACH
    OCDEF=F3DT(TEMP,NPT5,BND73,HCDFT)
    CALL ECALC(DELAPL,BND73(1),9,11)
    TEMP(2)=DELAPL
    OCDEF=F3DT(TEMP,NPT5,BND73,HCDFT)
    OCDEF=OCDEF+DEF
    OCDEF=OCDEF+DEF
* *
* RUDDER INCREMENT
1760 CALL ECALC(ALP,BND73(1),9,11)
    CALL ECALC(DELAPL,BND73(1),9,11)
    CALL ECALC(HRMACH,BND73(1),9,11)
    TEMP(1)=ALP
    TEMP(2)=DELAPL
    TEMP(3)=HRMACH
    OCDEF=F3DT(TEMP,NPT5,BND73,HCDFT)
    CALL ECALC(DELAPL,BND73(1),9,11)
    TEMP(2)=DELAPL
    OCDEF=F3DT(TEMP,NPT5,BND73,HCDFT)
    OCDEF=OCDEF+DEF
    OCDEF=OCDEF+DEF
* *
* DRAG INCREMENT DUE TO 4 PYLONS AND 2 GUN PDS
1765 WCDSTW=.00413

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82/10/72. 15.12.60

FTN 4.8+538

SUBROUTINE AEROYOB 74/175 QPT=2

```

**
** *****
** SIDE FORCE COEFFICIENT
** *****
** BASELINE + FLAP INCREMENT
** *****
**
** CALL FSRCH (RMACH, BRK42, 0, IN32, 1)
** CALL FCALC (ALP, BND41(3), 15, 2)
** CALL FCALC (ALP, BND41(5), 2, 3)
** TEMP(1) = OFLAPL
** HCYB = F2C(TEMP, NPT58, BND51, HCYRT)
** CALL FCALC (ALP, BND41(5), 2, 3)
** HCYB = F2C(TEMP, NPT58, BND51, HCYRT)
** HCYB = 0.0; HCYRT = (1/4)*ULLEL+HNDLRT)
** HCYB = HCYB+HCYRT
**
** *****
** AILERON INCREMENT
** *****
**
** CALL FCALC (DAL, BND52(1), 6, 1)
** CALL FCALC (DAL, BND52(1), 6, 1)
** TEMP(1) = DAL
** HCYDAL = F2C(TEMP, NPT61, BND52, HCYDAT)
** CALL FCALC (DAL, BND52(1), 6, 1)
** TEMP(1) = DAL
** HCYDAL = F2C(TEMP, NPT61, BND52, HCYDAT)
** HCYDA = HCYDAL-HCYDAR
**
** *****
** RUDDER INCREMENT
** *****
**
** CALL FSRCH (RMACH, BRK39, 0, IN40, 1)
** HCYDR = F2C(TEMP, NPT51, BND77, HCYVRT)
**
** *****
** YAW RATE INCREMENT
** *****
**
** CALL FSRCH (RMACH, BRK40, 0, IN41, 1)
** HCYR = F2C(TEMP, NPT51, BND78, HCYRT)
**
** *****
** TOTAL SIDE FORCE COEFFICIENT
** *****
**
** HCY = HCYB+HCTA+HCYDA+HCYDR+(ORUD9/15.0)
**
** *****
** TOTAL SIDE FORCE
** *****
**
** HCTF = HCY+QS+HCYR+HCTA+HCTD+TEMPX4/8
**
** *****
** TRANSFORMATIONS AND TOTAL FORCES AND MOMENTS
** *****
**
** HICL = HICL+QS*CLSTAR
** HICM = HICM+QS*DHICM+OS
** HICP = HICP+QS*HICL+HICM+HICP+HICL+HICM+HICP
** HIEZ = HIEZ+HICL+HICM+HICP+HICL+HICM+HICP
** HIRP = HIRP+HICL+HICM+HICP+HICL+HICM+HICP

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SYMBOLIC REFERENCE MAP (R=2)			REFERENCES
ENTRY	POINTS	DEF LINE	1906
VARIABLES	SN	TYPE	ARRAY
1750 A	REAL		RELATION FARRAY
7576	ARETAP	REAL	
2460	AEROL	REAL	FARRAY
2441	AEROM	REAL	FARRAY
2462	AEROM	REAL	FARRAY
2455	AEROM	REAL	FARRAY
2456	AFROY	REAL	FARRAY

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1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80	81	82	83	84	85	86	87	88	89	90	91	92	93	94	95	96	97	98	99	100
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80	81	82	83	84	85	86	87	88	89	90	91	92	93	94	95	96	97	98	99	100
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80	81	82	83	84	85	86	87	88	89	90	91	92	93	94	95	96	97	98	99	100
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80	81	82	83	84	85	86	87	88	89	90	91	92	93	94	95	96	97	98	99	100
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SUBROUTINE AERNOVR			74/175	OPT=2	FTN 5.0+38		R2/10/22. 15.17.40		PAGE	45
VARIABLES	SN	TYPE	RELOCATION							
10270 EPS2	10270	REAL	ARRAY	ARRAY	2794	DEFINED	793	801		
10271 EPS2	10271	REAL	ARRAY	ARRAY	1307	DEFINED	793	1307	957	948
10272 EPS2	10272	REAL	ARRAY	ARRAY	1308	DEFINED	1307	1308	1202	1232
10273 EPS2	10273	REAL	ARRAY	ARRAY	1309	DEFINED	1307	1309	1202	1232
10274 EPS2	10274	REAL	ARRAY	ARRAY	1310	DEFINED	1308	1310	1202	1232
10275 EPS2	10275	REAL	ARRAY	ARRAY	1311	DEFINED	1309	1311	1202	1232
10276 EPS2	10276	REAL	ARRAY	ARRAY	1312	DEFINED	1310	1312	1202	1232
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SUBROUTINE AEROY88			74/175 OPT-2		FIN 4.0.538		82/10/77. 15.12.40		PAGE	
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REFERENCES				592	593	594	595	597	888	889

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SUBROUTINE AFROVBB		74/174	NOT=2	DEF LINE		REFERENCES	FTN 4.8+538		02/10/22. 15.12.40	PAGE	55					
INLINE	FUNCTIONS	TYPE	ARGS	INTRIN	DEF LINE	REFERENCES										
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STATEMENT LABELS	74/175 OPT-2	FTN 4.8+38	82/10/22. 15.12.40	PAGE
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60      : 0.0 : 0.1 : 10.9 : 12.4 : 14.6 : 16.2 : 17.6 : 18.9 :
      : 0.0 : 10.0 : 11.9 : 13.4 : 15.5 : 17.3 : 18.6 : 19.8 :
      : 0.0 : 11.1 : 13.0 : 14.9 : 16.8 : 18.5 : 20.1 : 21.5 : 22.8 /

65      * RAM RECOVERY TABLE - 20 X 7
      * CORRECTED RPM - 74.0, 80.0, 86.0, 92.0, 98.0, 104.0, 110.0, 116.0, 122.0,
      * MACH 0 - 1.2, .2 INCREMENTS

70      * RAM RECOVERY RATIO
      * DATA (NRTAB(1), 1-1.63) /
      : .952 : .947 : .935 : .923 : .914 : .903 :
      : .947 : .940 : .929 : .917 : .907 : .897 :
      : .946 : .937 : .925 : .913 : .903 : .893 :
      : 1.0 : .981 : .965 : .949 : .933 : .918 : .900 :
      : .980 : .964 : .948 : .932 : .916 : .900 : .880 :
      : .975 : .959 : .943 : .927 : .911 : .895 : .875 :
      : .970 : .954 : .938 : .922 : .906 : .890 : .870 :
      : 1.0 : .980 : .964 : .948 : .932 : .916 : .900 : .880 :
      : .975 : .959 : .943 : .927 : .911 : .895 : .875 :
      : .970 : .954 : .938 : .922 : .906 : .890 : .870 :
      * DATA (NRTAB(1), 1-1.64, 126) /
      : .975 : .974 : .974 : .981 : .982 : .983 : .984 : .985 :
      : .984 : .983 : .983 : .989 : .990 : .991 : .992 : .993 :
      : .984 : .983 : .983 : .989 : .990 : .991 : .992 : .993 :
      : 1.0 : .980 : .964 : .948 : .932 : .916 : .900 : .880 :
      : .975 : .959 : .943 : .927 : .911 : .895 : .875 :
      : .970 : .954 : .938 : .922 : .906 : .890 : .870 :
      * DATA (NRTAB(1), 1-1.64, 126) /
      : .975 : .974 : .974 : .981 : .982 : .983 : .984 : .985 :
      : .984 : .983 : .983 : .989 : .990 : .991 : .992 : .993 :
      : .984 : .983 : .983 : .989 : .990 : .991 : .992 : .993 :
      : 1.0 : .980 : .964 : .948 : .932 : .916 : .900 : .880 :
      : .975 : .959 : .943 : .927 : .911 : .895 : .875 :
      : .970 : .954 : .938 : .922 : .906 : .890 : .870 :

100     : .910 : .915 : .920 : .925 : .930 : .935 : .940 : .945 :
      : .914 : .919 : .924 : .929 : .934 : .939 : .944 : .949 :
      : .918 : .923 : .928 : .933 : .938 : .943 : .948 : .953 :
      * DATA (NRTAB(1), 1-1.27, 147) /
      : 1.0 : .980 : .964 : .948 : .932 : .916 : .900 : .880 :
      : .975 : .959 : .943 : .927 : .911 : .895 : .875 :
      : .970 : .954 : .938 : .922 : .906 : .890 : .870 :

105     : .875 : .871 : .867 : .863 : .859 : .855 : .851 : .847 :
      : .871 : .867 : .863 : .859 : .855 : .851 : .847 : .843 :
      : .867 : .863 : .859 : .855 : .851 : .847 : .843 : .839 :
      * DATA (NRTAB(1), 1-1.27, 147) /
      : 1.0 : .980 : .964 : .948 : .932 : .916 : .900 : .880 :
      : .975 : .959 : .943 : .927 : .911 : .895 : .875 :
      : .970 : .954 : .938 : .922 : .906 : .890 : .870 :

110     * CORRECTED ALK FLOW TABLE - 21 X 7
      * CORRECTED RPM 0.0, 24.0, 30.0, 40.0, 50.0, 60.0, 70.0, 80.0, 90.0, 100.0, 110.0, 120.0, 130.0, 140.0, 150.0, 160.0, 170.0, 180.0, 190.0, 200.0, 210.0

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* * * * *
150
CORRECTED FUEL FLOW TABLE 12 X 2A
CORRECTED RPM - 0.0, 5.0, 10.0, 15.0, 20.0, 25.0, 30.0, 35.0, 40.0, 45.0, 50.0, 55.0, 60.0, 65.0, 70.0, 75.0, 80.0, 85.0, 90.0, 95.0, 100.0
DELTA T2 - 1.1, 1.2, 1.3, 1.4, 1.5, 1.6, 1.7, 1.8, 1.9, 2.0, 2.1, 2.2, 2.3, 2.4, 2.5, 2.6, 2.7, 2.8, 2.9, 3.0, 3.1, 3.2, 3.3, 3.4, 3.5, 3.6, 3.7, 3.8, 3.9, 4.0, 4.1, 4.2, 4.3, 4.4, 4.5, 4.6, 4.7, 4.8, 4.9, 5.0, 5.1, 5.2, 5.3, 5.4, 5.5, 5.6, 5.7, 5.8, 5.9, 6.0, 6.1, 6.2, 6.3, 6.4, 6.5, 6.6, 6.7, 6.8, 6.9, 7.0, 7.1, 7.2, 7.3, 7.4, 7.5, 7.6, 7.7, 7.8, 7.9, 8.0, 8.1, 8.2, 8.3, 8.4, 8.5, 8.6, 8.7, 8.8, 8.9, 9.0, 9.1, 9.2, 9.3, 9.4, 9.5, 9.6, 9.7, 9.8, 9.9, 10.0

```

	FUEL FLOW	DATA	INTEGRAL	TIME
155	0.0000	0.0000	0.0000	0.0000
160	0.0000	0.0000	0.0000	0.0000
165	0.0000	0.0000	0.0000	0.0000
170	0.0000	0.0000	0.0000	0.0000

PAGE

64-2102-1512-47

HEATH'S MIL

241875 107-2

SUBROUTINE YENG0

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SUBROUTINE	VENGO	74/174 OPT-2	FTM 4.0+30	02/10/22. 15.12.43	PAGE
290	* PCS CORRECTION TO FUEL FLOW - 55.0, 80.0, 60.0, 97.5, 105.0, 110.0			VENGN	286
	* DATA (WFRACSH(1),1-15.0) / 67.0, 66.0, 66.0 /			VENGN	287
295	***** HARRIER THROTTLE QUADRANT			VENGN	288
	** RPM COMMAND - 9			VENGN	289
	* POWER SPINDLE ANGLE - 20.0, 22.0, 30.0, 40.0, 45.0, 46.0, 60.0,			VENGN	290
300	* 71.5, 74.0			VENGN	291
	* DATA NITABU/			VENGN	292
	* 26.8, 26.8, 44.5, 70.0, 83.5, 87.9, 95.0, 102.8, 102.8 /			VENGN	293
305	***** FUEL FLOW COMMAND			VENGN	294
	* POWER SPINDLE ANGLE - 0.0, 18.0, 22.0, 25.0, 30.0, 35.0, 40.0,			VENGN	295
	* 42.5, 43.0, 47.5, 50.0, 65.0, 75.0			VENGN	296
310	* DATA VECTRU /			VENGN	297
	* 480.0, 1250.0, 1450.0, 1300.0, 2000.0, 3200.0,			VENGN	298
	* 3700.0, 6050.0, 6250.0, 11050.0, 27300.0,			VENGN	299
315	* GROSS THRUST SEA LEVEL STD DAY - 11 x 6			VENGN	300
	* CORRECTED RPM - 24.30, 40.50, 40.70, 40.85, 40.95, 5.100, 102.103.5			VENGN	301
	* MACH - 0.0, 0.756, 1.512, 2.2268, 3.024, 4.0, 6.0, 8.1.0			VENGN	302
320	* DATA (EGTANH(1),1-1.6P) /			VENGN	303
	* 580.0, 918.0, 1936.0, 3299.0, 4761.0, 6852.0, 9898.0,			VENGN	304
325	* 11740.0, 14143.0, 16233.0, 19572.0, 19206.0, 19680.0, 20151.0,			VENGN	305
	* 20701.0, 21423.0,			VENGN	306
	* 600.0, 950.0, 1960.0, 3350.0, 4820.0, 6899.0, 9961.0,			VENGN	307
330	* 11857.0, 14255.0, 16745.0, 14371.0, 19350.0, 19828.0, 20278.0,			VENGN	308
	* 26356.0, 21726.0,			VENGN	309
	* 649.0, 1003.0, 2030.0, 3440.0, 4935.0, 7052.0, 10159.0,			VENGN	310
	* 12089.0, 14530.0, 17083.0, 19067.0, 19750.0, 20235.0, 20660.0,			VENGN	311
	* 21287.0, 23160.0,			VENGN	312
335	* 699.0, 1057.0, 2111.0, 3332.0, 5036.0, 7207.0, 10356.0,			VENGN	313
	* 12304.0, 14741.0, 17176.0, 19433.0, 20100.0, 20598.0, 21094.0,			VENGN	314
	* 21665.0, 22514.0,			VENGN	315
	* DATA (EGTANH(1),1-69,149) /			VENGN	316
	* 710.0, 1000.0, 2150.0, 3545.0, 4892.0, 7312.0, 10400.0,			VENGN	317
340	* 12459.0, 14957.0, 17585.0, 19672.0, 20344.0, 20847.0, 21310.0,			VENGN	318
	* 21924.0, 22440.0,			VENGN	319

82/10122. 15.12.43

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SUBROUTINE YFNGD

A-137

74/175 DPY-2

THE EQUIPMENT TABLE LOOK-UP DATA HAS BEEN INCORPORATED FOR THE YAV-80

[illegible]

YAV-8B FGT LIMITS -	190 DEG.	9 R	A: GEAR UP
	174 DEG.	6 R	- NO. 6.1.1.6 A: GEAR DN
	132 DEG.	6 R	- NO. 6.1.1.6 U: GEAR DN
			- INCREASE FAN SPEED - + 4.1

** TYPE STATEMENTS

REAL
NR

COMMON STATEMENTS

A-144

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PAGE 3

82/13/22. 15.12.43

FTN 4.0+534

SUBROUTINE ENG08 74/175 007-2

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SUBROUTINE ENG08 74/175 UPT=2

2215	♦♦	DIMENSION STATEMENTS
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SUBROUTINE ENG04

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74/115 007-2

SUBROUTINE ENGOR

3345	..ALTAR / 0.0 , 500.0 , 1000.0 , 15000. , 20000. , 30000.0. ..RMT1L / 0.0 , .1 , .2 , .3 , .4 , .6 , .8 , 1.0 ..D3791 / 1.0 , 2.500. , 1000.6 , 1500.6 , 2000.0 , 3000.0. ..ALTAR / 5000. , .8 , .9 , .956 , .989 , 1. , 1.003 , 1.02 ..T49781 / 27.0 , 30.0 , 90.0 , 100.0 / ..RMTAL / 0.0 , 1.2 / DATA / 0.0 , 1.0 / ..RMT16TR / 0.0 , .0756 , .1512 , .2 , .2268 , .3024 , .4 , .6 , .8 ..RMT181 / 24.0 , 50.0 , 70.0 , 80.0 , 90.0 , 95.0 , 100.0 , 105.0 ..RMT19 / 0.0 , 10.0 , 20.0 , 55.0 , 60.0 , 61.0 , 90.0 , 94.5 / ..RMT20 / 40.0 , 50.0 , 60.0 , 70.0 , 80.0 , 90.0 , 100.0 , 105.0 ..RMT21 / 1.682 , 2.72 , 4.364 , 6.754 , 8.294 , 10.11 , 12.23 ..RMT22 / 60.0 , 70.0 , 80.0 , 90.0 , 100.0 , 105.0 , 110.0 / ..RMT23 / 0.0 , 10.0 , 20.0 / ..RMT24 / 20.0 , 27.0 , 30.0 , 35.0 , 40.0 , 45.0 , 50.0 , 55.0 ..RMT25 / 60.0 , 65.0 , 70.0 , 75.0 , 80.0 , 85.0 , 90.0 , 95.0 , 100.0 ..RMT26 / 10.0 , 10.0 / ..RMT27 / 0.0 , 35.0 , 70.0 , 81.0 , 98.0 / ..RMT28 / 0.0 , 20.0 / ..RMT29 / 70.0 , 80.0 / ..RMT30 / 1.0 / ..RMT31 / 1.0 / ..RMT32 / 1.0 / ..RMT33 / 1.0 / ..RMT34 / 1.0 / ..RMT35 / 1.0 / ..RMT36 / 1.0 / ..RMT37 / 1.0 / ..RMT38 / 1.0 / ..RMT39 / 1.0 / ..RMT40 / 1.0 / ..RMT41 / 1.0 / ..RMT42 / 1.0 / ..RMT43 / 1.0 / ..RMT44 / 1.0 / ..RMT45 / 1.0 / ..RMT46 / 1.0 / ..RMT47 / 1.0 / ..RMT48 / 1.0 / ..RMT49 / 1.0 / ..RMT50 / 1.0 / ..RMT51 / 1.0 / ..RMT52 / 1.0 / ..RMT53 / 1.0 / ..RMT54 / 1.0 / ..RMT55 / 1.0 / ..RMT56 / 1.0 / ..RMT57 / 1.0 / ..RMT58 / 1.0 / ..RMT59 / 1.0 / ..RMT60 / 1.0 / ..RMT61 / 1.0 / ..RMT62 / 1.0 / ..RMT63 / 1.0 / ..RMT64 / 1.0 / ..RMT65 / 1.0 / ..RMT66 / 1.0 / ..RMT67 / 1.0 / ..RMT68 / 1.0 / ..RMT69 / 1.0 / ..RMT70 / 1.0 / ..RMT71 / 1.0 / ..RMT72 / 1.0 / ..RMT73 / 1.0 / ..RMT74 / 1.0 / ..RMT75 / 1.0 / ..RMT76 / 1.0 / ..RMT77 / 1.0 / ..RMT78 / 1.0 / ..RMT79 / 1.0 / ..RMT80 / 1.0 / ..RMT81 / 1.0 / ..RMT82 / 1.0 / ..RMT83 / 1.0 / ..RMT84 / 1.0 / ..RMT85 / 1.0 / ..RMT86 / 1.0 / ..RMT87 / 1.0 / ..RMT88 / 1.0 / ..RMT89 / 1.0 / ..RMT90 / 1.0 / ..RMT91 / 1.0 / ..RMT92 / 1.0 / ..RMT93 / 1.0 / ..RMT94 / 1.0 / ..RMT95 / 1.0 / ..RMT96 / 1.0 / ..RMT97 / 1.0 / ..RMT98 / 1.0 / ..RMT99 / 1.0 / ..RMT100 / 1.0 / ..RMT101 / 1.0 / ..RMT102 / 1.0 / ..RMT103 / 1.0 / ..RMT104 / 1.0 / ..RMT105 / 1.0 / ..RMT106 / 1.0 / ..RMT107 / 1.0 / ..RMT108 / 1.0 / ..RMT109 / 1.0 / ..RMT110 / 1.0 / ..RMT111 / 1.0 / ..RMT112 / 1.0 / ..RMT113 / 1.0 / ..RMT114 / 1.0 / ..RMT115 / 1.0 / ..RMT116 / 1.0 / ..RMT117 / 1.0 / ..RMT118 / 1.0 / ..RMT119 / 1.0 / ..RMT120 / 1.0 / ..RMT121 / 1.0 / ..RMT122 / 1.0 / ..RMT123 / 1.0 / ..RMT124 / 1.0 / ..RMT125 / 1.0 / ..RMT126 / 1.0 / ..RMT127 / 1.0 / ..RMT128 / 1.0 / ..RMT129 / 1.0 / ..RMT130 / 1.0 / ..RMT131 / 1.0 / ..RMT132 / 1.0 / ..RMT133 / 1.0 / ..RMT134 / 1.0 / ..RMT135 / 1.0 / ..RMT136 / 1.0 / ..RMT137 / 1.0 / ..RMT138 / 1.0 / ..RMT139 / 1.0 / ..RMT140 / 1.0 / ..RMT141 / 1.0 / ..RMT142 / 1.0 / ..RMT143 / 1.0 / ..RMT144 / 1.0 / ..RMT145 / 1.0 / ..RMT146 / 1.0 / ..RMT147 / 1.0 / ..RMT148 / 1.0 / ..RMT149 / 1.0 / ..RMT150 / 1.0 / ..RMT151 / 1.0 / ..RMT152 / 1.0 / ..RMT153 / 1.0 / ..RMT154 / 1.0 / ..RMT155 / 1.0 / ..RMT156 / 1.0 / ..RMT157 / 1.0 / ..RMT158 / 1.0 / ..RMT159 / 1.0 / ..RMT160 / 1.0 / ..RMT161 / 1.0 / ..RMT162 / 1.0 / ..RMT163 / 1.0 / ..RMT164 / 1.0 / ..RMT165 / 1.0 / ..RMT166 / 1.0 / ..RMT167 / 1.0 / ..RMT168 / 1.0 / ..RMT169 / 1.0 / ..RMT170 / 1.0 / ..RMT171 / 1.0 / ..RMT172 / 1.0 / ..RMT173 / 1.0 / ..RMT174 / 1.0 / ..RMT175 / 1.0 / ..RMT176 / 1.0 / ..RMT177 / 1.0 / ..RMT178 / 1.0 / ..RMT179 / 1.0 / ..RMT180 / 1.0 / ..RMT181 / 1.0 / ..RMT182 / 1.0 / ..RMT183 / 1.0 / ..RMT184 / 1.0 / ..RMT185 / 1.0 / ..RMT186 / 1.0 / ..RMT187 / 1.0 / ..RMT188 / 1.0 / ..RMT189 / 1.0 / ..RMT190 / 1.0 / ..RMT191 / 1.0 / ..RMT192 / 1.0 / ..RMT193 / 1.0 / ..RMT194 / 1.0 / ..RMT195 / 1.0 / ..RMT196 / 1.0 / ..RMT197 / 1.0 / ..RMT198 / 1.0 / ..RMT199 / 1.0 / ..RMT200 / 1.0 / ..RMT201 / 1.0 / ..RMT202 / 1.0 / ..RMT203 / 1.0 / ..RMT204 / 1.0 / ..RMT205 / 1.0 / ..RMT206 / 1.0 / ..RMT207 / 1.0 / ..RMT208 / 1.0 / ..RMT209 / 1.0 / ..RMT210 / 1.0 / ..RMT211 / 1.0 / ..RMT212 / 1.0 / ..RMT213 / 1.0 / ..RMT214 / 1.0 / ..RMT215 / 1.0 / ..RMT216 / 1.0 / ..RMT217 / 1.0 / ..RMT218 / 1.0 / ..RMT219 / 1.0 / ..RMT220 / 1.0 / ..RMT221 / 1.0 / ..RMT222 / 1.0 / ..RMT223 / 1.0 / ..RMT224 / 1.0 / ..RMT225 / 1.0 / ..RMT226 / 1.0 / ..RMT227 / 1.0 / ..RMT228 / 1.0 / ..RMT229 / 1.0 / ..RMT230 / 1.0 / ..RMT231 / 1.0 / ..RMT232 / 1.0 / ..RMT233 / 1.0 / ..RMT234 / 1.0 / ..RMT235 / 1.0 / ..RMT236 / 1.0 / ..RMT237 / 1.0 / ..RMT238 / 1.0 / ..RMT239 / 1.0 / ..RMT240 / 1.0 / ..RMT241 / 1.0 / ..RMT242 / 1.0 / ..RMT243 / 1.0 / ..RMT244 / 1.0 / ..RMT245 / 1.0 / ..RMT246 / 1.0 / ..RMT247 / 1.0 / ..RMT248 / 1.0 / ..RMT249 / 1.0 / ..RMT250 / 1.0 / ..RMT25
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82710/22, 1, 12.43

FTN 4.8453H

SUBROUTINE ENCOR 74/175 70T=2

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* INITIALIZATION-FIRST PASS THROUGH PROGRAM
IF((INITIAL .EQ. 0) .A. (.RESET .NE. 0)) GO TO 120
C***** CALCULATE FUEL REMAINING
      IF ((IN FUEL .NE. 0) GO TO 110
      POFUEL = POFUEL - POFUEL*.000277*HFT
      110 CONTINUE
* PERCENT FUEL CALCULATION
      POFUEL = 100.*POFUEL / 71P5
      IF (POFUEL .GT. 100.0) POFUEL = 100.0
C**** CHECK FOR FUEL LOW OR RINGO FUEL WARNING
      IF (POFUEL .LE. 6) IFUELLOW = 1
      IF (POFUEL .LE. 5) IORINGO = 1
      IF (INITIAL .EQ. 0) GO TO 120
C*** RETURN TO MAIN PROGRAM AFTER OBTAINING FUEL WEIGHT
*
* FIRST PASS CALCULATION OF PHFCOP AND PFG
      PNECHN = 2.*100.0 - 12.25
      PNECOP = PNECHN*.5
      PNECOP = PNECOP*.5
      CALL FSRCH(PNECOP, PNEFB, 17, INFA, 1)
      CALL FSRCH(PNECOP, PNEFB, 10, INCH2, 2)
      TEMPI(1) = PNECOP
      PEGCOP = PFC(TEMP, MPTE, 1, BNDEL, FGTARU)
      PFG = PEGCOP*DELTO
      IF (INITIAL .EQ. 0) RETURN
      120 CONTINUE
C***** CALCULATE PAM RECOVERY
*
* MACH NUMBER INDEX AND RATIO
      CALL FSRCH(PNECOP, PNEFB, 1, INFL, 1)
      CALL FSRCH(PNECOP, PNEFB, 7, 2)
      NP-F2C(TEMP, MPTE, 2, BNDEL, 2, NRTABU)
      DELT12 = DELT1*NR

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515 C***** BLEED AIR CORRECTION FACTORS
* COMPUTE ENGINE AIRFLOW - 185/SEC
  CALL ESRCN (PNECOR,PNEFB,2,INER,1)
  PMA = (PMACOR + DELTY2) / ASORTT2
520
***+
* COMPUTE REACTION CONTROL BLEED LEAKAGE -ADD TO TOTAL FROM RCS ROUTINE
***+
  DURCS = (PHOZPOS - 0.017) / 1333
  DURCS = INT(14.4 * DURCS)
* FAN SPEEDS - 1000 RPM - 24.011 * 0.16705
  PNECS = (PNEFB - 24.011) / 0.16705
  DURCS = DURCS + PNECS * PMA
  RWTOT = RWTOT + DURCS
  IF RWTOT > 60.0 GO TO 130
  PFCBLDC = 0.0
  PFCBLDC = 0.0
  PFCBLDC = 0.0
  GO TO 140
130 CONTINUE
540 CALL ESRCN (PNECOR,PNEFB,7,INER,1)
  PFCBLDC = PFCBLDC + PNEFB * PMA
* COMPUTE BLEED CORRECTION FOR FUEL FLOW
  CALL ESRCN (PNECOR,PNEFB,10,6,INER,1)
  PFCBLDC = PFCBLDC + PNEFB * PMA
545 * COMPUTE BLEED CORRECTION FOR JET PIPE TEMPERATURE
  CALL ESRCN (PNECOR,PNEFB,11,4,INER,1)
  PFCBLDC = PFCBLDC + PNEFB * PMA
* COMPUTE BLEED CORRECTION FOR COMPRESSOR DISCHARGE PRESSURE
  CALL ESRCN (PNECOR,PNEFB,12,7,INER,1)
  PFCBLDC = PFCBLDC + PNEFB * PMA
140 CONTINUE
* WATER INJECTION SYSTEM
* COMPUTE NOZZLE POSITION EFFECTS ON JET PIPE TEMPERATURE - DRY
  CALL ESRCN (PNECOR,PNEFB,13,4,INER,1)
  PFCBLDC = PFCBLDC + PNEFB * PMA
  PFCBLDC = PFCBLDC + PNEFB * PMA
550
* COMPUTE NOZZLE POSITION EFFECTS ON JET PIPE TEMPERATURE - WET
  CALL ESRCN (PNECOR,PNEFB,14,5,INER,1)
  PFCBLDC = PFCBLDC + PNEFB * PMA
* CHECK FOR WATER SWITCH ON
  IF PFCBLDC > 10.0 GO TO 160
* COMPUTE WATER INJECTION CORRECTION TO FUEL FLOW WHEN WATER SWITCH ON
  CALL ESRCN (PNECOR,PNEFB,15,1,INER,1)
  PFCBLDC = PFCBLDC + PNEFB * PMA
* WATER FLOWS IF PUMP SPINDLE ANGLE GREATER THAN PSAN AND WATER AVAIL

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8210122. 15.12.43

1945-1946

SUBROUTINE ENG08 74/175 (081=2

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685  GO TO 240
220 CONTINUE
      QM1 = QM1 - QM1
      * SMDR1 = (1.0 - QM1) * QM1
      * SMDR2 = (1.0 - QM2) * QM2
      * SMDR3 = (1.0 - QM3) * QM3
      * SMDR4 = (1.0 - QM4) * QM4
      * SMDR5 = (1.0 - QM5) * QM5
      * SMDR6 = (1.0 - QM6) * QM6
      * SMDR7 = (1.0 - QM7) * QM7
      * SMDR8 = (1.0 - QM8) * QM8
      * SMDR9 = (1.0 - QM9) * QM9
      * SMDR10 = (1.0 - QM10) * QM10
      * SMDR11 = (1.0 - QM11) * QM11
      * SMDR12 = (1.0 - QM12) * QM12
      * SMDR13 = (1.0 - QM13) * QM13
      * SMDR14 = (1.0 - QM14) * QM14
      * SMDR15 = (1.0 - QM15) * QM15
      * SMDR16 = (1.0 - QM16) * QM16
      * SMDR17 = (1.0 - QM17) * QM17
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      * SMDR20 = (1.0 - QM20) * QM20
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      * SMDR157 = (1.0 - QM157) * QM157
      * SMDR158 = (1.0 - QM158) * QM158
      * SMDR159 = (1.0 - QM159) * QM159
      * SMDR160 = (1.0 - QM160) * QM160
      * SMDR161 = (1.0 - QM161) * QM161
      * SMDR162 = (1.0 - QM162) * QM162
      * SMDR163 = (1.0
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SUBROUTINE ENG08      74/175  OPT-2      82/10/22. 17.12.43      PAGE5

      *
      800      *      FKALY = E3C1EMPT,MPTE11,ANDEL7,FKALTU)
      *      COMPUTE SLAY ANGLE CORRECTION
      *      CALL FSRCH(PWFCOR,PNT19,10,INFIN,1)
      *      CALL FSRCH(PWFCOR,PNT21,10,INFIN,1)
      *      TEMPT(12) = PW0715
      *      PKSPLAY = E2CITEMPT,MPTE12,BNDEL6,FSCLAYU)
      *      PEG = (PWFCOR + PWFCG + PWGBLOC) * PKSPLAY + FKALT
      *      IF (PEG .LT. 0) PEG = 0.0
      *      INITIAL EGT = PWFCOR + EKKDAY + EKKND - PWFCINC - PWEGTC + PWGBLOC
      *      PEGDID = PEGICOR + AT1?
      *
      810      *      RAMP UNCORRECTED EGT TO TABLE VALUE
      *      IF (OUT1.EQ.1) PEGID = Y10
      *      PEG = (PEGDID - PEGIP) * PK4 + DELT + PEGTP
      *      EGT = DEGREES C/FUSUS
      *      PEGTC = 0.555 * (PEGI - 491.69) +
      *      PBN = PPHORX+DEL11? - PWGBLOC - 15.0
      *      PPHLD = PWBCOR*AT1?
      *
      820      *
      *      THERMOCOMPILE TEMPERATURE LIMIT WARNING
      *
      825      *      INITIALIZE
      *
      830      *      IF (ISTART.EQ.0) GO TO 260
      *      ISTART = PEGID
      *      PEGIP = PEGID
      *      PTC = PSA
      *      TIC = PEGIP
      *      PEGTI = PEGIP
      *      PEGCI = PEGIP
      *      PEGTA = PEGIP
      *      280 CONTINUE
      *
      840      *      PSARA = (PSA - PSAP) / DELT
      *      PSAP = PSA
      *      PEGTA = PEGIP
      *
      *      DETERMINE TANKOTTE SLAM
      *
      845      *      GO AROUND SLAM LOGIC IF DURING ENGINE START
      *      IF (PNCORP .LT. 1) PSARA = 0.0
      *      IF (PSARA .GT. 1) PSARA = PSARA + 5.0) GO TO 320
      *      IF (PSARA .GT. 1) PSARA = PSARA
      *      RAMP OUT DELT FGI IF RPM = RPM COMMANDED
      *
      850      *      IF (PNCORP .GT. PWFCOR) - XK1) GO TO 300
      *      IF (PSAR .LT. 100.0) GO TO 280
      *
      855      *

```

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PAGE 16

02/17/22. 15.12.43

FTN 4.8+53R

SUBROUTINE ENG08 74/175 OPT-2

```

*      ADD 135 DEGREES R IF LARGE SLAM
      PEGT = PEGT + 135.0
      IF (PTK .EQ. 1) PSAR = 0
      GO TO 320
290 CONTINUE
*      RAMP IN DELT EGT FOR SMALL SLAM
      PEGT = PEGT + (135.0 * (PSAR - 5.0) * .01052)
      IF (PTK .EQ. 1) PSAR = 0
      GO TO 320
300 CONTINUE
*      RAMP OUT DELT EGT
      TEMP = PNECOM1 - XK1 - PNERP4 + XK2
      IF (PSAR .GE. 100.0) GO TO 310
      PEGT = PEGT + (135.0 * (TEMP / XK2) * (PSAR - 5.0) * 0.01052)
      GO TO 320
310 PEGT = PEGT + (135.0 * (TEMP / XK2))
      PSAR = PSAR + (TEMP / XK2)
      GO TO 320
320 CONTINUE
      DELPEGT = PEGT - PEGTI
      TEMP = DELPEGT * 0.5
*      CALCULATE THERMOCOUPLE TEMPERATURE
      DELTW = (TEMP + PEGTI - TW) * 0.11 + DELT
      DELTTC = (DELW / 1.0 + 0.11 * DT02)
      IF (DELW .GT. 0.0) DELTTC = 1.0 + DT02
      IF (DELW .LT. 0.0) DELTTC = 0.0
      TW = TW + DELTTC
      PEGTI = PEGT
      TFC = (TFC - 491.69) * 0.555
      IF (TTC .GT. 1845.0 .A. 1) TFC = 1845.0
      IF (TTC .GT. 1803.0 .A. 1) TFC = 1803.0
*      CALCULATE THRUST FORCES AND MOMENTS
C ***
C      ANGLE TO ENGINE AXIS
      PNDP = (PNDP02 * 1.5) + DTOR
      PNDPJ = SIN(PNDP)
      PNDPI = COS(PNDP)
*      RAMP DRAG = PNDPI * V/C
*      SCRUB DRAG

```

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98-4609 M13

SUBROUTINE ENGON3 741175 MPI=2

61 1948

$$\begin{aligned} \text{PNOZCD} &= 0.96 + \text{PCNOZ} + 2. \\ \text{ONZG} &= \text{PNOZCD} - \text{PHZGOS} \\ \text{TEMPE} &= 98.5 + \text{DEI} \\ \text{ONZG} &= \text{AMN1}(\text{TEMPE} - \text{AMN1}(\text{ONZG} - \text{TEMPE})) \\ \text{PNOZPG} &= \text{PHZGOS} + \text{ONZG} \\ \text{PNOZPGS} &= \text{AMN1}(98.5 + \text{AMN1}(\text{PNOZPGS} - 2.)) \end{aligned}$$

```

1035 C***** UPDATE ENGINE RPM
      RPM = PNFRPM
      RETURN
1040 END

```

SYMBOLIC REFERENCE MAP (R=2)	DEF LINE	REFERENCES
ENTRY POINTS	1	497
ENG08		1039

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A-165

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VARIABLES	SUBROUTINE	ENGOR	SM	TYPE	74/175	OPT=2	REFLOCATION	FTN 4.8-534	82/10/22. 15.12.43	PAGE	24
3322	PNOITB	REAL			ARRAY			907	907	1032	1033
3323	PNOITB	REAL			ARRAY			908	908		
3324	PNOITB	REAL			ARRAY			909	909		
3325	PPH	REAL			ARRAY			910	910		
3326	PPHLOC	REAL			ARRAY			911	911		
3327	PPHLOC	REAL			ARRAY			912	912		
3328	PPHLOC	REAL			ARRAY			913	913		
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3333	PPHLOC	REAL			ARRAY			918	918		
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SOUTH ATLANTIC OCEAN MAP (R-2)

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PAGE 3

82710770, 15.12.50

FTN 4.81538

SURROUTINE PCS07 74/176 001-2

SURROUTINE PCS07

COMMON / FARRY / S(1001)

TYPE STATEMENTS

INTEGER

POINTER

POINTER

EQUIVALENCE STATEMENTS

EQUIVALENCE

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PAGE 1

02/10/22, 15.12.52

FTM 4.6+38

SUBROUTINE DECAT 74/175 3P122

SUBROUTINE DECAT

COMMON / FORTY / F(1001)

10 EQUIVALENCE STATEMENTS

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80 EQUIVALENCE (F(1131),

82 EQUIVALENCE (F(1131),

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PAGE 3

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SUBROUTINE SFC07 74/175 OPT=2

SUBROUTINE SFC07

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* TYPE STATEMENTS

* REAL LVFR

* COMMON STATEMENTS

* COMMON / FAPRAY / F(1001)

* EQUIVALENCE STATEMENTS

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FVN 4. A + 53A

SUBROUTINE SFC07 74/175 DPT-2

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FTN 4.8+530

74/175 OPT-2

SUBROUTINE SF07

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230 * 113 CONTINUE
231 * SIMULSTE = 27 DEG VOLTAGE BIAS DIFFERENTIAL WITH MONF SWITCH DOWN
232 * DELTAOMT = 10.0
233 * VEL = 170. + DV
234 * IF VKT.LT.VEL GO TO 115
235 * DV = DV + DV0
236 * VFLAG = 1
237 * RATE1 = 25.0
238 * RATE2 = -RATE1
239 * DELTA = 11.0 * DELTAOMT
240 * IF DELTA.LT.0.01 * VELR :A: DELTA = 0.01 * VELR :B: RATE1 = -RATE2
241 * GO TO 102
242 * DOWN MONF FOR AIRSPEEDS LT 155 KTS
243 * 115 CONTINUE
244 * IF DELTA.LT.0.01 * VELR :A: DELTA = 0.01 * VELR :B: RATE1 = -RATE2
245 * RATE2 = -RATE1
246 * GO TO 102
247 * 121 CONTINUE
248 * IF DELTA.LT.0.01 * VELR :A: DELTA = 0.01 * VELR :B: RATE1 = -RATE2
249 * RATE2 = -RATE1
250 * GO TO 102
251 * 120 CONTINUE
252 * IF DELTA.LT.0.01 * VELR :A: DELTA = 0.01 * VELR :B: RATE1 = -RATE2
253 * RATE2 = -RATE1
254 * GO TO 102
255 * 102 CONTINUE
256 * ORIGINATED ALTERN LOGIC
257 * IF MONF.NE.01 GO TO 107
258 * RATE1 = 0.0
259 * GO TO 108
260 * 107 CONTINUE
261 * IF MONF.EQ.1.0 * TIME8.GT.0.1 GO TO 108
262 * GO TO 140
263 * 141 CONTINUE
264 * TIME8 = TIME8 - DTOT2
265 * IF MONF.EQ.1.0 * TIME8 - DTOT2
266 * RATE1 = 0.0
267 * GO TO 108
268 * 140 CONTINUE
269 * IF VKT.LT.10.0 * DV
270 * VFLAG = 1
271 * GO TO 109

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PAGE

02/11/08, 19.01.59

FTN 4.8+538

74/175 OPT-2

SURPRITIME SECT

DEF LINE REFERENCES

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82/11/0A. 19.01.59

FTN 6. A + 538

SURPOUTINE WTRAL07 74/175 OPT#2

A-209

ORIGINAL PAGE IS
OF POOR QUALITY

PAGE 3

82/11/09. 19.01.59

FTN 4.8.538

SURROUTINE WTRAL07 74/175 OPT=2

```

115      :      RMLTOST / 53.0 , 0.0 , 11.0 / , 26.0 , 0.0 , 0.0 , 0.0 , 0.0 /
120      IF (INITIAL .EQ. 0) GO TO 1
125      *      OPERATING WEIGHT CLEAN AIRCRAFT - 12952
130      *      UNUSABLE FUEL - 45
135      *      CENTERLINE PYLON - 52
140      *      INTERMEDIATE PYLONS - 210
145      *      INTERMEDIATE PYLONS - 193
150      *      GUN PINS - 58
155      *      WEIGHT EMPTY FLIGHT TEST AIRCRAFT - 13847
160      *      MOMENTS IN LB-IN.
165      *      DRYMMX = 4772002.
170      *      DRYMMY = 911.
      *      DRYMMZ = 1336961.

1      CONTINUE
      *      GEAR AND LIDS LOGIC
10  DO 10 I=1,7
15  RGEAR(I) = RMLNOST(I) * 0.0
20  IF (RGEAR(I) .GT. 0.0) GO TO 20
30  DO 30 J=1,7
35  RGEAR(I,J) = RGEAR(I)
40  IF (RMLNOST(I) .GT. 0.0) GO TO 40
50  RMLNOST(I) = RMLNOST(I)
60  CONTINUE
      *      CALCULATE FUEL INERTIAS
      *      CALL FSCHE(FUEL, SWT, 7, WTA, 1)
      *      RXY = FSCHE(FUEL, 7, WTA, 1)
      *      RYZ = FSCHE(FUEL, 7, WTA, 1)
      *      RZX = FSCHE(FUEL, 7, WTA, 1)
      *      RZY = FSCHE(FUEL, 7, WTA, 1)
      *      RZX = FSCHE(FUEL, 7, WTA, 1)
      *      RZY = FSCHE(FUEL, 7, WTA, 1)
      *      CALCULATE FUEL MOMENTS
      *      FUELX = FSCHE(FUEL, 7, WTA, 1)
      *      FUELZ = FSCHE(FUEL, 7, WTA, 1)
      *      CALCULATE WATER INERTIAS
      *      CALL FSCHE(WATER, SWT, 3, WTA, 1)
      *      RXY = FSCHE(WATER, 3, WTA, 1)
      *      RYZ = FSCHE(WATER, 3, WTA, 1)
      *      RZX = FSCHE(WATER, 3, WTA, 1)
      *      RZY = FSCHE(WATER, 3, WTA, 1)
      *      RZX = FSCHE(WATER, 3, WTA, 1)
      *      RZY = FSCHE(WATER, 3, WTA, 1)

```

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OF POOR QUALITY

PAGE 4

92/11/08, 19.01.59

FTN 4.4+538

SUBROUTINE WTRAL07 74/175 DPT=2

```

* *
* * CALCULATE WATER MOMENTS
* *
175 H2OMOMX = FIB(PWATER,3,BUD,HMOMX)
   H2OMOMZ = FIB(PWATER,3,BUD,HMOMZ)

180 WEIGHT = DRY + FUEL + PWATER
   MASS = WEIGHT / G
* *
* * RTASES (RSMOMX,ETC.) CAN BE ADDED TO TOTAL MOMENTS.
* *
185 TOTMOMX = DRYMOMX + FUELHMX + H2OMOMX + RMGEAR(1) + RM[DS(1)] + RSMOMX
   TOTMOMY = DRYMOMY + FUELHY + H2OMOMY + RMGEAR(2) + RM[DS(2)] + RSMOMY
   TOTMOMZ = DRYMOMZ + FUELHZ + H2OMOMZ + RMGEAR(3) + RM[DS(3)] + RSMOMZ
* *
* * CG LOCATION IN INCHES.
* *
190 CGXS = TOTMOMX/WEIGHT
   CGYL = TOTMOMY/WEIGHT
* *
* * CG IN PERCENT MAC
* *
195 CG = (CGXS - 336.3) / 99.792
* *
* * COMPUTE TOTAL INERTIAS
* *
200 R1XX = R1XX + H2OPXX + RMGEAR(4) + RM[DS(4)]
   R1YY = R1YY + H2OPYY + RMGEAR(5) + RM[DS(5)]
   R1ZZ = R1ZZ + H2OPZZ + RMGEAR(6) + RM[DS(6)]
   R1XZ = R1XZ + H2OPXZ + RMGEAR(7) + RM[DS(7)]
   TEMP = R1XX*R1ZZ - R1XZ*R1XZ
   ICON(1) = R1ZZ/TEMP
   ICON(2) = R1XZ/TEMP
   ICON(3) = R1XX/TEMP - R1YY + R1ZZ/TEMP
   ICON(4) = (R1ZZ*(R1YY - R1ZZ) - R1XZ*(R1XZ + R1Z)) / TEMP
   ICON(5) = (R1XZ*(R1YY - R1ZZ) - R1XX*(R1XZ + R1Z)) / TEMP
   ICON(6) = (R1XZ*(R1YY - R1ZZ) - R1XX*(R1XZ + R1Z)) / TEMP
   ICON(7) = (R1XZ*(R1YY - R1ZZ) - R1XX*(R1XZ + R1Z)) / TEMP
   ICON(8) = (R1XZ*(R1YY - R1ZZ) - R1XX*(R1XZ + R1Z)) / TEMP
   ICON(9) = (R1XZ*(R1YY - R1ZZ) - R1XX*(R1XZ + R1Z)) / TEMP
   ICON(10) = (R1XZ*(R1YY - R1ZZ) - R1XX*(R1XZ + R1Z)) / TEMP
   END

```

SYMBOLIC REFERENCE MAP (P=2)

ORIGINAL PAGE
OF POOR QUALITY

SURPOUTLINE WTRAL07		74/175	OPT-2	FTN 4.0+538		P2/11/08. 19.01.59	PAGE	6
VARIABLES	SN	TYPE	RELOCATION					
2352 RIXZ	REAL		FARFAY	203	211	212	2+213	214
2360 RIVY	REAL		FARFAY	204	213	214	215	216
2361 R177	REAL		FARFAY	205	210	212	2+213	215
2363 RMAS	REAL		FARFAY	206	210	205		
445 RMGEAR	REAL		FARFAY	207	210	205		
427 RMGEART	REAL		ARRAY	208	210	203	204	205
454 RMLINS	REAL		ARRAY	209	210	203	204	205
436 RMLDST	REAL		ARRAY	210	210	203	204	205
315 RMLDST	REAL		ARRAY	211	210	203	204	205
316 RMLDST	REAL		ARRAY	212	210	203	204	205
317 RMLDST	REAL		ARRAY	213	210	203	204	205
2342 RMLDST	REAL		ARRAY	214	210	203	204	205
EXTERNALS	TYPE	APGS	REFERENCES					
FSRCH	REAL	5	156					
FIN	REAL	4	157					
STATEMENT LABELS			REFERENCES					
10 1			156					
20 10			157					
30 30			158					
40 30			159					
50 50			160					
100PS LABEL	INDEX	FROM-TO	LENGTH					
11 10		145	38					
12 10		146	38					
25 50		147	38					
COMMON BLOCKS	LENGTH							
COMMON FARFAY	2000							
STATISTICS								
COMMON LENGTH	3728							
COMMON LENGTH	2000							
COMMON CM USED								

ORIGINAL PAGE 13
OF POOR QUALITY

PAGE 1

8710720 15.12.50

ETH 4.843A

74175 10702

SEQUENCE 1001(4)

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** THIS SUBROUTINE IS PART 1 OF THE TRANSLATIONAL EQUATIONS OF MOTION.
** IN CALL ARGUMENT IS (M)
** AIRCRAFT NUMBER (1,2,3,...,M) WHERE M IS THE TOTAL NUMBER OF
** AIRCRAFT.
**
** C-ARRAY INPUT DEFINITIONS
**
** DEGR-5 TO 9: RADIAN CONVERSION FACTOR
** DEGR-10 TO 14: RADIAN CONVERSION FACTOR
** DEGR-15 TO 19: RADIAN CONVERSION FACTOR
** DEGR-20 TO 24: RADIAN CONVERSION FACTOR
** DEGR-25 TO 29: RADIAN CONVERSION FACTOR
** DEGR-30 TO 34: RADIAN CONVERSION FACTOR
** DEGR-35 TO 39: RADIAN CONVERSION FACTOR
** DEGR-40 TO 44: RADIAN CONVERSION FACTOR
** DEGR-45 TO 49: RADIAN CONVERSION FACTOR
** DEGR-50 TO 54: RADIAN CONVERSION FACTOR
** DEGR-55 TO 59: RADIAN CONVERSION FACTOR
** DEGR-60 TO 64: RADIAN CONVERSION FACTOR
** DEGR-65 TO 69: RADIAN CONVERSION FACTOR
** DEGR-70 TO 74: RADIAN CONVERSION FACTOR
** DEGR-75 TO 79: RADIAN CONVERSION FACTOR
** DEGR-80 TO 84: RADIAN CONVERSION FACTOR
** DEGR-85 TO 89: RADIAN CONVERSION FACTOR
** DEGR-90 TO 94: RADIAN CONVERSION FACTOR
** DEGR-95 TO 99: RADIAN CONVERSION FACTOR
**
** A-ARRAY INPUT DEFINITIONS
**
** X: AIRCRAFT X MEDIAL VELOCITY COMPONENT IN FEET/SECOND
** Y: AIRCRAFT Y MEDIAL VELOCITY COMPONENT IN FEET/SECOND
** Z: AIRCRAFT Z MEDIAL VELOCITY COMPONENT IN FEET/SECOND
** ATN: AIRCRAFT ATAN OF ALTITUDE IN DEGREES
** VS: AIRCRAFT VS LOCAL SPEED OF SOUND IN FEET/SECOND
** WE: AIRCRAFT WE WIND NORTH-EAST-PATH COMPONENT IN FEET/SECOND
**
** A-ARRAY OUTPUT DEFINITIONS
**
** PCOS1: AIRCRAFT PCOS1 PROJECTION ON INITIAL X-Y PLANE IN FEET
** PCOS2: AIRCRAFT PCOS2 PROJECTION ON INITIAL X-Y PLANE IN FEET
** COS1: COSINE OF AIRCRAFT LATITUDE
** COS2: COSINE OF AIRCRAFT LATITUDE
** SIN1: SINE OF AIRCRAFT LATITUDE
** SIN2: SINE OF AIRCRAFT LATITUDE
** TAN1: AIRCRAFT TAN LATITUDE IN DEGREES
** TAN2: AIRCRAFT TAN LATITUDE IN DEGREES
** RAD1: AIRCRAFT RAD LATITUDE IN FEET
** RAD2: AIRCRAFT RAD LATITUDE IN FEET
** ALT1: AIRCRAFT ALTITUDE IN FEET
** ALT2: AIRCRAFT ALTITUDE IN FEET
** ALT3: AIRCRAFT ALTITUDE IN FEET
** ALT4: AIRCRAFT ALTITUDE IN FEET
** ALT5: AIRCRAFT ALTITUDE IN FEET
** ALT6: AIRCRAFT ALTITUDE IN FEET
** ALT7: AIRCRAFT ALTITUDE IN FEET
** ALT8: AIRCRAFT ALTITUDE IN FEET
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** ALT98: AIRCRAFT ALTITUDE IN FEET
** ALT99: AIRCRAFT ALTITUDE IN FEET

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A-216

A-219

VARIABLE	STATEMENT	TYPE	SYMBOL	ADDRESS	LENGTH	OFF LINE	DIFFERENCES	FIN	4,000-510	02/10/22, 15.12.59	0000
2013	STATE	STATE	STATE	200	100	100	100	213	256	00000000	252
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2015	STATE	STATE	STATE	200	100	100	100	215	256	00000000	252
2016	STATE	STATE	STATE	200	100	100	100	216	256	00000000	252
2017	STATE	STATE	STATE	200	100	100	100	217	256	00000000	252
2018	STATE	STATE	STATE	200	100	100	100	218	256	00000000	252
2019	STATE	STATE	STATE	200	100	100	100	219	256	00000000	252
2020	STATE	STATE	STATE	200	100	100	100	220	256	00000000	252
2021	STATE	STATE	STATE	200	100	100	100	221	256	00000000	252
2022	STATE	STATE	STATE	200	100	100	100	222	256	00000000	252
2023	STATE	STATE	STATE	200	100	100	100	223	256	00000000	252
2024	STATE	STATE	STATE	200	100	100	100	224	256	00000000	252
2025	STATE	STATE	STATE	200	100	100	100	225	256	00000000	252
2026	STATE	STATE	STATE	200	100	100	100	226	256	00000000	252
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2029	STATE	STATE	STATE	200	100	100	100	229	256	00000000	252
2030	STATE	STATE	STATE	200	100	100	100	230	256	00000000	252
2031	STATE	STATE	STATE	200	100	100	100	231	256	00000000	252
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2038	STATE	STATE	STATE	200	100	100	100	238	256	00000000	252
2039	STATE	STATE	STATE	200	100	100	100	239	256	00000000	252
2040	STATE	STATE	STATE	200	100	100	100	240	256	00000000	252
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2044	STATE	STATE	STATE	200	100	100	100	244	256	00000000	252
2045	STATE	STATE	STATE	200	100	100	100	245	256	00000000	252
2046	STATE	STATE	STATE	200	100	100	100	246	256	00000000	252
2047	STATE	STATE	STATE	200	1						

ORIGINAL PAGE IS
OF POOR QUALITY

4

PAGE

02/10/72, 15,12,59

FTN 4,00030

SYMBOL	TYPE	76/176	007-2
STATISTICS	TYPE	AGES	REFERENCES
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0	1	111	200

2219122. 15.12.44

FTN 4. H453A

741175 10102

10010630 701106015

*** THIS SUBMITTER IS NOT A LEAD ORGANIZATIONAL FOUNDATIONS OF AMERICA. ***
 *** THE CALL ARGUMENT IS (M) ***
 *** THE DISCRETE NUMBER (1,2,3,...,M) WHERE M IS THE TOTAL NUMBER OF ***
 *** ALLELES. ***

1. ARCADE IN-OUT OPERATIONS
 2. DEGREES TO Radians CONVERSION FACTOR
 3. DEGREES TO DECIMALS CONVERSION FACTOR
 4. CURRENT LOCATION TIME CURRENT TIME
 5. TIME SET FLAG

4-APR 1964 OFFICIALS

[illegible]

4-1004Y CURTIS DEFECTION 9

* CXX	AIRCRAFT IN FREIGHT	TRANSPORTATION MATRIN
* CXX	AIRCRAFT IN FRESH-CASE	CONV TO BODY TRANSPORTATION MATRIN
* CXX	AIRCRAFT IN YAW ANGLE	IN DEGREES
* CXX	AIRCRAFT IN PITCH ANGLE	IN DEGREES

+ COS11 SINE OF ARC 11° 11' 11" IN RADIANS
 + COS12 SINE OF ARC 12° 12' 12" IN RADIANS
 + COS13 SINE OF ARC 13° 13' 13" IN RADIANS
 + COS14 SINE OF ARC 14° 14' 14" IN RADIANS
 + COS15 SINE OF ARC 15° 15' 15" IN RADIANS
 + COS16 SINE OF ARC 16° 16' 16" IN RADIANS
 + COS17 SINE OF ARC 17° 17' 17" IN RADIANS
 + COS18 SINE OF ARC 18° 18' 18" IN RADIANS
 + COS19 SINE OF ARC 19° 19' 19" IN RADIANS
 + COS20 SINE OF ARC 20° 20' 20" IN RADIANS
 + COS21 SINE OF ARC 21° 21' 21" IN RADIANS
 + COS22 SINE OF ARC 22° 22' 22" IN RADIANS
 + COS23 SINE OF ARC 23° 23' 23" IN RADIANS
 + COS24 SINE OF ARC 24° 24' 24" IN RADIANS
 + COS25 SINE OF ARC 25° 25' 25" IN RADIANS
 + COS26 SINE OF ARC 26° 26' 26" IN RADIANS
 + COS27 SINE OF ARC 27° 27' 27" IN RADIANS
 + COS28 SINE OF ARC 28° 28' 28" IN RADIANS
 + COS29 SINE OF ARC 29° 29' 29" IN RADIANS
 + COS30 SINE OF ARC 30° 30' 30" IN RADIANS
 + COS31 SINE OF ARC 31° 31' 31" IN RADIANS
 + COS32 SINE OF ARC 32° 32' 32" IN RADIANS
 + COS33 SINE OF ARC 33° 33' 33" IN RADIANS
 + COS34 SINE OF ARC 34° 34' 34" IN RADIANS
 + COS35 SINE OF ARC 35° 35' 35" IN RADIANS
 + COS36 SINE OF ARC 36° 36' 36" IN RADIANS
 + COS37 SINE OF ARC 37° 37' 37" IN RADIANS
 + COS38 SINE OF ARC 38° 38' 38" IN RADIANS
 + COS39 SINE OF ARC 39° 39' 39" IN RADIANS
 + COS40 SINE OF ARC 40° 40' 40" IN RADIANS
 + COS41 SINE OF ARC 41° 41' 41" IN RADIANS
 + COS42 SINE OF ARC 42° 42' 42" IN RADIANS
 + COS43 SINE OF ARC 43° 43' 43" IN RADIANS
 + COS44 SINE OF ARC 44° 44' 44" IN RADIANS
 + COS45 SINE OF ARC 45° 45' 45" IN RADIANS
 + COS46 SINE OF ARC 46° 46' 46" IN RADIANS
 + COS47 SINE OF ARC 47° 47' 47" IN RADIANS
 + COS48 SINE OF ARC 48° 48' 48" IN RADIANS
 + COS49 SINE OF ARC 49° 49' 49" IN RADIANS
 + COS50 SINE OF ARC 50° 50' 50" IN RADIANS
 + COS51 SINE OF ARC 51° 51' 51" IN RADIANS
 + COS52 SINE OF ARC 52° 52' 52" IN RADIANS
 + COS53 SINE OF ARC 53° 53' 53" IN RADIANS
 + COS54 SINE OF ARC 54° 54' 54" IN RADIANS
 + COS55 SINE OF ARC 55° 55' 55" IN RADIANS
 + COS56 SINE OF ARC 56° 56' 56" IN RADIANS
 + COS57 SINE OF ARC 57° 57' 57" IN RADIANS
 + COS58 SINE OF ARC 58° 58' 58" IN RADIANS
 + COS59 SINE OF ARC 59° 59' 59" IN RADIANS
 + COS60 SINE OF ARC 60° 60' 60" IN RADIANS
 + COS61 SINE OF ARC 61° 61' 61" IN RADIANS
 + COS62 SINE OF ARC 62° 62' 62" IN RADIANS
 + COS63 SINE OF ARC 63° 63' 63" IN RADIANS
 + COS64 SINE OF ARC 64° 64' 64" IN RADIANS
 + COS65 SINE OF ARC 65° 65' 65" IN RADIANS
 + COS66 SINE OF ARC 66° 66' 66" IN RADIANS
 + COS67 SINE OF ARC 67° 67' 67" IN RADIANS
 + COS68 SINE OF ARC 68° 68' 68" IN RADIANS
 + COS69 SINE OF ARC 69° 69' 69" IN RADIANS
 + COS70 SINE OF ARC 70° 70' 70" IN RADIANS
 + COS71 SINE OF ARC 71° 71' 71" IN RADIANS
 + COS72 SINE OF ARC 72° 72' 72" IN RADIANS
 + COS73 SINE OF ARC 73° 73' 73" IN RADIANS
 + COS74 SINE OF ARC 74° 74' 74" IN RADIANS
 + COS75 SINE OF ARC 75° 75' 75" IN RADIANS
 + COS76 SINE OF ARC 76° 76' 76" IN RADIANS
 + COS77 SINE OF ARC 77° 77' 77" IN RADIANS
 + COS78 SINE OF ARC 78° 78' 78" IN RADIANS
 + COS79 SINE OF ARC 79° 79' 79" IN RADIANS
 + COS80 SINE OF ARC 80° 80' 80" IN RADIANS
 + COS81 SINE OF ARC 81° 81' 81" IN RADIANS
 + COS82 SINE OF ARC 82° 82' 82" IN RADIANS
 + COS83 SINE OF ARC 83° 83' 83" IN RADIANS
 + COS84 SINE OF ARC 84° 84' 84" IN RADIANS
 + COS85 SINE OF ARC 85° 85' 85" IN RADIANS
 + COS86 SINE OF ARC 86° 86' 86" IN RADIANS
 + COS87 SINE OF ARC 87° 87' 87" IN RADIANS
 + COS88 SINE OF ARC 88° 88' 88" IN RADIANS
 + COS89 SINE OF ARC 89° 89' 89" IN RADIANS
 + COS90 SINE OF ARC 90° 90' 90" IN RADIANS
 + COS91 SINE OF ARC 91° 91' 91" IN RADIANS
 + COS92 SINE OF ARC 92° 92' 92" IN RADIANS
 + COS93 SINE OF ARC 93° 93' 93" IN RADIANS
 + COS94 SINE OF ARC 94° 94' 94" IN RADIANS
 + COS95 SINE OF ARC 95° 95' 95" IN RADIANS
 + COS96 SINE OF ARC 96° 96' 96" IN RADIANS
 + COS97 SINE OF ARC 97° 97' 97" IN RADIANS
 + COS98 SINE OF ARC 98° 98' 98" IN RADIANS
 + COS99 SINE OF ARC 99° 99' 99" IN RADIANS
 + COS100 SINE OF ARC 100° 100' 100" IN RADIANS
 + COS101 SINE OF ARC 101° 101' 101" IN RADIANS
 + COS102 SINE OF ARC 102° 102' 102" IN RADIANS
 + COS103 SINE OF ARC 103° 103' 103" IN RADIANS
 + COS104 SINE OF ARC 104° 104' 104" IN RADIANS
 + COS105 SINE OF ARC 105° 105' 105" IN RADIANS
 + COS106 SINE OF ARC 106° 106' 106" IN RADIANS
 + COS107 SINE OF ARC 107° 107' 107" IN RADIANS
 + COS108 SINE OF ARC 108° 108' 108" IN RADIANS
 + COS109 SINE OF ARC 109° 109' 109" IN RADIANS
 + COS110 SINE OF ARC 110° 110' 110" IN RADIANS
 + COS111 SINE OF ARC 111° 111' 111" IN RADIANS
 + COS112 SINE OF ARC 112° 112' 112" IN RADIANS
 + COS113 SINE OF ARC 113° 113' 113" IN RADIANS
 + COS114 SINE OF ARC 114° 114' 114" IN RADIANS
 + COS115 SINE OF ARC 115° 115' 115" IN RADIANS
 + COS116 SINE OF ARC 116° 116' 116" IN RADIANS
 + COS117 SINE OF ARC 117° 117' 117" IN RADIANS
 + COS118 SINE OF ARC 118° 118' 118" IN RADIANS
 + COS119 SINE OF ARC 119° 119' 119" IN RADIANS
 + COS120 SINE OF ARC 120° 120' 120" IN RADIANS
 + COS121 SINE OF ARC 121° 121' 121" IN RADIANS
 + COS122 SINE OF ARC 122° 122' 122" IN RADIANS
 + COS123 SINE OF ARC 123° 123' 123" IN RADIANS
 + COS124 SINE OF ARC 124° 124' 124" IN RADIANS
 + COS125 SINE OF ARC 125° 125' 125" IN RADIANS
 + COS126 SINE OF ARC 126° 126' 126" IN RADIANS
 + COS127 SINE OF ARC 127° 127' 127" IN RADIANS
 + COS128 SINE OF ARC 128° 128' 128" IN RADIANS
 + COS129 SINE OF ARC 129° 129' 129" IN RADIANS
 + COS130 SINE OF ARC 130° 130' 130" IN RADIANS
 + COS131 SINE OF ARC 131° 131' 131" IN RADIANS
 + COS132 SINE OF ARC 132° 132' 132" IN RADIANS
 + COS133 SINE OF ARC 133° 133' 133" IN RADIANS
 + COS134 SINE OF ARC 134° 134' 134" IN RADIANS
 + COS135 SINE OF ARC 135° 135' 135" IN RADIANS
 + COS136 SINE OF ARC 136° 136' 136" IN RADIANS
 + COS137 SINE OF ARC 137° 137' 137" IN RADIANS
 + COS138 SINE OF ARC 138° 138' 138" IN RADIANS
 + COS139 SINE OF ARC 139° 139' 139" IN RADIANS
 + COS140 SINE OF ARC 140° 140' 140" IN RADIANS
 + COS141 SINE OF ARC 141° 141' 141" IN RADIANS
 + COS142 SINE OF ARC 142° 142' 142" IN RADIANS
 + COS143 SINE OF ARC 143° 143' 143" IN RADIANS
 + COS144 SINE OF ARC 144° 144' 144" IN RADIANS
 + COS145 SINE OF ARC 145° 145' 145" IN RADIANS
 + COS146 SINE OF ARC 146° 146' 146" IN RADIANS
 + COS147 SINE OF ARC 147° 147' 147" IN RADIANS
 + COS148 SINE OF ARC 148° 148' 148" IN RADIANS
 + COS149 SINE OF ARC 149° 149' 149" IN RADIANS

[illegible]

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[illegible]

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PAGE 2

*2/10/22. 15.12.58

FIN 4.84538

74/175 001.2

SMO2000110F 4:00M

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SYMBOLIC REFERENCE MAP (R-2)

74/175 00122

FTN 4.0+33A

02/10/22, 15.12.50

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SYMBOLIC REFERENCE MAP (R-2)

74/175 00122

FTN 4.0+33A

02/10/22, 15.12.50

DIFF 4

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A-230

2280111 10.12.99

FIN 40A+53A

741175 75132

A-232

ORIGINAL PAGE IS
OF POOR QUALITY

PAGE 1

R2710/22, 15,13,04

FIN 4.8+534

74/175 OPT=2

```

1  SUBROUTINE STNDAY
5
10  ** U.S. STANDARD ATMOSPHERE, 1962 -- PREPARED UNDER SPONSORSHIP OF:
    ** ENVIRONMENTAL SCIENCE SERVICES ADMINISTRATION
    ** NATIONAL AERONAUTICS AND SPACE ADMINISTRATION
    ** UNITED STATES AIR FORCE
15  ** 1962 STANDARD ATMOSPHERE (45M, SPRING/FALL) - SEA LEVEL TO 100000 FEET
    **
    ** DATA (GEOMETRIC ALTITUDE POINTS(1), I=1, 511)
    ** A 0.00, 2000.00, 3000.00, 4000.00, 5000.00,
    ** B 1000.00, 7000.00, 3000.00, 1000.00, 1000.00,
    ** C 1000.00, 12000.00, 1000.00, 1000.00, 1000.00,
    ** D 1000.00, 12000.00, 1000.00, 1000.00, 1000.00,
    ** E 1000.00, 12000.00, 1000.00, 1000.00, 1000.00,
    ** F 1000.00, 12000.00, 1000.00, 1000.00, 1000.00,
    ** G 1000.00, 12000.00, 1000.00, 1000.00, 1000.00,
    ** H 1000.00, 12000.00, 1000.00, 1000.00, 1000.00,
    ** I 1000.00, 12000.00, 1000.00, 1000.00, 1000.00,
    ** J 1000.00, 12000.00, 1000.00, 1000.00, 1000.00,
    ** K 1000.00, 12000.00, 1000.00, 1000.00, 1000.00,
    ** L 1000.00, 12000.00, 1000.00, 1000.00, 1000.00,
    ** M 1000.00, 12000.00, 1000.00, 1000.00, 1000.00,
    ** N 1000.00, 12000.00, 1000.00, 1000.00, 1000.00,
    ** O 1000.00, 12000.00, 1000.00, 1000.00, 1000.00,
    ** P 1000.00, 12000.00, 1000.00, 1000.00, 1000.00,
    ** Q 1000.00, 12000.00, 1000.00, 1000.00, 1000.00,
    ** R 1000.00, 12000.00, 1000.00, 1000.00, 1000.00,
    ** S 1000.00, 12000.00, 1000.00, 1000.00, 1000.00,
    ** T 1000.00, 12000.00, 1000.00, 1000.00, 1000.00,
    ** U 1000.00, 12000.00, 1000.00, 1000.00, 1000.00,
    **
    ** DATA (GEOMETRIC ALTITUDE POINTS(1), I=52, 1011)
    ** A 1000.00, 52000.00, 52000.00, 52000.00, 52000.00,
    ** B 1000.00, 52000.00, 52000.00, 52000.00, 52000.00,
    ** C 1000.00, 52000.00, 52000.00, 52000.00, 52000.00,
    ** D 1000.00, 52000.00, 52000.00, 52000.00, 52000.00,
    ** E 1000.00, 52000.00, 52000.00, 52000.00, 52000.00,
    ** F 1000.00, 52000.00, 52000.00, 52000.00, 52000.00,
    ** G 1000.00, 52000.00, 52000.00, 52000.00, 52000.00,
    ** H 1000.00, 52000.00, 52000.00, 52000.00, 52000.00,
    ** I 1000.00, 52000.00, 52000.00, 52000.00, 52000.00,
    ** J 1000.00, 52000.00, 52000.00, 52000.00, 52000.00,
    ** K 1000.00, 52000.00, 52000.00, 52000.00, 52000.00,
    ** L 1000.00, 52000.00, 52000.00, 52000.00, 52000.00,
    ** M 1000.00, 52000.00, 52000.00, 52000.00, 52000.00,
    ** N 1000.00, 52000.00, 52000.00, 52000.00, 52000.00,
    ** O 1000.00, 52000.00, 52000.00, 52000.00, 52000.00,
    ** P 1000.00, 52000.00, 52000.00, 52000.00, 52000.00,
    ** Q 1000.00, 52000.00, 52000.00, 52000.00, 52000.00,
    ** R 1000.00, 52000.00, 52000.00, 52000.00, 52000.00,
    ** S 1000.00, 52000.00, 52000.00, 52000.00, 52000.00,
    ** T 1000.00, 52000.00, 52000.00, 52000.00, 52000.00,
    ** U 1000.00, 52000.00, 52000.00, 52000.00, 52000.00,
    **
    ** COMMON STATEMENT(S)
    ** COMMON / ATMDATA / NH, RH(2), ATMPTS(101), VSP(101)
    ** DATA STATEMENT(S)
    **
    ** NUMBER OF POINTS PER TABLE - NH
    ** DATA NH / 101 /
    **
    ** LOWER AND UPPER BOUNDS OF TABLE POINTS - BH
    ** DATA BH / 0.0, 100000.0 /
    **
    ** SQUARE ROOT OF AIR DENSITY / 2.0 TABLE - ATMPTS
    ** DATA (ATMPTS(1), I=1, 511) /
    ** A 0.0344740,
  
```


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PAGE 2

15.13.04

FTN 4.4+5.3D

74/175 OPT=2

```

SUBROUTINE STNDAY
  60  R=0.0339720,0.0334770,0.0322700,0.0320800,0.0320000,0.0320000,
  65  C=0.0331440,0.0270400,0.0233000,0.0227900,0.0227900,0.0227900,
  70  D=0.0064040,0.0264040,0.0264040,0.0264040,0.0264040,0.0264040,
  75  E=0.0064040,0.0264040,0.0264040,0.0264040,0.0264040,0.0264040,
  80  F=0.0064040,0.0264040,0.0264040,0.0264040,0.0264040,0.0264040,
  85  G=0.0064040,0.0264040,0.0264040,0.0264040,0.0264040,0.0264040,
  90  H=0.0064040,0.0264040,0.0264040,0.0264040,0.0264040,0.0264040,
  95  I=0.0064040,0.0264040,0.0264040,0.0264040,0.0264040,0.0264040,
  100 J=0.0064040,0.0264040,0.0264040,0.0264040,0.0264040,0.0264040,
  105 K=0.0064040,0.0264040,0.0264040,0.0264040,0.0264040,0.0264040,
  DATA (ATPTS(I),I=1,101)
  L=0.031710,0.0123500,0.0123500,0.0123500,0.0123500,0.0123500,
  M=0.011600,0.011600,0.011600,0.011600,0.011600,0.011600,
  N=0.0103000,0.0103000,0.0103000,0.0103000,0.0103000,0.0103000,
  P=0.0092018,0.0092018,0.0092018,0.0092018,0.0092018,0.0092018,
  Q=0.008115,0.008115,0.008115,0.008115,0.008115,0.008115,
  R=0.007200,0.007200,0.007200,0.007200,0.007200,0.007200,
  S=0.006300,0.006300,0.006300,0.006300,0.006300,0.006300,
  T=0.005400,0.005400,0.005400,0.005400,0.005400,0.005400,
  U=0.004400,0.004400,0.004400,0.004400,0.004400,0.004400,
  DATA (VSPIS(I),I=1,51)
  A=0.031710,0.0123500,0.0123500,0.0123500,0.0123500,0.0123500,
  B=0.011600,0.011600,0.011600,0.011600,0.011600,0.011600,
  C=0.0103000,0.0103000,0.0103000,0.0103000,0.0103000,0.0103000,
  D=0.0092018,0.0092018,0.0092018,0.0092018,0.0092018,0.0092018,
  E=0.008115,0.008115,0.008115,0.008115,0.008115,0.008115,
  F=0.007200,0.007200,0.007200,0.007200,0.007200,0.007200,
  G=0.006300,0.006300,0.006300,0.006300,0.006300,0.006300,
  H=0.005400,0.005400,0.005400,0.005400,0.005400,0.005400,
  I=0.004400,0.004400,0.004400,0.004400,0.004400,0.004400,
  DATA (VSPIS(I),I=52,101)
  L=0.031710,0.0123500,0.0123500,0.0123500,0.0123500,0.0123500,
  M=0.011600,0.011600,0.011600,0.011600,0.011600,0.011600,
  N=0.0103000,0.0103000,0.0103000,0.0103000,0.0103000,0.0103000,
  P=0.0092018,0.0092018,0.0092018,0.0092018,0.0092018,0.0092018,
  Q=0.008115,0.008115,0.008115,0.008115,0.008115,0.008115,
  R=0.007200,0.007200,0.007200,0.007200,0.007200,0.007200,
  S=0.006300,0.006300,0.006300,0.006300,0.006300,0.006300,
  T=0.005400,0.005400,0.005400,0.005400,0.005400,0.005400,
  U=0.004400,0.004400,0.004400,0.004400,0.004400,0.004400,
  RETURN
  END

```

SYMBOLIC REFERENCE MAP (R=1)

MDC A7910
Volume II

A-238

ORIGINAL PAGE 13
OF POOR QUALITY

PAGE 1

82/10/22. 15.13.04

FTN 4.8+538

74/175 OPT=2

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1  SUBROUTINE ATMOS(1)
5  **
10  THIS SUBROUTINE CALCULATES THE FOLLOWING PARAMETERS AS A FUNCTION OF
15  ALTITUDE FOR A STANDARD ATMOSPHERE:
20  SQUARE ROOT OF ONE HALF THE ATMOSPHERIC
25  DENSITY, SPEED OF SOUND IN FEET/SECOND,
30  LOCAL STATIC PRESSURE IN POUNDS/SQ. FT.,
35  ATMOSPHERIC TEMPERATURE IN DEGREES RANKINE,
40  ATMOSPHERIC TEMPERATURE IN DEGREES FAHRENHEIT.
45  COMMON / FARRAY / F(1001)
50  COMMON / ATMDATA / NH, BH(2), ATMPTS(1)
55  EQUIVALENCE STATEMENT(S)
EQUIVALENCE (A,F(1001))
EQUIVALENCE
      NH, A(1), LATH, A(174), US, A(172),
      PRESHP, A(179), TEMPHR, A(175),
      PRESHP, A(181), TEMPHR, A(182), INSTD, A(195),
      LCASE, A(196)

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PAGE 2

82/10/22, 15.12.04

FTN 4.46-38

SUBROUTINE ATMOS 74/175 OPT-2

```
60 * DIMENSION STATEMENT(S)
    * DIMENSION A(1000)
    DIMENSION
    *H(1)
    *TEMPRH(1) *PRESHP(1) *VS(1) *PHO(1) *PRESHP(1)
    * BYPASS STANDARD DAY ATMOSPHERE DEFINITIONS IF NON-STANDARD
    * INPUTS HAVE BEEN SPECIFIED
    IF(INSTD.EQ.1) GO TO 40
    ATM(1) = F14(M1),M1,MH,ATMPS)
    VS(1) = F18(M1),M1,MH,MH,ATMPS(MH,1))
    RH(1) = 2.0*ATM(1)*ATM(1)
    TEMPRH(1) = 0.0002191416*VS(1)*VS(1)
    TEMPRH(1) = TEMPRH(1) - 459.67
    PRESHP(1) = 1716.5619*RH(1)+TEMPRH(1)
    PRESHP(1) = 0.00694444*PRESHP(1)
    GO TO 50
    * NON-STANDARD DAY INPUTS SHOULD BE SPECIFIED BELOW
    40 CONTINUE
    TEMPRH(1) = -56.74
    TEMPRH(1) = 402.33
    VS(1) = 0.04
    PRESHP(1) = 3.000
    PRESHP(1) = 361.5
    RH(1) = .00021
    ATM(1) = .02015
    50 CONTINUE
    RETURN
    END
```

SYMBOLIC REFERENCE MAP (R-1)

ENTRY POINTS
3 ATMOS

VARIABLES SN TYPE
1750 3 ATMPHS
0 4

RELOCATION
ARRAY F14M1
ARRAY F18M1
ARRAY F18M1

2227 ATM
1762 N

REAL
REAL
REAL

F14M1
F18M1
F18M1

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A-241

ORIGINAL PAGE IS
OF POOR QUALITY

PAGE 1

02/10/22, 15.13.10

FTN 4.0.538

74/175 OCT-2

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1  SUBROUTINE RPDATA
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10 *****
15 *****
20 *****
25 *****
30 *****
35 *****
40 *****
45 *****
50 *****
55 *****

THIS SUBROUTINE PROVIDES AN EASY-TO-USE INTERFACE WITH SUBROUTINE
RTP. SUBROUTINE RPDATA PROVIDES ALL EXECUTIVE PROGRAM
SPECIFIED INPUT DATA REQUIRED BY SUBROUTINE RTP AND CONTAINS ALL
REQUIRED CALLS TO RTP AND ITS ENTRY POINTS. THE PRIMARY PURPOSE
OF RPDATA IS TO SUPPLY POINTERS FOR DATA TO BE BUFFERED OUT IN THE
SUBROUTINE RTP CAN LOCATE THE DATA PARAMETERS WITH RESPECT TO THE
F-ARRAY.

THE LOGIC AND STRUCTURE IN THIS LISTING IS INTENDED AS A GUIDE
AND EXAMPLE TO SHOW HOW ALL THE INPUTS CAN BE SPECIFIED IN A
GENERAL WAY TO PROVIDE FLEXIBILITY. THE USER MUST DECIDE TO WHAT
EXTENT IT MEETS THE REQUIREMENTS OF HIS STUDY, AND MAY NEED TO
DELETE OR ADD SECTIONS.

THE FOLLOWING VARIABLES ARE INPUTS TO RTP AND ARE COMPUTED OR IN
DATA STATEMENTS IN RPDATA:

-- REQUIRED --
NU
TAPDEN
NP
YBU
YBUHF
YBUHF

-- OPTIONAL --
TAPFLIM
NPF
NP2
YBUEN
YBUHF
NPA
YBUFA

THE FOLLOWING ARE ITEMS TO CONSIDER:

1. THE POINTERS ARRAY *IN* MUST CONTAIN IN SEQUENCE *NP* TIME
HISTORY DATA POINTERS. *IN* STARTS OF RUN DATA POINTERS AND *NP*
END OF RUN DATA POINTERS. THE LOGIC SHOWN PROVIDES THE STRUCTURE,
AND ALL OF THE POINTERS *WITHIN* EACH SECTION OF *IN* FOR RUN
AND END OF RUN DATA. *IN* IS OPTIONAL. THE RESPECTIVE SECTIONS COULD BE
OBTAINED, AND *NP* AND *NP* WOULD THEN BE USED.

2. THE NAMES ARRAY *IN* PROVIDES FOR THE CAPABILITY OF STORING
VARIABLE NAMES IN THE START OF RUN RECORD FOR AUTOMATIC OFFLINE
PRINTOUT. IF THIS OPTION IS USED, THE *IN* ARRAY MUST CONTAIN
NAMES IN THE SAME ORDER AS APPEARING IN THE VARIABLE POINTERS
IN THE *IN* ARRAY. IF THE NAMES OPTION IS NOT USED, THE VARIABLE
NAMES *MUST* BE *IN* AND ALL REFERENCES TO THE *IN* ARRAY CAN BE
DELETED. WITH THE FOLLOWING REFERENCES TO THE *IN* ARRAY STILL IN
DIMENSIONED TO AT LEAST ONE AND LOCATED AFTER THE *IN* ARRAY IN
COMMON BLOCK *IN* AND VARIABLE *IN* SHOULD BE COMPUTED AS SHOWN
SO THE ERROR CHECK CAN STILL BE PERFORMED.

3. THE DO-LOOPS INVOLVING VARIABLE *IN* ARE USEFUL ONLY IF NAMES
ARE USED, AND DATA POINTERS ARE COMPUTED AS SHOWN FOR MULTIPLE INTO
AIRCRAFT. THEY INSERT AN AIRCRAFT NUMBER OR AN AIRCRAFT PAIR INTO

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OF POOR QUALITY

PAGE 3

82/10/22, 15.13.10

FTM 4.0+539

74/175 OPT-2

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115 * MISS CODE FOR NUMBER OF PASSES IN WHICH DATA WAS NOT BUFFERED OUT
116 * AND EXCEEDED TAPE LIMIT (-1 FLAG
117 * SIMULATION RUNNING TIME IN SECONDS
118 * IRTPBUF RIP BUFFER OUT FLAG
120 * F-ARRAY OUTPUT DEFINITIONS
121 *
122 * NU RIP OUTPUT TAPE LOGICAL UNIT NUMBER
123 * TAPEDEN RIP TAPE DENSITY IN FPI
124 * TAPELIM RIP TAPE LIMIT IN FEET
125 * NP NUMBER OF RIP PARAMETERS OUTPUT AT THE BASIC RATE
126 * NPF NUMBER OF RIP PARAMETERS OUTPUT AT THE FAST RATE
127 * NPS NUMBER OF RIP USER SPECIFIED START OF RUN PARAMETERS
128 * NPP NUMBER OF RIP USER SPECIFIED END OF RUN PARAMETERS
129 * NPT BUFFERED OUT RECORD SIZE
130 * NBU F-ARRAY INDEX OF RIP PARAMETERS POINTERS ARRAY
131 * NBD F-ARRAY INDEX OF RIP PARAMETERS NAMES ARRAY
132 * NDBUF BASIC DATA OUTPUT INTERVAL IN SECONDS
133 * NDBUF FAST DATA OUTPUT INTERVAL IN SECONDS
134 * NDBUF FAST DATA OUTPUT INTERVAL IN SECONDS
135 * NAMES RIP NAMES OUT FLAG
136 * IRTPLO RIP LOAD FLAG
137 *
138 *****
139 * COMMON STATEMENTS(S)
140 *
141 * COMMON / FARRAY / F(1001)
142 *
143 * COMMON / BUFF1 / BUFL(1500),BUF2(1500),IB(250),IN(250)
144 *
145 * EQUIVALENCE STATEMENTS(S)
146 *
147 * RIP INTERFERENCE
148 * EQUIVALENCE
149 * .F(521), (TAPEDEN, F(531)), (TAPELIM, F(541)),
150 * .F(551), (NPF, F(561)), (NPS, F(571)),
151 * .F(581), (NPP, F(591)), (NPT, F(601)),
152 * .F(611), (NBD, F(621)), (NDBUF, F(631)),
153 * .F(641), (NDBUF, F(651)), (NDBUF, F(661)),
154 * .F(671), (NDBUF, F(681)), (NDBUF, F(691)),
155 * .F(701), (NDBUF, F(711)), (NDBUF, F(721))
156 *
157 * EXEC/STUDY INTERFERENCE
158 * EQUIVALENCE
159 * .F(11F, F(121)), (IRTPLO, F(171)), (IRTPBUF, F(179))
160 *
161 * EQUIVALENCE (4,F(1001))
162 *
163 * DIMENSION STATEMENTS(S)
164 *
165 * DIMENSION
166 * A(1000)
167 *
168 *****
169 *****
170 *****
171 *****

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PAGE 4

H2/10/22. 15.13.10

FIN 4.90*38

SUBROUTINE RTDATA 74/17% OPT=2

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175 * DATA STATEMENTS
176 *
177 * DATA
178 * : NU / 1600.0 /
179 * : TAPLEN / 2000.0 /
180 *
181 * DATA
182 * : DTBUF / 0.1 /
183 * : DTBUF / 0.0 /
184 *
185 * DATA
186 * : NAMES / 1 /
187 *
188 * DATA
189 * : IRTPLD / 1 /
190 *
191 *
192 *
193 *
194 *
195 * RTDATA CALCULATION
196 *
197 *
198 *
199 *
200 * IF (IRTPLD .LE. 0) RETURN
201 *
202 *
203 *
204 *
205 * CALL RTP
206 *
207 * RETURN
208 *
209 *
210 *
211 *
212 *
213 * ENTRY INTDAT
214 *
215 * ILF = LOC(F(1))
216 *
217 * ILF1 = ILF - 1
218 *
219 * IRL = LOC(I(1))
220 *
221 * IRL1 = IRL - ILF1
222 *
223 * INI = LOC(IN(1))
224 *
225 * INI1 = INI - INI1
226 *
227 * IRLN = INI - IRL
228 *
229 * IRL1 = IRL - IRLN
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SUBROUTINE QTPDATA 74/175 NET=2

A-246

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OF POOR QUALITY

PAGE 6

82/10/22, 15.13.10

FTN 4.81530

SUBROUTINE RTPDATA 74/175 OPT=2

```

290      NP = N
291      NB = 6 * NP
292      ITEMP = LOCF(RUE2(1)) - LOCF(RUE1(1))
293      CALL M5GAT(150H, 65 * RTPDATA - RUE1 DIMENSION TOO SMALL)
294      *
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998      *
999      *
1000      *

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400
9010 FORMAT(5X, *PIP END - MISS = *, I7)
RETURN
END

SYMBOLIC REFERENCE MAP (R=2)

ENTRY POINTS	DEF LINE	REFERENCES
407 PIPDATA	395	403
408 PIPDATA	397	208
409 PIPDATA	399	
410 PIPDATA	401	
411 PIPDATA	403	
412 PIPDATA	405	

FIN 4, P+534

27/10/12, 15.13.10

PAGE 8

400
9010 FORMAT(5X, *PIP END - MISS = *, I7)
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FIN 4, P+534

27/10/12, 15.13.10

PAGE 8

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FIN 4, P+534

27/10/12, 15.13.10

PAGE 8

400
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SYMBOLIC REFERENCE MAP (R=2)

ENTRY POINTS	DEF LINE	REFERENCES
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409 PIPDATA	399	
410 PIPDATA	401	
411 PIPDATA	403	
412 PIPDATA	405	

FIN 4, P+534

27/10/12, 15.13.10

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APPENDIX B
YAV-8B NONLINEAR
PROGRAM ARRAY SEARCH

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SEARCH F ARRAY

YAV-88 ARRAY SEARCH

1	RTPDATA								
2	----	28							
29	RTPDATA ILF								
30	----	40							
41	CARDS TITLE		RTP TITLE						
42	----	43							
44	RTP CLASS								
45	----	46							
47	YAV88 JDATE		CARDS JDATE		RTP JDATE				
48	YAV88 JTIME		CARDS JTIME		RTP JTIME				
49	YAV88 NRUN		RTP NRUN						
50	----	51							
52	RTP NU		RTPDATA NU						
53	RTP TAPEDE		RTPDATA TAPEDE						
54	RTP TAPELIN		RTPDATA TAPELIN						

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SEARCH F ARRAY

YAV-8B ARRAY SEARCH

55	RTP RECL		
56	RTP TAPEL		
57			
58	RTP NP	RTPDATA NP	
59	RTP NPF		
60	RTP NPS	RTPDATA NPS	
61	RTP NPE	RTPDATA NPE	
62	RTP NB	RTPDATA NB	
63	RTP IBUFP	RTPDATA IBUFP	
64	RTP IBUFN	RTPDATA IBUFN	
65	YAV8B DTBUF	RTP DTBUF	RTPDATA DTAUF
66	RTP DTFBUF	RTPDATA DTFBUF	
67	RTP NAMES	RTPDATA NAMES	
68	RTP NPA		

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SEARCH F ARRAY

YAV-8B ARRAY SEARCH

69	RIP I8UFA	RIPDATA I8UFA						
70	RIP NPC	RIPDATA NPC						
71	RIP IRTPON	RIPDATA IRTPON						
72	RIP MISS	RIPDATA MISS						
73	----- 90							
91	YAV8B DTOR	AEROY8B DTOR	ENG08 DTOR	RCS07 D2R	TEOM1 DTOR	REOM1 DTOR		
92	YAV8B RTOD	ISOMS RTOD	AEROY8B RTOD	PFC07 RTOD	TEOM1 RTOD	REOM1 RTOD		
93	YAV8B PI	REOM1 PI						
94	----- 99							
100	YAV8B 6	ISOMS 6	ENG08 6	PFC07 6	WTBAL07 6			
101	TEOM1 DREGAD							
102	TEOM1 DREGAR							
103	TEOM1 BEARTH							
104	TEOM1 ESQ							
105	TEOM1 GRAV							

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YAV-8B ARRAY SEARCH		SEARCH F ARRAY				
106	----- 108					
109	IFOM2 A1	REOM2 A1				
110	IFOM2 A2	REOM2 A2				
111	IFOM2 A3	REOM2 A3				
112	----- 117					
118	YAV8B FOM2	ABO7	BOF			
119	YAV8B COF	ISOM2 COF	ACOF	SEC07 DIF	REOM1 COF	REOM2 COF
120	----- 125					
126	RTP HYBRID					
127	----- 135					
136	IFOM2 INH1					
137	REOM2 INH1					
138	----- 145					
146	YAV8B NOCARDS	CARDS NOCARDS				
147	RTP ITEM					

YAV-88 ARRAY SEARCH		SEARCH F ARRAY						
148	----- 149							
150	YAV88 I STOPD							
151	YAV88 RUNTIME	ISOMS TIME	TEOM1 TIME	RTP TIME	RTPDATA TIME	AC07 INITIAL	PFC07 INITIAL	SFC07 INITIAL
152								WTBAL07 INITIAL
153	YAV88 INITIAL	ISOMS INITIAL	AEROY88 INITIAL	ENG08 INITIAL	AC07 INITIAL			
154								
155	YAV88 IRESET	ENG08 IRESET	TEOM1 IRESET	TEOM2 IRESET	REOM1 IRESET		REOM2 IRESET	
156	YAV88 NPASS							
157	YAV88 NPASSD							
158	----- 177							
178	RTPDATA IRIPLD							
179	YAV88 IRIPBUF	RTP IRIPBUF	RTPDATA IRIPBUF					
180	----- 276							
277	YAV88 IAC	AC07 IAC						
278	----- 999							
1000	CARDS	RTP						

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YAV-8B ARRAY SEARCH		SEARCH F ARRAY	
1001	YAV8B A PPC07 REQM1	150MS A PPC07 A REQM1 A	AEROY8B A WTBAL07 A ATMOS
		SFC07 A REQM2 A	AEROY8B A WTBAL07 A ATMOS
1002	----- 1999		ENG08 A WTBAL07 A ATMOS A
2000	ENG08		AC07 A TEOM1 A RTPDATA A
2001	----- 2999		AC07 A TEOM1 A RTPDATA A
3000	YAV8B		RCS07 A TEOM2 A

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OF POOR QUALITY

SEARCH A ARRAY

YAV-8B ARRAY SEARCH

1	TEOM1 RCOSL				
2	TEOM1 RAC				
3	TEOM1 COSL				
4	TEOM1 SINL				
5	TEOM1 COSLAM				
6	TEOM1 SINLAM				
7	TEOM1 L				
8	TEOM1 LAM				
9	TEOM1 LAMR				
10	TEOM1 RE				
11	AEROY8B H	ENG08 H	TEOM1 H	ATMOS H	
12	TEOM1 CNX	REOM1 CNX			
13	-----	20			
21	TEOM1 VIN				

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SEARCH A ARRAY

YAV-88 ARRAY SEARCH

22	----	23			
24		TEOM1 VGN			
25		TEOM1 VGE			
26		TEOM1 VGO			
27		TEOM1 VN	REOM1 VN		
28		TEOM1 VE			
29		TEOM1 VO			
30		AFRDY88 VF	ENG08 VF	TEOM1 VF	REOM1 VF
31		I50MS GAMMA	TEOM1 GAM		
32		TEOM1 SIG			
33		TEOM1 COSGAM			
34		TEOM1 SINGAM			
35		TEOM1 COSSIG			
36		TEOM1 SINSIG			

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OF POOR QUALITY

SEARCH A ARRAY

YAV-88 ARRAY SEARCH

37	TEOM1 VG		
38	TEOM1 PSIV		
39	AEROY8B QBAR	PFC07 OB	TEOM1 QBAR
40	AEROY8B RHACH	ENG08 RHACH	TEOM1 MACH
41	TEOM1 GX	TEOM2 GX	
42	TEOM1 GY		
43	TEOM1 GZ		
44	TEOM1 VFI	REOM1 VFI	
45	TEOM1 FTPDLA		
46	TEOM1 FTPDL0		
47	----	48	
49	ENG08 RHACHP		
50	ENG08 YHACH2		
51	TEOM2 AXR		

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SEARCH A ARRAY

YAV-8B ARRAY SEARCH

52	PFC07 AY8	REOM1 AY8	
53	ISONS AZ	PFC07 AZ8	REOM1 AZ8
54	TEOM2 AX		
55	----	56	
57	TEOM2 XDD		
58	----	59	
60	TEOM2 XDD1		
61	----	62	
63	TEOM2 XDD2		
64	----	65	
66	TEOM1 XD	TEOM2 XD	
67	----	68	
69	TEOM2 XD1		
70	----	71	
72	TEOM2 XD2		
73	----	74	

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SEARCH A ARRAY

YAV-88 ARRAY SEARCH

75	TEOM1 X	TEOM2 X	
76	TEOM1 Y	TEOM2 Y	
77	TEOM1 Z	TEOM2 Z	
78	---	83	
84	TEOM2 CXX	REOM1 CXX	
85	---	92	
93	REOM1 CXN		
94	---	101	
102	REOM1 PST		
103	TSOMS THETA	AEROY8B THA	REOM1 THA
104	AEROY8B PHY	REOM1 PHY	
105	REOM1 SINPST		
106	REOM1 COSPST		
107	REOM1 SINTHA		
108	REOM1 COSTHA		

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SEARCH A ARRAY

YAV-8B ARRAY SEARCH

109	REOM1 SINPHI		
110	AEROY8B COSPHI	REOM1 COSPHI	
111	----	113	
114	AEROY8B U	ENG08 U	REOM1 U
115	AEROY8B V		
116			
117	ISONS ALPHA	AEROY8B ALP	REOM1 ALPHA
118	AEROY8B BETA	REOM1 BETA	
119	AEROY8B SYNALP	ENG08 SYNALP	REOM1 SYNALP
120	AEROY8B COSALP	ENG08 COSALP	REOM1 COSALP
121	ENG08 SYNBET	REOM1 SYNBET	
122	ENG08 COSBET	REOM1 COSBET	
123	AEROY8B ALPD	REOM1 ALPHA0	
124	REOM1 ALPHA1		
125	REOM1 BETA0		

YAV-88 ARRAY SEARCH

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YAV-8B ARRAY SEARCH			SEARCH A ARRAY			
149	150MS R	AEROY88 R	ENG08 R	PFC07 R	REOM1 R	REOM2 R
150	REOM1 E1	REOM2 E1				
151	REOM1 E2	REOM2 E2				
152	REOM1 E3	REOM2 E3				
153	REOM1 E4	REOM2 E4				
154	REOM2 PD2					
155	---	156				
157	REOM2 PD1					
158	---	159				
160	REOM2 E1D2					
161	REOM2 E2D2					
162	REOM2 E3D2					
163	REOM2 E4D2					
164	REOM2 E1D1					
165	REOM2 E2D1					

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SEARCH A ARRAY

Y4V-8B ARRAY SEARCH

166	REDM2 E301		
167	REDM2 E401		
168	REDM2 DELTA		
169	REDM2 KDELTA		
170	----	175	
176	TEOM1 ATM	ATMOS ATM	
177	ENG08 VS	TEOM1 VS	ATMOS VS
178	AEROY88 RHO	ATMOS RHO	
179	ATMOS PRESHPF		
180	ENG08 TEMPHR	ATMOS TEMPHR	
181	ENG08 PRESHP I	RCS07 PAMB	ATMOS PRESHP I
182	ATMOS TEMPHF		
183	ENG08 DELTD		
184	ENG08 ATT2		

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OF POOR QUALITY

SEARCH A APRAY

YAV-8B ARRAY SEARCH

185	ENG08 ASQRTT2			
186	----- 194			
195	ATMOS INSTD			
196	----- 200			
201	TEOM1 WN			
202	----- 250			
251	WTBAL07 WEIGHT			
252	WTBAL07 RMAS5	TEOM2 MASS		
253	AEROY8B CGFS	ENG08 CGFS	RC507 CGFS	WTBAL07 CGFS
254	AEROY8B CGHL	ENG08 CGHL	RC507 CGHL	WTBAL07 CGHL
255	AEROY8B CGWL	ENG08 CGWL	RC507 CGWL	WTBAL07 CGWL
256	WTBAL07 RIX			
257	WTBAL07 RIY			
258	WTBAL07 RIZ			
259	WTBAL07 RIX			

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SEARCH A ARRAY

YAV-88 ARRAY SEARCH

260	WTBAL07 ICON	REDN2 ICON
261	-----	269
270	AEROY88 CLG	WTBAL07 CLG
271	-----	272
273	WTBAL07 BSHOMX	
274	WTBAL07 BSHOMY	
275	WTBAL07 BSHOMZ	
276	-----	300
301	AEROY88 CLNR	
302	AEROY88 CLNP	
303	AEROY88 DCLNF	
304	AEROY88 DCLNFJN	
305	AEROY88 YMOGE	
306	AEROY88 CLNBAT	
307	AEROY88 HCY	

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OF POOR QUALITY

SEARCH A ARRAY

YAV-88 ARRAY SEARCH

308	AEROY88 HCYR
309	AEROY88 HCLL
310	AEROY88 CLNH
311	AEROY88 PSTAR
312	AEROY88 PSTAR
313	PEC07 DS
314	PFC07 DLA
315	PFC07 DRA
316	----- 317
318	AEROY88 HCLLAF
319	----- 320
321	AEROY88 ALPY
322	AEROY88 ALPF
323	AEROY88 CMT62
324	AEROY88 CMF62

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SEARCH A ARRAY

YAV-8B ARRAY SEARCH

325	AEROY88 EPS	
326	ISOMS AEROX	TEOM2 AEROX
327	ISOMS AEROY	AEROY88 AEROY
328	ISOMS AEROZ	AEROY88 AEROZ
329	AEROY88 AEROL	REOM2 AEROL
330	AEROY88 AEROM	
331	AEROY88 AERON	
332	AEROY88 S	
333	AEROY88 B	
334	AEROY88 CMAR	
335	-----	340
341	AEROY88 CGREF	
342	AEROY88 CMQ	
343	AEROY88 CHALPD	

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SEARCH A ARRAY

YAV-8B ARRAY SEARCH

344	AEROY8B RLIFT
345	AEROY8B RDRAG
346	AEROY8B CL
347	AEROY8B CD
348	AEROY8B CN
349	AEROY8B CA
350	AEROY8B CH
351	AEROY8B RK4
352	----- 354
355	AEROY8B CNCE
356	AEROY8B CAGE
357	AEROY8B CHGE
358	AEROY8B CNPWER
359	AEROY8B CAPWER

ORIGINAL PAGE 13
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SEARCH A ARRAY

YAV-8B ARRAY SEARCH

360	AEROY8B CMPWR
361	AEROY8B CVDR
362	AEROY8B CLDR
363	AEROY8B CLNDR
364	
365	AEROY8B DCDFL
366	AEROY8B DCDFR
367	AEROY8B HCLLB
368	AEROY8B HCVB
369	AEROY8B CNB
370	AEROY8B CNDA
371	AEROY8B HCLLDA
372	AEROY8B HCVDA
373	AEROY8B CNDR

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SEARCH A ARRAY

YAV-8B ARRAY SEARCH

374	AEROY8B HCLLDR
375	AEROY8B HCYDR
376	----- 377
378	AEROY8B HCLBPNW
379	AEROY8B CMBASE
380	AEROY8B CLBASE
381	AEROY8B CDBASE
382	AEROY8B HCMPOW
383	AEROY8B DCLPNW
384	AEROY8B DCMFL
385	AEROY8B DCMFR
386	AEROY8B DCLFL
387	AEROY8B DCLFR
388	AEROY8B HCMDA

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SEARCH A ARRAY

YAV-88 ARRAY SEARCH

389	AEROY88 DCLAL
390	AEROY88 DCLAR
391	AEROY88 DCDAL
392	AEROY88 DCDAR
393	----- 394
395	AEROY88 DCMFJI
396	AEROY88 DCMSTAB
397	AEROY88 CLSTAB
398	AEROY88 CDSTAB
399	AEROY88 HCDSTW
400	AEROY88 CDOR
401	AEROY88 CMSTING
402	AEROY88 H7CM
403	AEROY88 H7CL

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SEARCH A ARRAY

YAV-8B ARRAY SEARCH

404	AEROY8B HICD
405	AEROY8B HYAV
406	AEROY8B HRNL
407	AEROY8B HISF
408	AEROY8B HIFX
409	AEROY8B HIFZ
410	AEROY8B HYRM
411	AEROY8B HYVM
412	AEROY8B VEO
413	--- 414
415	AEROY8B RTHALP
416	AEROY8B RETAP
417	AEROY8B HP
418	--- 421
422	AEROY8B CHGE10

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SEARCH A ARRAY

YAV-8B ARRAY SEARCH

423	AEROY8B THALP
424	AEROY8B RNIGE
425	AEROY8B YHIGE
426	AEROY8B SFYGE
427	AEROY8B SCALR
428	----- 429
430	AEROY8B YDSFTB
431	AEROY8B YDSFTP
432	AEROY8B DYNIP
433	AEROY8B DYNBIAS
434	AEROY8B YK
435	AEROY8B DYNPHI
436	AEROY8B TERN
437	AEROY8B DRNIGE

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SEARCH A ARRAY

YAV-8B ARRAY SEARCH

438	AEROY8B DRMPHI
439	AEROY8B RK6
440	AEROY8B RC5
441	AEROY8B GKCLLP
442	AEROY8B GKCHP
443	AEROY8B CY
444	AEROY8B CYBASIC
445	AEROY8B CYPPOWER
446	AEROY8B CYBASE
447	AEROY8B DCYAIL
448	AEROY8B DCYRUD
449	AEROY8B SFQGE
450	AEROY8B CLL
451	----- 454

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SEARCH A ARRAY

YAV-8B ARRAY SEARCH

455	AEROY8B CHQT
456	AEROY8B CHALPDT
457	----- 477
478	PFC07 SYLON
479	PFC07 SYLAT
480	PFC07 PEDAL
481	PFC07 TRIMLON
482	PFC07 TRIMLAT
483	PFC07 TRIMDIR
484	----- 485
486	PFC07 ETHDIR
487	PFC07 TRATDIR
488	PFC07 PEDALT
489	----- 494
495	PFC07 YSASLON

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SEARCH A ARRAY

YAV-88 ARRAY SEARCH

496	PFC07 ISASLAT		
497	PFC07 ISASDIR		
498	PFC07 RCSE		
499	----- 502		
503	ISOMS DHTD	AEROY88 DHTD	PFC07 DHTD
504			
505	AEROY88 DAL	PFC07 DLAD	
506	AEROY88 DAR	PFC07 DRAD	
507	PFC07 DAD		
508	----- 512		
513	AEROY88 DRUD	PFC07 DRUD	
514	AEROY88 RK7		
515	----- 518		
519	PFC07 FBWG		
520	AEROY88 CILBAS		

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SEARCH A ARRAY

YAV-88 ARRAY SEARCH

521	AEROY88 CLLPOR	
522	AEROY88 CLLBASE	
523	AEROY88 DELLATE	
524	AEROY88 RK10	
525	AEROY88 TEMPX3	
526	150MS SYLDP	PFC07 SYLDP
527	150MS SYLAP	PFC07 SYLAP
528	150MS RUDPC	PFC07 RUDPC
529	PFC07 YLDP	
530	PFC07 YLAP	
531	-----	549
550	AEROY88 CMGE01	
551	AEROY88 CMGE55	
552	AEROY88 CAGE55	

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SEARCH A ARRAY

YAV-8B ARRAY SEARCH

553	AEROY8B CHGE55
554	----- 556
557	AEROY8B DCN60
558	AEROY8B DCN60
559	
560	AEROY8B DCN60
561	AEROY8B CLLR
562	AEROY8B CLLP
563	
564	PFC07 POS80
565	----- 568
569	AEROY8B DCA60
570	AEROY8B DCN50
571	AEROY8B DCA50
572	AEROY8B DCN50

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SEARCH A ARRAY

YAV-8A ARRAY SEARCH

573	AEROY88 DCM10
574	AEROY88 PKO
575	AEROY88 RMGE00
576	AEROY88 RM1P2
577	AEROY88 RM4P12
578	AEROY88 RM7P05
579	PEC07 PGAIN
580	PEC07 RGAIN
581	PEC07 AYGN
582	PEC07 QGAIN
583	----- 593
594	SFC07 DYME
595	SFC07 DELTHJ
596	----- 597
598	AEROY88 SFGE60

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SEARCH A ARRAY

YAV-88 ARRAY SEARCH

599	AEROY88 SFGE81
600	
601	SFC07 DRDPLTH
602	SFC07 DVU
603	SFC07 DVD
604	SFC07 RATE1
605	
606	SFC07 RATE2
607	---- 611
612	SFC07 HML
613	---- 615
616	SFC07 RDROPD
617	
618	PFC07 DRDOP
619	---- 621
622	SFC07 VLA

SFC07
DRDOP

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SEARCH A ARRAY

YAV-8B ARRAY SEARCH

623			
624	SFC07 DNFLAPM		
625	----- 626		
627	150MS INODE	PFC07 INODE	SFC07 INODE
628	SFC07 ILTD		
629			
630	SFC07 R		
631	----- 632		
633	SFC07 DEFLAP		
634	AEROY88 FLAP	SFC07 FLAP	
635	150MS IFLAP	SFC07 IFLAP	
636	SFC07 DNFLAP		
637	150MS DNFLAPL	AEROY88 DNFLAPL	SFC07 DNFLAPL
638	AEROY88 DNFLAPR	SFC07 DNFLAPR	
639	AEROY88 DNFLD	SFC07 DNFLD	WTBAL07 DNFLD

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SEARCH A ARRAY

YAV-8B ARRAY SEARCH

640	SFC07 DROP	
641	----- 642	
643	SFC07 TERP	
644	----- 645	
646	SFC07 RDR0PU	
647		
648	SFC07 TEMP	
649	SFC07 DFLAPC	
650		
651	ENG08 RFTX	RCS07 RFTX
652	ENG08 RFTY	RCS07 RFTY
653	ENG08 RFTZ	RCS07 RFTZ
654	ENG08 RMR	RCS07 RMR
655	ENG08 RMP	RCS07 RMP
656	ENG08 RMY	RCS07 RMY

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SEARCH A ARRAY

YAV-8B ARRAY SEARCH

	ENG08 RWTOT	RCS07 PWTOT
657		
658	RCS07 PDUCT	
659		
660	RCS07 RPIUP3	
661	RCS07 RPDP3	
662	RCS07 RPFPP3	
663	RCS07 RPTP3	
664	RCS07 RPT	
665	RCS07 RPF	
666	RCS07 RPU	
667	RCS07 RPP	
668	RCS07 REUN	
669	RCS07 REDW	
670	RCS07 REWF	

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SEARCH A ARRAY

YAV-8B ARRAY SEARCH

671	RCS07 REWT
672	RCS07 REFR
673	RCS07 REFT
674	RCS07 REFN
675	RCS07 RETFW
676	RCS07 RMFT
677	RCS07 RMFF
678	RCS07 RMFND
679	RCS07 RMFNU
680	RCS07 RMT
681	RCS07 RMF
682	RCS07 RWND
683	RCS07 RWNU
684	

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SEARCH A ARRAY

YAV-8B ARRAY SEARCH

685	RCS07 RXRPTG	
686	RCS07 RXYPTG	
687	RCS07 RXVF	
688	RCS07 PXVND	
689	RCS07 RXVMU	
690	RCS07 RFGX	
691	RCS07 RFGY	
692	RCS07 RFGF	
693	RCS07 RFGWD	
694	RCS07 RFGVU	
695	RCS07 RAWUL	PFC07 DARCSUL
696	RCS07 RAWDL	PFC07 DARCSDL
697	RCS07 RAYS	PFC07 DRRCS
698	RCS07 RAF	PFC07 DHRCSE

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SEARCH A ARRAY

YAV-8B ARRAY SEARCH

699	RCS07 RAPR	PFC07 DHRC5A
700	RCS07 RACF	
701	RCS07 RASR	
702		
703	RCS07 RAWUR	PFC07 DARCSUR
704	RCS07 RAWDR	PFC07 DARCSOR
705	----	708
709	AEROY8B DCLLF	
710	----	713
714	AEROY8B DCLLFJD	
715	AEROY8B ADGE	
716	----	723
724	AEROY8B CYBAT	
725	AEROY8B CLLBAT	
726	AEROY8B CLN	

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SEARCH A ARRAY

YAV-8B ARRAY SEARCH

727	AEROY8B CLNBAS
728	AEROY8B CLNPNOR
729	AEROY8B CLNBASE
730	AEROY8B DCLNATL
731	AEROY8B DCLNRUD
732	ISOMS POEG
733	ISOMS QDEG
734	ISOMS RDEG
735	----- 736
737	PFC07 TGO
738	PFC07 PFLTO
739	
740	PFC07 DLAN
741	PFC07 ARTL
742	PFC07 DRAD

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SEARCH A ARRAY

YAV-88 ARRAY SEARCH

743	PFC07 ANTR		
744	PFC07 YRCS		
745	PFC07 YRATE		
746	PFC07 DTRCSF		
747	PFC07 DTRCSA		
748	PFC07 ANY		
749	PFC07 AYHUB		
750	ENG08 PBLT		
751	I50MS FTX	ENG08 FTX	TEOM2 THX
752	I50MS FTY	ENG08 FTY	
753	I50MS FTZ	ENG08 FTZ	
754	ENG08 THL	REDM2 THL	
755	ENG08 THN		
756	ENG08 THN		

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SEARCH A ARRAY

YAV-88 ARRAY SEARCH

757	ENG08 PVFGC	
758	ENG08 PKSPLAY	
759		
760	ENG08 DTHR	
761	ENG08 FKALT	
762	ENG08 DELT72	
763	----- 768	
769	AEROY88 FGTHR	ENG08 PFG
770		
771	ENG08 RPM	
772	----- 775	
776	ISOMS PCTHR	ENG08 PCTHR
777	ISOMS PCNOZ	ENG08 PCNOZ
778	ENG08 PWACNR	
779	----- 780	

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SEARCH A ARRAY

YAV-8B ARRAY SEARCH

781	ENG08 YDEFUEL		
782	ENG08 POFUEL	WTBAL07 FUEL	
783			
784	ENG08 PWFT		
785	ENG08 PUFSS		
786	ENG08 KINGO		
787	ENG08 FUELOW		
788	AEROY8B THEYAJ	ENG08Pos	RC807Pos THEYAJ
789	ENG08 PFGCDR		
790	ENG08 PCFUEL		
791	WTBAL07 FUELMX		
792	ENG08 T7ERD		
793	ENG08 PEGBLDC		
794	ENG08 PWFRDC		

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SEARCH A ARRAY

YAV-88 ARRAY SEARCH

795	ENG08 PFGRDC
796	ENG08 PWFCOR
797	
798	ENG08 PWFCOM1
799	ENG08 PWFCOM
800	ENG08 PTMP
801	ENG08 PWFAEL
802	ENG08 PWFCOL
803	ENG08 PDELNF
804	ENG08 PNFRPM
805	ENG08 PNFCOR
806	ENG08 PSD
807	ENG08 PEGTCOR
808	
809	ENG08 PPHCOR

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Volume II

SEARCH A ARRAY

YAV-88 APRAY SEARCH

810	ENG08 PT8CDR		
811			
812	ENG08 PRAH		
813	ENG08 PE8YB		
814	ENG08 PEGT		
815	ENG08 PPH	RCS07 PPH	
816	150MS PY8LD	ENG08 PY8LD	RCS07 PY8LD
817			
818	ENG08 PEGYC		
819	ENG08 PWATER	WTBAL07 PWATER	
820			
821	ENG08 PMP		
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825		ENG08 PWA	
826			

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SEARCH A ARRAY

YAV-88 ARRAY SEARCH

827	ENG08 PKWF2	
828	ENG08 TRTNGO	
829	ENG08 YFUELOW	
830		
831	ENG08 IENGFO	
832		
833	ENG08 TCFS	
834	ENG08 TCWL	
835	ISOMS IWATER	ENG08 IWATER
836	ENG08 PSA	
837	ENG08 NR	
838		
839	ENG08 PCDP	
840		
841	ENG08 TTC	

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SEARCH A ARRAY

YAV-8B ARRAY SEARCH

842	ENG08 PK1
843	ENG08 PK2
844	ENG08 PK6
845	ENG08 PK3
846	ENG08 DWRC5
847	ENG08 PMFRC5
848	ENG08 PKOPER
849	ENG08 FGDFGM
850	ENG08 TTCC
851	ENG08 JBYC
852	ENG08 XK1
853	ENG08 XK2
854	ENG08 PSAR
855	ENG08 TTIME

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SEARCH A ARRAY

YAV-8B ARRAY SEARCH

856	----	864							
865		ENG08 PMINLTT							
866	----	867							
868		ENG08 RLIMLTT							
869	----	870							
871		ENG08 YMINLTT							
872	----	873							
874		ENG08 ELIMOFF							
875		ENG08 IJP							
876		TEOM2 GGX							
877	----	878							
879		REOM2 GGL							
880	----	881							
882		SFC07 IGEAR							
883		AEROY88 ONGEAR	ENG08 ONGEAR	PFC07 DELGEAR	SFC07 ONGEAR	WTBAL07 ONGEAR			
884	----	887							

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SEARCH A ARRAY

YAV-8B ARRAY SEARCH

888	ENG08 DTCFS			
889	----- 893			
894	ENG08 IWAIFLO			
895	----- 899			
900	PECO7 IWIOWW	SECO7 IWIOWW		
901	----- 928			
929	ENG08 SVCAL	PECO7 VCAL	SECO7 VKTS	
930	----- 942			
943	I50MS PODEG			
944	I50MS QODEG			
945	I50MS RDEG			
946	----- 958			
959	I50MS ICASE	ATMOS ICASE		
960	----- 964			
965	ENG08 SUCAL			
966	----- 972			

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Volume II

SEARCH A ARRAY

YAV-8B ARRAY SEARCH

973	150MS XTOT
974	150MS YTOT
975	150MS ZTOT
976	----- 999
1000	150MS ANZB



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APPENDIX C
YAV-8B DATA PLOTS

INDEX TO ENGINE DATA PLOTS

DEPENDENT VARIABLE	DEFINITION	DATA TABLE NAME	PAGE
EGKDAY	Ambient temperature corrections to EGT as a function of altitude and ambient temperature ratio	EGKDAYU	C-4
EGKMO	Mach number correction to EGT as a function of corrected fan speed and Mach number	EGKMOU	C-5
FKALT	Altitude correction to gross thrust as a function of corrected fan speed and ambient pressure	FKALTU	C-6
FKSCRUB	Nozzle correction to scrub drag as a function of nozzle position	FKSCRBU	C-7
NR	Ram recovery ratio factor as a function of corrected fan speed and Mach number	NRTABU	C-8
PBLI	Inlet and boundary layer bleed drag as a function of corrected airflow and Mach number	PBLIU	C-9
PEGBLDC	RCS bleed correction to EGT as a function of corrected fan speed	EKRCSTU	C-10
PEGTCOR	Jet pipe temperature as a function of corrected fan speed and ram recovery ratio	EGTABU	C-11
PENTMPD	EGT corrections due to nozzle position (dry) as a function of corrected fan speed and nozzle position	EKNOZDU	C-12
PENTMPW	EGT corrections due to nozzle position (wet) as a function of corrected fan speed and nozzle position	EKNOZWU	C-13
PFGBLDC	RCS bleed correction to gross thrust as a function of corrected fan speed	PFGABU	C-14
PFGCOR	Corrected gross thrust as a function of corrected fan speed and Mach number	FGTABU	C-15
PFGMAX	Maximum corrected gross thrust as a function of Mach number at 100% corrected fan speed	FGTABU	C-16

INDEX TO ENGINE DATA PLOTS (Cont'd)

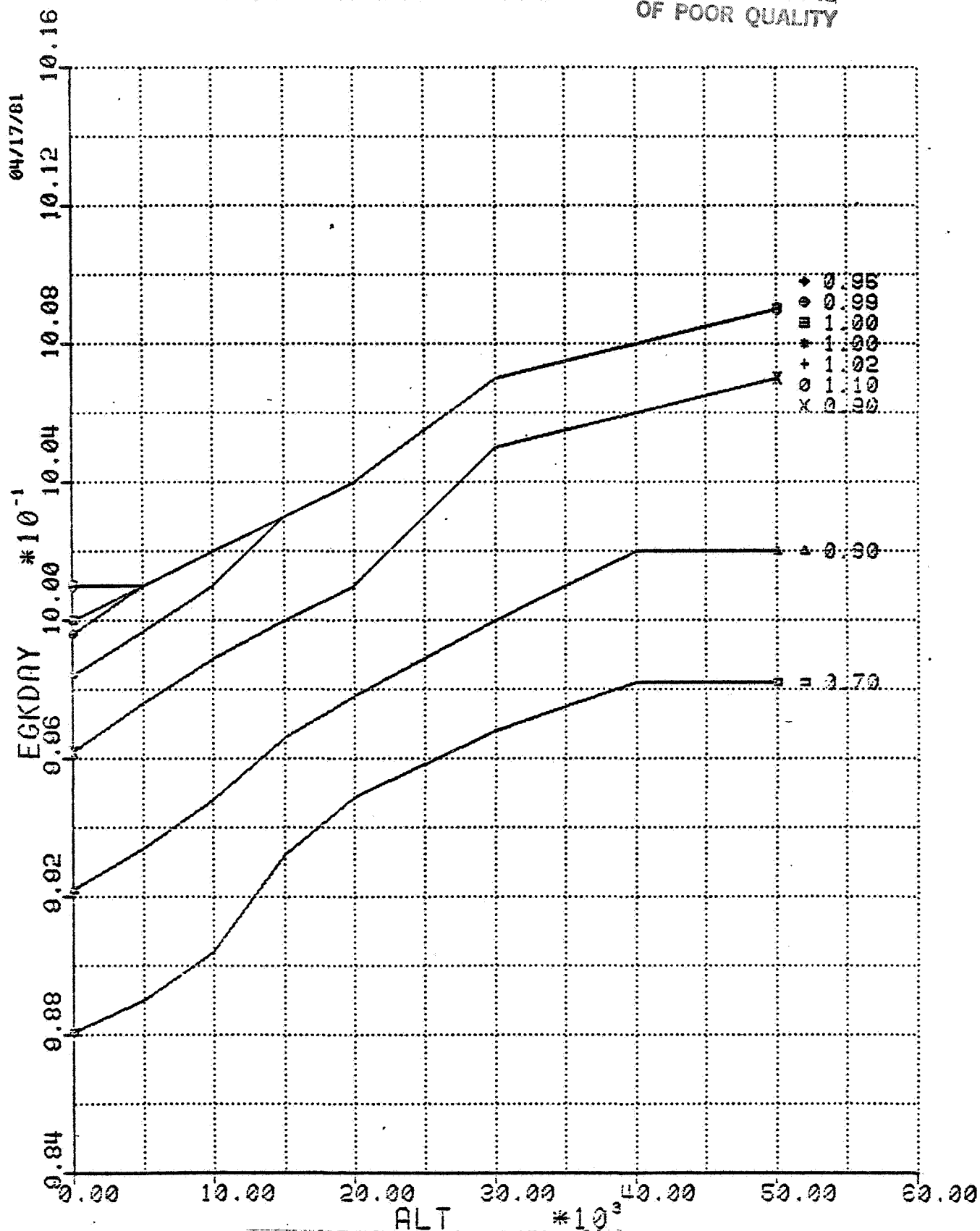
DEPENDENT VARIABLE	DEFINITION	DATA TABLE NAME	PAGE
PKSPLAY	Splay angle correction to gross thrust as a function of corrected fan speed and nozzle position	FSPLAYU	C-17
PK3	Fan speed acceleration factor as a function of fan speed	PK3PT	C-18
PNFCOM1 (vs. PSA)	Commanded RPM as a function of power spindle angle	N1TABU	C-19
PNFCOM1 (vs. SUCAL)	Windmill fan RPM as a function of calibrated airspeed and altitude	WDMLLU	C-20
PPHBLDC	RCS bleed correction to compressor discharge pressure as a function of corrected fan speed	PHRCSU	C-21
PPHCOR	Compressor discharge pressure as a function of corrected fan speed and Mach number	PHTABU	C-22
PSDU	Scrub drag as a function of corrected fan speed and Mach number	DSCRUBU	C-23
PTBCOR	Compressor discharge temperature as a function of corrected fan speed and Mach number	TBTABU	C-24
PWACOR	Corrected airflow as a function of corrected fan speed and Mach number	WATABU	C-25
PWEGTC	Water injection correction to EGT as a function of corrected fan speed	EKWATRU	C-26
PWFBLDC	RCS bleed correction to fuel flow as a function of corrected fan speed	WFRCSU	C-27
PWFCOM	Commanded fuel flow as a function of power spindle angle	WFCTBU	C-28
PWFCOR	Fuel flow parameter as a function of corrected fan speed and ram recovery ratio	WFTABU	C-29

INDEX TO ENGINE DATA PLOTS (Cont'd)

DEPENDENT VARIABLE	DEFINITION	DATA TABLE NAME	PAGE
PWWFC	Water injection correction to fuel flow as a function of corrected fan speed	WFWIU	C-30
TCF	Engine thrust center (fuselage station) as a function of corrected fan speed and nozzle position	TCFSU	C-31
TCRCS	RCS correction to thrust center (fuselage station) as a function of total RCS bleed and corrected fan speed	FSRCSU	C-32
TCWL	Engine thrust center (waterline) as a function of corrected fan speed	TCWLU	C-33
TZERO	Fan speed acceleration limit as a function of percent maximum gross thrust	TOPTS	C-34
WFKDAY	Ambient temperature corrections to fuel flow as a function of ambient temperature ratio and altitude	WFKDAYU	C-35
WFKMO	Mach number corrections to fuel flow as a function of corrected fan speed and Mach number	WFKMOU	C-36

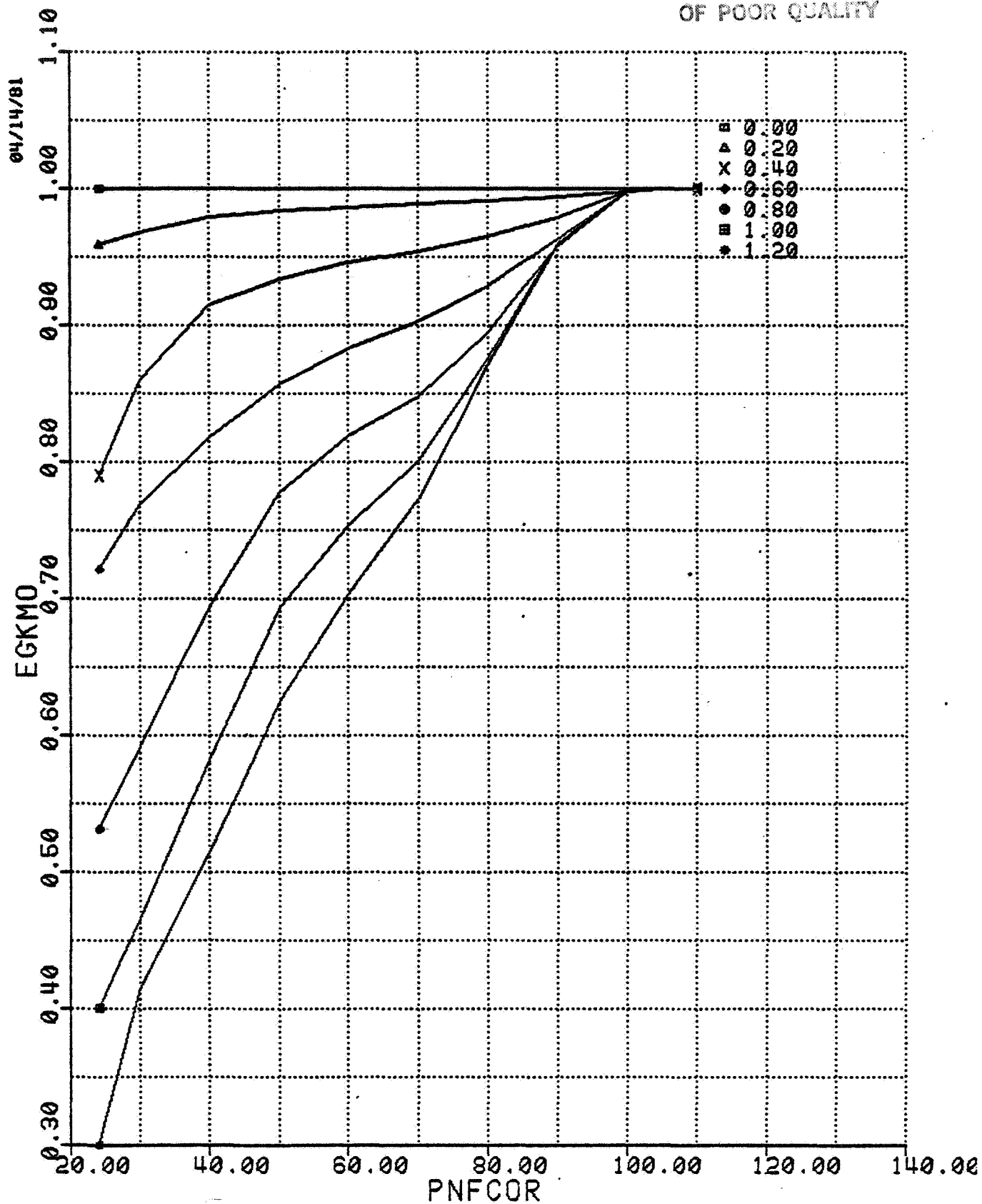
EGKDAY VS ALT
FOR VARYING TAMB

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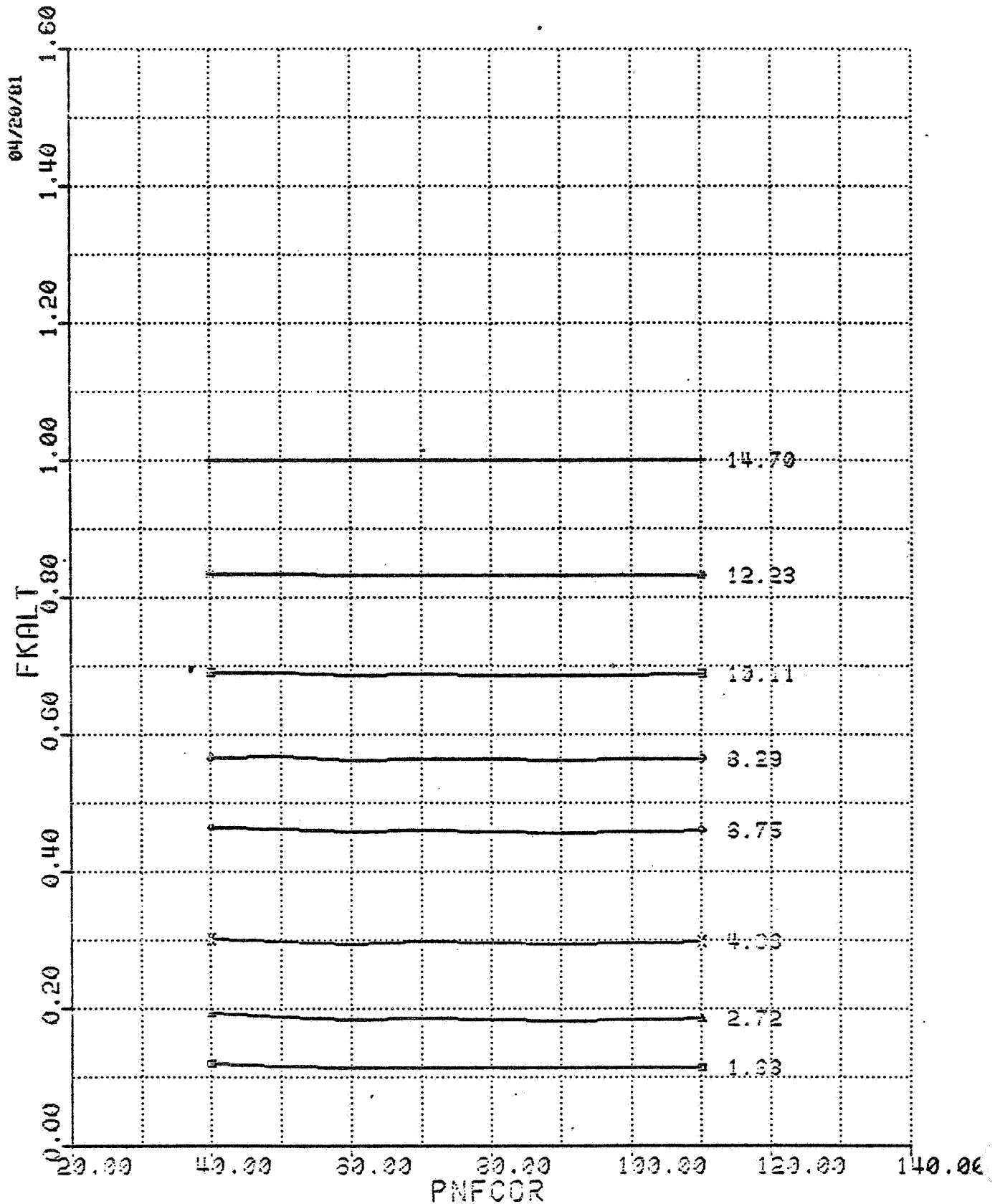


EGKMO VS PNFCOR FOR VARYING MACH NO.

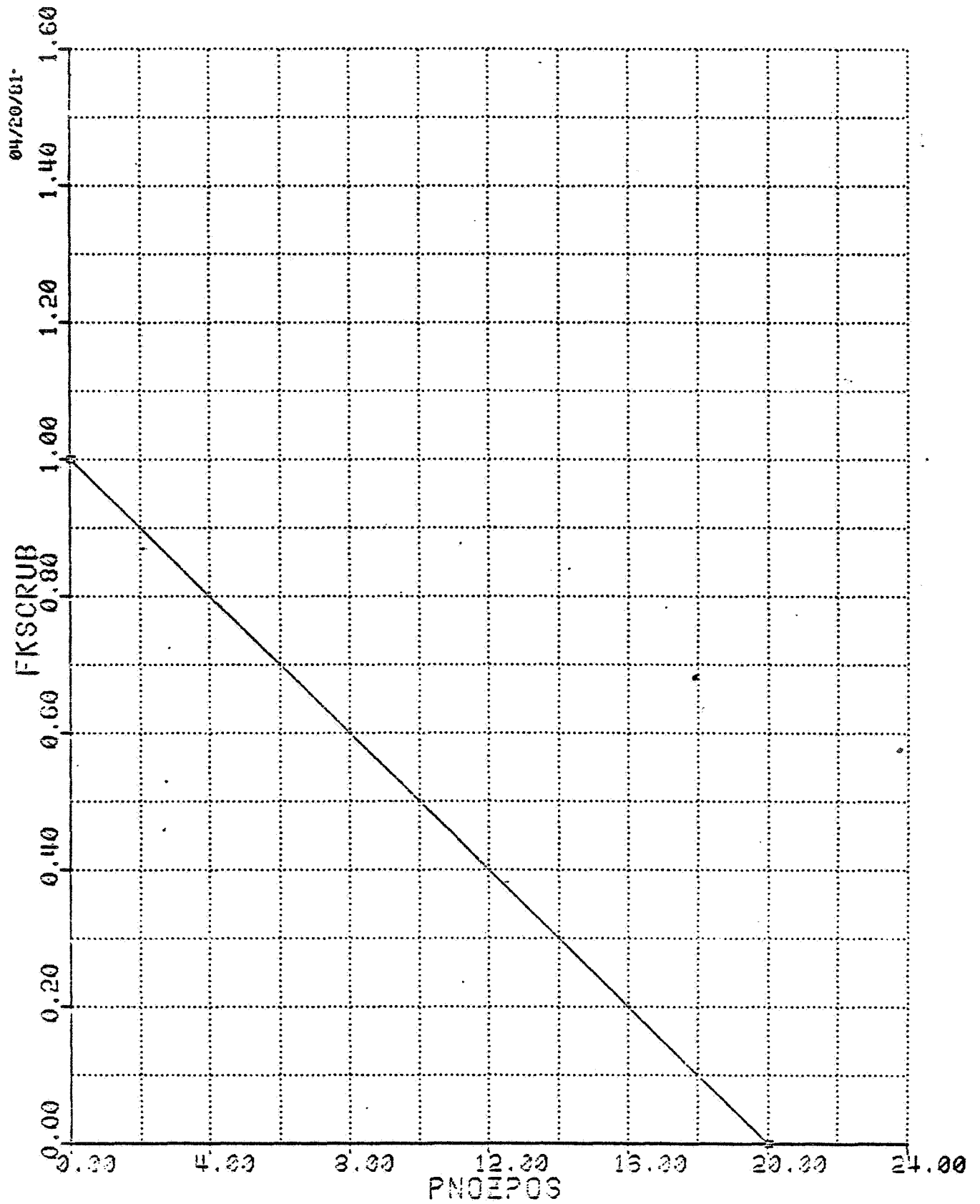
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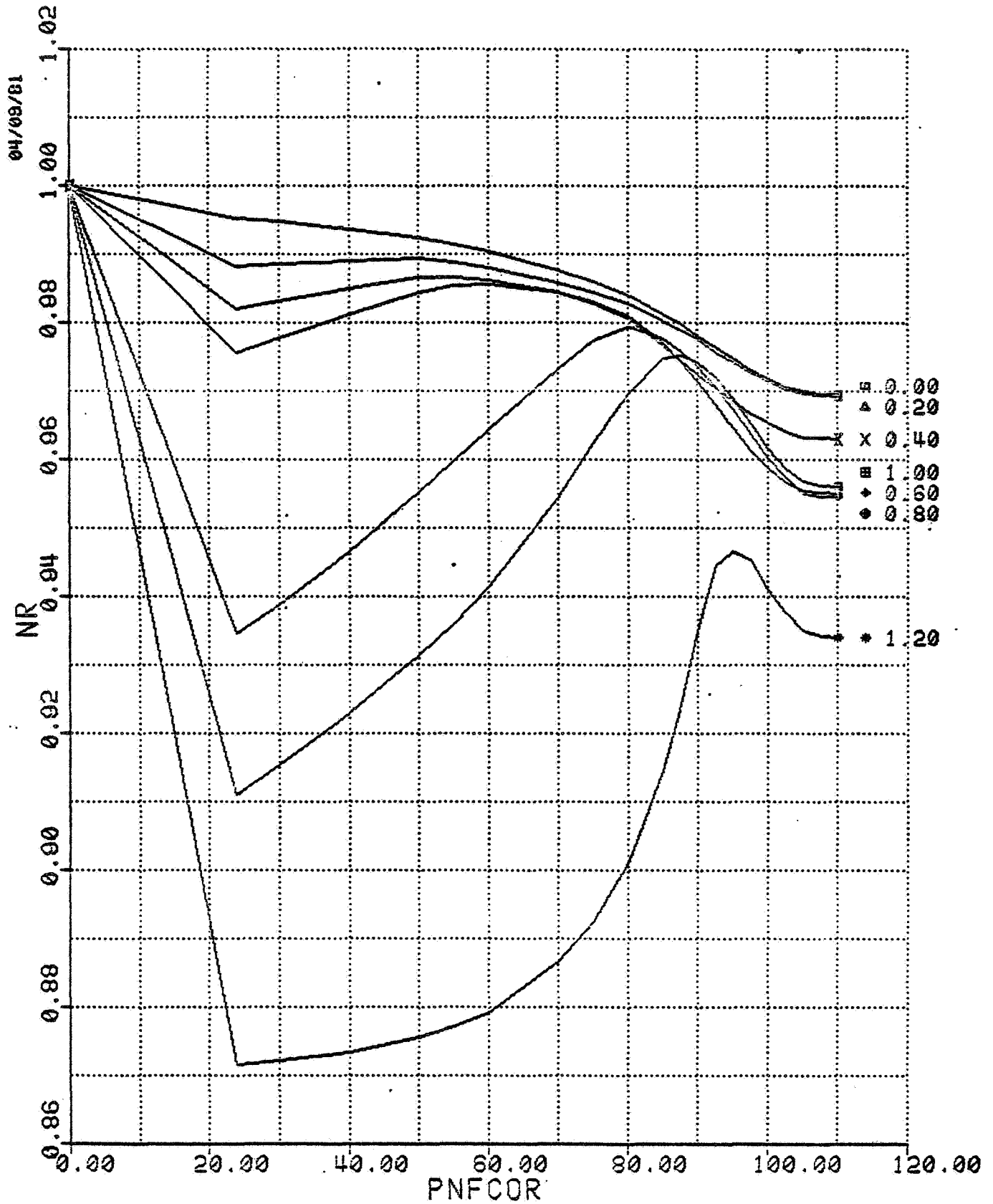
FKALT VS PNFCOR
FOR VARYING FRESHP1



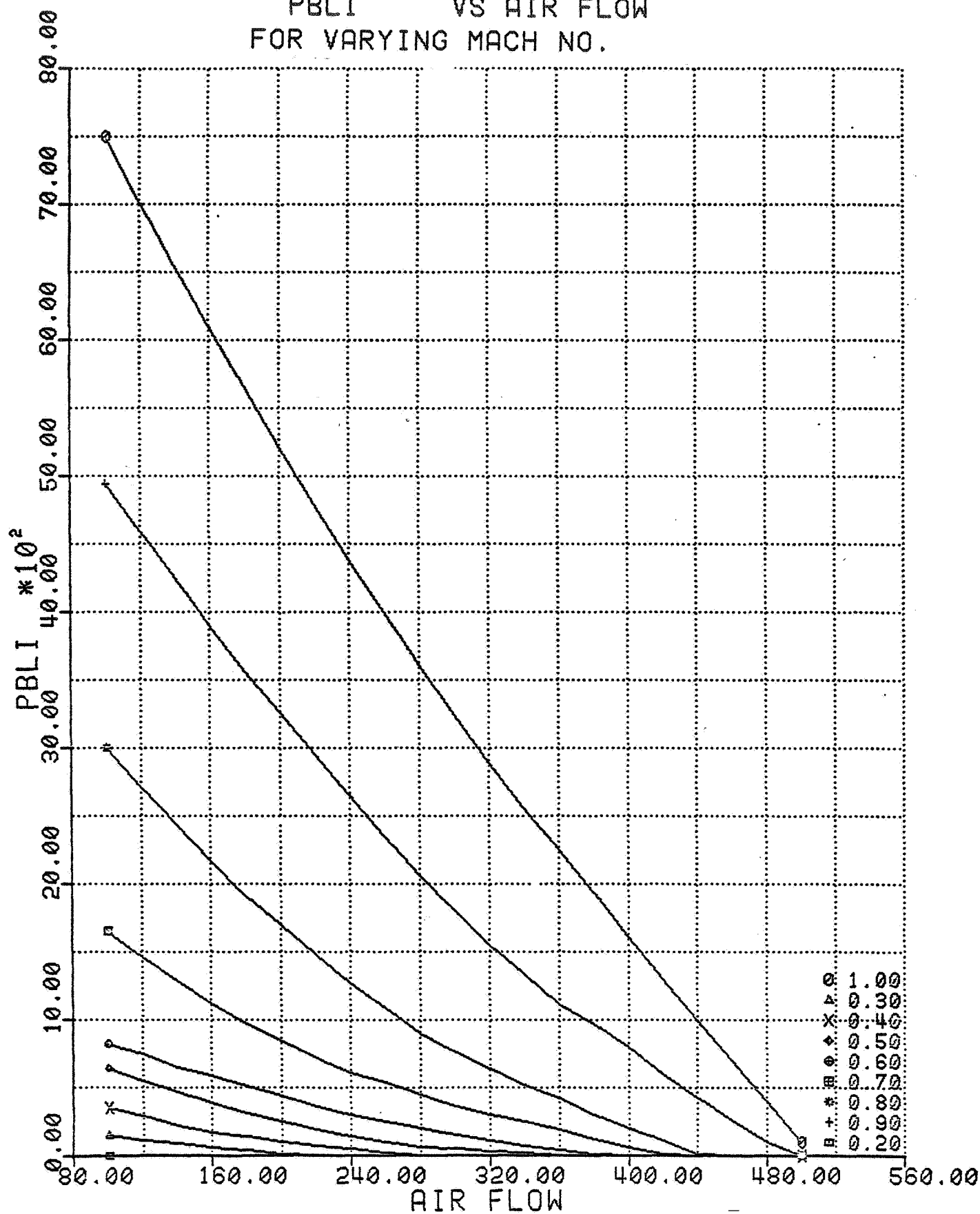
FKSCRUB VS PNOEPOS



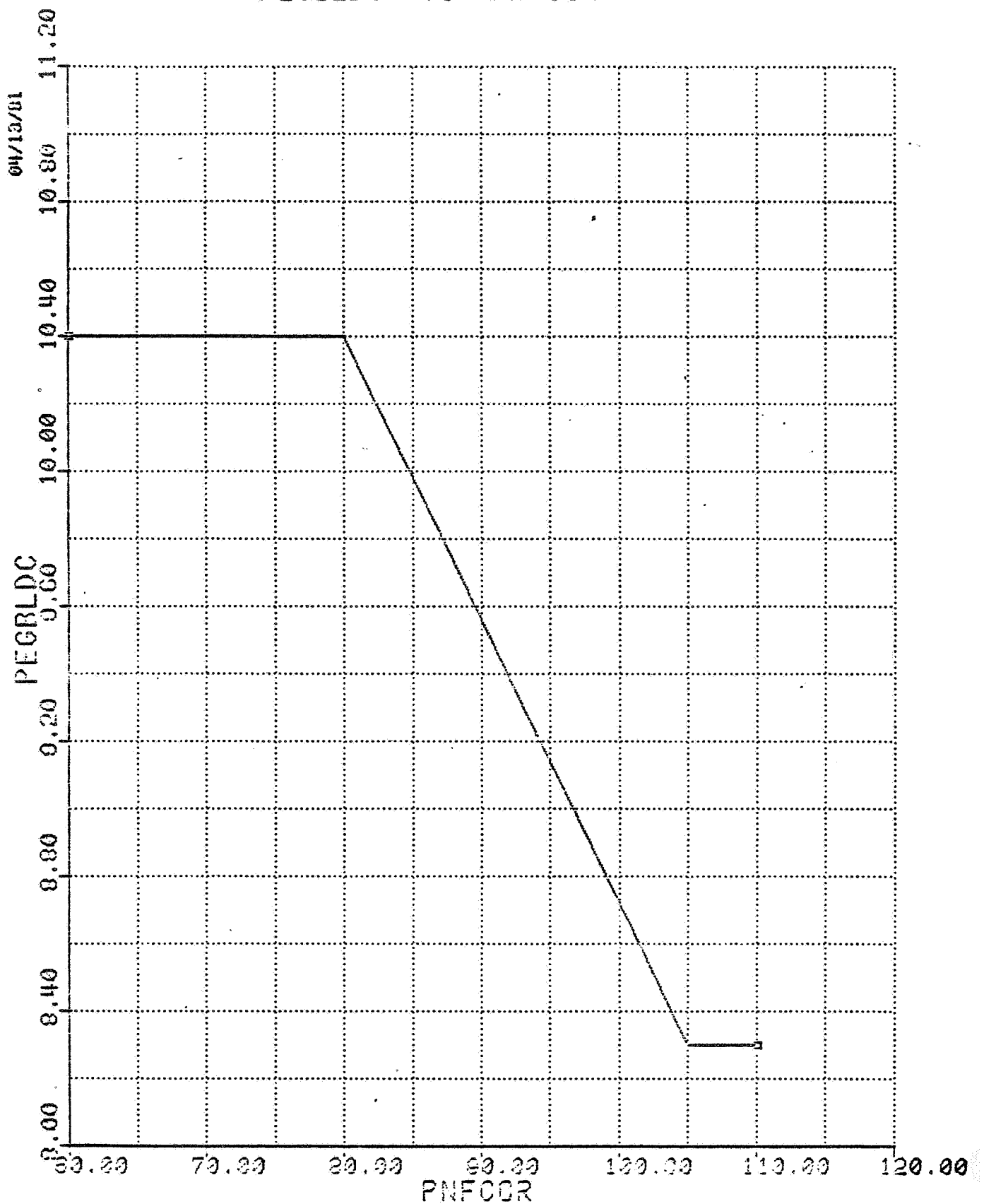
NR VS PNFCOR
FOR VARYING MACH NO.



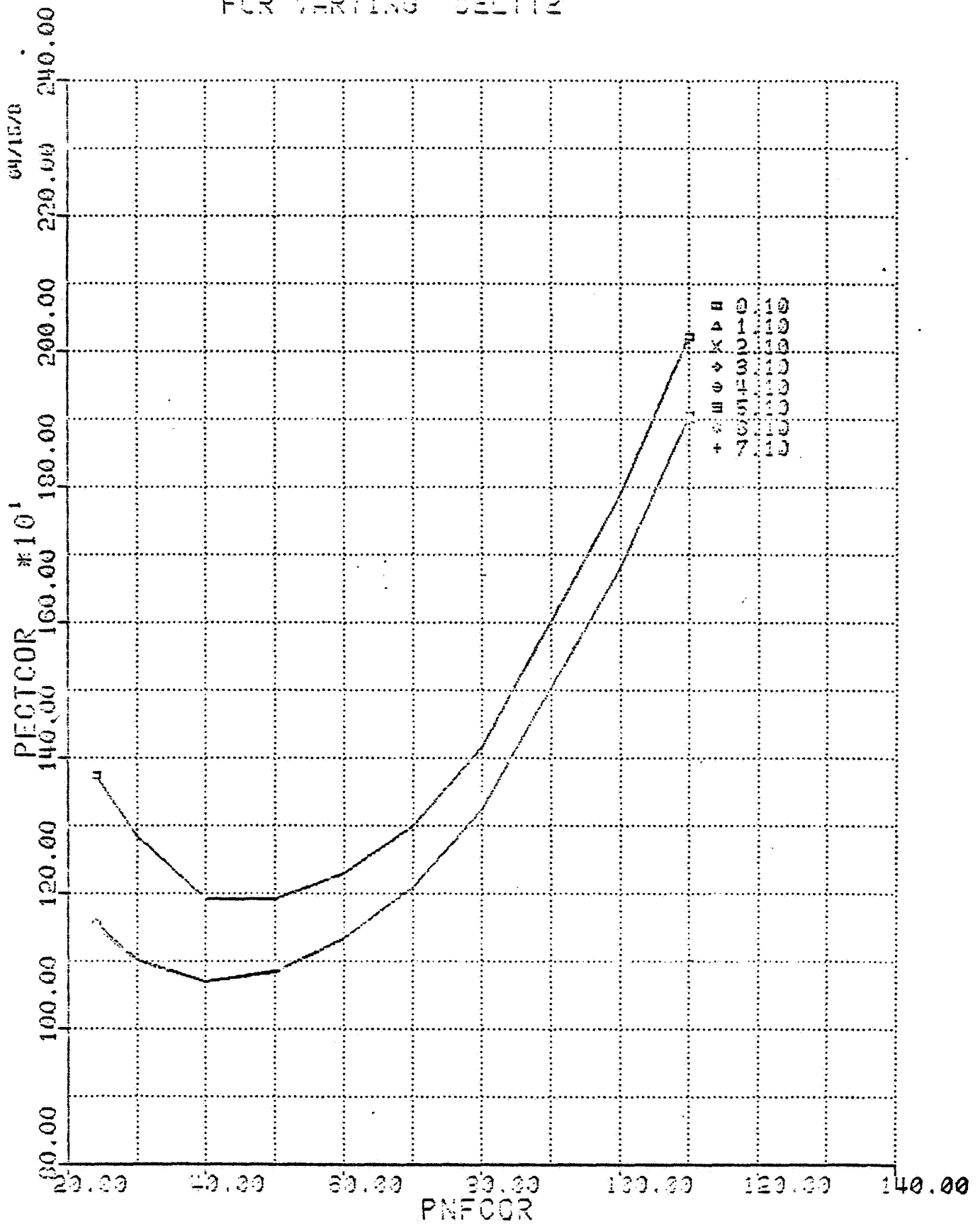
PBLI VS AIR FLOW
FOR VARYING MACH NO.



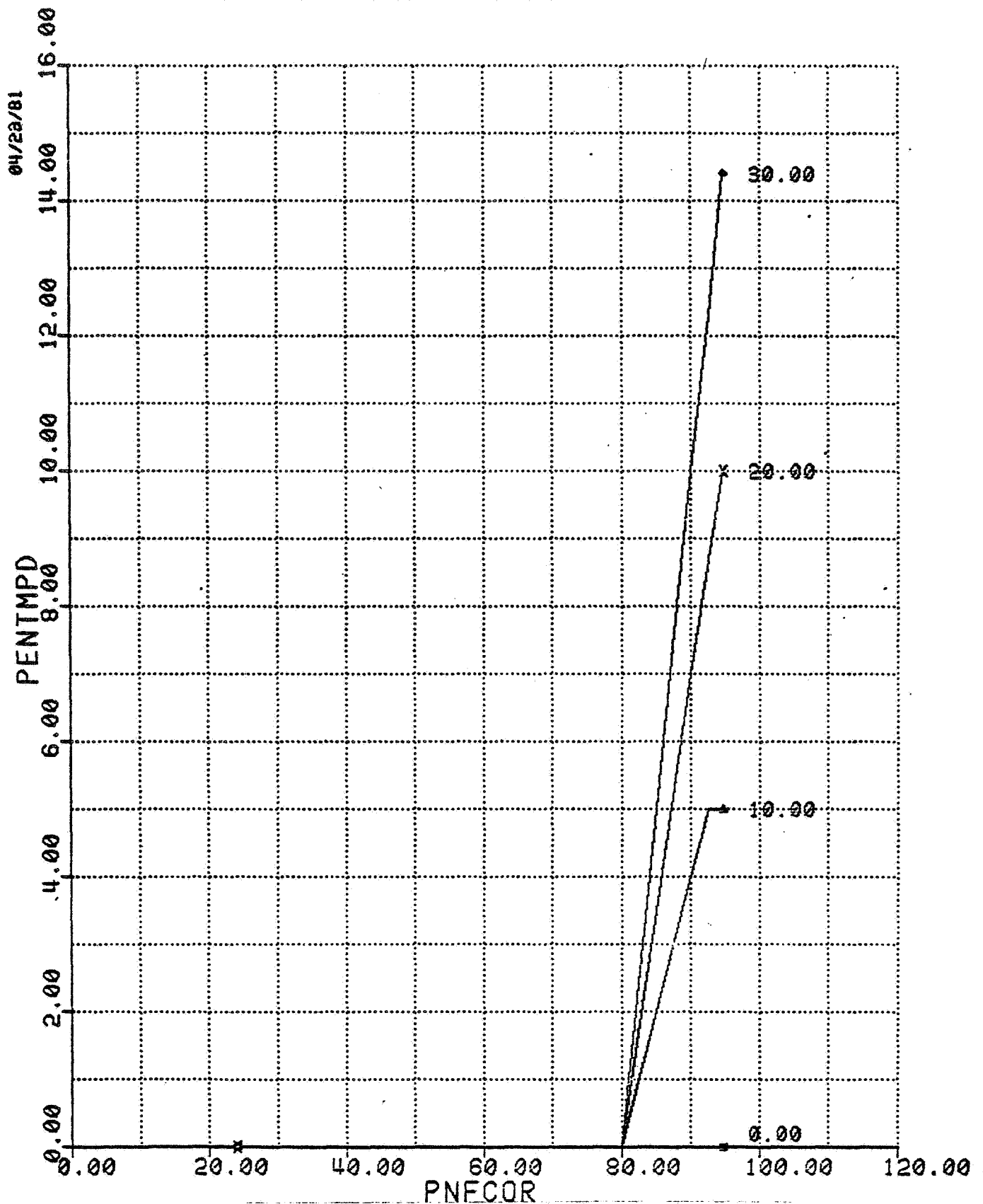
PEGELDC VS PNFCOR



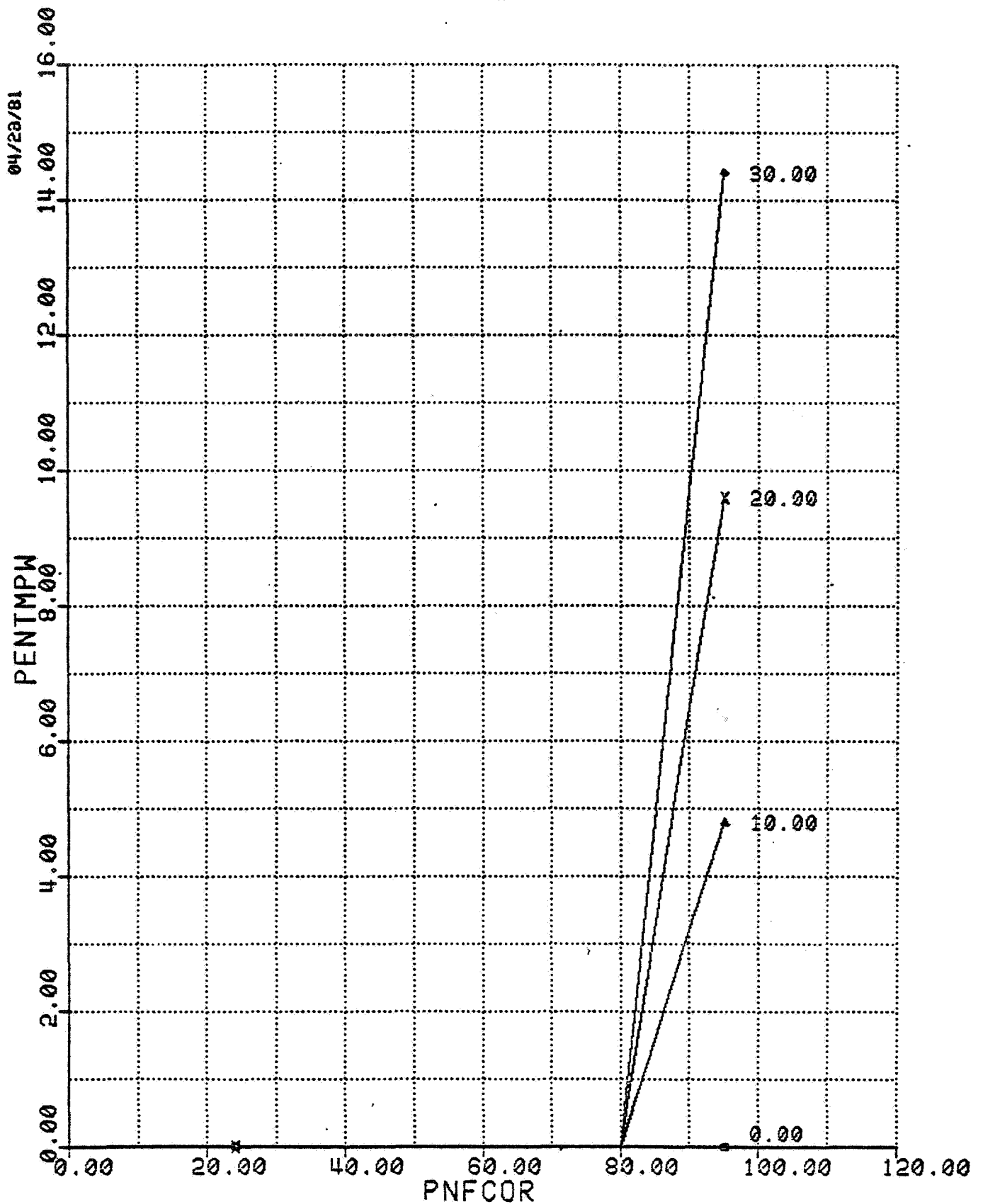
PECTCOR VS PNFCOR
FOR VARYING DELTT2



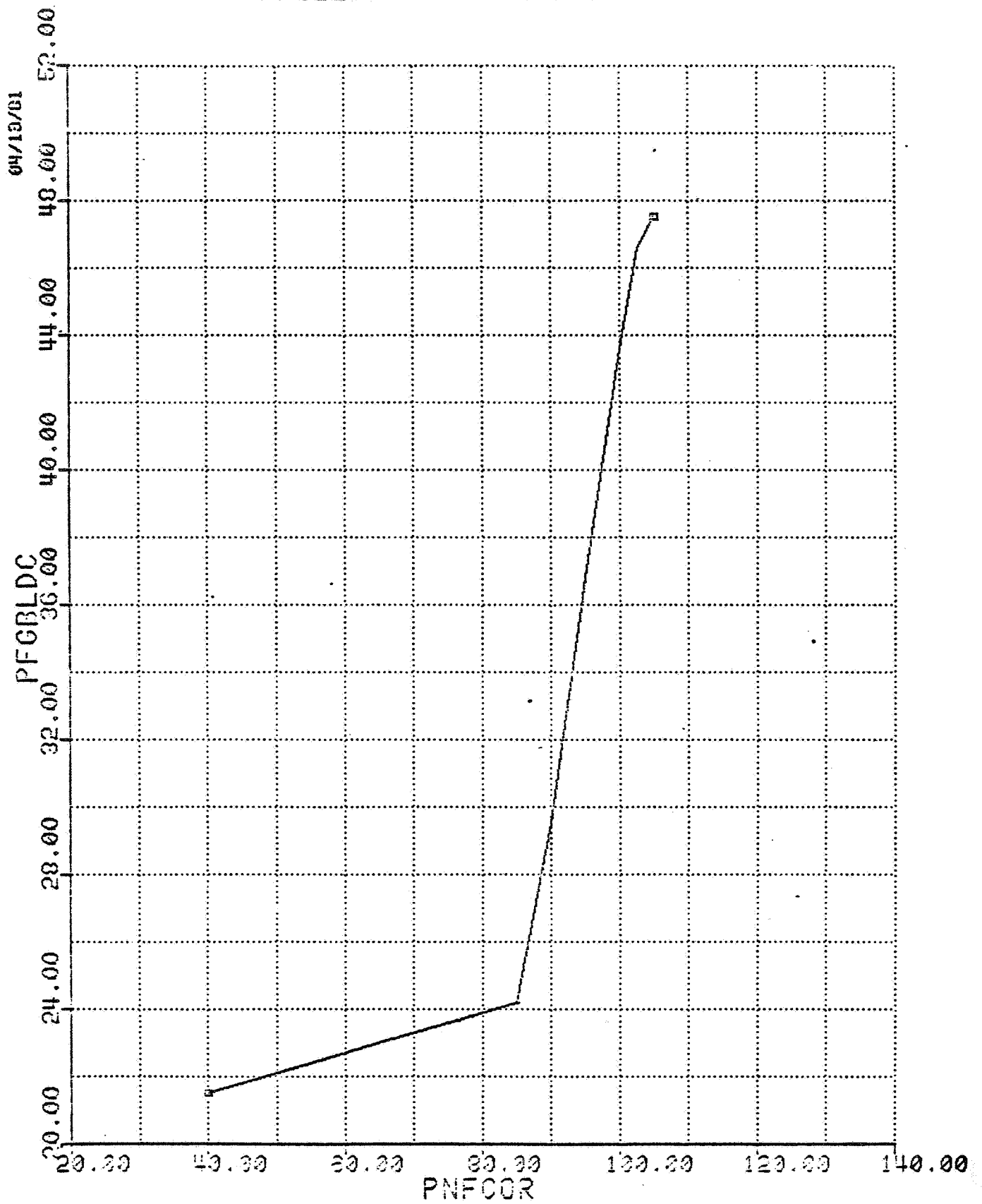
PENTMPD VS PNFCOR
FOR VARYING THETAJ



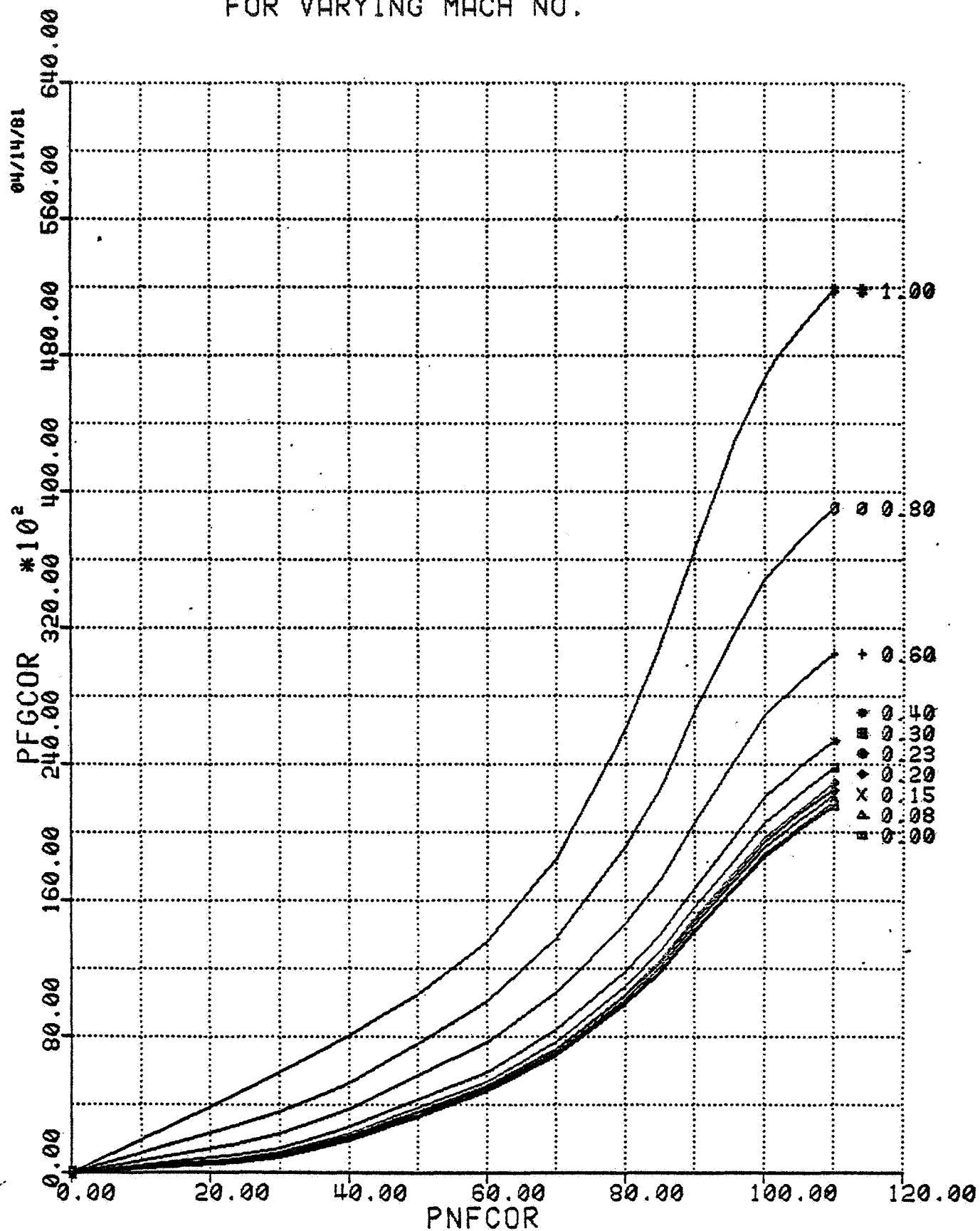
PENTMPW VS PNFCOR
FOR VARYING THETAJ



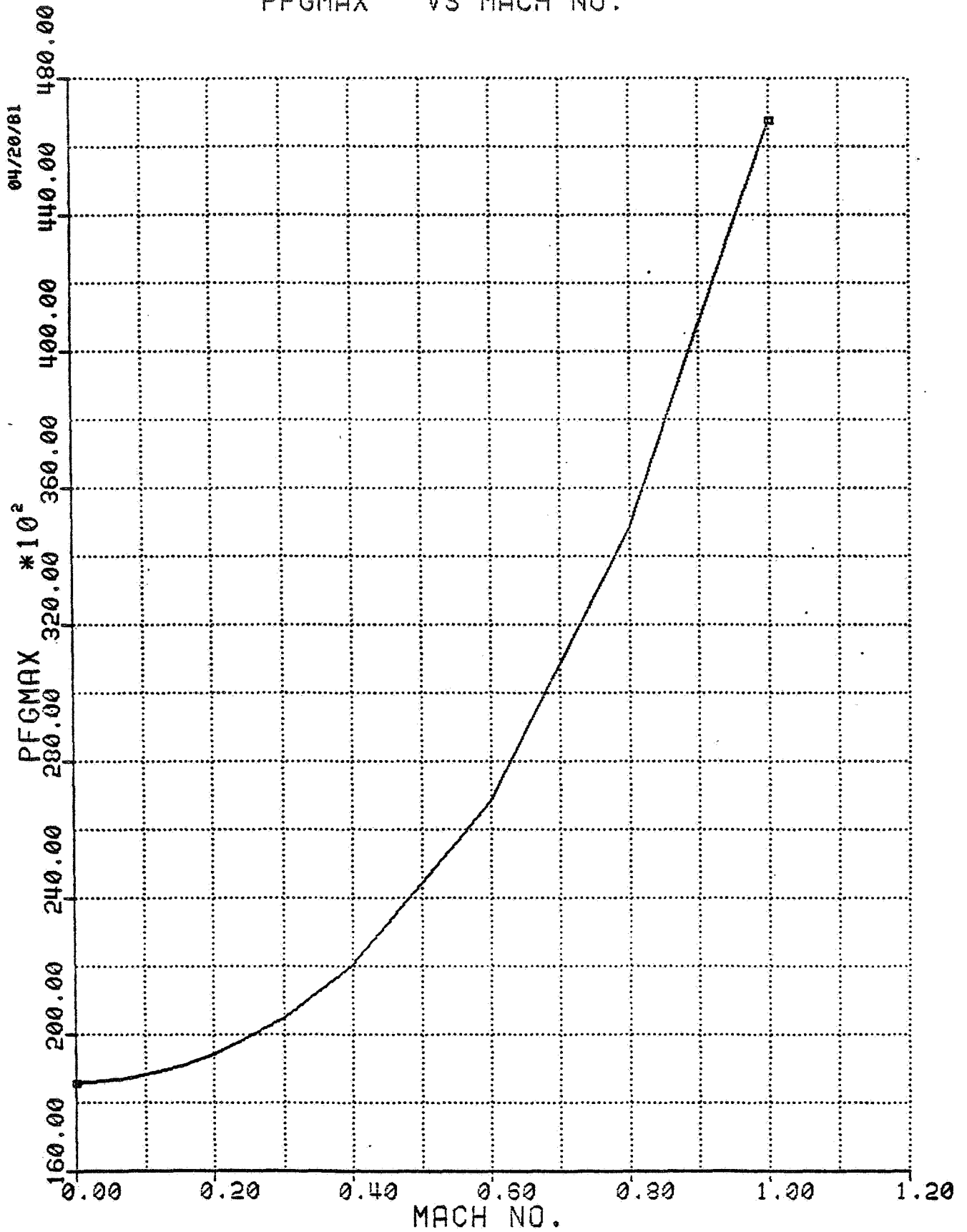
PFGBLDC VS PNFCOR



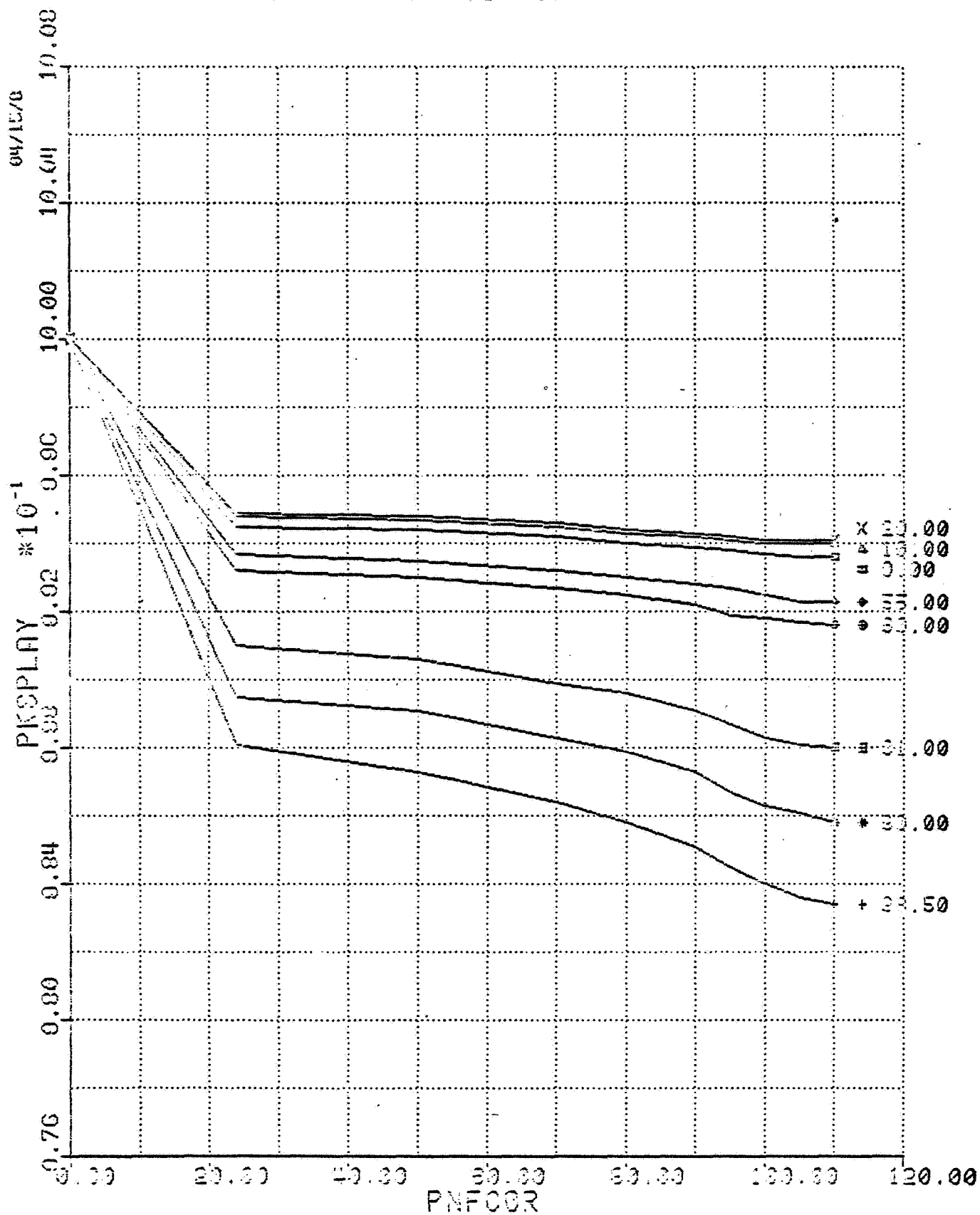
PFGCOR VS PNFCOR
FOR VARYING MACH NO.



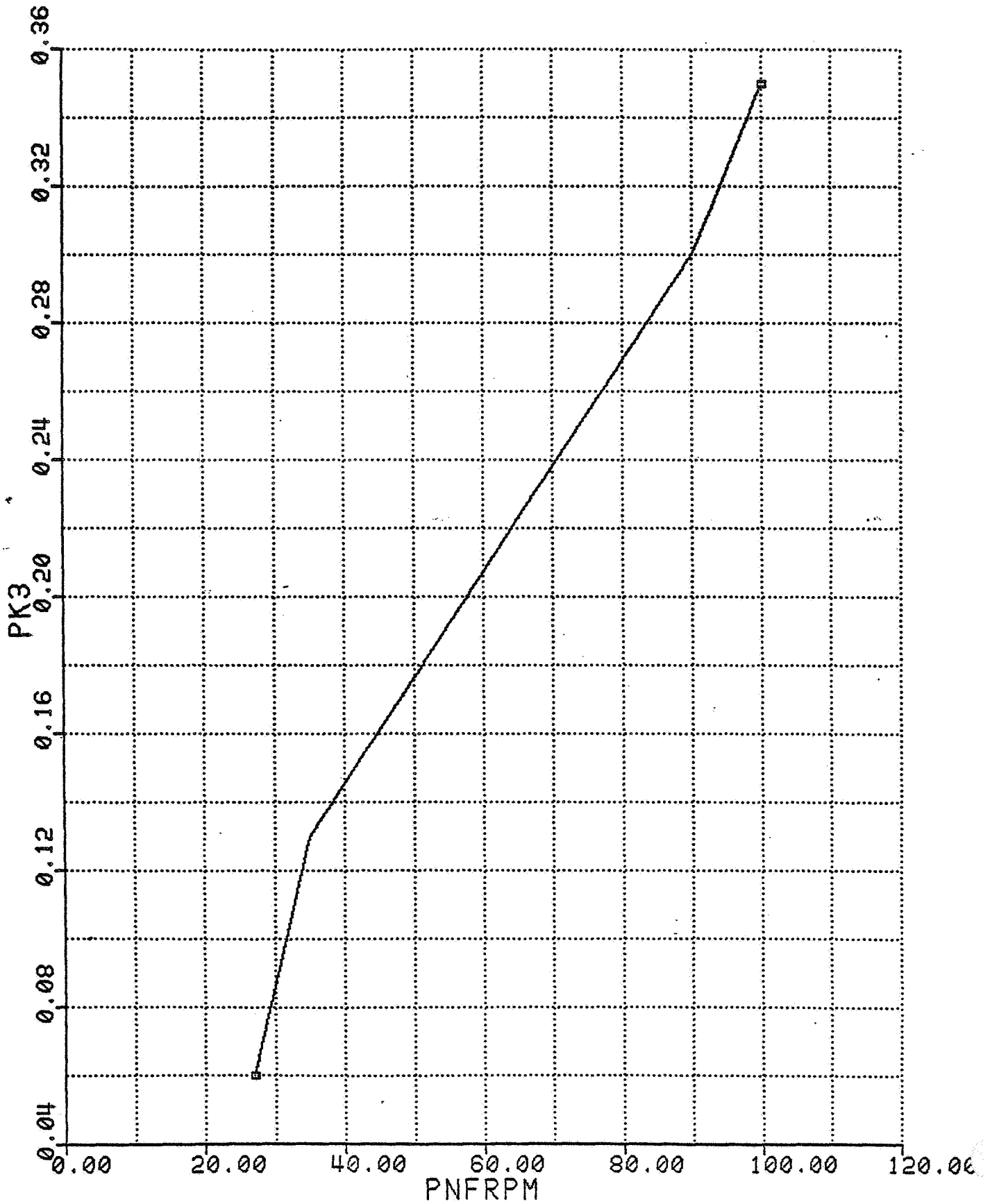
PFGMAX VS MACH NO.



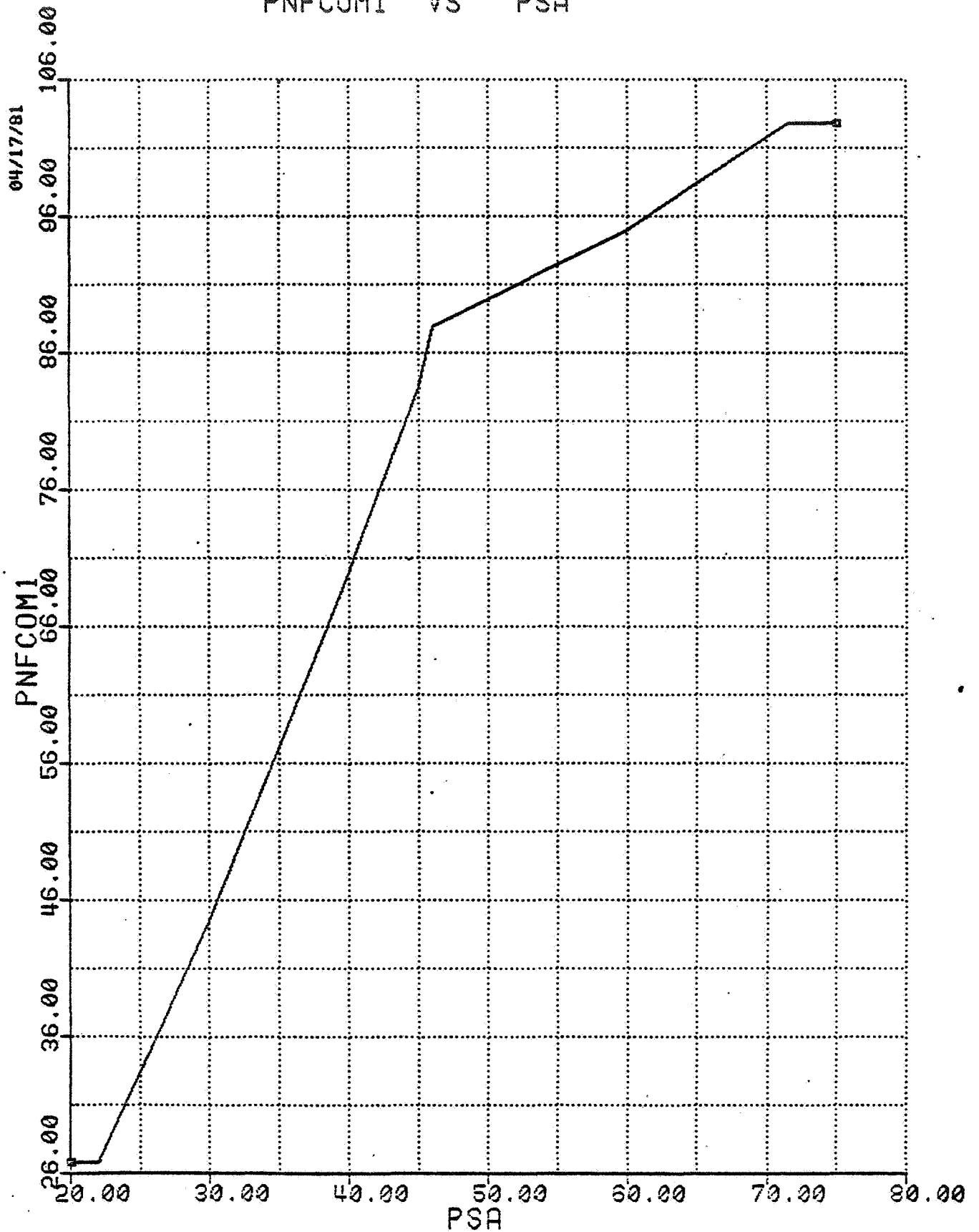
PKSPLAY VS PNFCOR
FOR VARYING NCE.FCS.



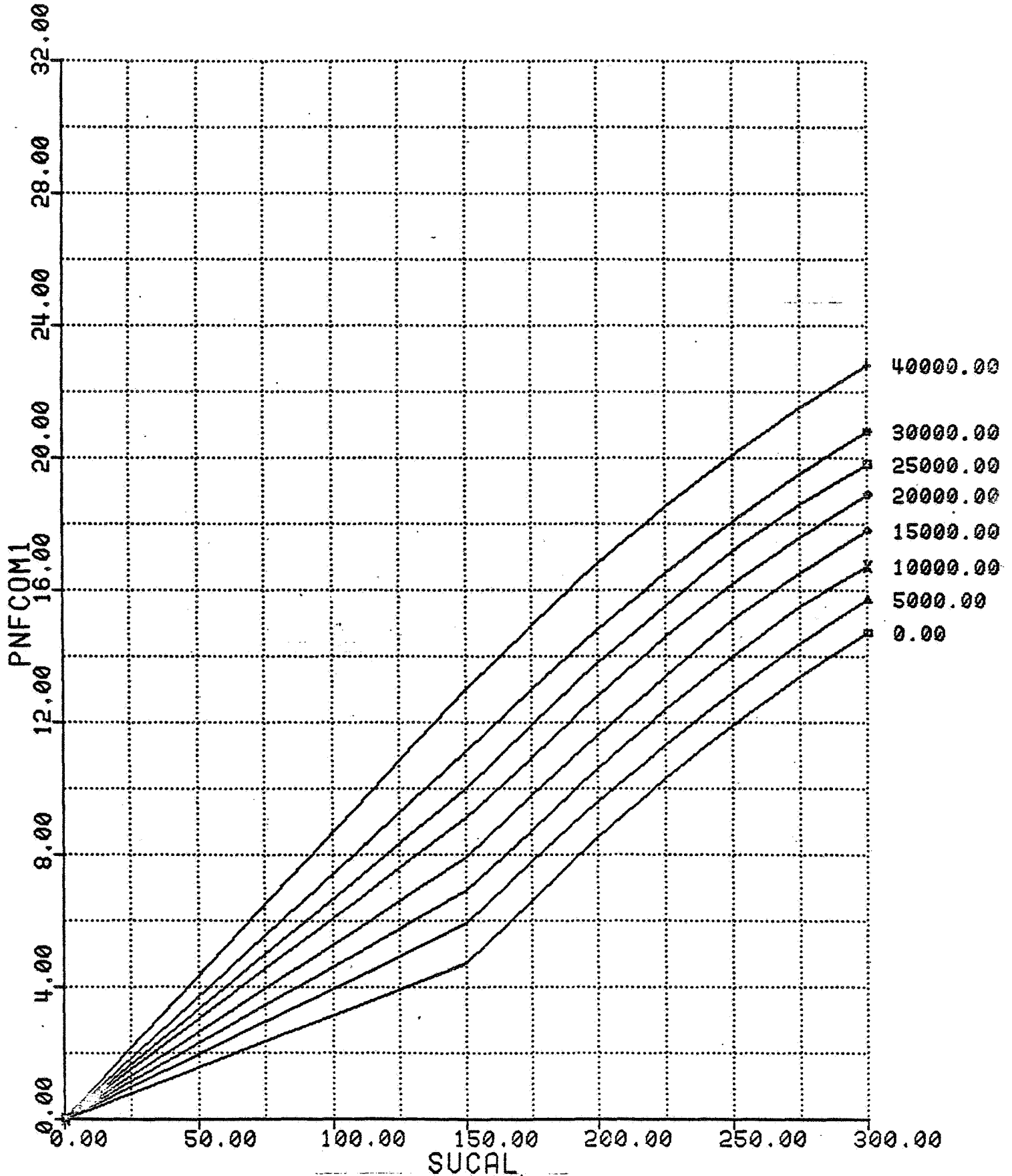
PK3 VS PNFRPM



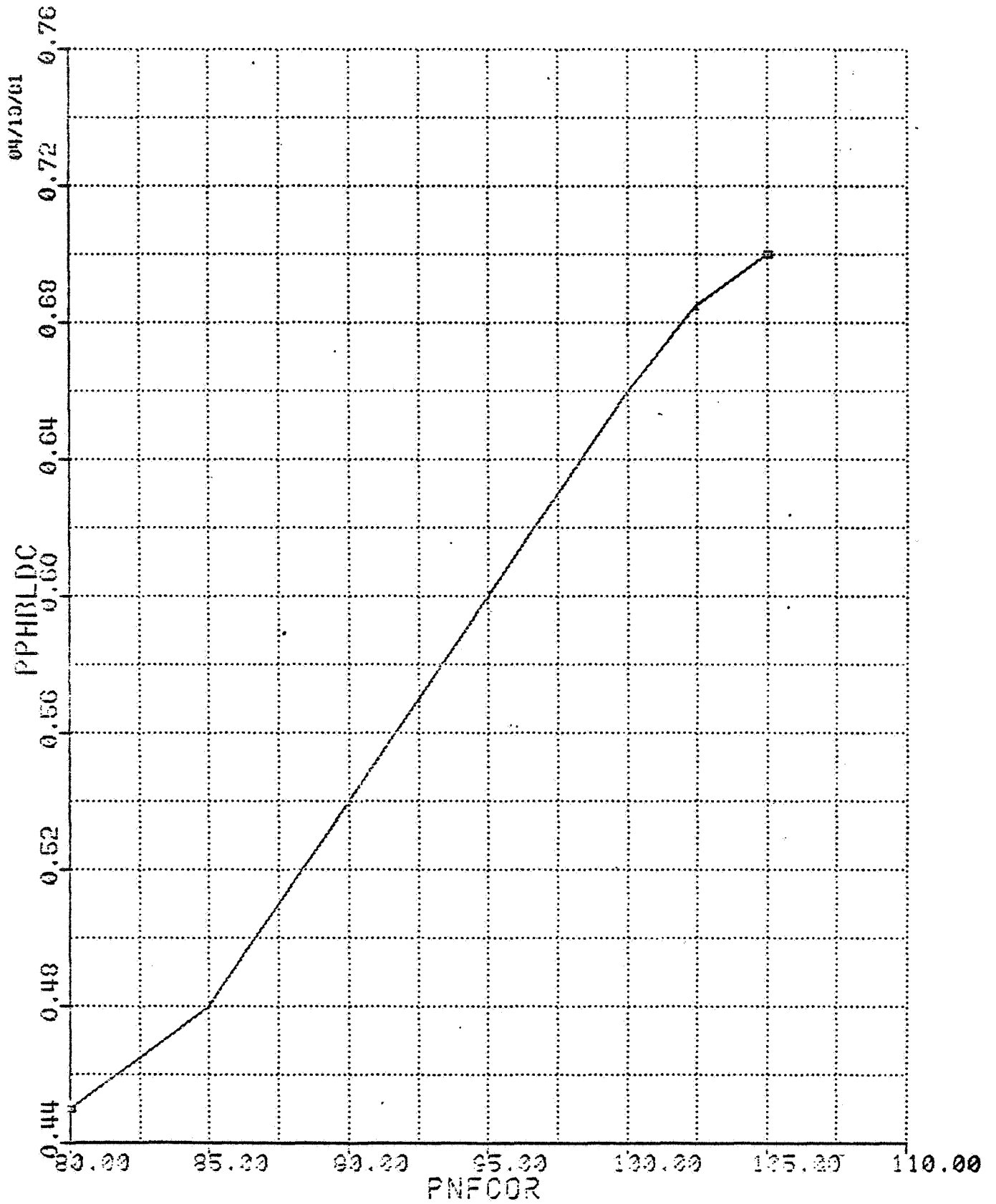
PNFCOM1 VS PSA



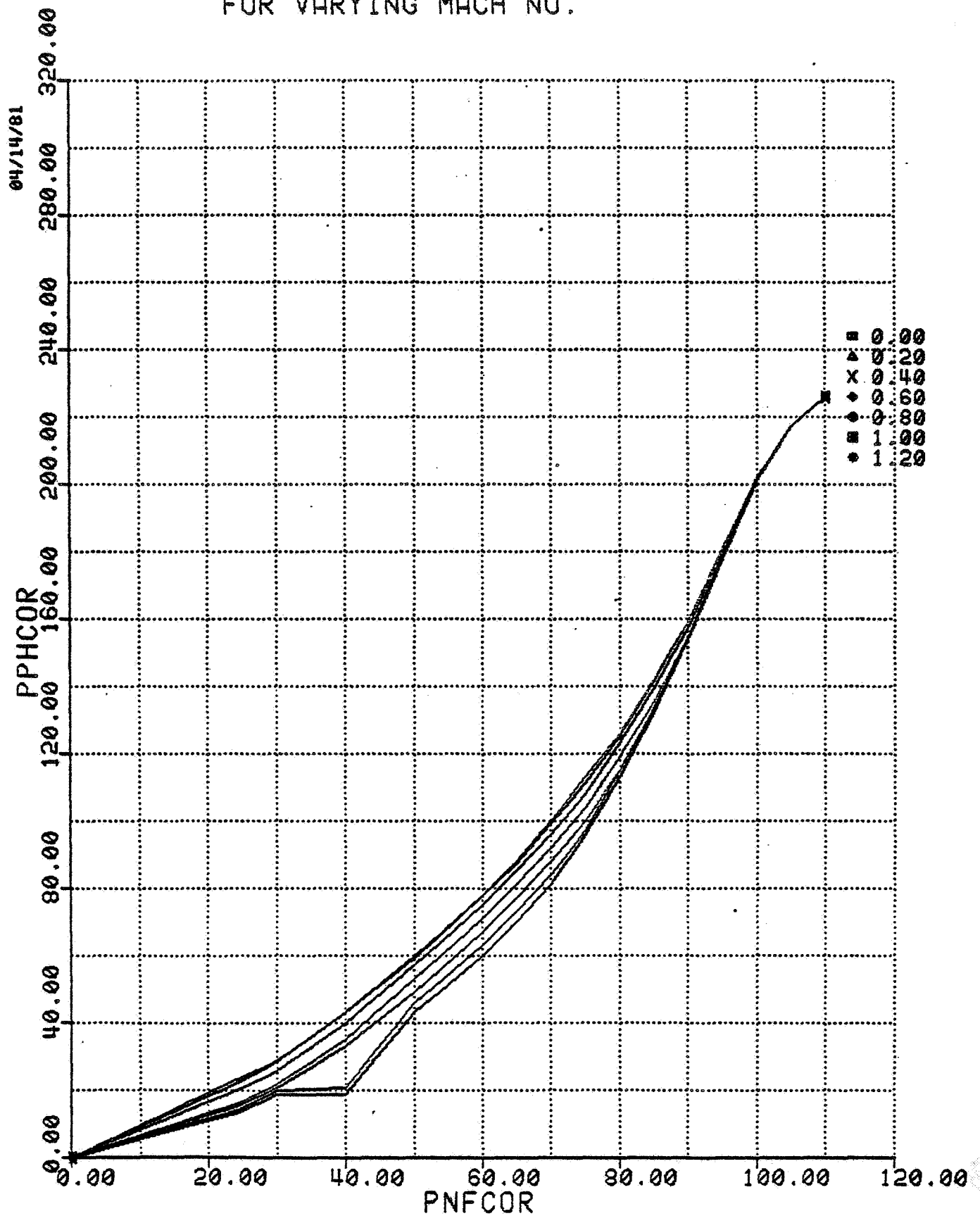
PNFCOM1 VS SUCAL
FOR VARYING H



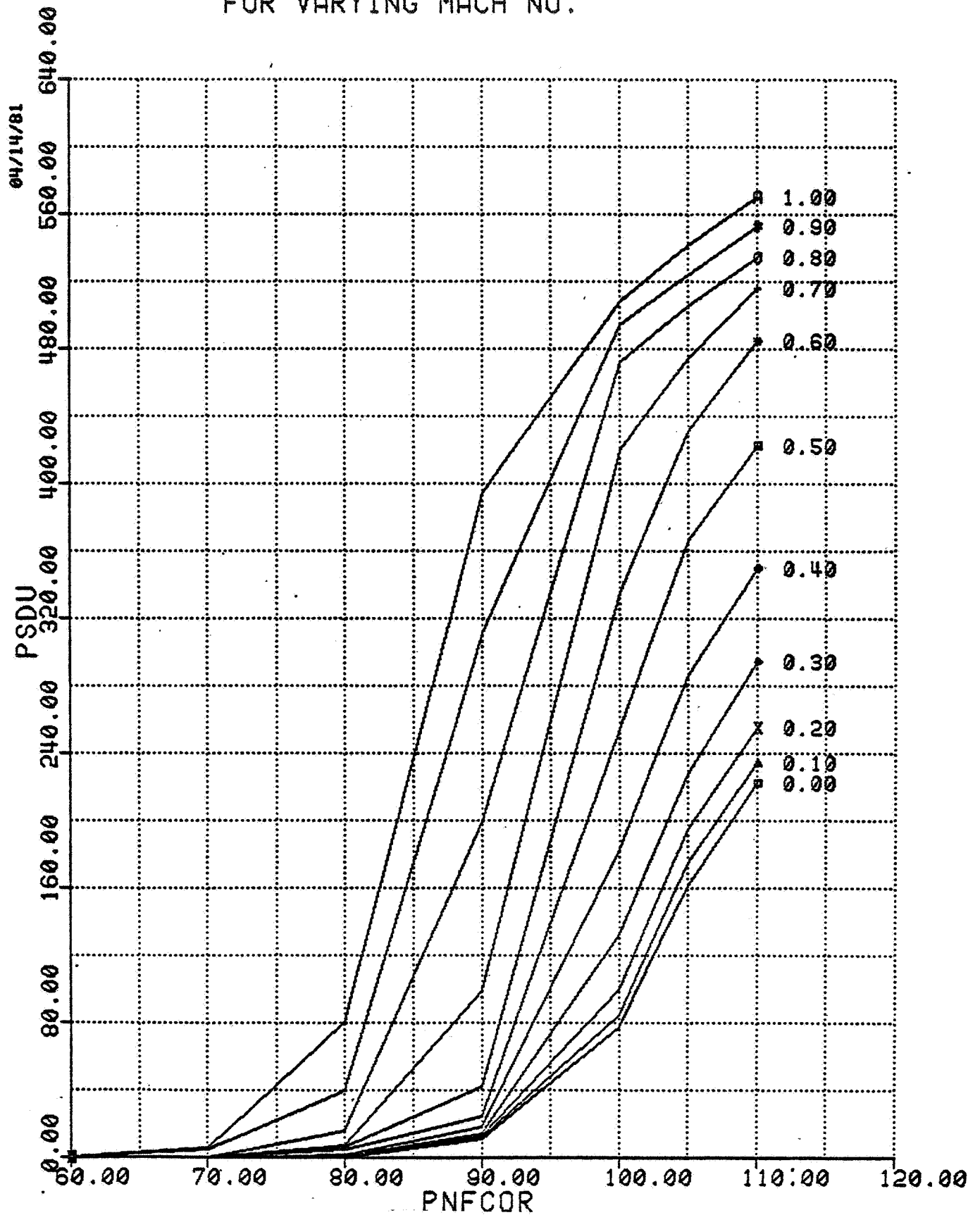
PPHBLDC VS PNFCOR



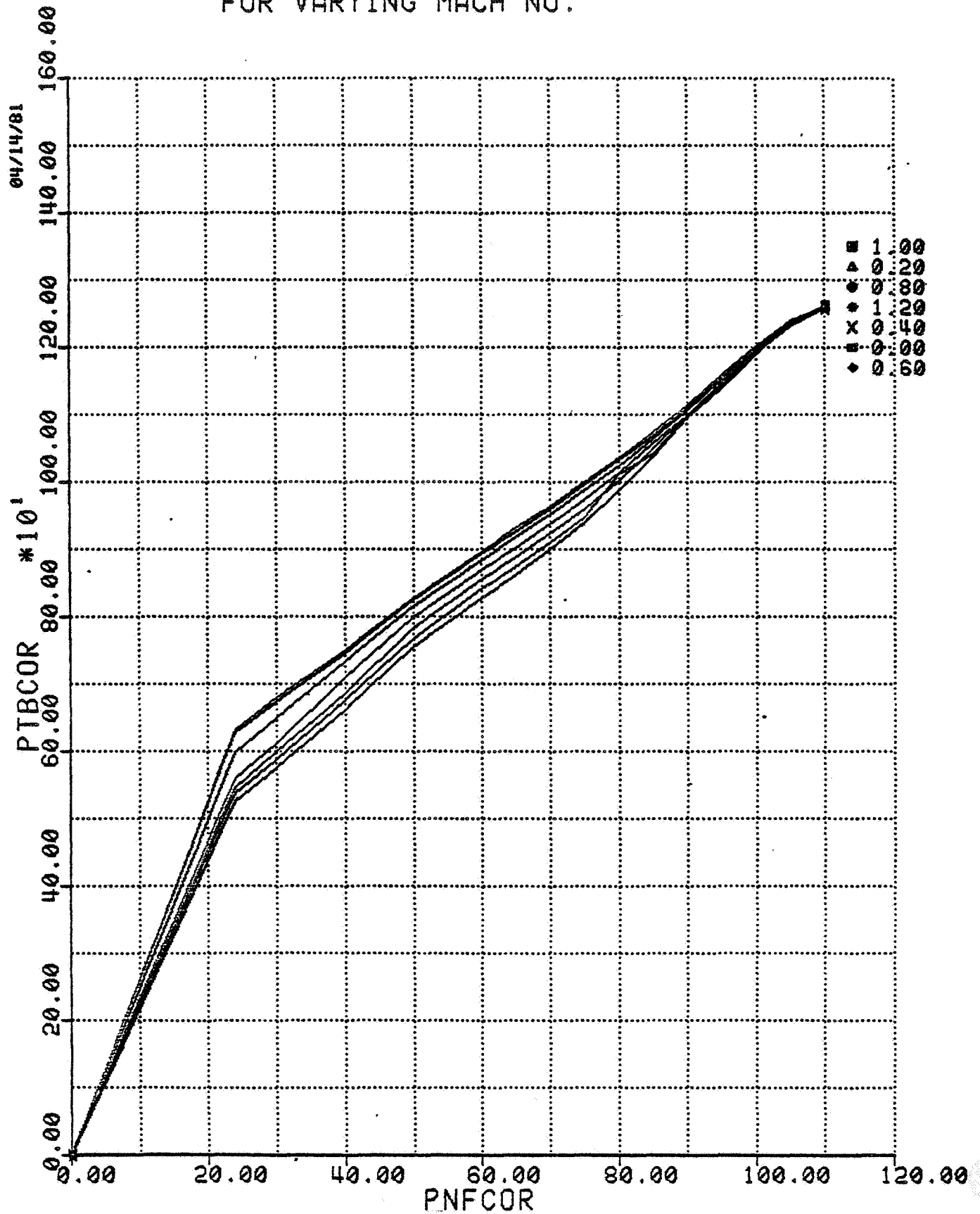
PPHCOR VS PNFCOR
FOR VARYING MACH NO.



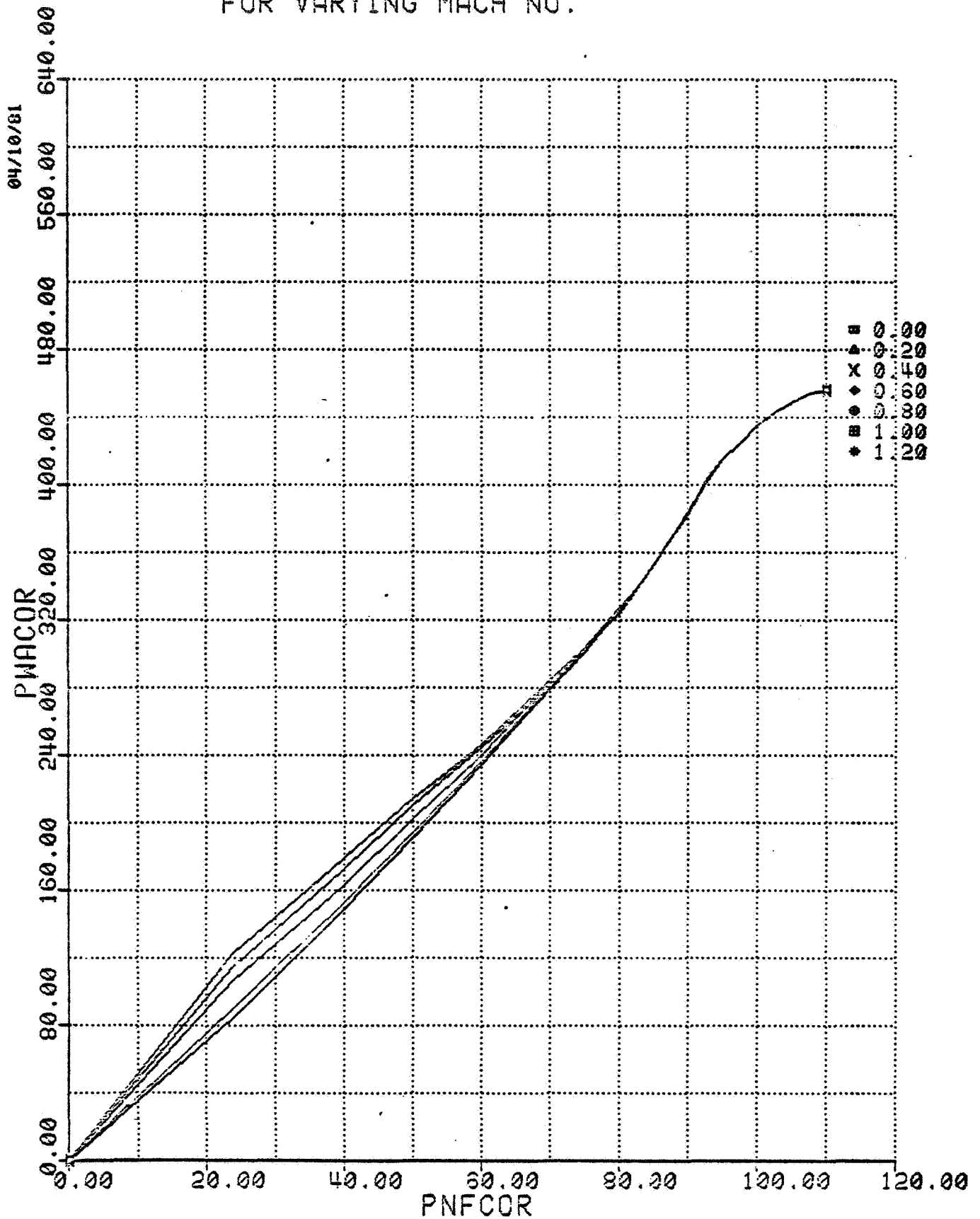
PSDU VS PNFCOR
FOR VARYING MACH NO.



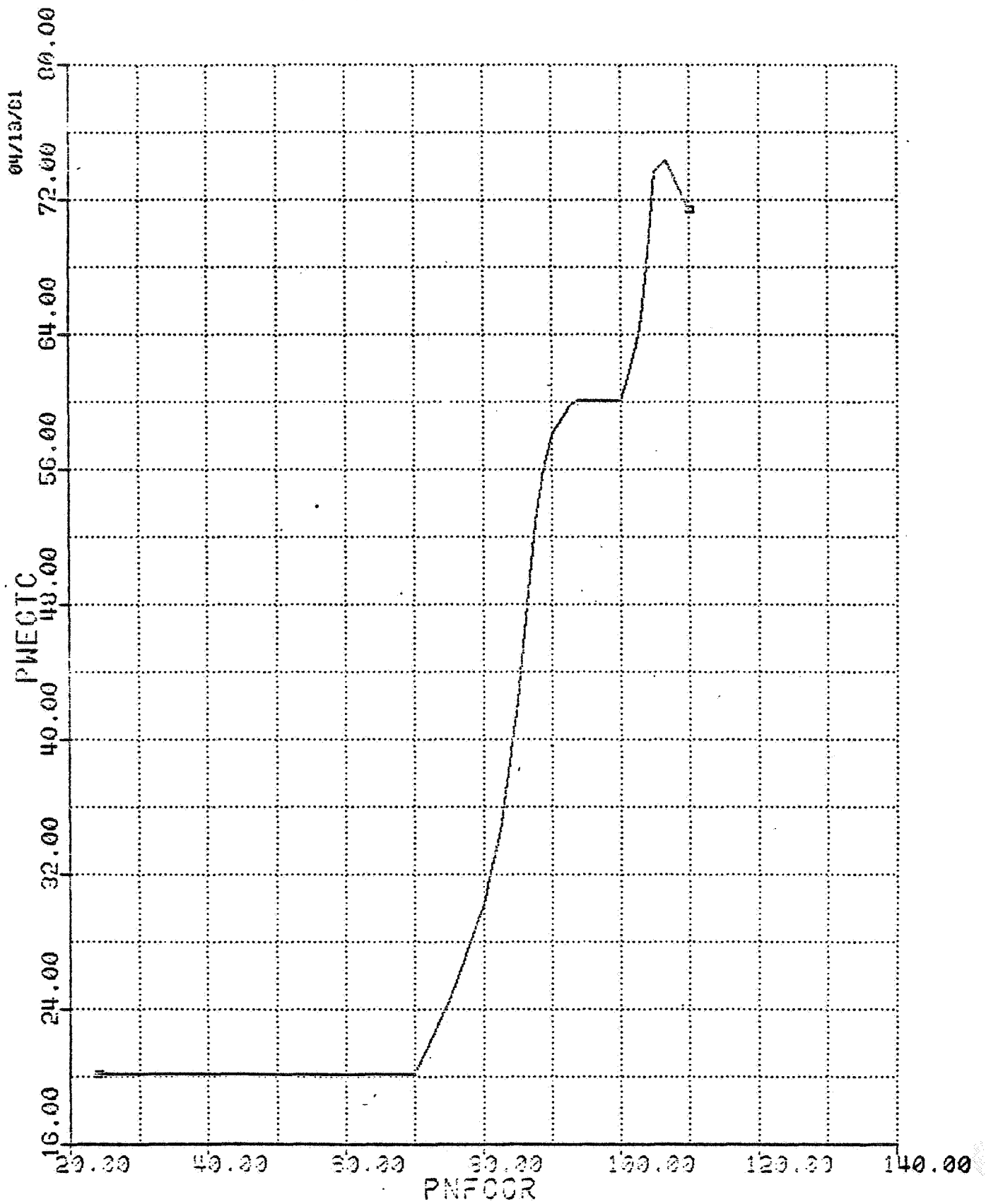
PTBCOR VS PNFCOR
FOR VARYING MACH NO.



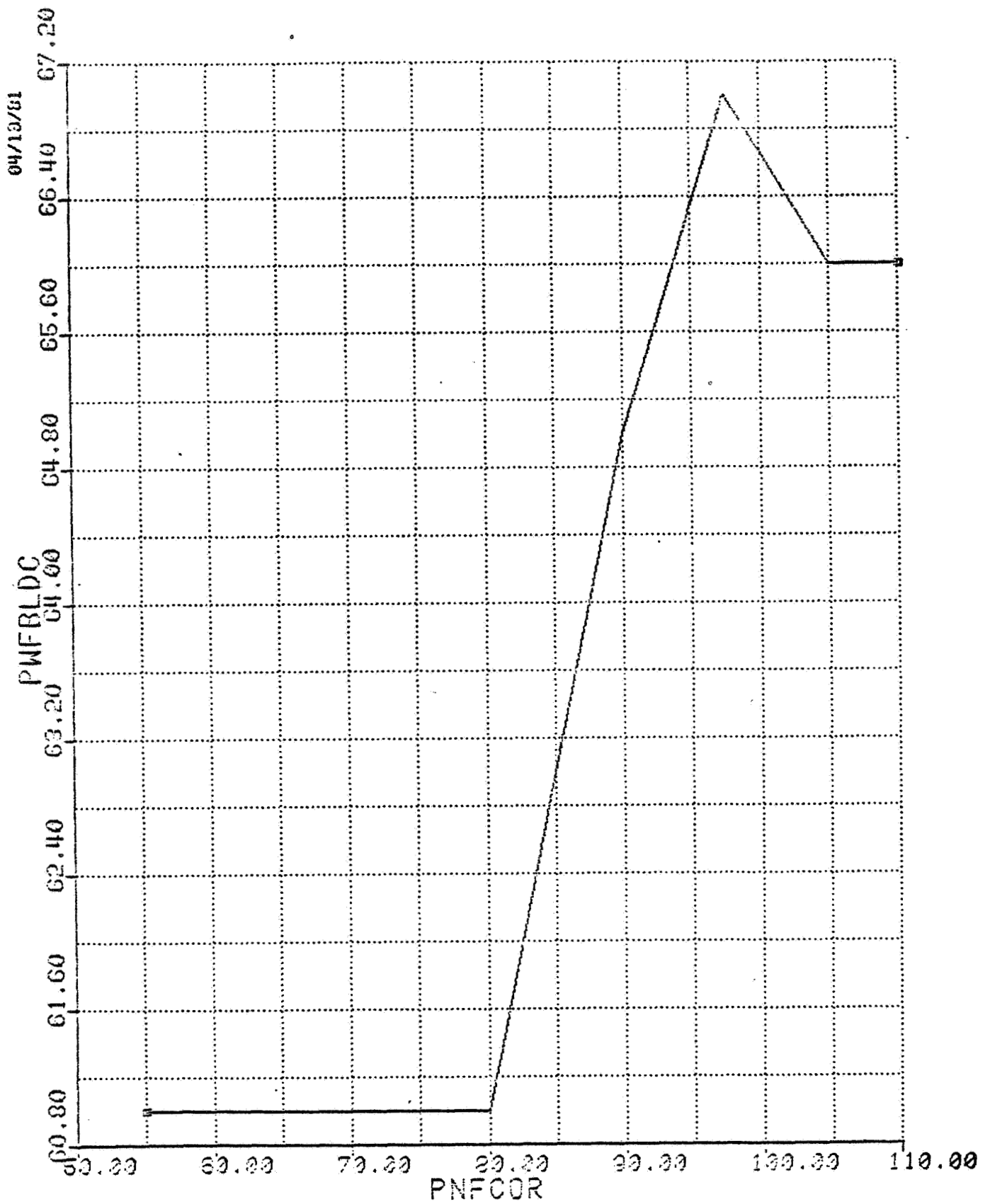
PWACOR VS PNFCOR
FOR VARYING MACH NO.



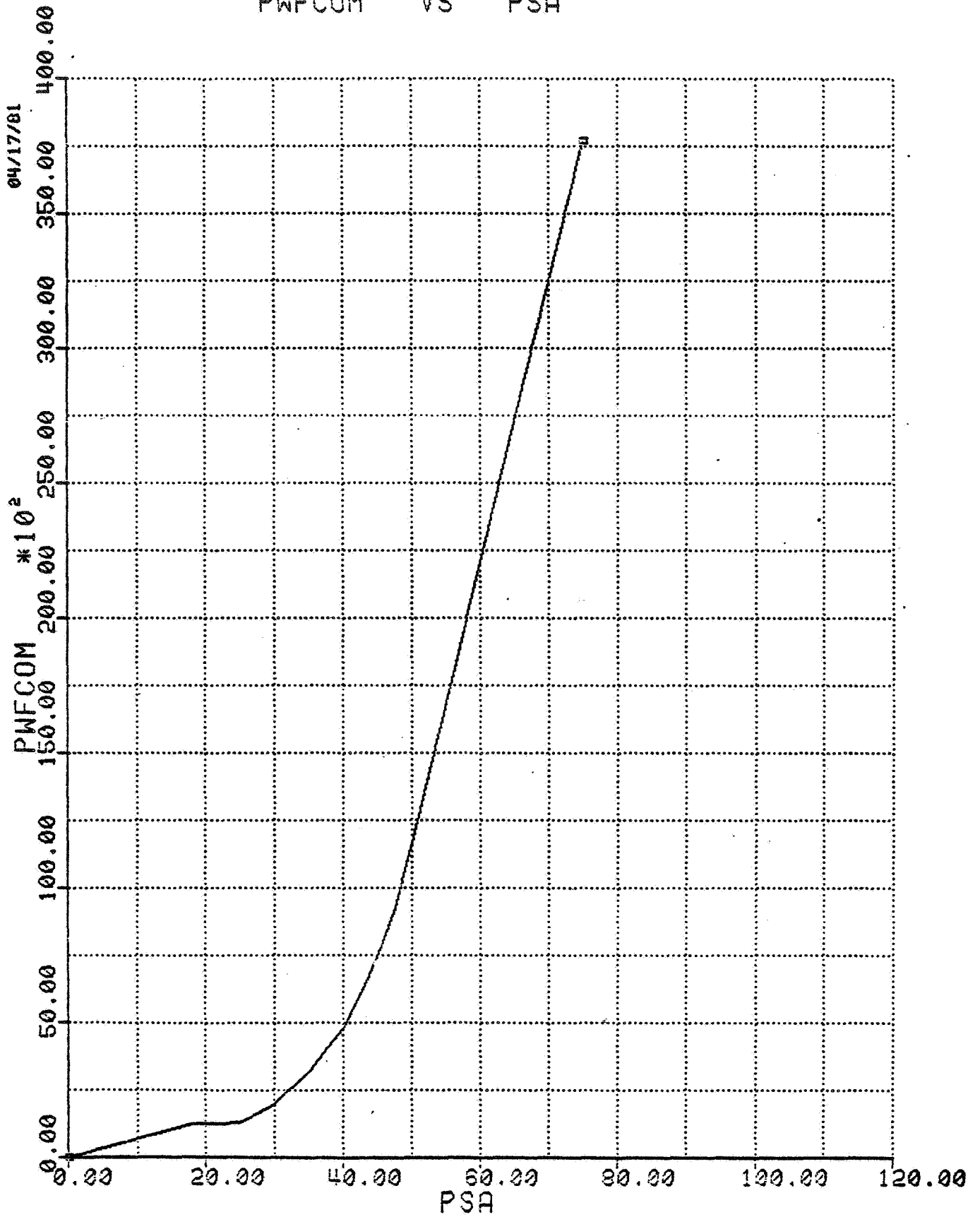
PNEGTC VS PNFCOR



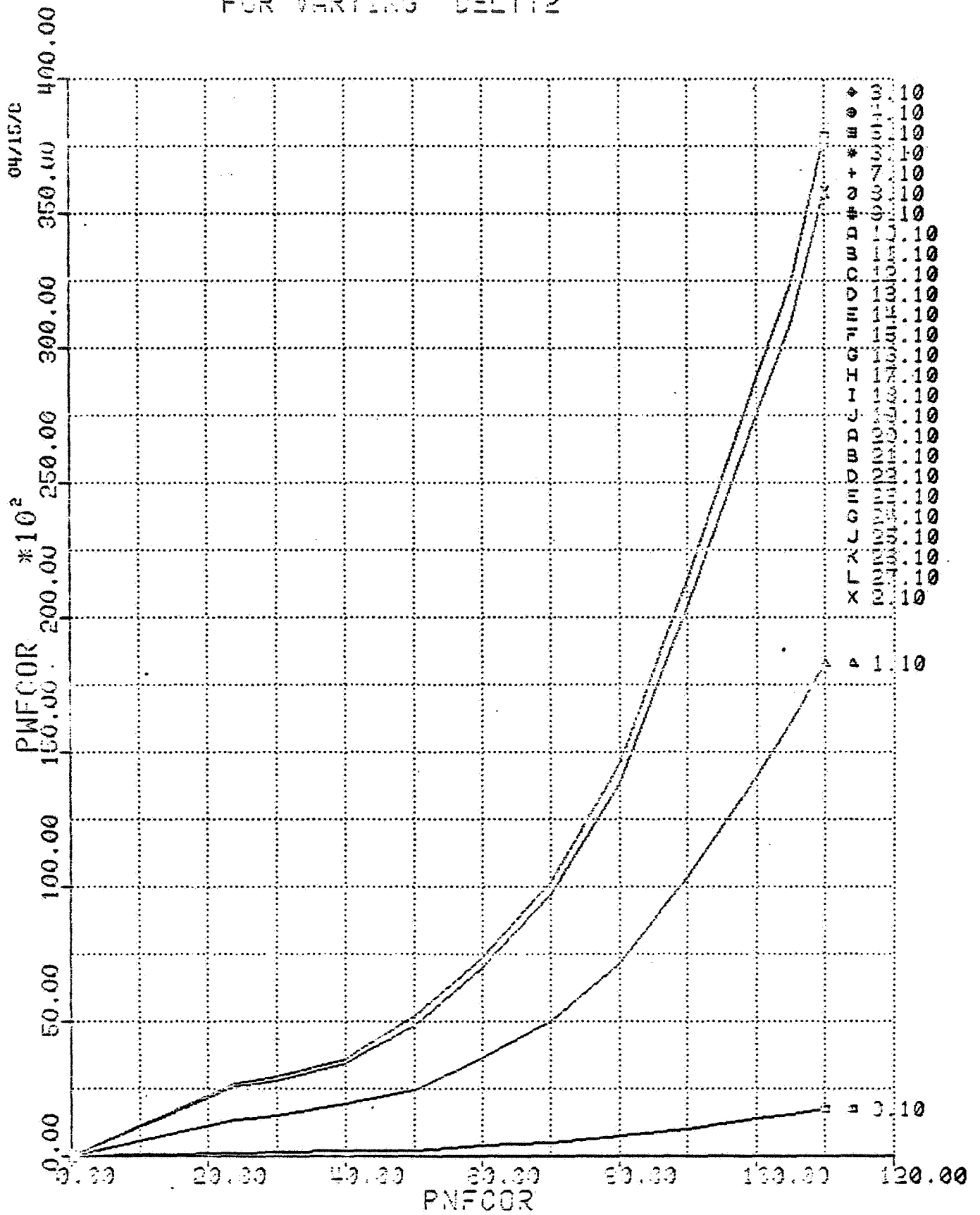
PNFBLDC VS PNFCOR



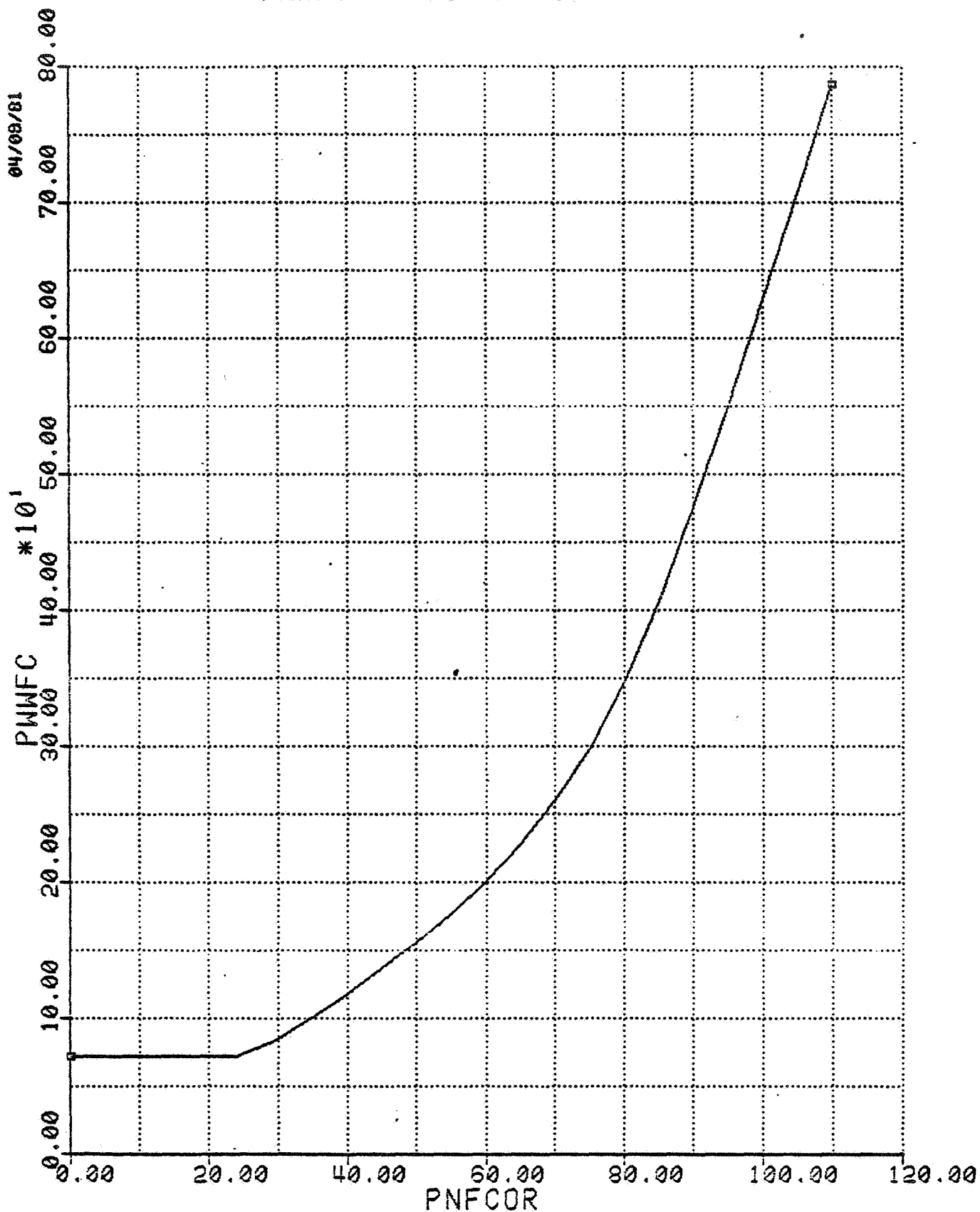
PWFCOM VS PSA



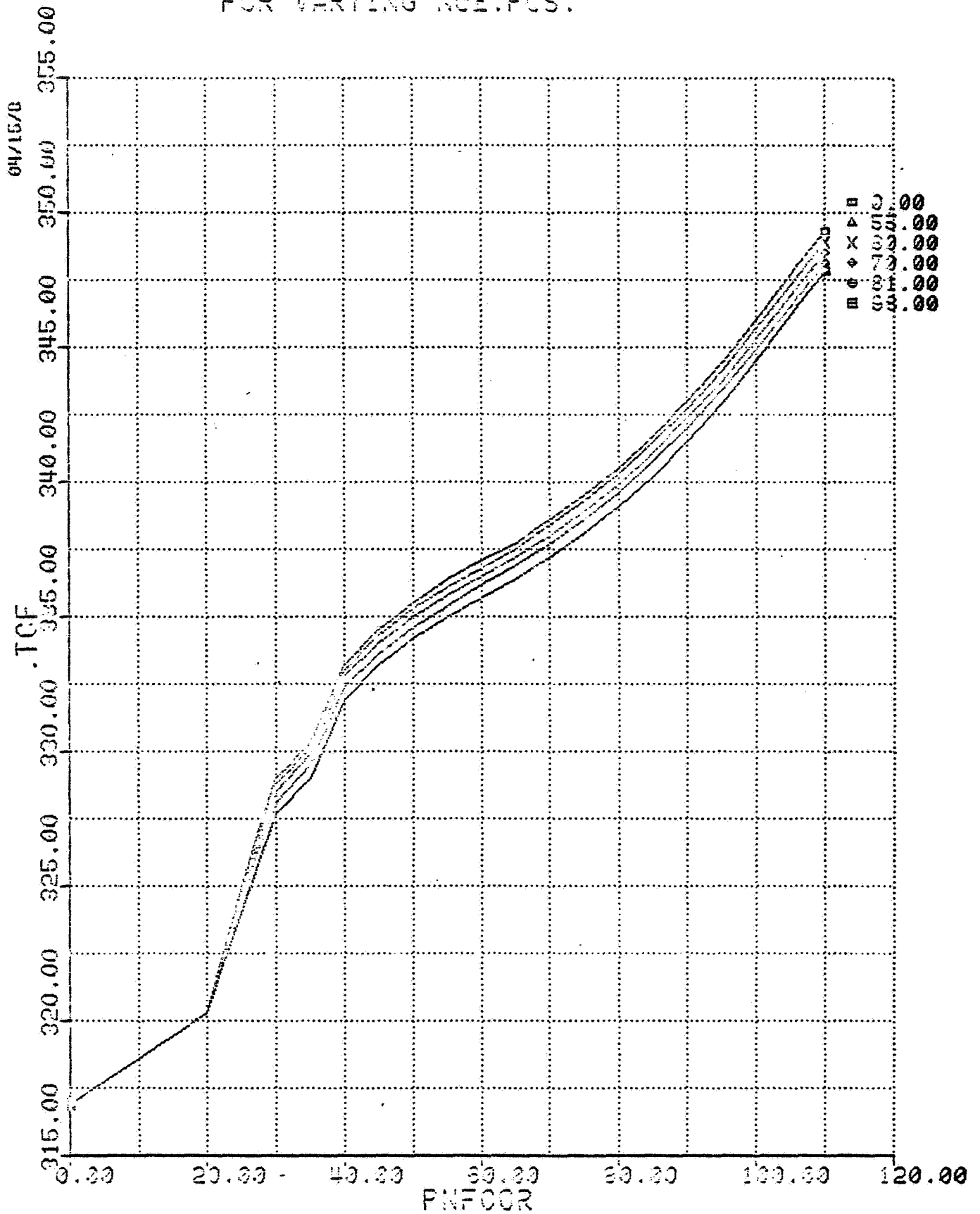
PNFCOR VS PNFCOR
FOR VARYING DELTT2



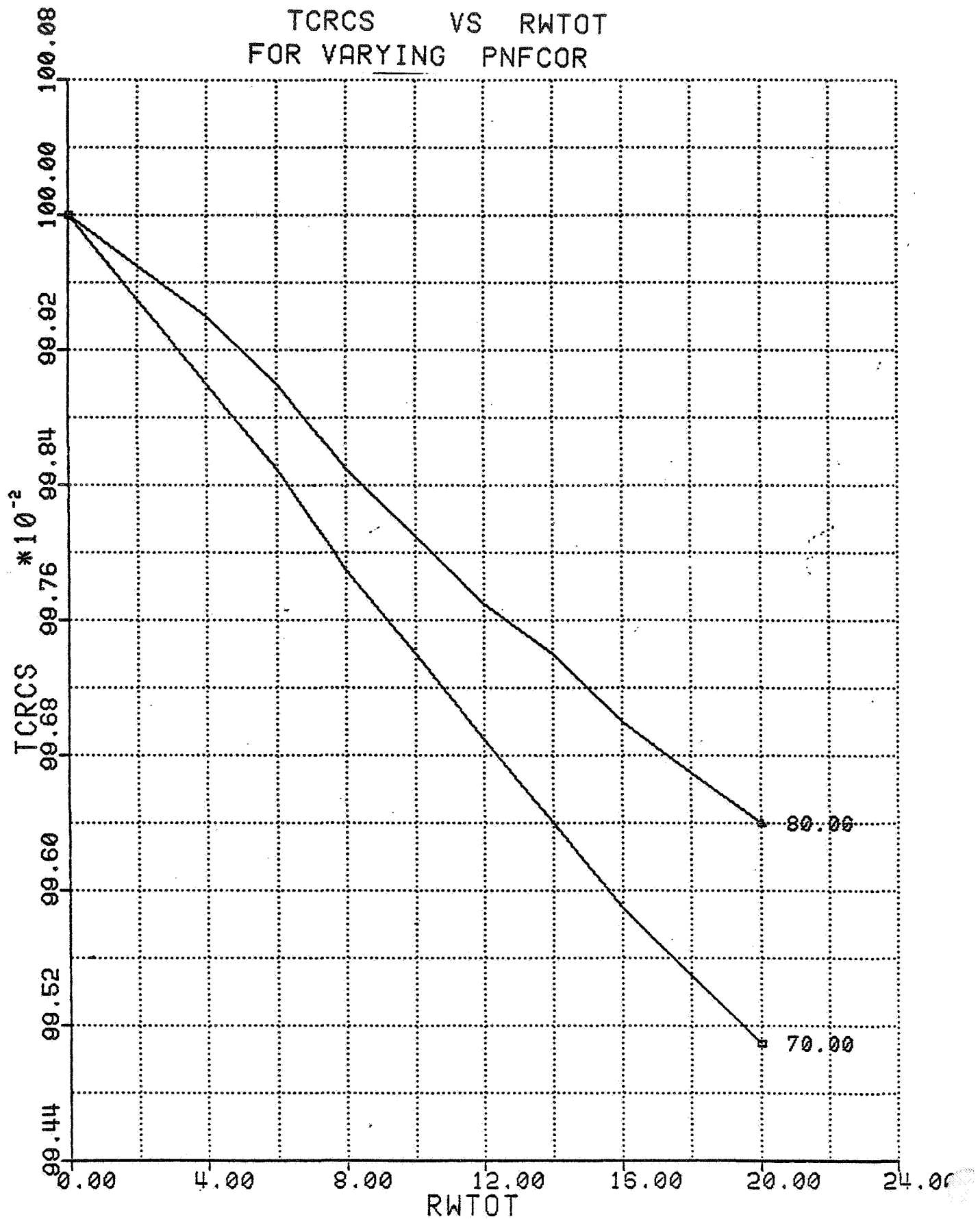
PWWFC VS PNFCOR



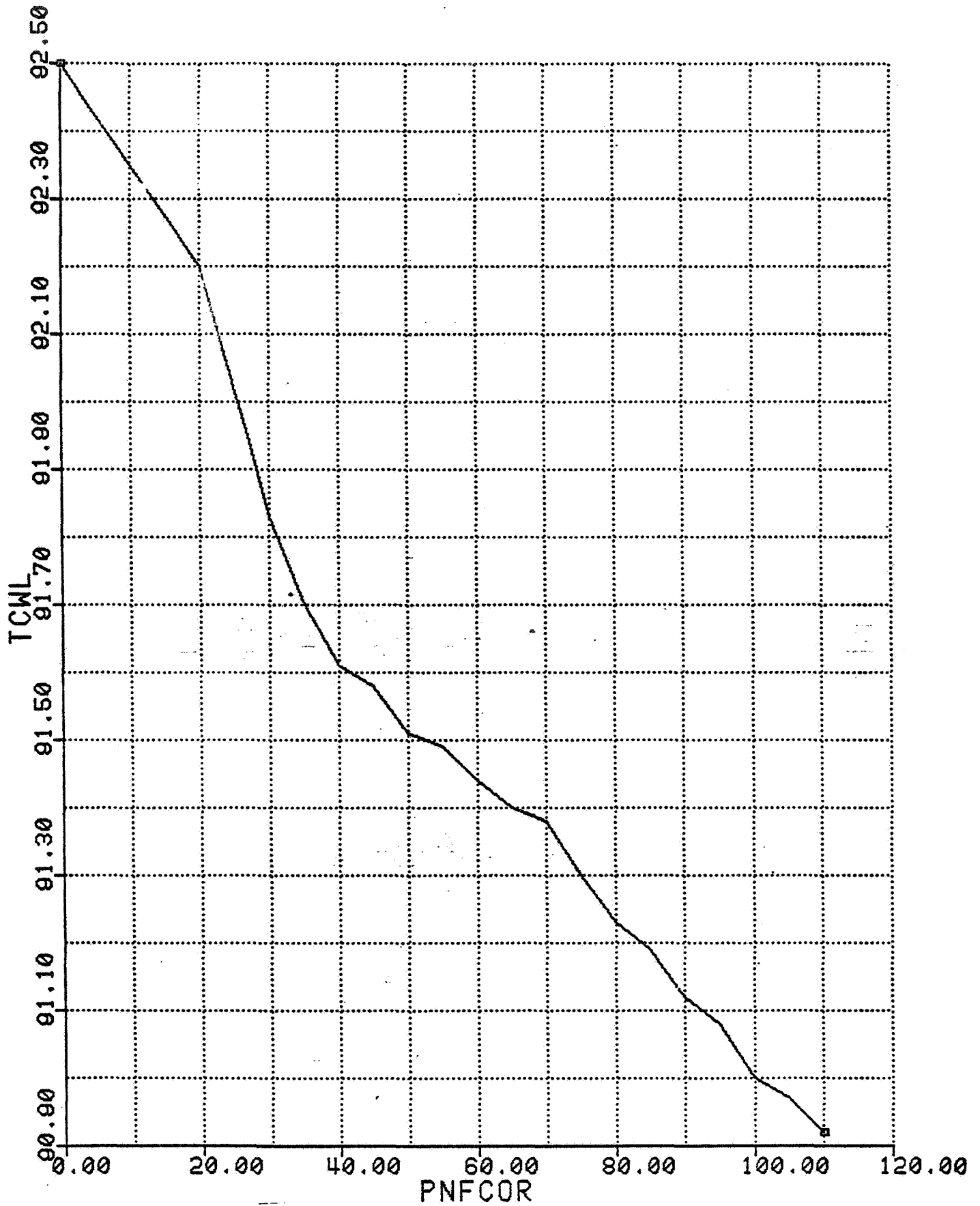
TCF VS PNFCOR
FOR VARYING NOZ.FCS.



TCRCS VS RWTOT
FOR VARYING PNFCOR

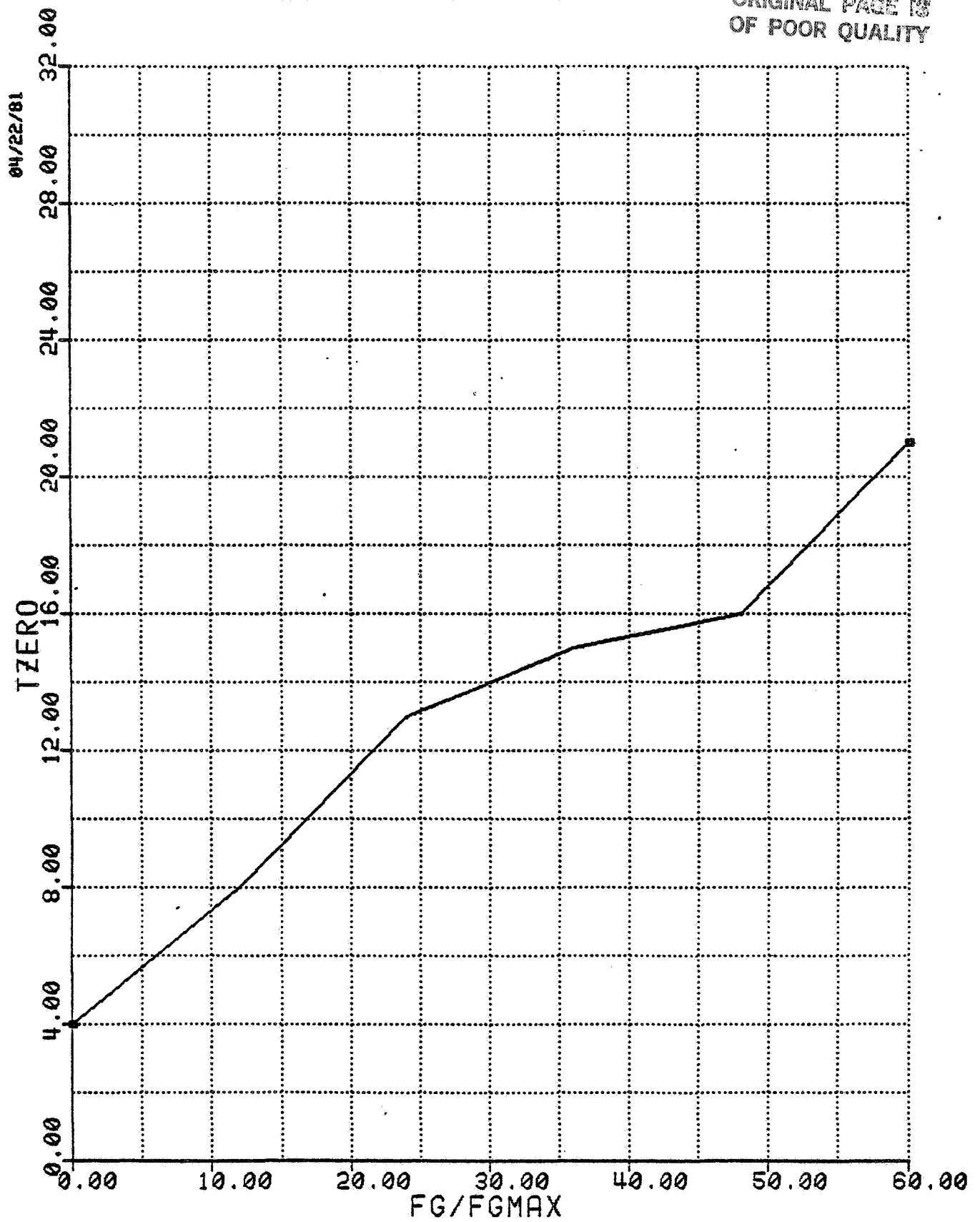


TCWL VS PNFCOR



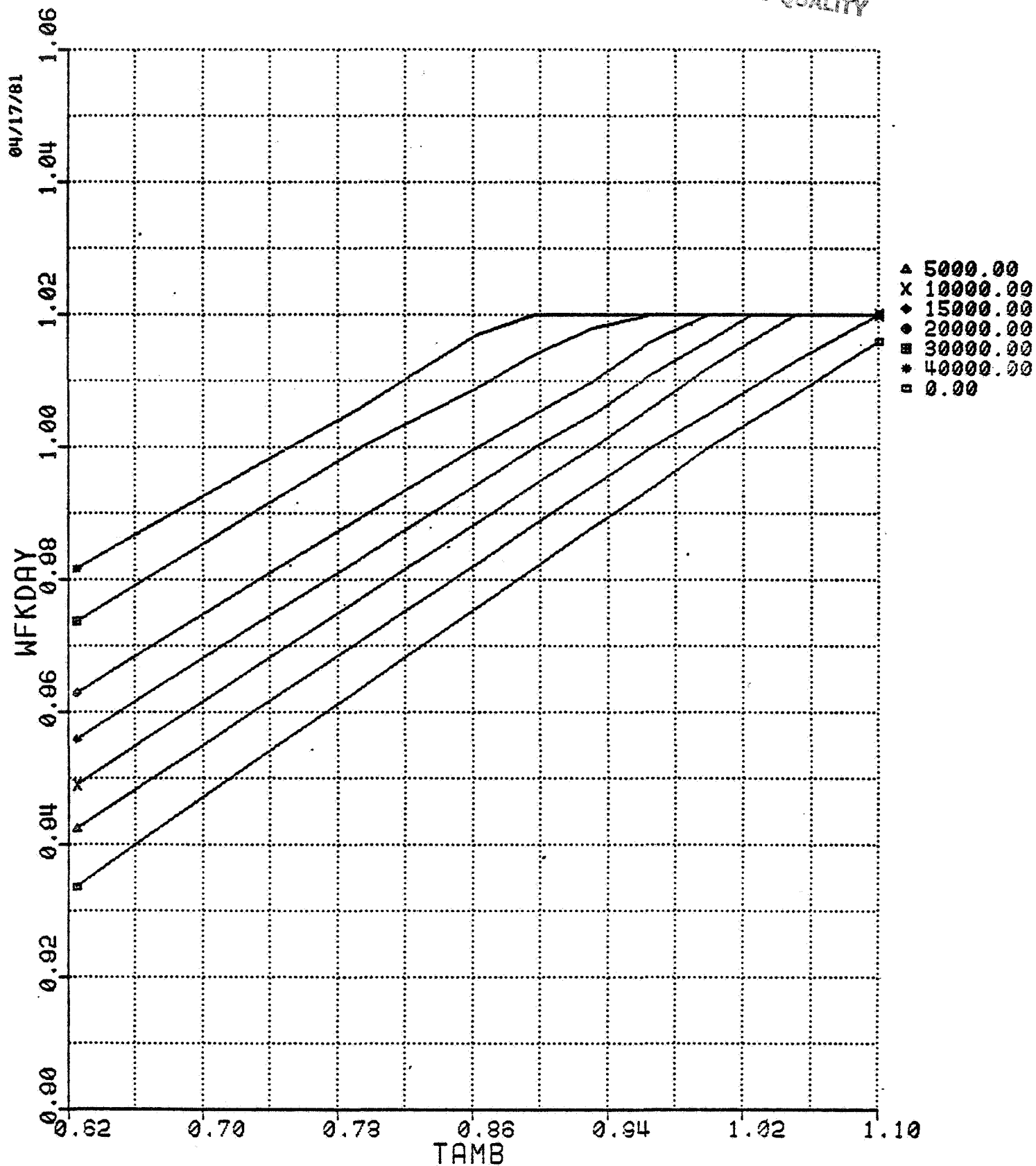
TZERO VS FG/FGMAX

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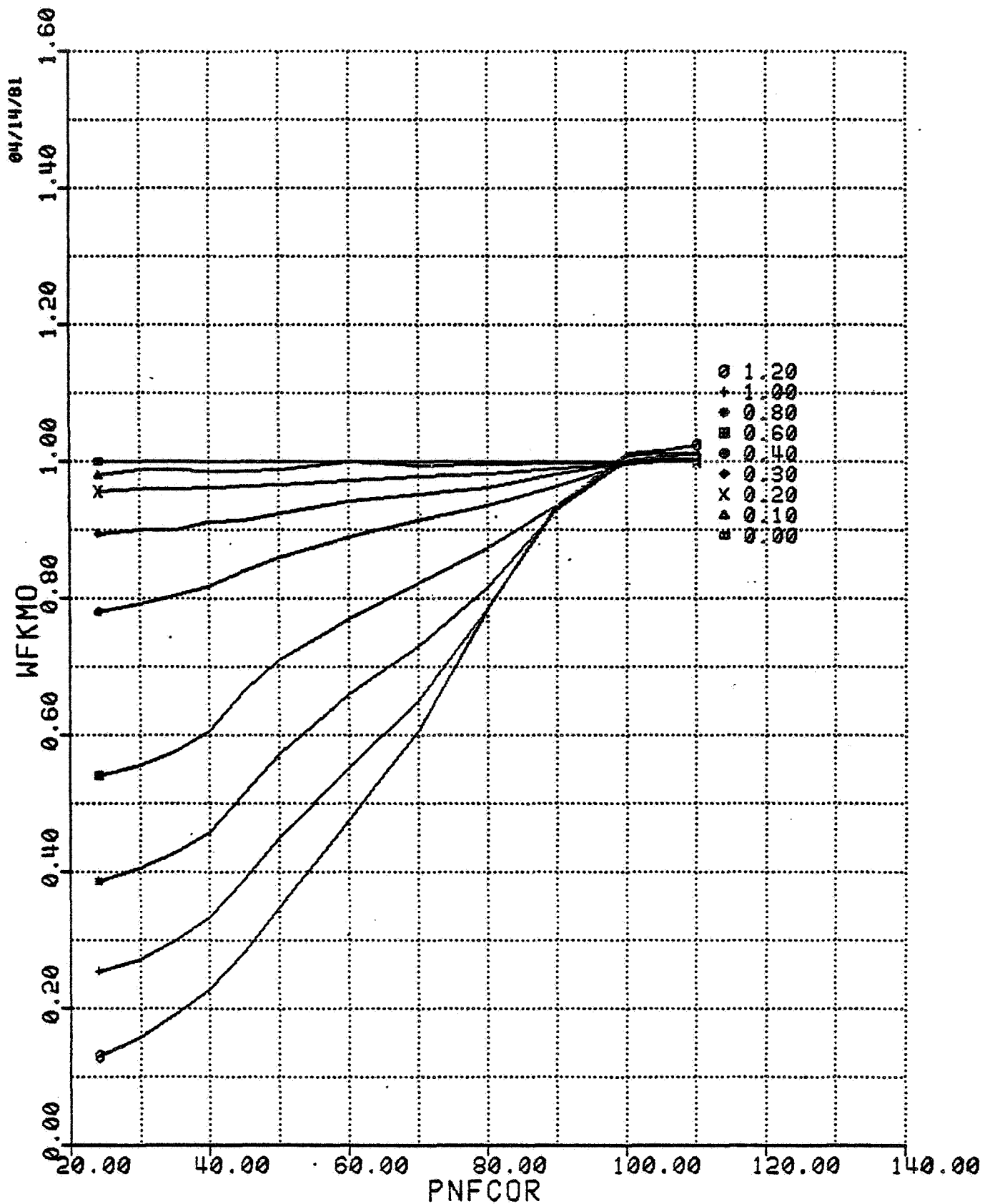


WFKDAY VS TAMB
FOR VARYING ALT

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WFKMO VS PNFCOR
FOR VARYING MACH NO.



INDEX TO LOW SPEED AERODYNAMIC PLOTS

DEPENDENT VARIABLE	DEFINITION	DATA TABLE NAME	PAGE
BETAK06	Side force and yawing moment criteria due to phi break lines as a function of VET, altitude and K factor; nozzles = 60 deg	YMSF60U	C-43
BETAK08	Side force and yawing moment criteria due to phi break lines as a function of VET, altitude, and K factor; nozzles = 81 deg	YMSF81U	C-44
CAAILL	Increment of axial force coefficient due to aileron as a function of aileron deflection and alpha	CAAILT	C-45
CABASE	Baseline axial force coefficient as a function of alpha	CABAS1T	C-46
CABASE2	Baseline axial force coefficient as a function of alpha; high alpha	CABAS2T	C-47
CAFLAPL	Increment of axial force coefficient due to flap as a function of alpha and flap deflection	CAFLAPT	C-48
CAGE55	Increment of axial force coefficient due to ground effects as a function of THALP, altitude and VEQ; nozzles = 55 deg	CAGE55T	C-49
CAGE81	Increment of axial force coefficient due to ground effects as a function of THALP and altitude; nozzle \geq 81 deg	CAGE81T	C-53
CA10	Increment of axial force coefficient due to power effects as a function of alpha, VEQ, and THETAJ = 0, 10 deg	CAPOWT	C-54
CA55	Increment of axial force coefficient due to power effects as a function of alpha, VEQ, and THETAJ = 55 deg	CA55T	C-56
CLLAILL	Increment of rolling moment coefficient due to aileron as a function of alpha and aileron deflection	CLLAILT	C-57
CLLBASE	Rolling moment coefficient due to sideslip angle as a function of alpha and flap deflection	CLLBAST	C-58

INDEX TO LOW SPEED AERODYNAMIC PLOTS (Cont'd)

DEPENDENT VARIABLE	DEFINITION	DATA TABLE NAME	PAGE
CLLP	Rolling moment coefficient due to roll rate as a function of alpha	CLLPT	C-59
CLLPOW	Rolling moment coefficient due to power effects as a function of VEQ and alpha	CLLPOWT	C-60
CLLR	Rolling moment coefficient due to yaw rate as a function of alpha	CLLRT	C-61
CLNAILL	Increment of yawing moment coefficient due to aileron as a function of alpha and aileron deflection	CLNAILT	C-62
CLNBASE	Yawing moment due to sideslip angle as a function of alpha and flap deflection	CLNBAST	C-63
CLNP	Yawing moment coefficient due to roll rate as a function of alpha	CLNPT	C-64
CLNPOW	Yawing moment coefficient due to power effects as a function of VEQ and alpha	CLNPOWT	C-65
CLNR	Yawing moment coefficient due to yaw rate as a function of alpha	CLNRT	C-66
CMAILL	Increment of pitching moment coefficient due to aileron as a function of aileron deflection and alpha	CMAILT	C-67
CMBASE	Baseline pitching moment coefficient as a function of alpha	CMBAS1T	C-68
CMBASE2	Baseline pitching moment coefficient as a function of alpha; high alpha	CMBAS2T	C-69
CMFLAL	Increment of pitching moment coefficient as a function of ALPC, flap deflection, and THETAJ	CMFLAPT	C-70
CMGE55	Increment of pitching moment coefficient due to ground effects as a function of THALP, altitude, and VEQ; nozzles = 55 deg	CMGE55T	C-71

INDEX TO LOW SPEED AERODYNAMIC PLOTS (Cont'd)

DEPENDENT VARIABLE	DEFINITION	DATA TABLE NAME	PAGE
CMGE81	Increment of pitching moment coefficient due to ground effects as a function of THALP and altitude; nozzles ≥ 81 deg	CMGE81T	C-75
CMJ25	Increment of pitching moment coefficient due to flap-jet impingement as a function of VEQ, alpha, and THETAJ; flaps ≤ 25 deg	CMFJIT	C-76
CMJ45	Increment of pitching moment coefficient due to flap-jet impingement as a function of THETAJ; flaps < 61 deg	CMFJI1T	C-78
CMJ62	Increment of pitching moment coefficient due to flap-jet impingement as a function of THETAJ; flaps ≥ 61.7 deg	CMFJI2T	C-79
CMTUP	Increment of pitching moment coefficient due to stabilator as a function of ALPT, alpha, and VEQ; flaps = 0 deg	DCMUPT	C-80
CMT25	Increment of pitching moment coefficient due to stabilator as a function of ALPT; 25 deg flaps	DCM25T	C-82
CMT62	Increment of pitching moment coefficient due to stabilator as a function of ALPT, and VEQ; 61.7 deg flaps	DCM62T	C-83
CNAILL	Increment of normal force coefficient due to aileron as a function of aileron deflection and alpha	CNAILT	C-84
CNBASE	Baseline normal force coefficient as a function of alpha	CNBAS1T	C-85
CNBASE2	Baseline normal force coefficient as a function of alpha; high alpha	CNBAS2T	C-86
CNFLAPL	Increment of normal force coefficient due to flaps as a function of ALPC, flap deflection, and THETAJ	CNFLAPT	C-87
CNGE55	Increment of normal force coefficient due to ground effects as a function of THALP, altitude, and VEQ; nozzles = 55 deg	CNGE55T	C-90

INDEX TO LOW SPEED AERODYNAMIC PLOTS (Cont'd)

DEPENDENT VARIABLE	DEFINITION	DATA TABLE NAME	PAGE
CNGE81	Increment of normal force coefficient due to ground effects as a function of THALP and altitude; nozzles ≥ 81 deg	CNGE81T	C-91
CYAILL	Increment of side force coefficient due to aileron as a function of alpha and aileron deflection	CYAILT	C-92
CYBASE	Side force coefficient due to side-slip angle as a function of alpha and flap deflection	CYBAST	C-93
CYPOW	Increment of side force coefficient due to power effects as a function of VEQ and alpha	CYPOWT	C-94
DALPC	Delta correction to flap AOA as a function of THETAJ and VEQ	ALPCT	C-95
DCA	Delta correction to axial force coefficient due to flaps as a function of VEQ	DCAT	C-96
DCAJ25	Increment of axial force coefficient due to flap-jet interference as a function of VEQ, flaps ≤ 25 deg	CAFJIT	C-97
DCAJ45	Increment of axial force coefficient due to flap-jet interference as a function of THETAJ, flaps < 61 deg	CAFJ11T	C-98
DCAJ62	Increment of axial force coefficient due to flap-jet interference as a function of THETAJ, flaps ≥ 61.7 deg	CAFJ12T	C-99
DCA50	Increment of axial force coefficient due to ground effects as a function of THALP and altitude; nozzle = 50 deg	DCA50T	C-100
DCA60	Increment of axial force coefficient due to ground effects as a function of THALP and altitude; nozzle = 60 deg	DCA60T	C-101

INDEX TO LOW SPEED AERODYNAMIC PLOTS (Cont'd)

DEPENDENT VARIABLE	DEFINITION	DATA TABLE NAME	PAGE
DCLNHI	Yawing moment coefficient due to sideslip angle as a function of alpha for high beta	DCLNHIT	C-102
DCMFJI	Increment to CMJ25 as a function of alpha	DCMFJIT	C-103
DCML	Increment of pitching moment coefficient due to flaps as a function of alpha, VEQ, and flap deflection	DCMT	C-104
DCMPOW	Increment of pitching moment coefficient due to power effects as a function of alpha, VEQ, and THETAJ	DCMPOWT	C-107
DCM10	Increment of pitching moment coefficient due to ground effects as a function of THALP, altitude, and VET; nozzles = 10 deg	DCM10T	C-116
DCM50	Increment of pitching moment coefficient due to ground effects as a function of THALP and altitude; nozzle = 50 deg	DCM50T	C-118
DCM60	Increment of pitching moment coefficient due to ground effects as a function of THALP and altitude; nozzle = 60 deg	DCM60T	C-119
DCNJ25	Increment of normal force coefficient due to flap-jet interference as a function of ALPC and VEQ, flaps \leq 25 deg	CNFJIT	C-120
DCNJ45	Increment of normal force coefficient due to flap-jet interference as a function of THETAJ; flaps < 61 deg	CNFJI1T	C-121
DCNJ62	Increment of normal force coefficient due to flap-jet interference as a function of THETAJ; flaps \geq 61.7 deg	CNFJI2T	C-122
DCNPOT	Increment of normal force coefficient due to power effects as a function of THETAJ and alpha; VEQ < .05	DCNPOWT	C-123

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INDEX TO LOW SPEED AERODYNAMIC PLOTS (Cont'd)

DEPENDENT VARIABLE	DEFINITION	DATA TABLE NAME	PAGE
DCNPOW	Increment of normal force coefficient due to power effects as a function of THETAJ, VEQ, and alpha; $VEQ \geq .05$	CNPOWT	C-124
DCN50	Increment of normal force coefficient due to ground effects as a function of THALP and altitude; nozzle = 50 deg	DCN50T	C-132
DCN60	Increment of normal force coefficient due to ground effects and altitude; nozzle = 60 deg	DCN60T	C-133
DCYHI	Side force coefficient due to side-slip angle as a function of alpha for high beta	DCYHIT	C-134
DRMB81	Increment to DRMP81 as a function of ABETAP, altitude, and VET; nozzle = 81 deg	DRMB81U	C-135
DRMP60	Phi bias to rolling moment as a function of phi, beta, and altitude; nozzle = 0 to 60 deg	DRMP60U	C-137
DRMP81	Phi bias to rolling moment as a function of phi and beta, altitude, and VET	DRMP81U	C-141
DSFT	Side force out of ground effects as a function of THALP, THETAJ, and VEQ	DSFTU	C-144
EPS1	Downwash angle for flaps $< 25^\circ$, as a function of alpha and VEQ	EPS1T	C-149
EPS2	Downwash angle for flaps $\geq 25^\circ$, as a function of alpha, VEQ, and flap deflection	EPS2T	C-150
PBSF60	Phi bias to side force as a function of ABETAP, altitude, and VET; nozzles = 60 deg	PBSF60U	C-152
PBSF81	Phi Bias to side force as a function of ABETAP, altitude, and VET; nozzles = 81 deg	PBSF81U	C-154

INDEX TO LOW SPEED AERODYNAMIC PLOTS (Cont'd)

DEPENDENT VARIABLE	DEFINITION	DATA TABLE NAME	PAGE
PBYM60	Phi bias to yawing moment as a function of ABETAP, altitude, and VET; nozzles = 60 deg	PBYM60U	C-156
PBYM81	Phi bias to yawing moment as a function of ABETAP, altitude, and VET; nozzles = 81 deg	PBYM81U	C-158
RC	Correction factor to pitching moment coefficient as a function of alpha and VEQ	RCT	C-160
RCA	K Factor for delta correction to axial force coefficient as a function of VEQ	RCAT	C-161
RK	Correction factor to pitching moment coefficient due to stabilator for zero deg. flaps	RKT	C-162
RKO	Ground effect on longitudinal control power as a function of THALP	RKOT	C-162.1
RMBE00	Rolling moment out of ground effects as a function of THALP and VEQ; nozzles = 0 deg	RMBE00U	C-163
RMBE60	Rolling moment out of ground effects as a function of THALP and VEQ; nozzles = 60 deg	RMBE60U	C-164
RMBE81	Increment of rolling moment out of ground effects as a function of ABETAP, THALP, and VEQ; nozzles = 81 deg, VEQ = .025	RMBE81U	C-165
RMBE96	Increment of rolling moment out of ground effects as a function of ABETAP and THALP; nozzles = 81 deg, VEQ = .096	RMBE96U	C-168
RMGE00	Rolling moment in ground effects as a function of THALP, altitude, and VET; nozzles = 0 deg	RMGE00U	C-169
RMPB81	Lookup term for DRMP81 as a function of ABETAP, altitude, and VET; nozzles = 81 deg	RMPB81U	C-171

INDEX TO LOW SPEED AERODYNAMIC PLOTS (Cont'd)

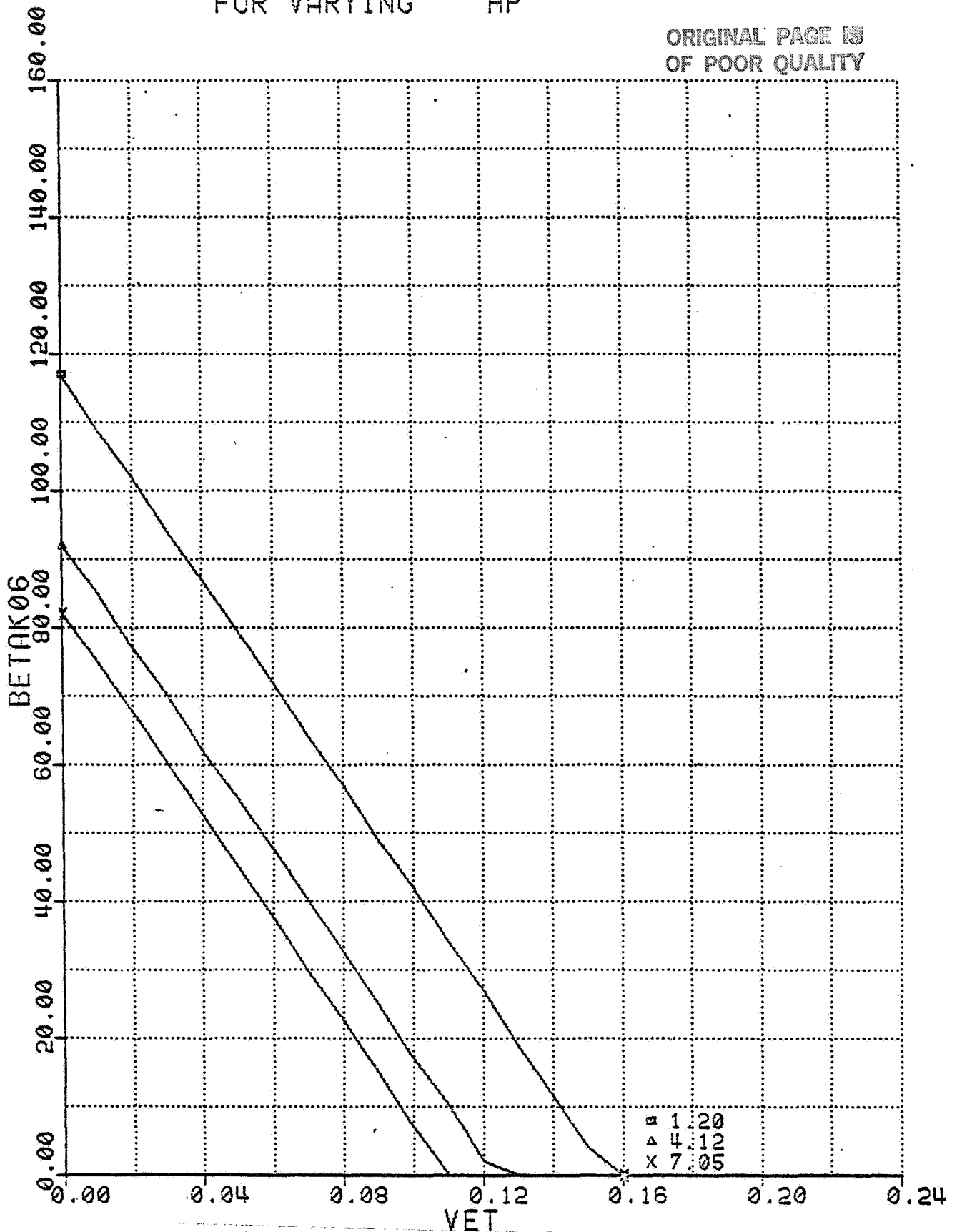
DEPENDENT VARIABLE	DEFINITION	DATA TABLE NAME	PAGE
RM1P2	Rolling moment in ground effects as a function of ABETAP, THALP, and VET; nozzles = 81; altitude = 1.2 feet	RMAT81U	C-174
RM2P47	Increment of rolling moment out of ground effects as a function of ABETAP and THALP; nozzles = 81, VEQ = .247	RM2P47U	C-177
RM4P12	Rolling moment in ground effects as a function of ABETAP, THALP, and VET; nozzles = 81, altitude = 4.12 feet	RM4P12U	C-178
RM7P05	Rolling moment in ground effects as a function of ABETAP, THALP, and VET; nozzles = 81; altitude = 7.05 feet	RM7P05U	C-181
SFGE60	Side Force in ground effects as a function of THALP and altitude; nozzles = 60 deg	SGFE60U	C-184
SFGE81	Side Force in ground effects as a function of THALP, altitude and VET; nozzles = 81 deg	SFGE81U	C-185
SFTB60	Bias to side force as a function of BETAP, altitude, and VET; nozzles = 60 deg	SFTB60U	C-189
SFTB81	Bias to side force as a function of ABETAP, altitude and VET; nozzles = 81 deg	SFTB81U	C-191
SFTP60	Phi bias to side force as a function of YPHIE, altitude and VET; nozzles = 60 deg	SFTP60U	C-195
SFTP81	Phi bias to side force as a function of YPHIE, altitude, and VET; nozzles = 81 deg	SFTP81U	C-197

INDEX TO LOW SPEED AERODYNAMIC PLOTS (Cont'd)

DEPENDENT VARIABLE	DEFINITION	DATA TABLE NAME	PAGE
YMBS60	Bias to yawing moment as a function of ABETAP, altitude, and VET; nozzles = 60 deg	YMBS60U	C-202
YMBS81	Bias to yawing moment as a function of ABETAP, altitude, and VET; nozzles = 81 deg	YMBS81U	C-204
YMGE60	Yawing moment in ground effects as a function of THALP and altitude; nozzles = 60 deg	YMGE60U	C-208
YMGE81	Yawing moment in ground effects as a function of THALP, altitude, and VET; nozzles = 81 deg	YMGE81U	C-209
YMPE60	Phi bias to yawing moment as a function of YPHIE, altitude, and VET; nozzles = 60 deg	YMPE60U	C-213
YMPE81	Phi Bias to yawing moment as a function of YPHIE, altitude, and VET; nozzles = 81 deg	YMPE81U	C-215
YMTB00	Yawing moment out of ground effects as a function of THALP and VEQ; nozzles = 0 deg	YMTB00U	C-220
YMTB60	Yawing moment out of ground effects as a function of THALP and VEQ; nozzles = 60 deg	YMTB60U	C-221
YMTB81	Yawing moment out of ground effects as a function of THALP and VEQ; nozzles = 81 deg	YMTB81U	C-222

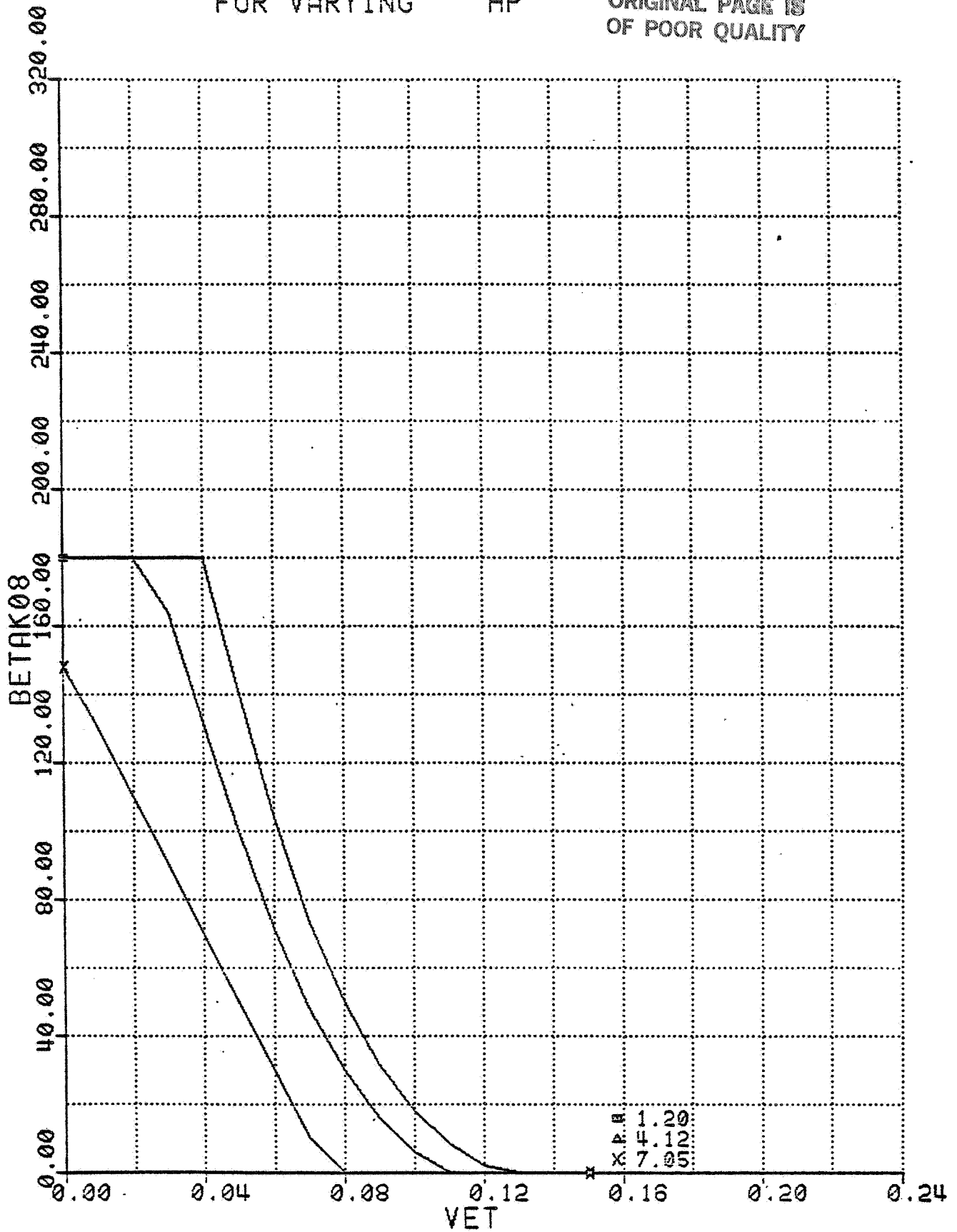
BETAK06 VS VET
FOR VARYING HP

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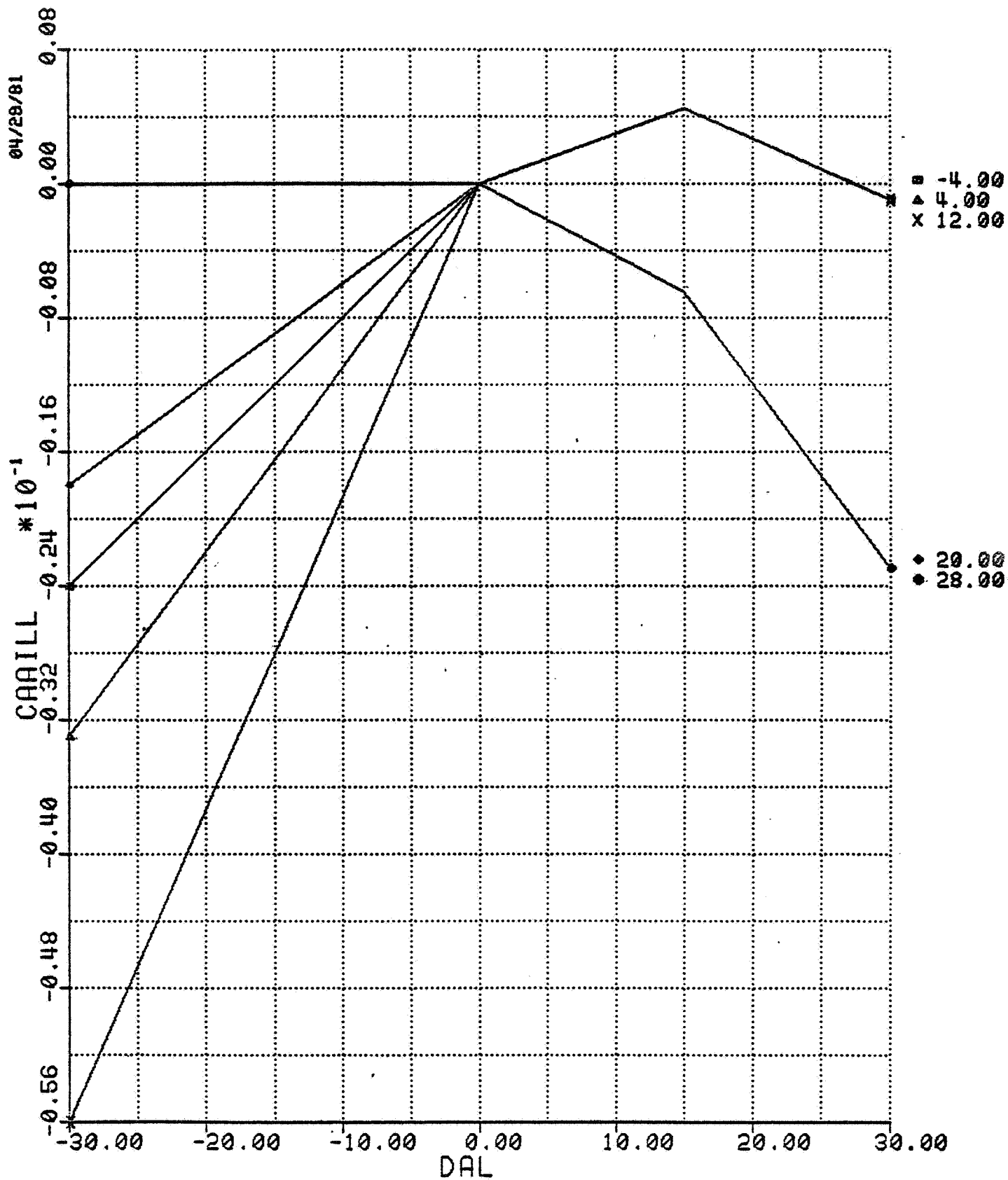
BETAK08 VS VET
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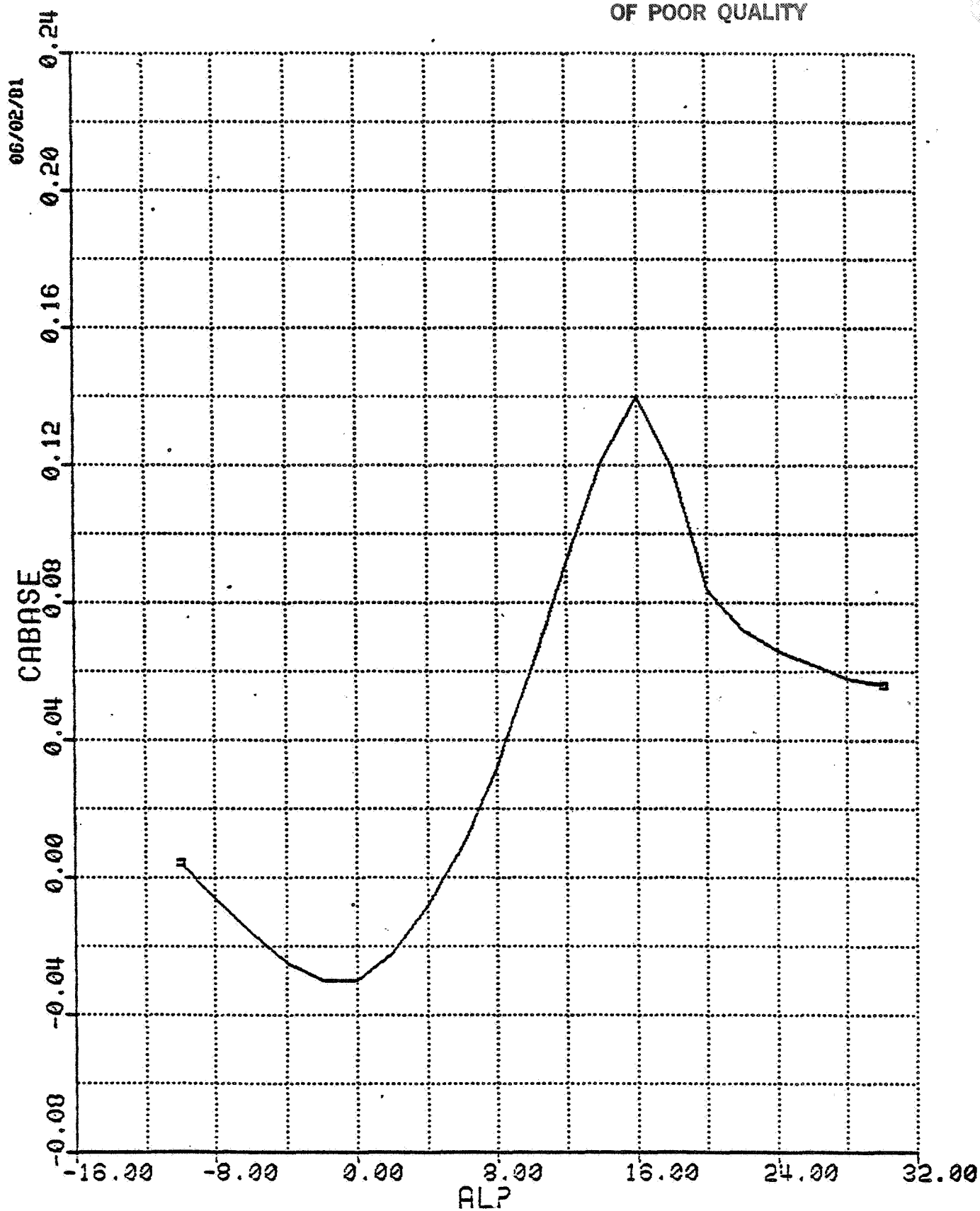
CRAILL VS DAL
FOR VARYING ALPHA

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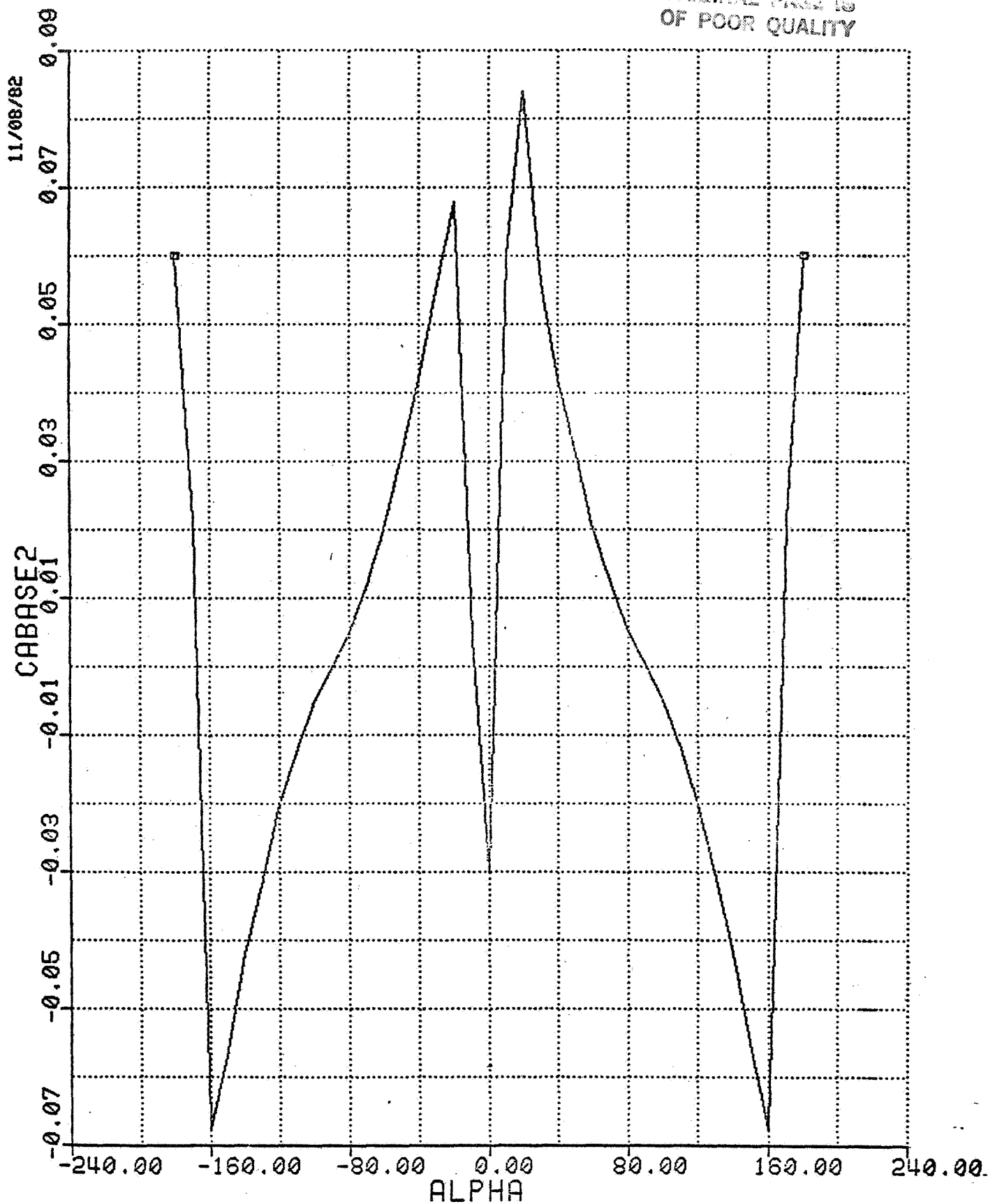
CABASE VS ALP

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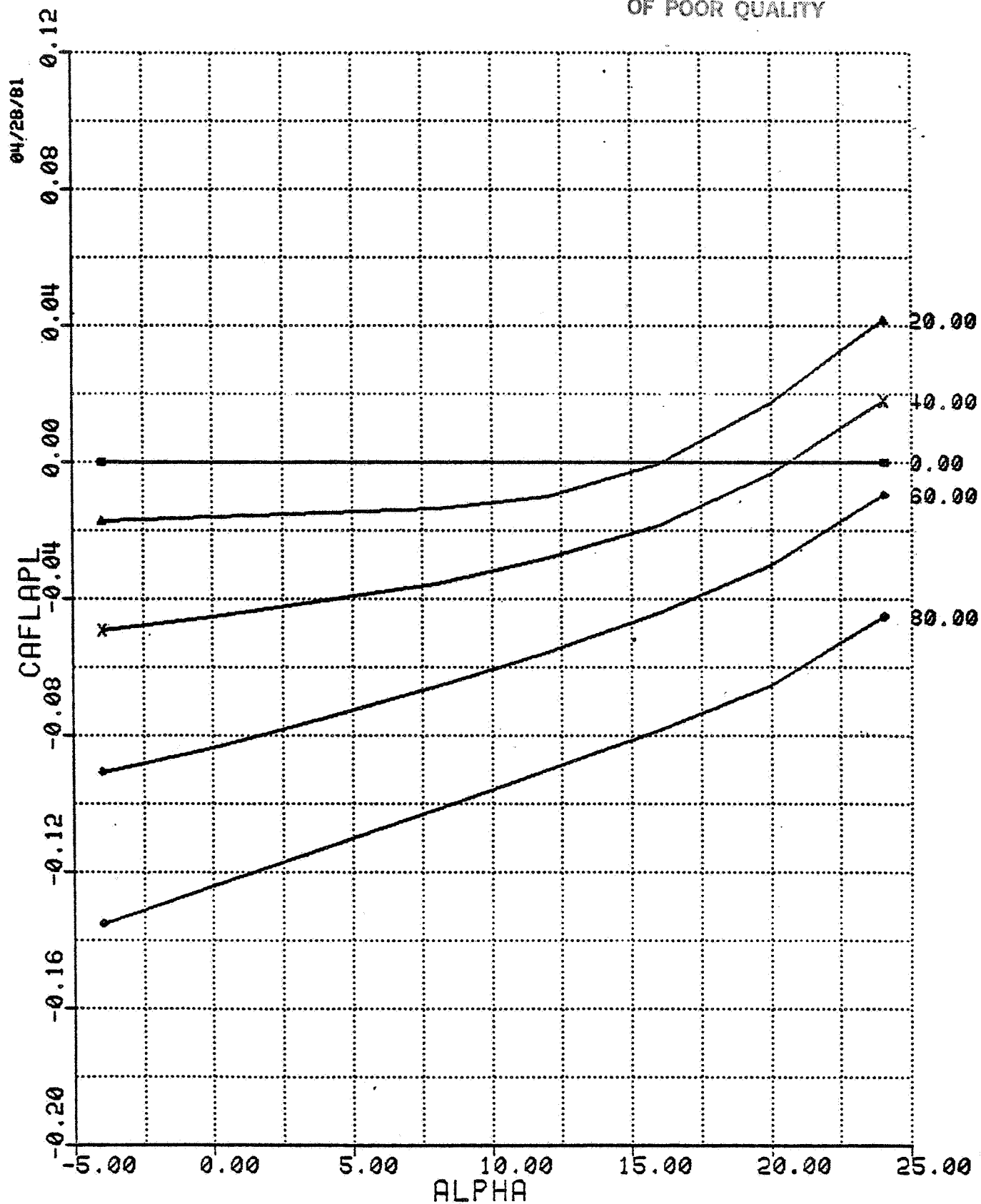
CABASE2 VS ALPHA

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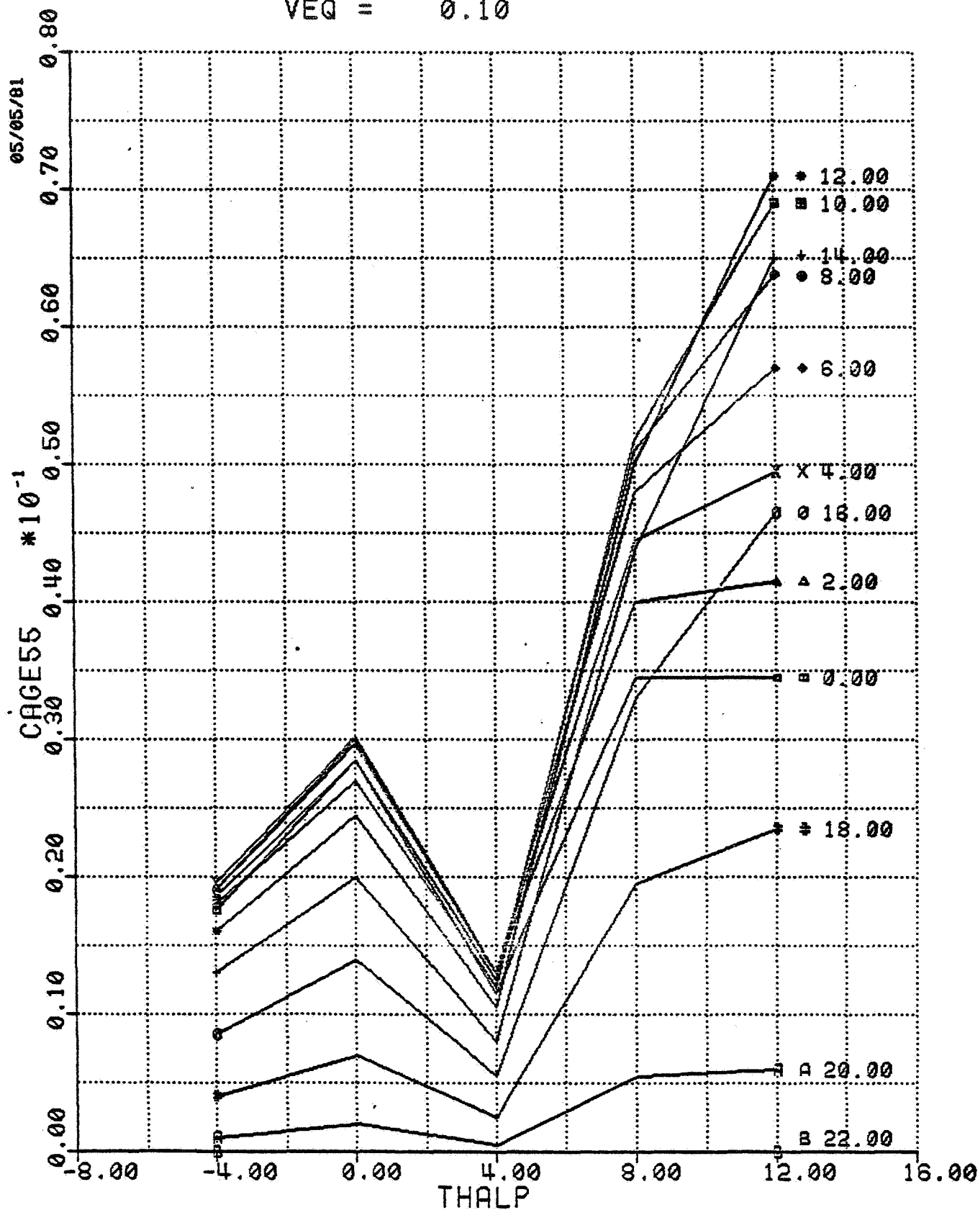
CAFLAPL VS ALPHA
FOR VARYING DFLAPL

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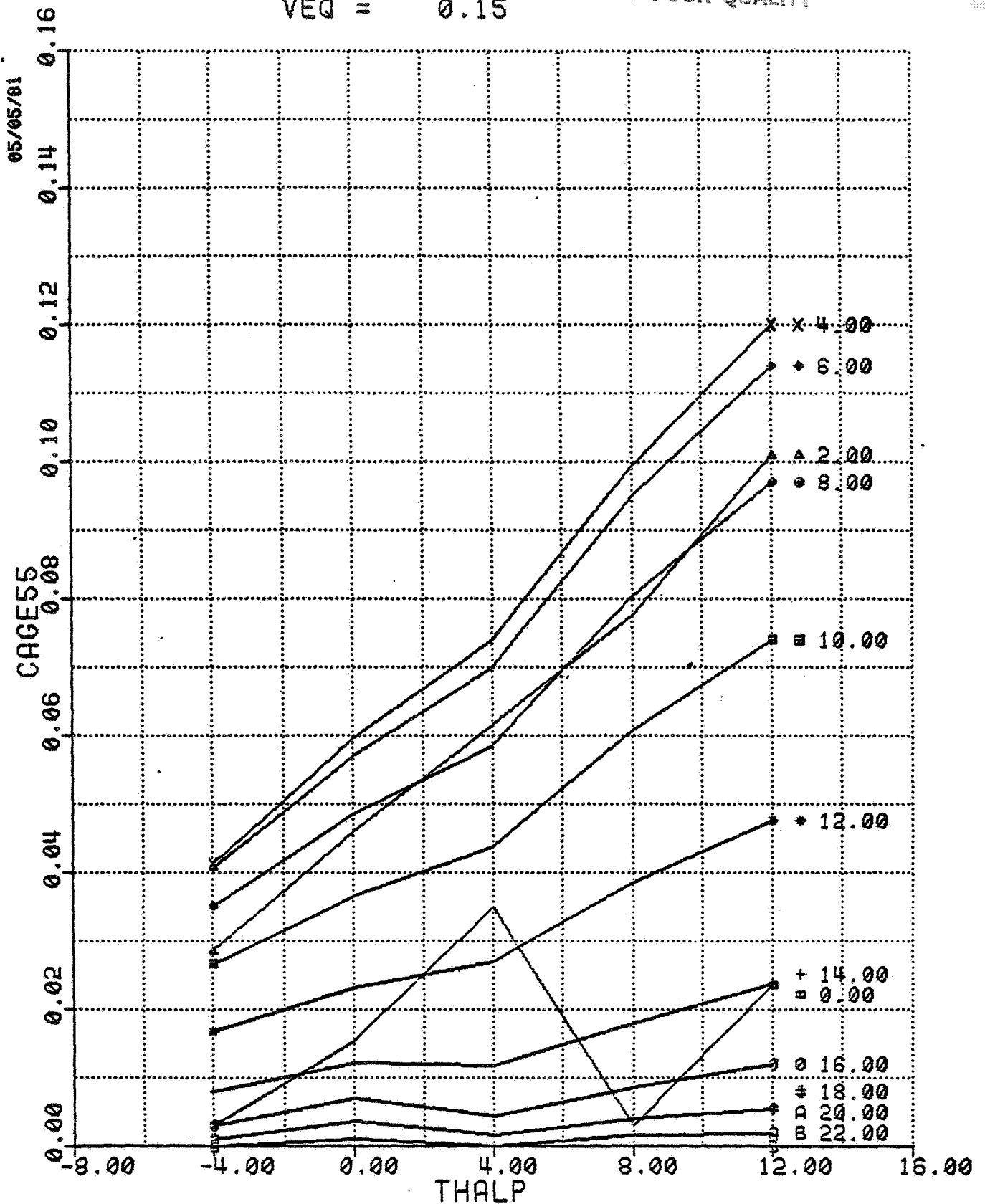
CAGE55 VS THALP
FOR VARYING HP
VEQ = 0.10

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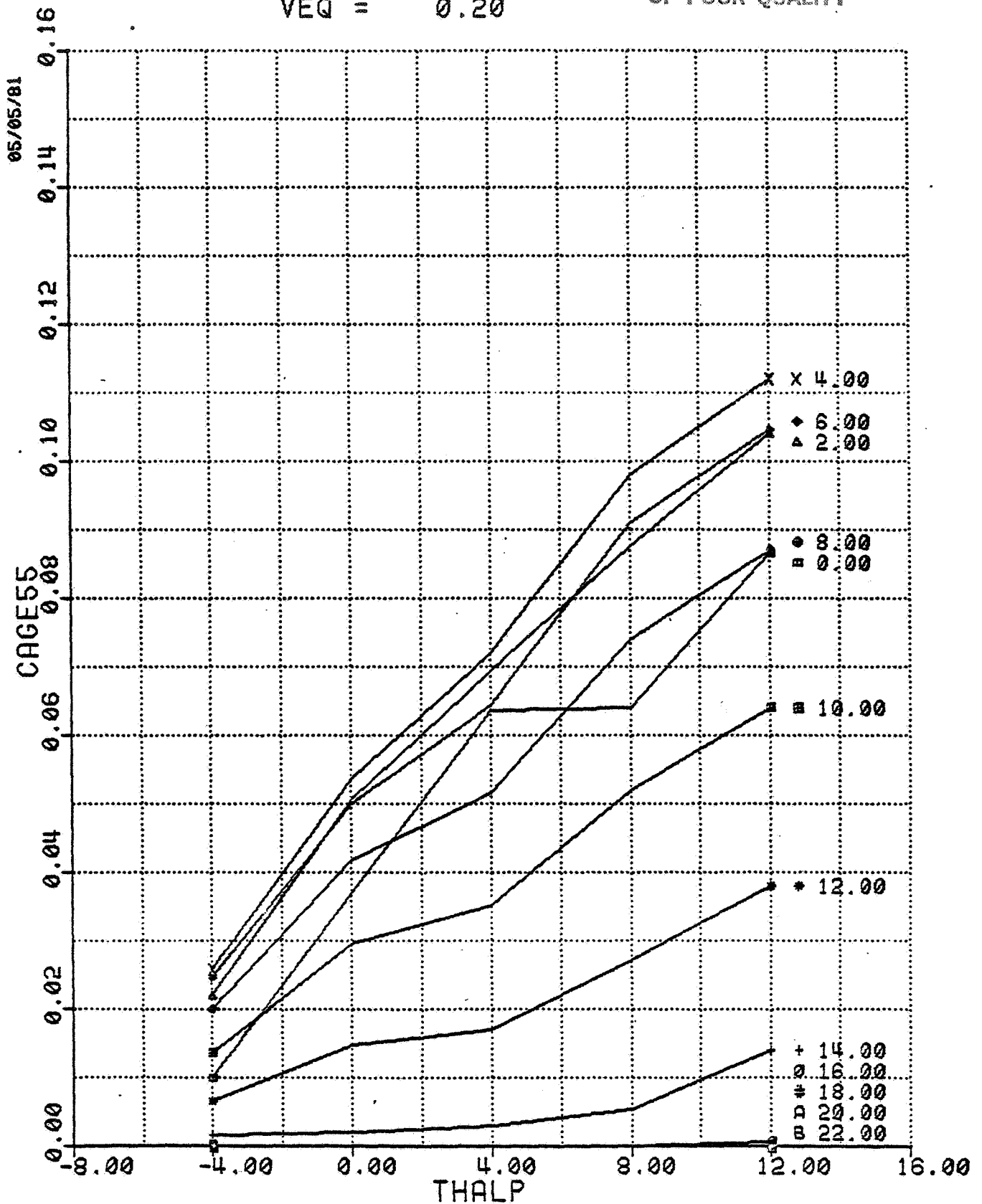
CAGE55 VS THALP
FOR VARYING HP
VEQ = 0.15

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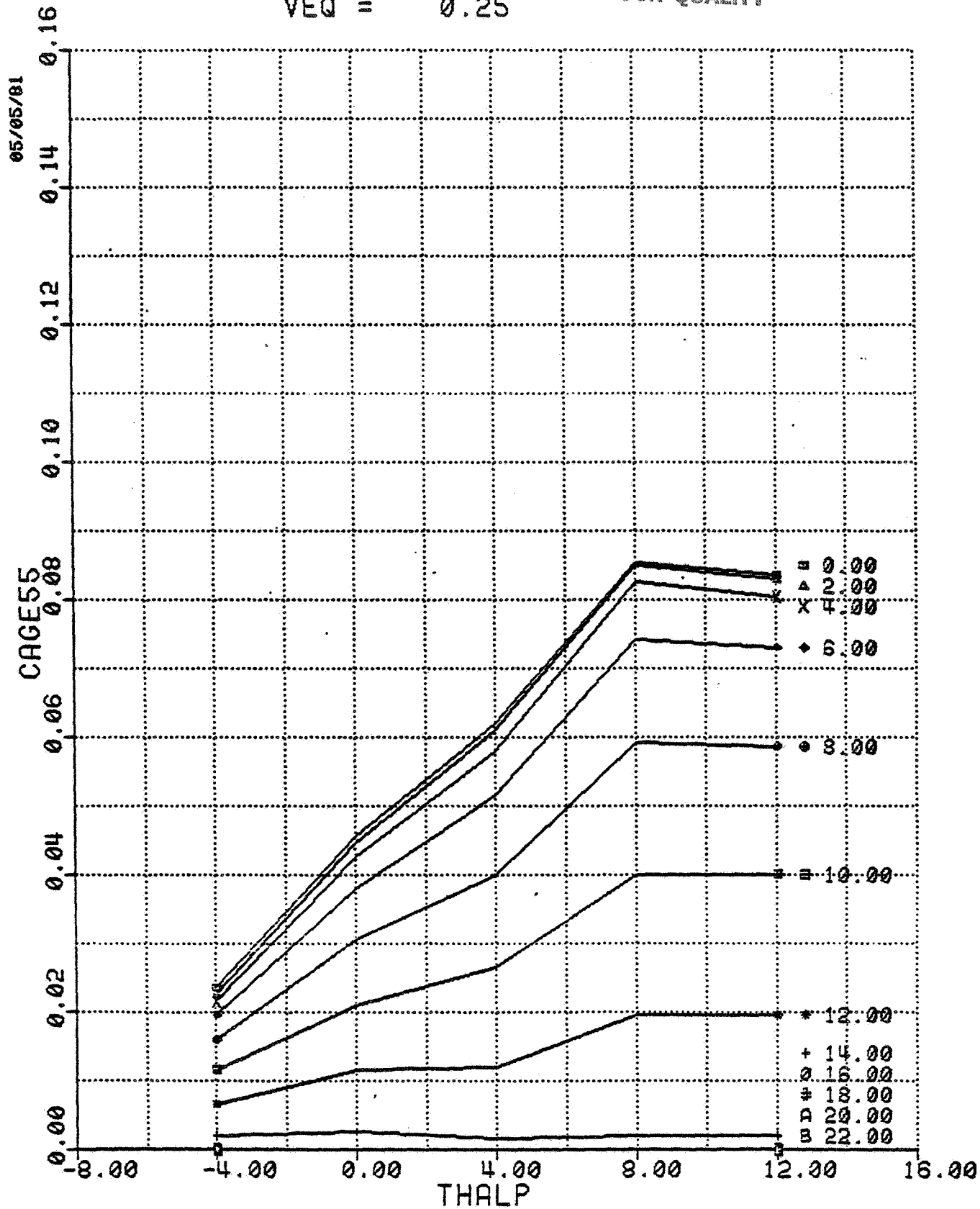


CAGE55 VS THALP
FOR VARYING HP
VEQ = 0.20

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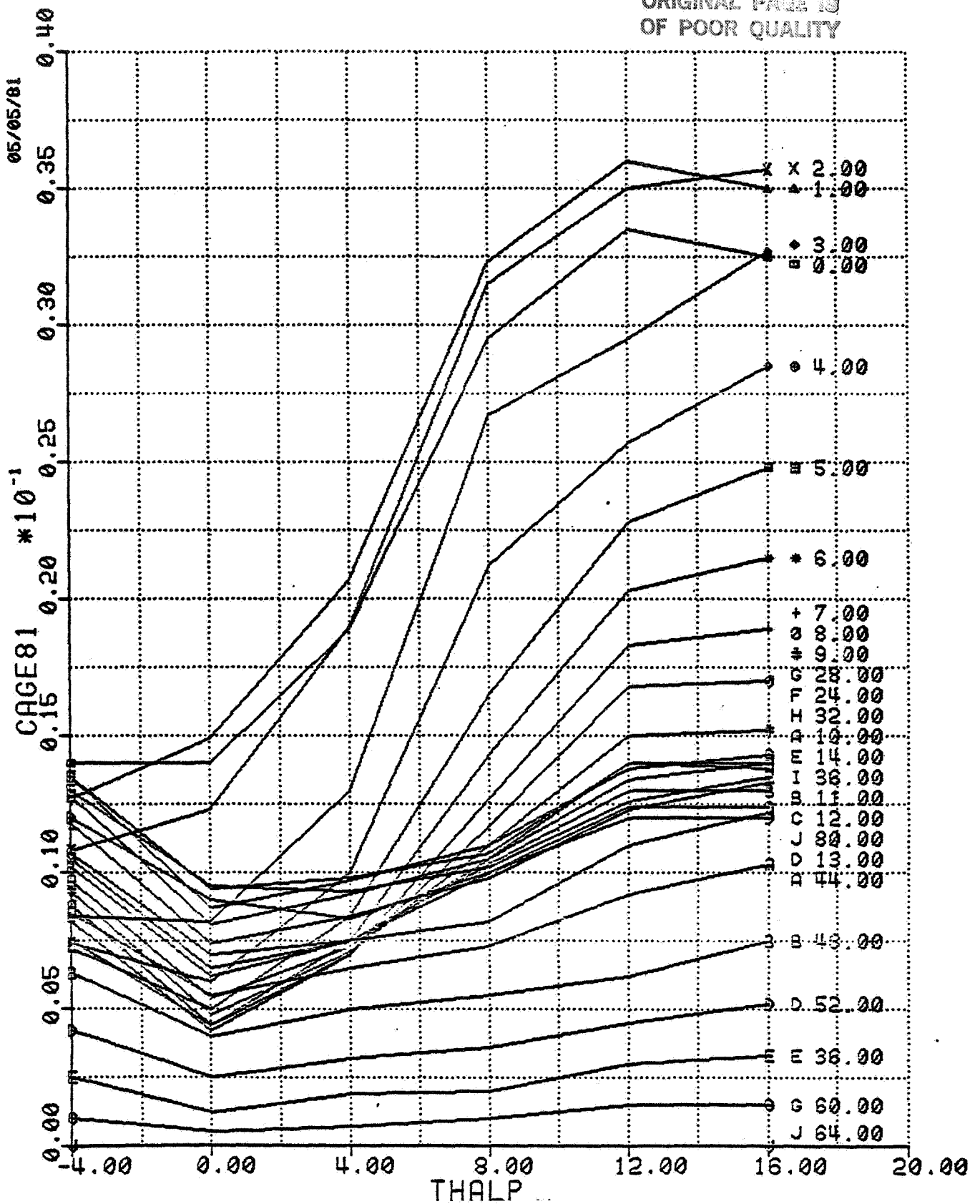


CAGE55 VS THALP
FOR VARYING HP ORIGINAL PAGE IS
VEQ = 0.25 OF POOR QUALITY



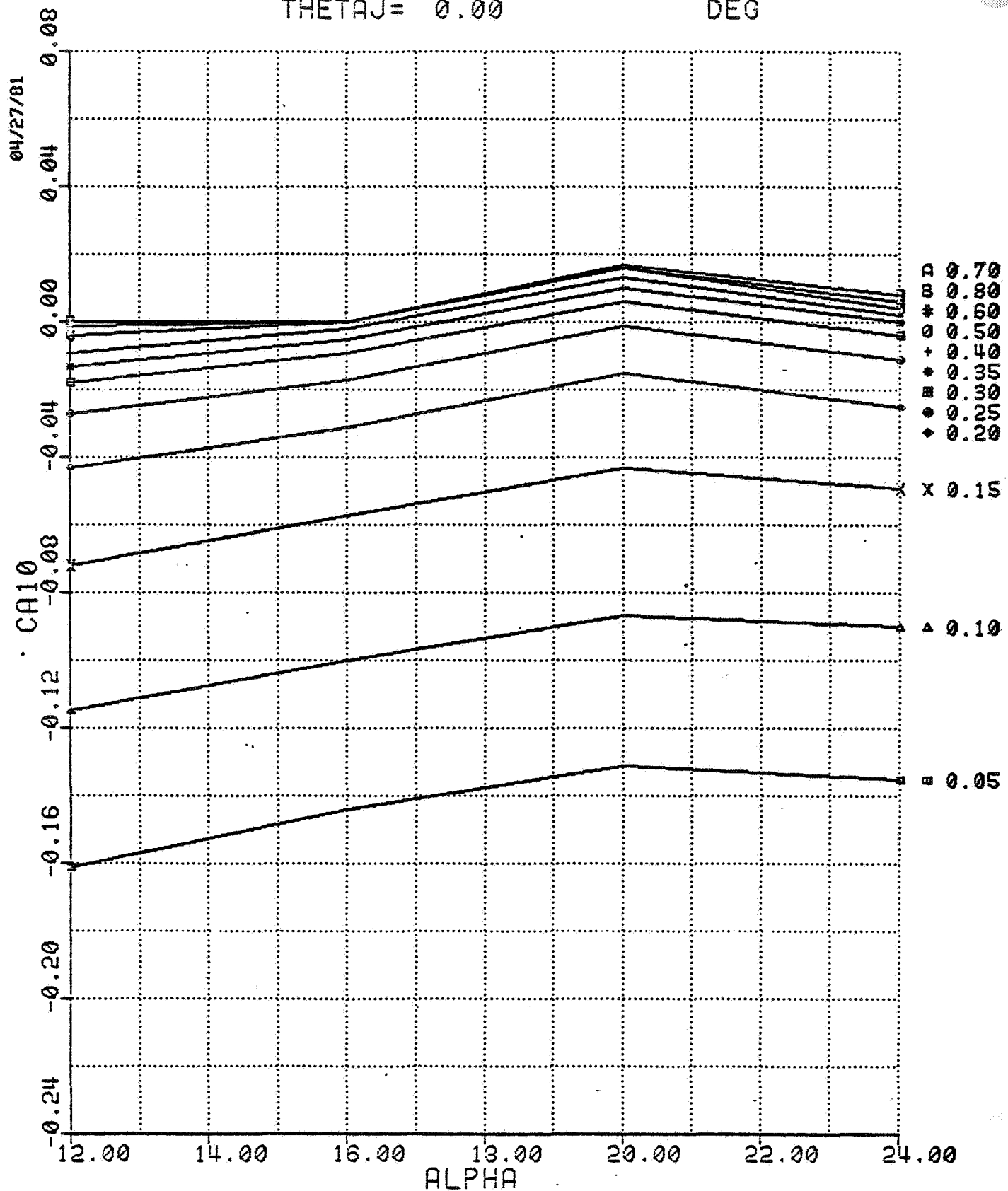
CAGE81 VS THALP FOR VARYING HP

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CA10 VS ALPHA
FOR VARYING VEQ
THETAJ = 0.00

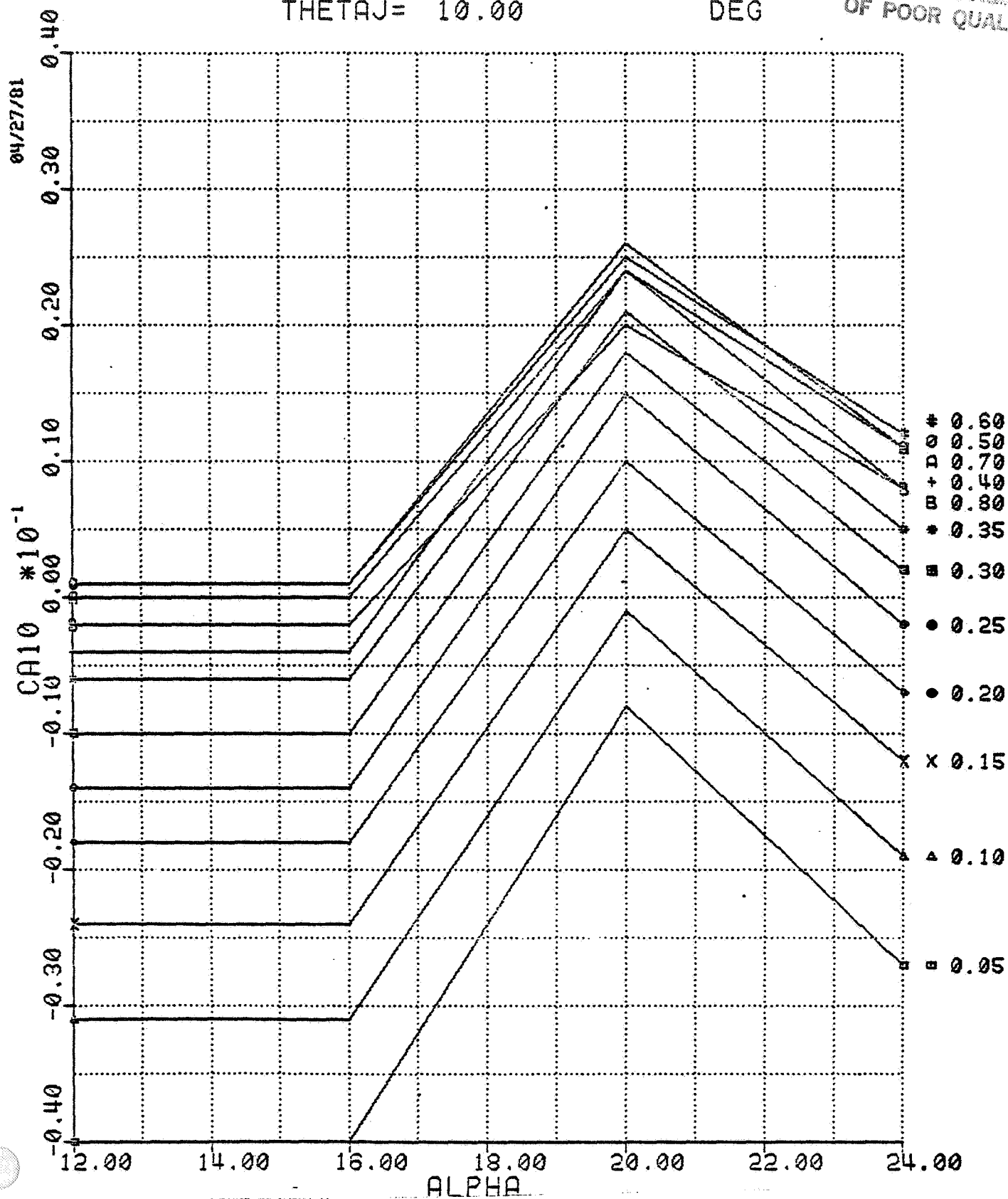
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CA10 VS ALPHA
FOR VARYING VEQ
THETAJ= 10.00

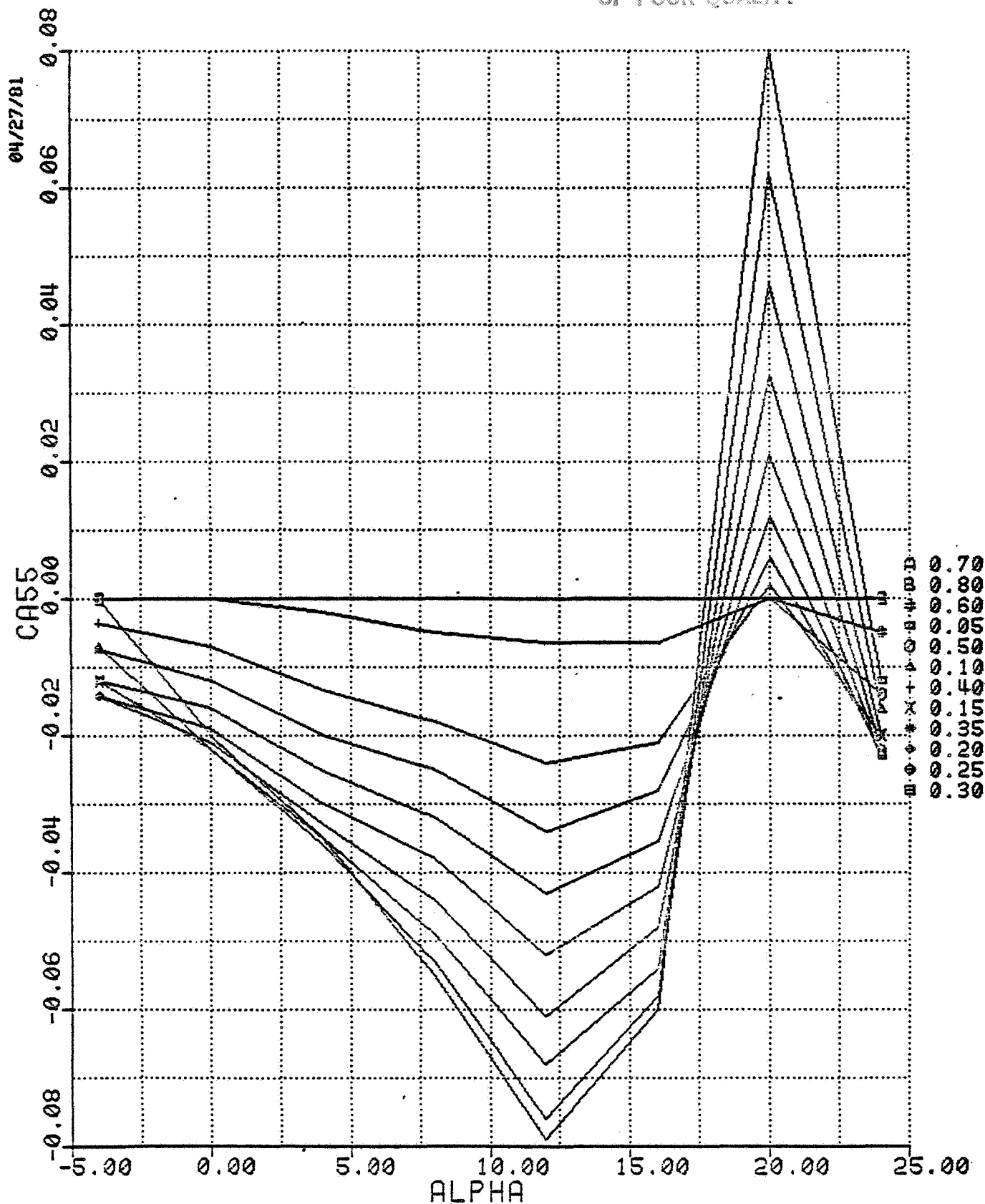
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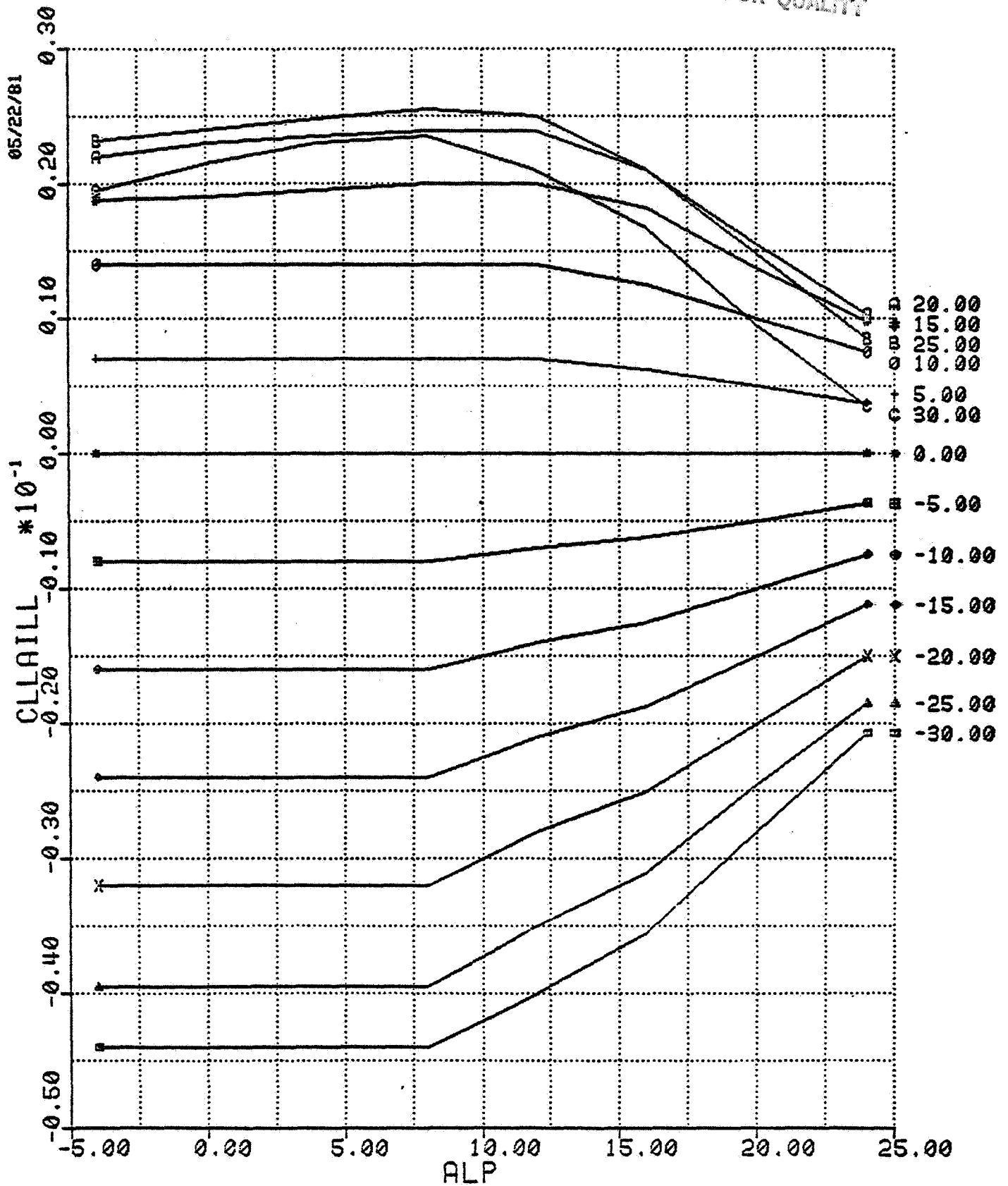
CA55 VS ALPHA
FOR VARYING VEQ

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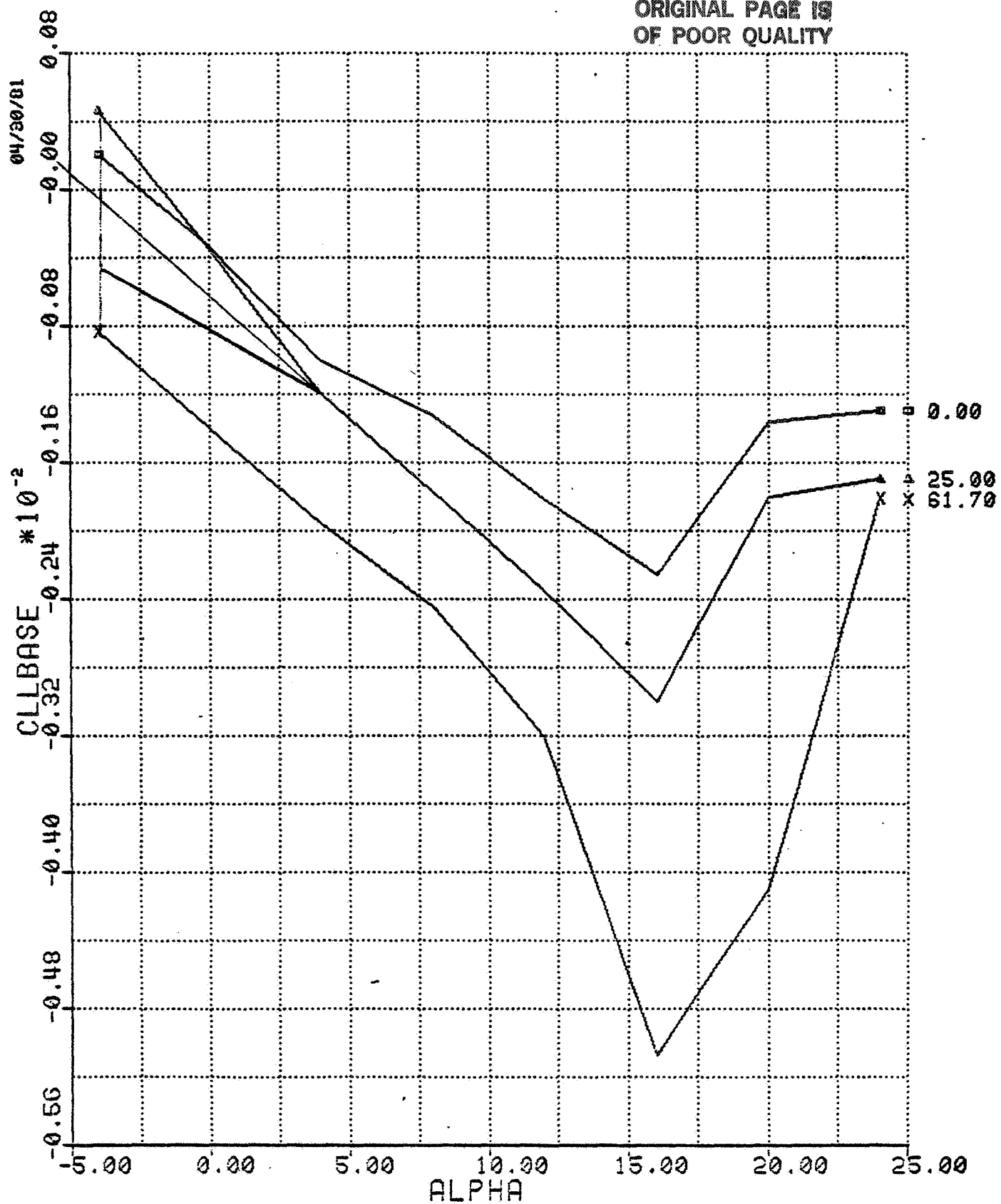
CLLAILL VS ALP
FOR VARYING DAL

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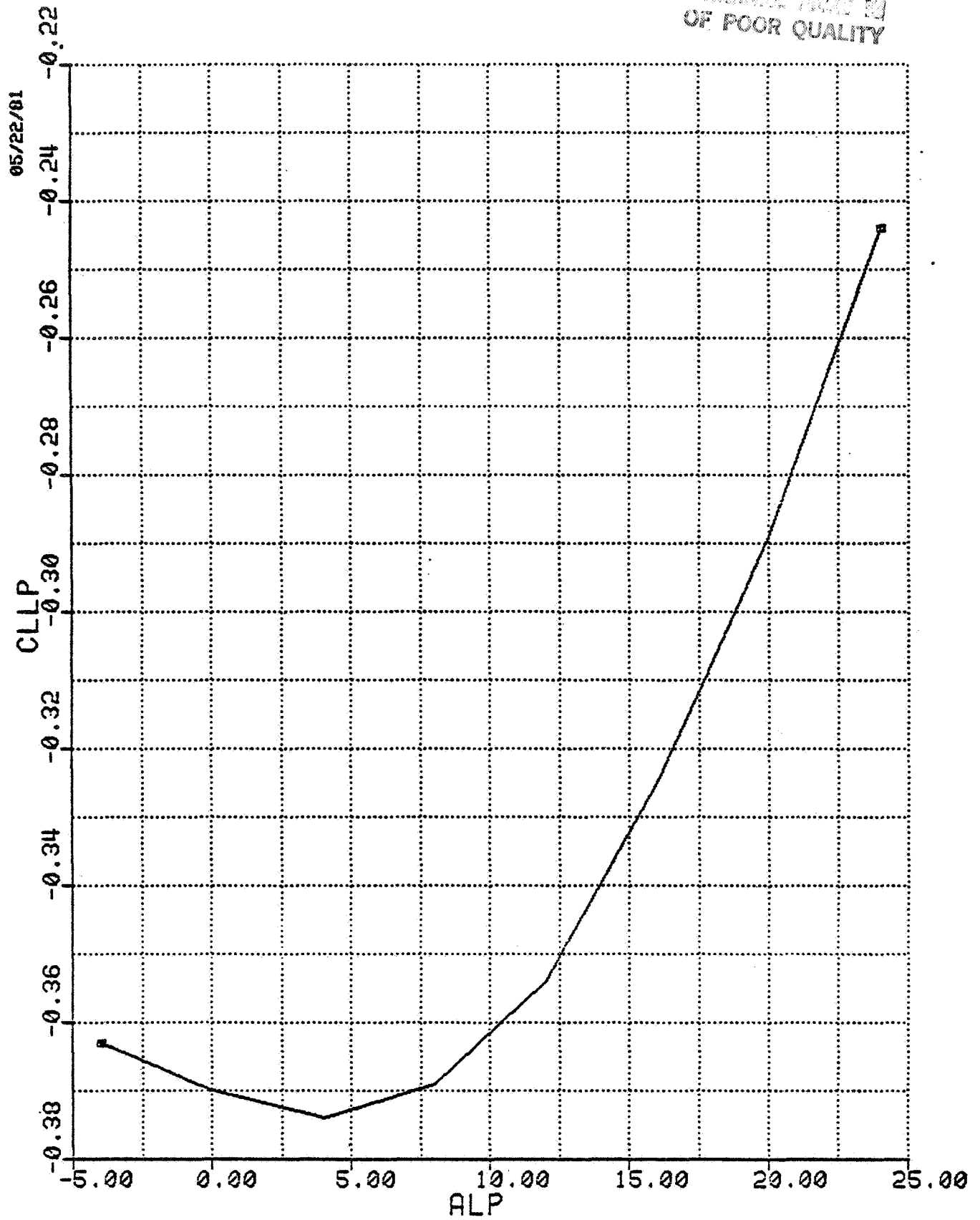
CLLBASE VS ALPHA
FOR VARYING FLAP

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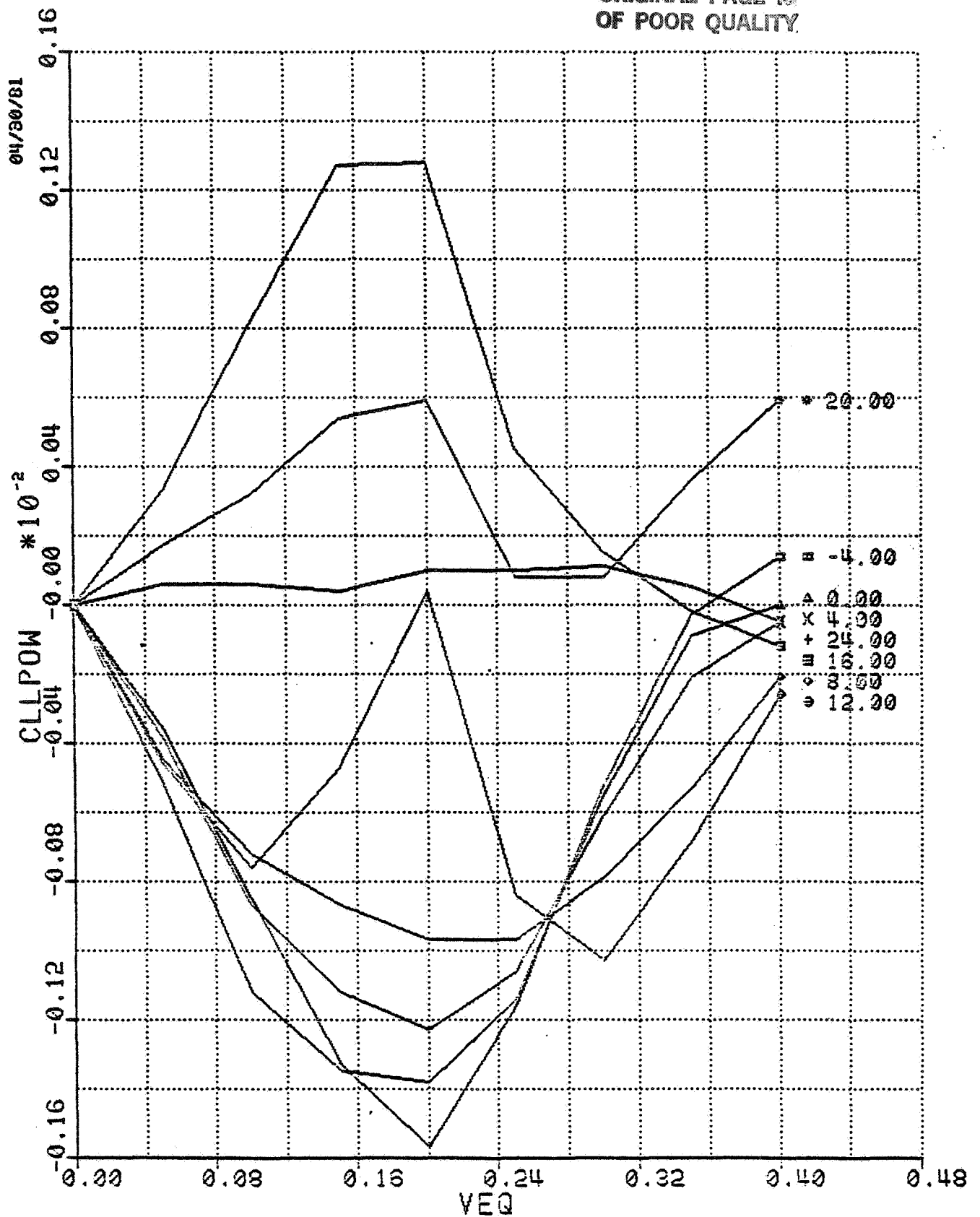
CLLP VS ALP

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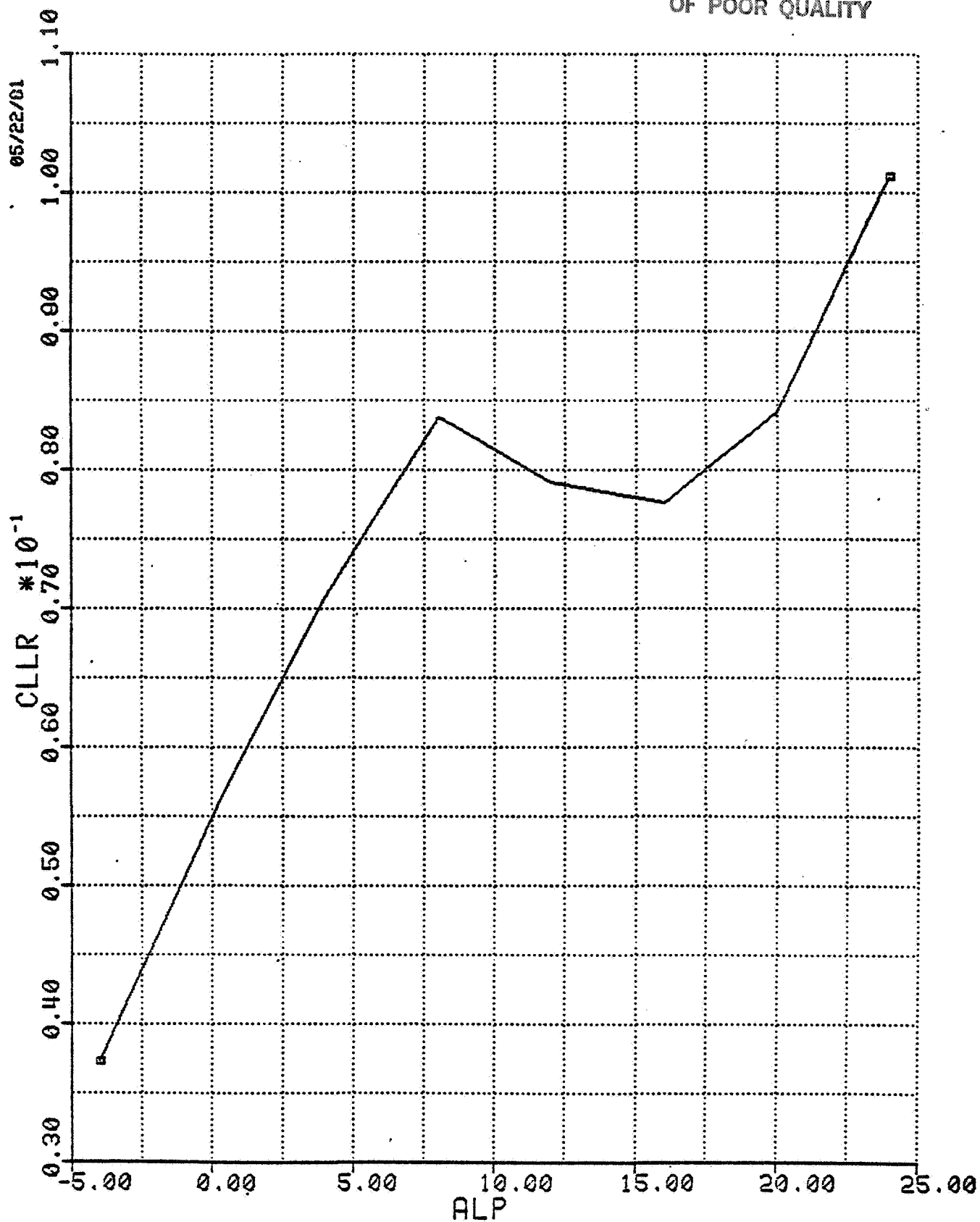
CLLPW VS VEQ
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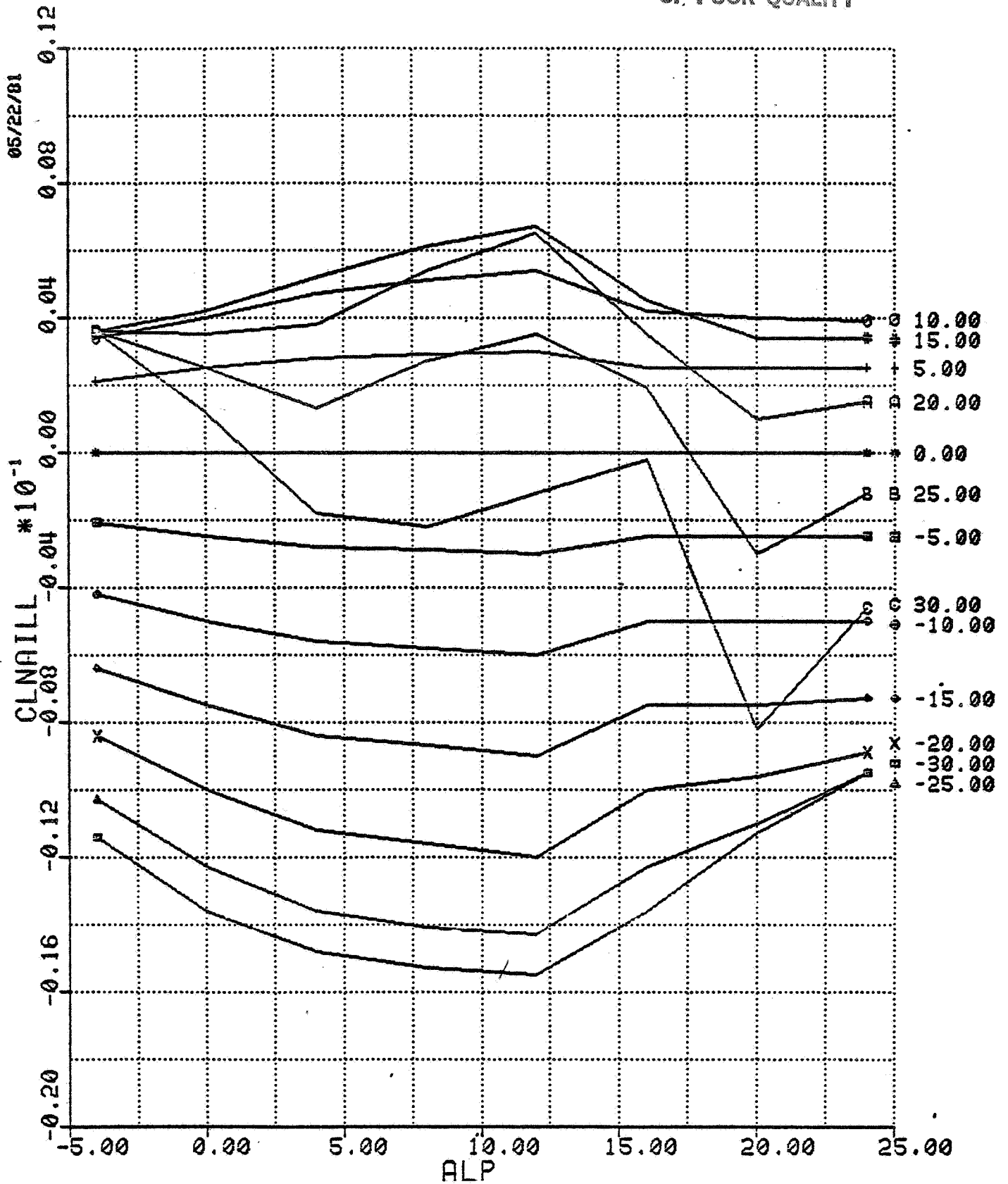
CLLR VS ALP

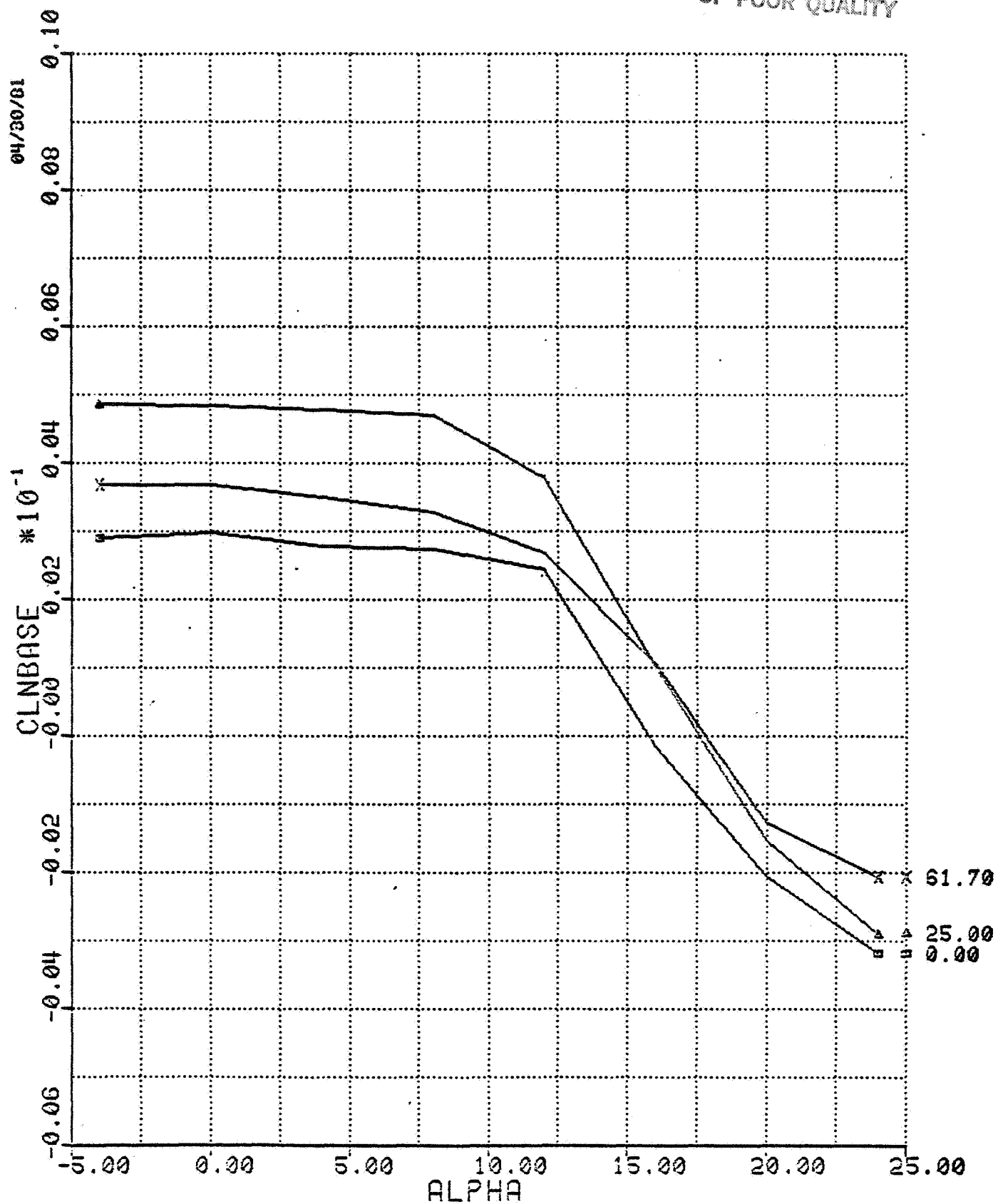
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CLNAILL VS ALP
FOR VARYING DAL

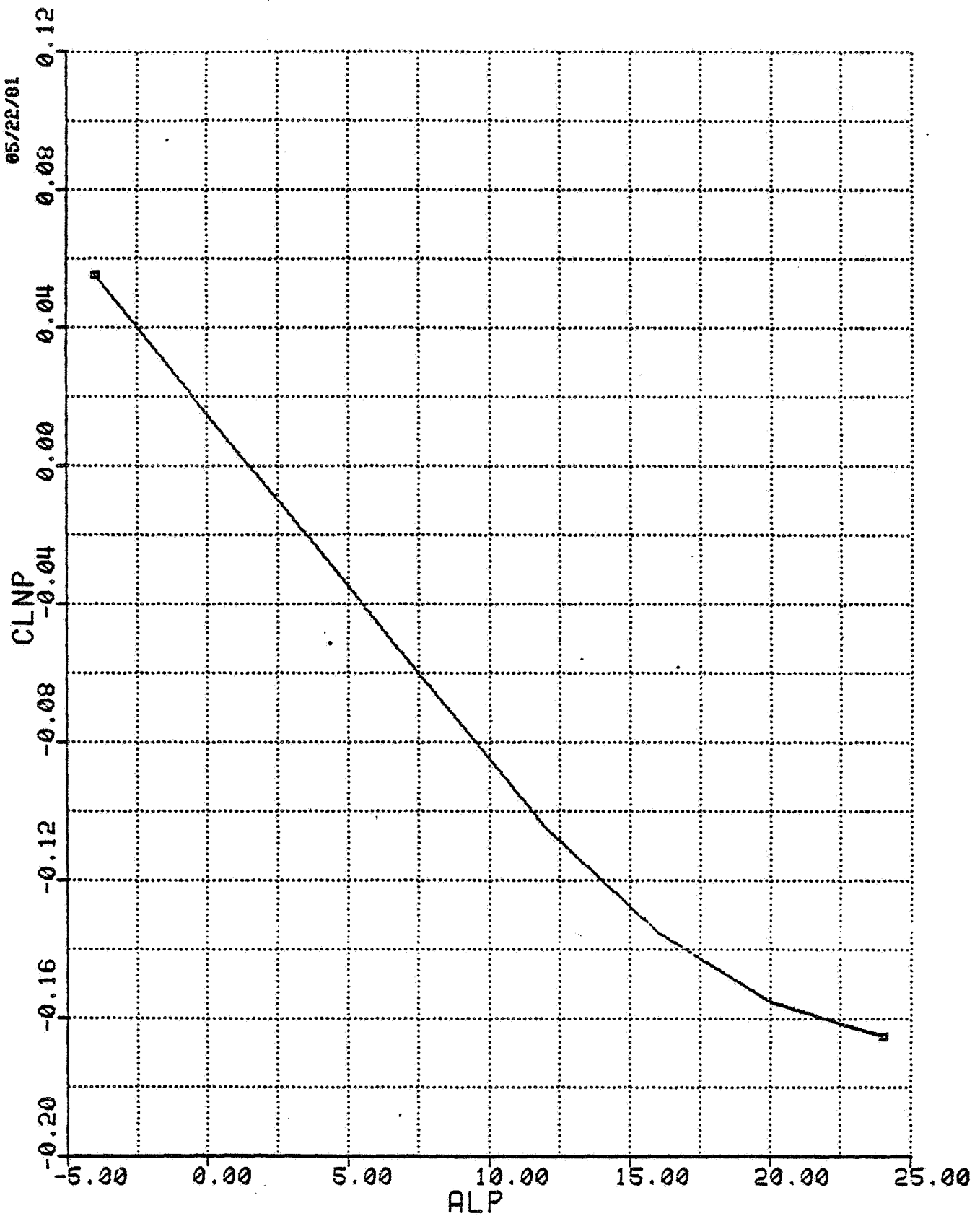
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CLNBASE VS ALPHA
FOR VARYING FLAPORIGINAL PAGE 13
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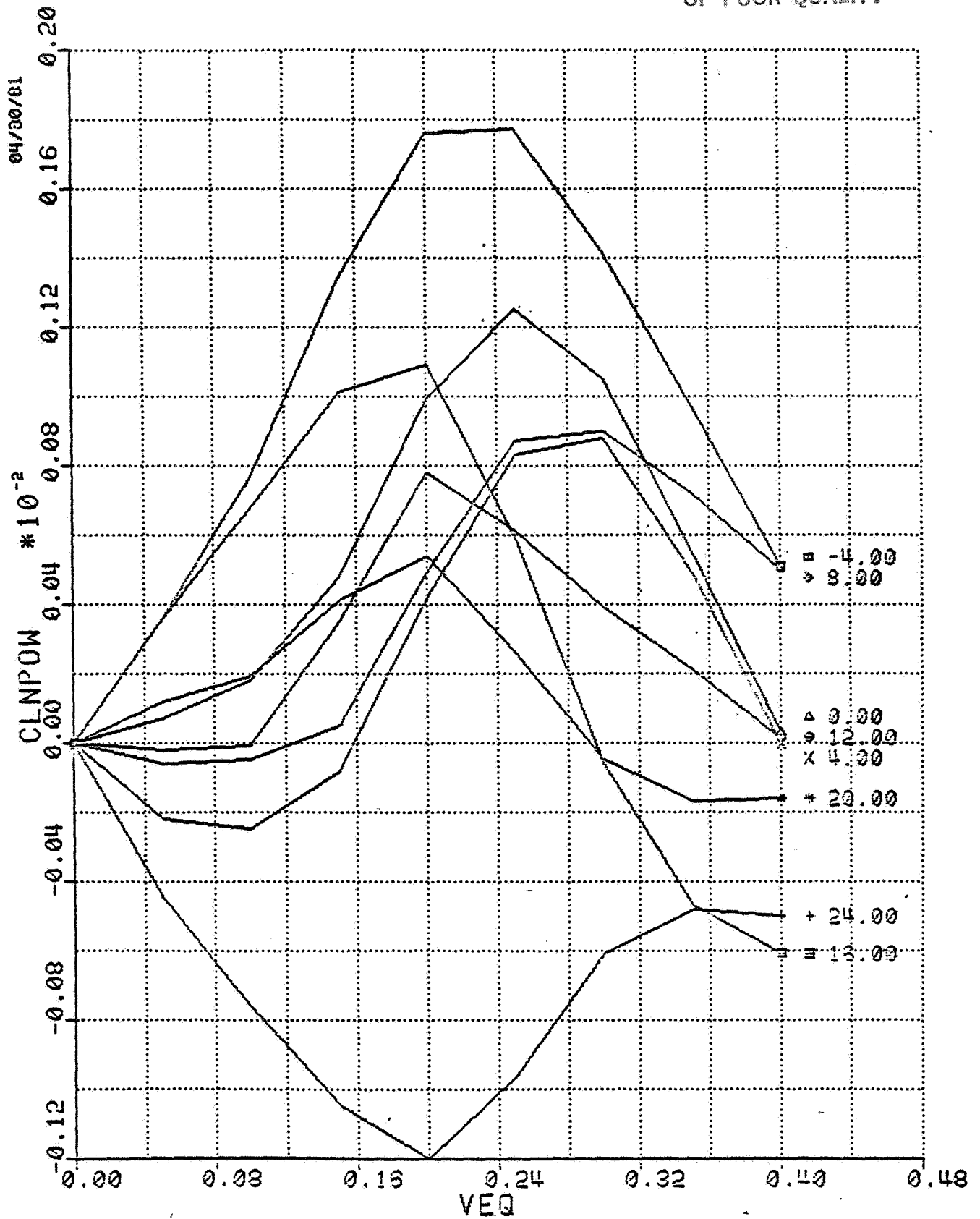
CLNP VS ALP

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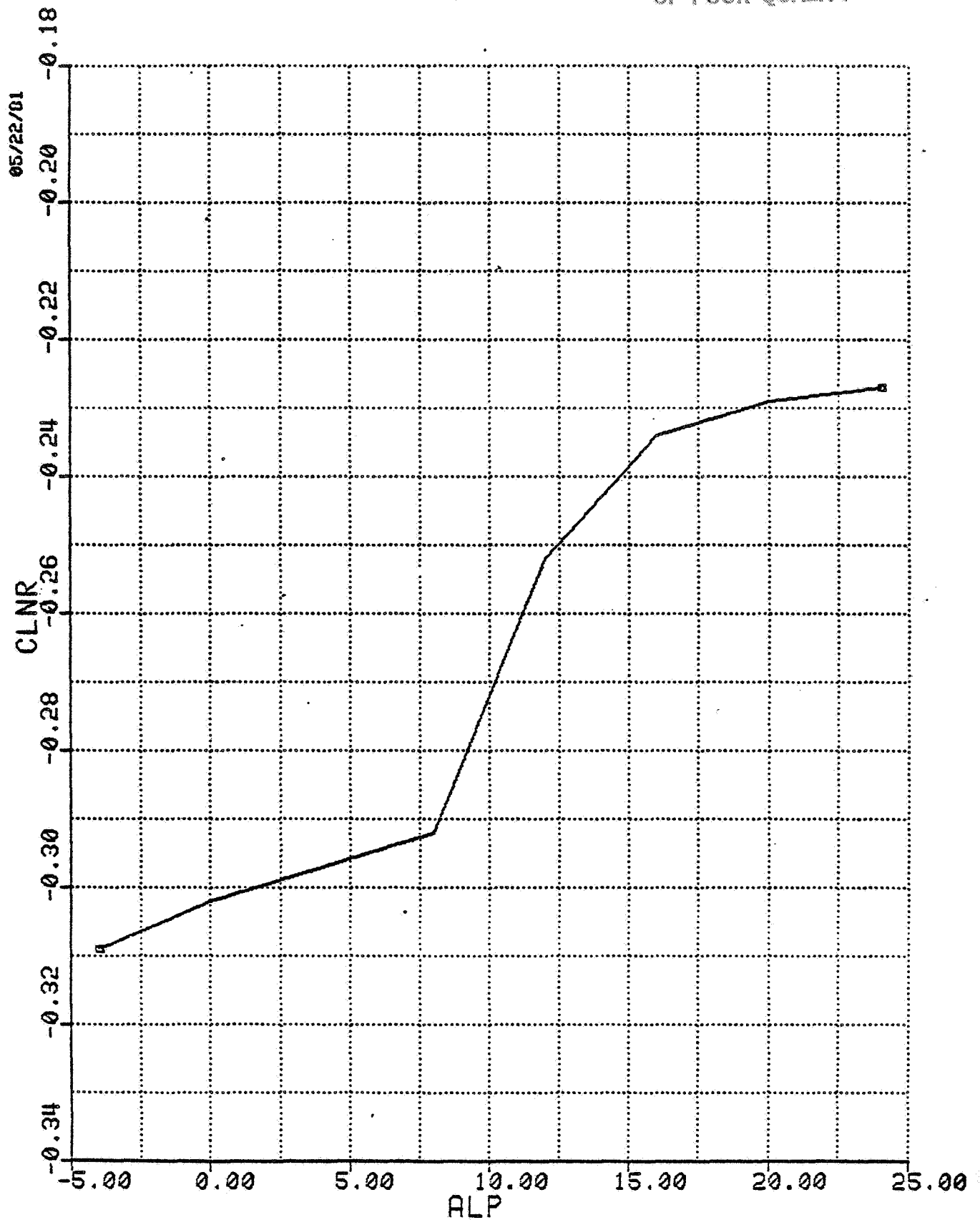
CLNPOW VS VEQ
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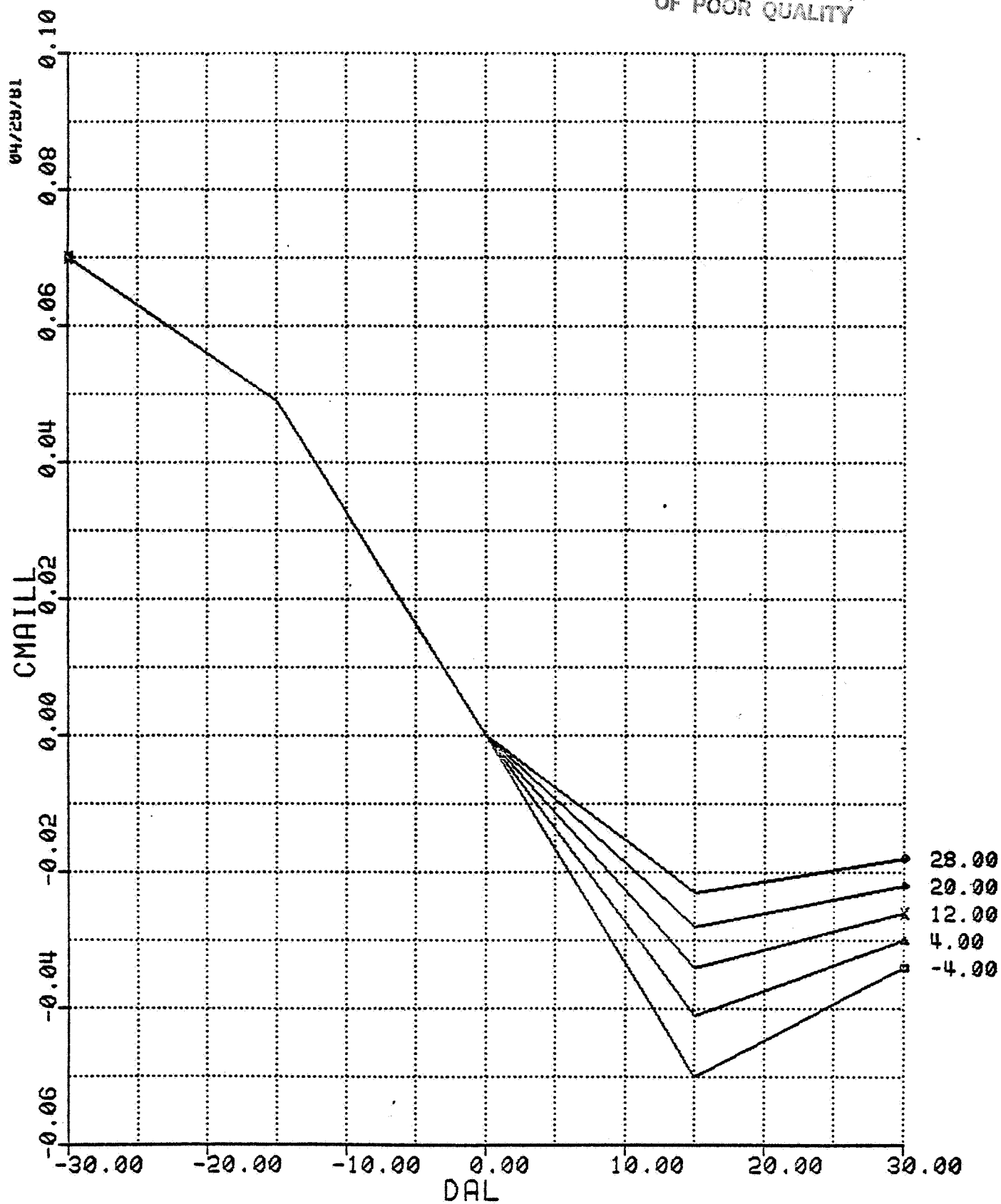
CLNR VS ALP

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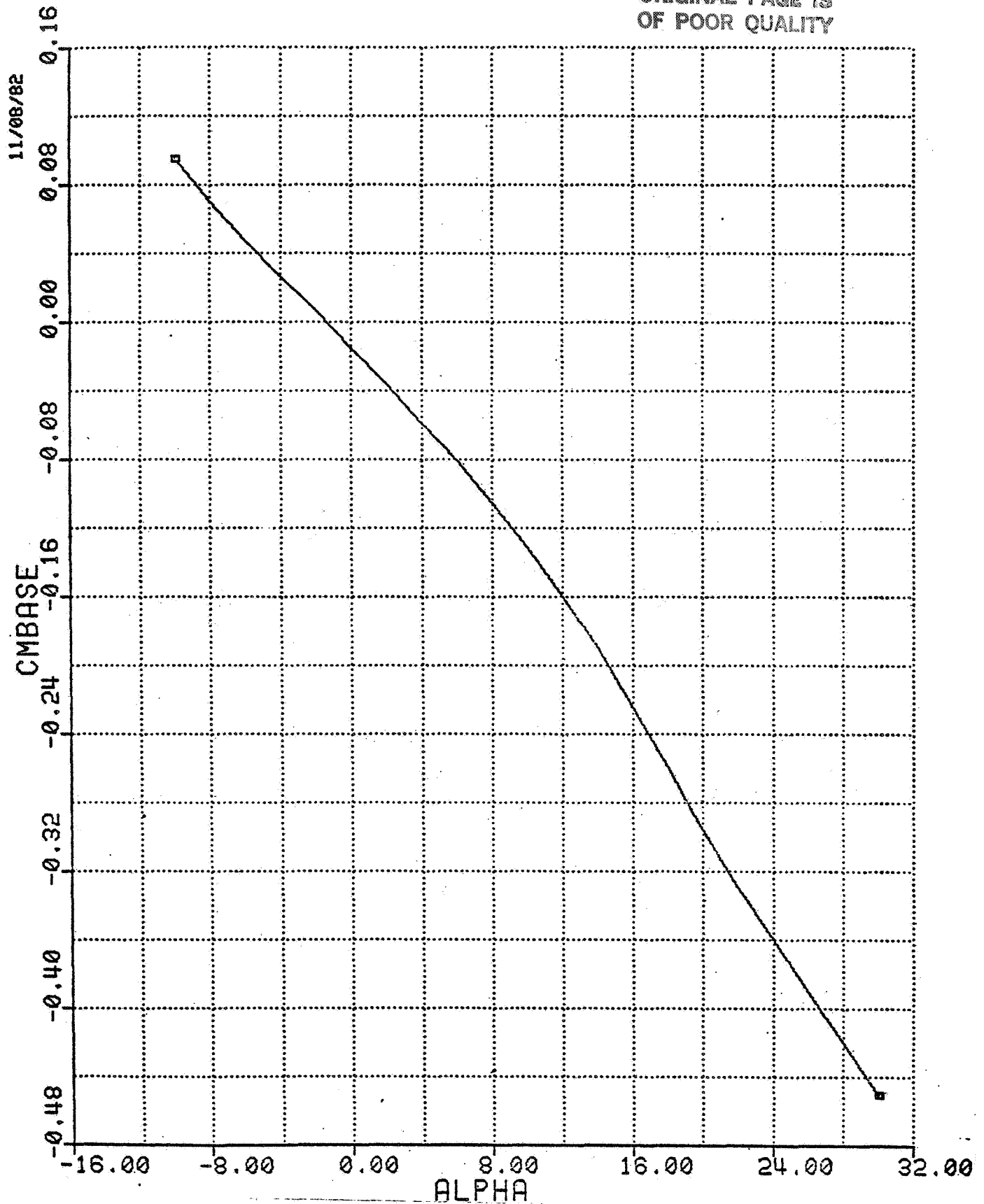
CMAILL VS DAL
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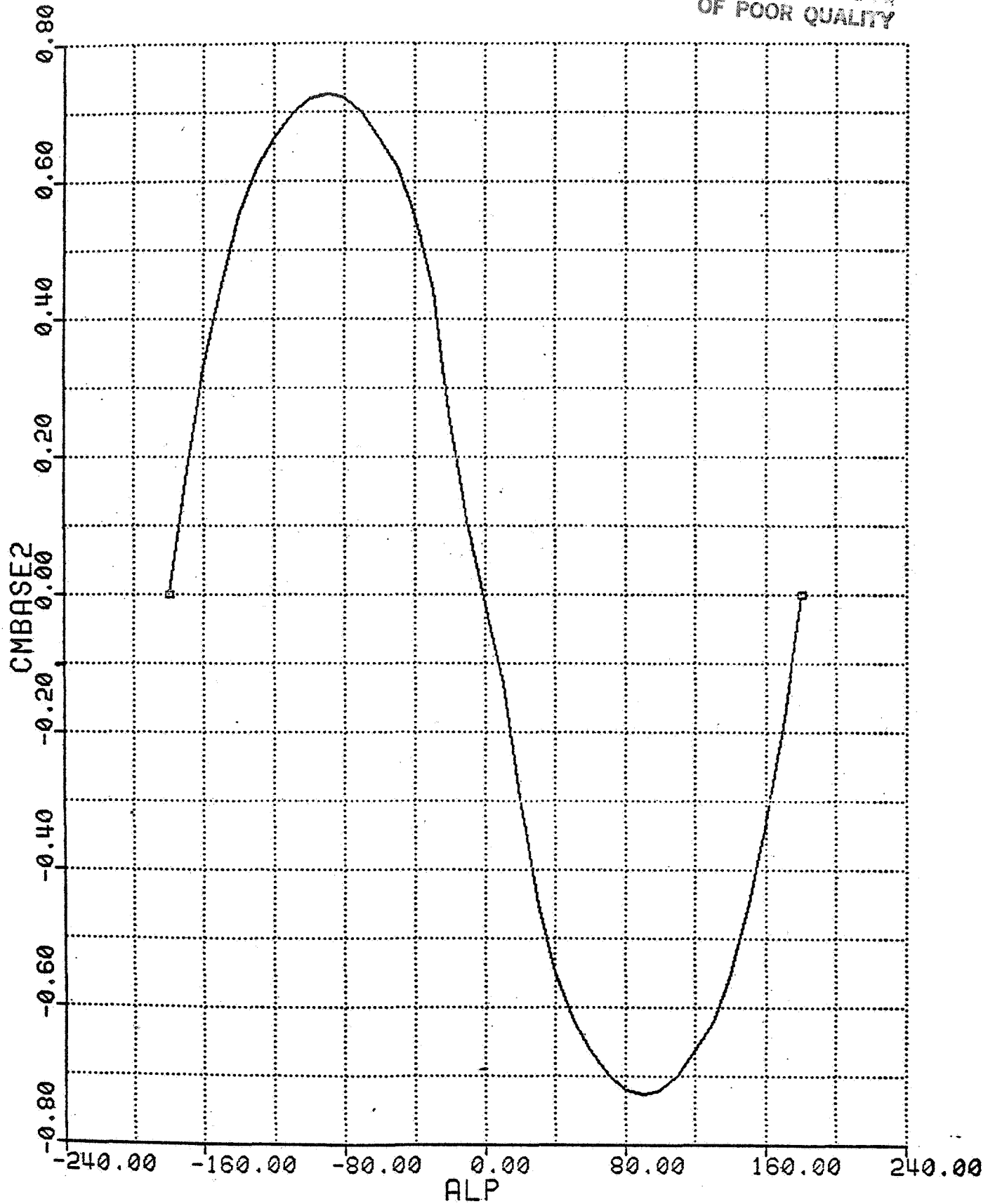
CMBASE VS ALPHA

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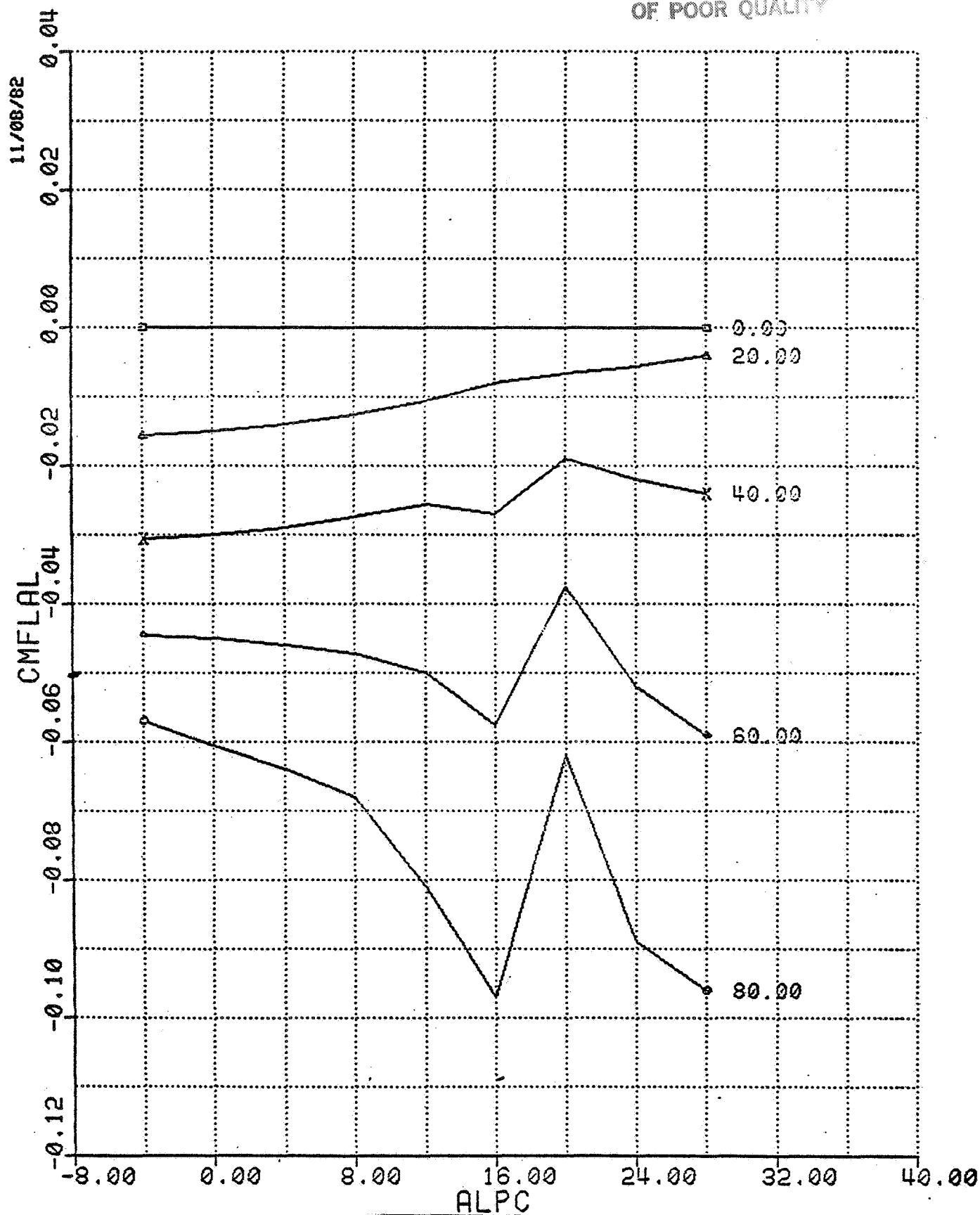
CMBASE2 VS ALP

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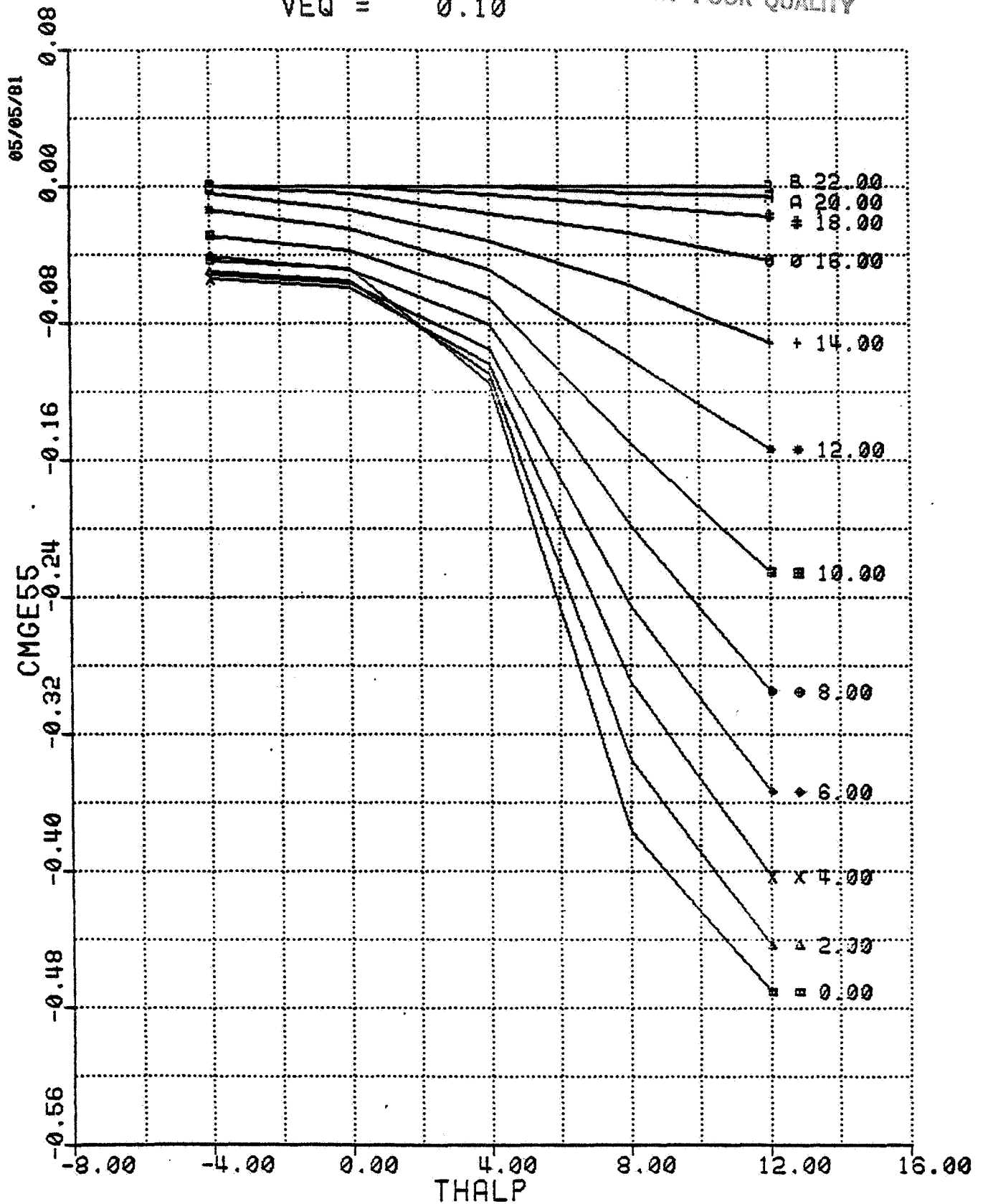
CMFLAL VS ALPC
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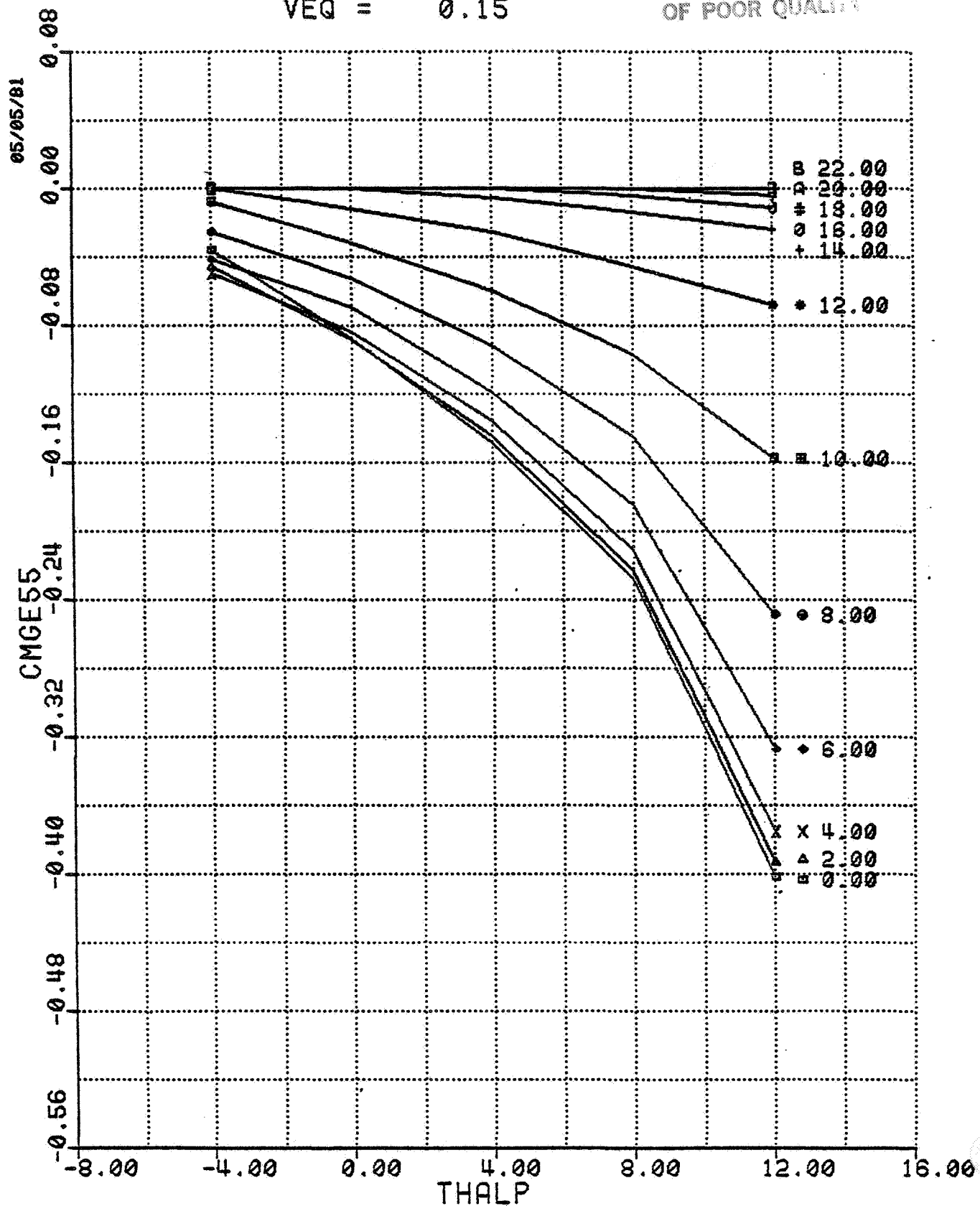
CMGE55 VS THALP
FOR VARYING HP
VEQ = 0.10

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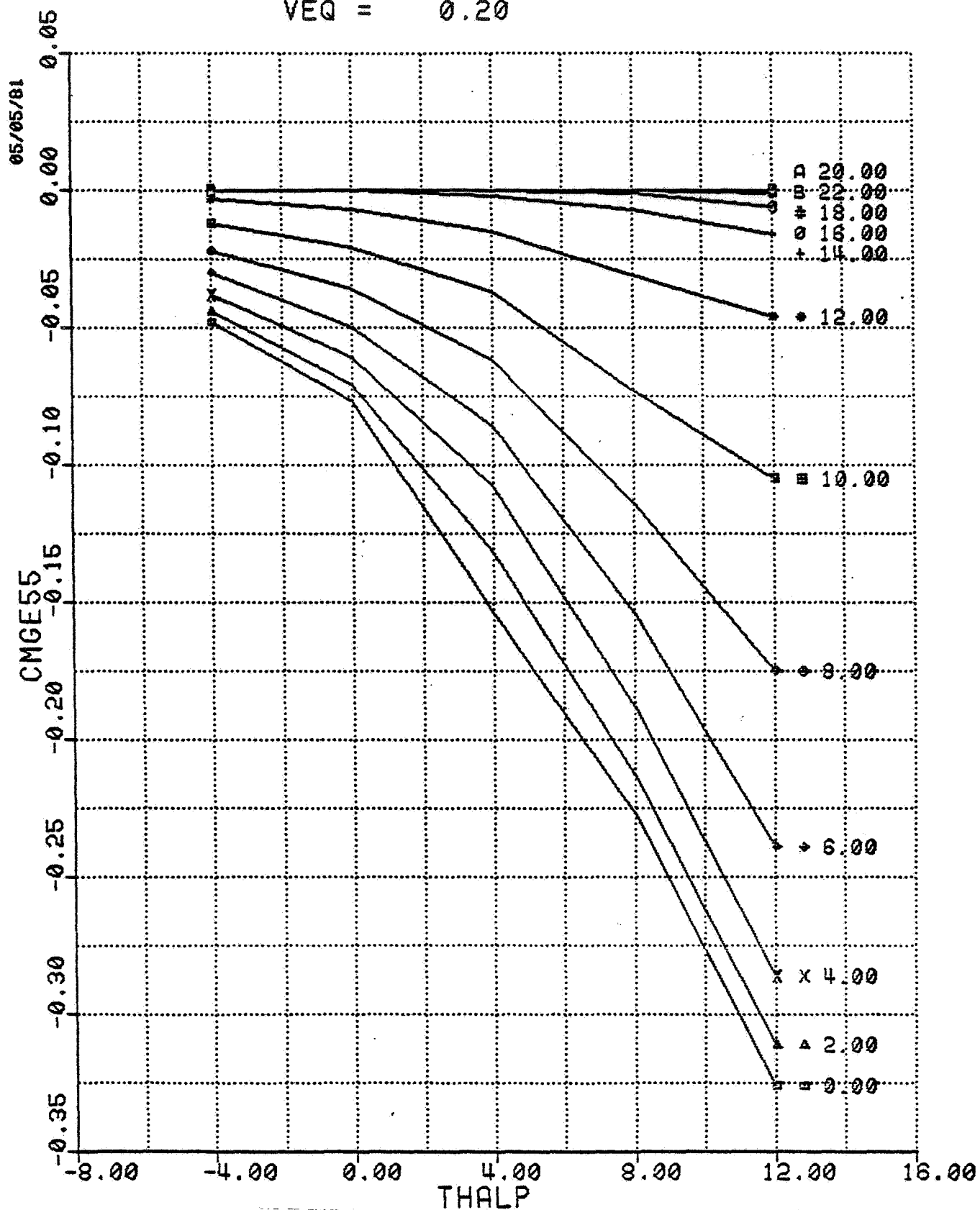
CMGE55 VS THALP
FOR VARYING HP
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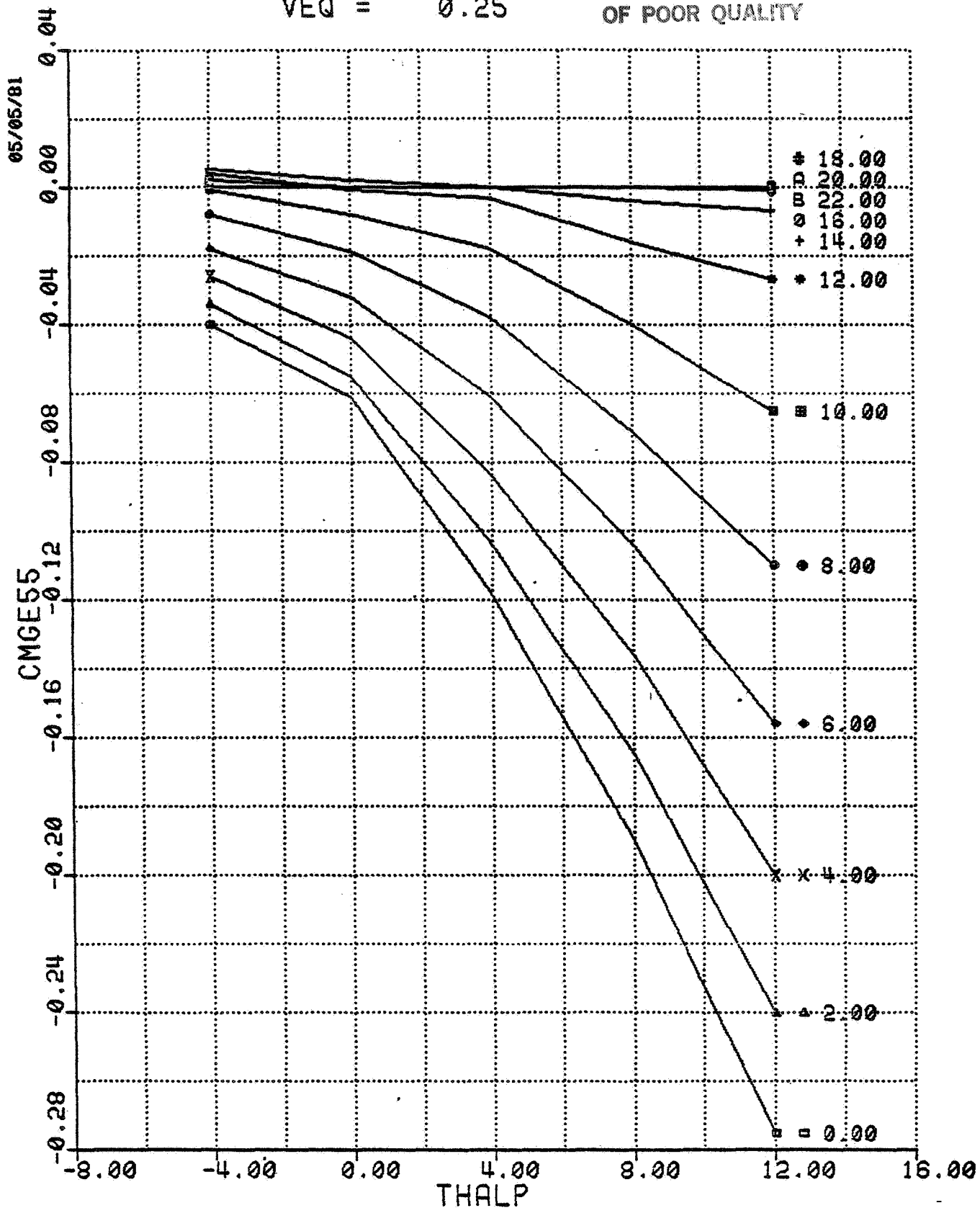
CMGE55 VS THALP
FOR VARYING HP
VEQ = 0.20

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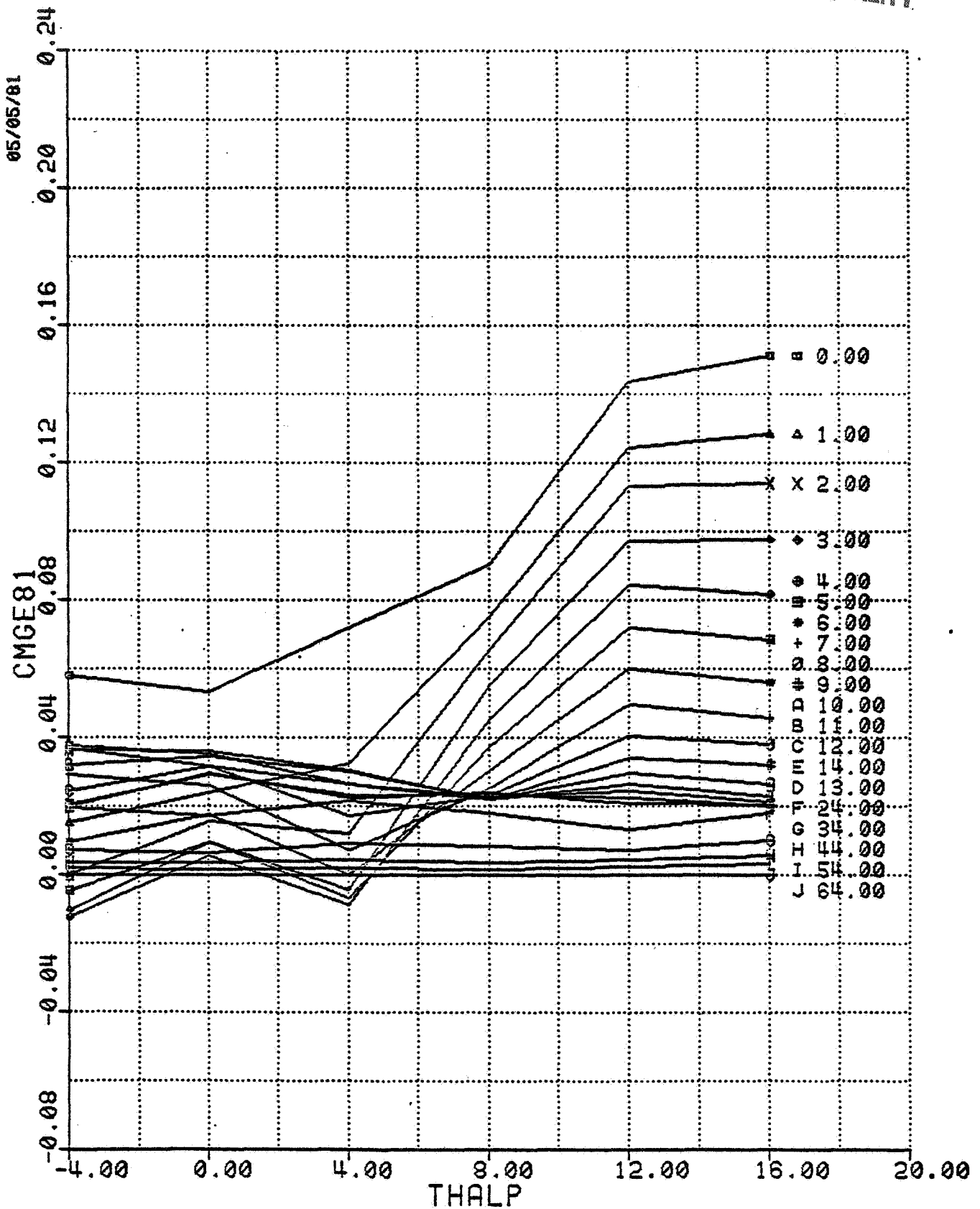
CMGE55 VS THALP
FOR VARYING HP
VEQ = 0.25

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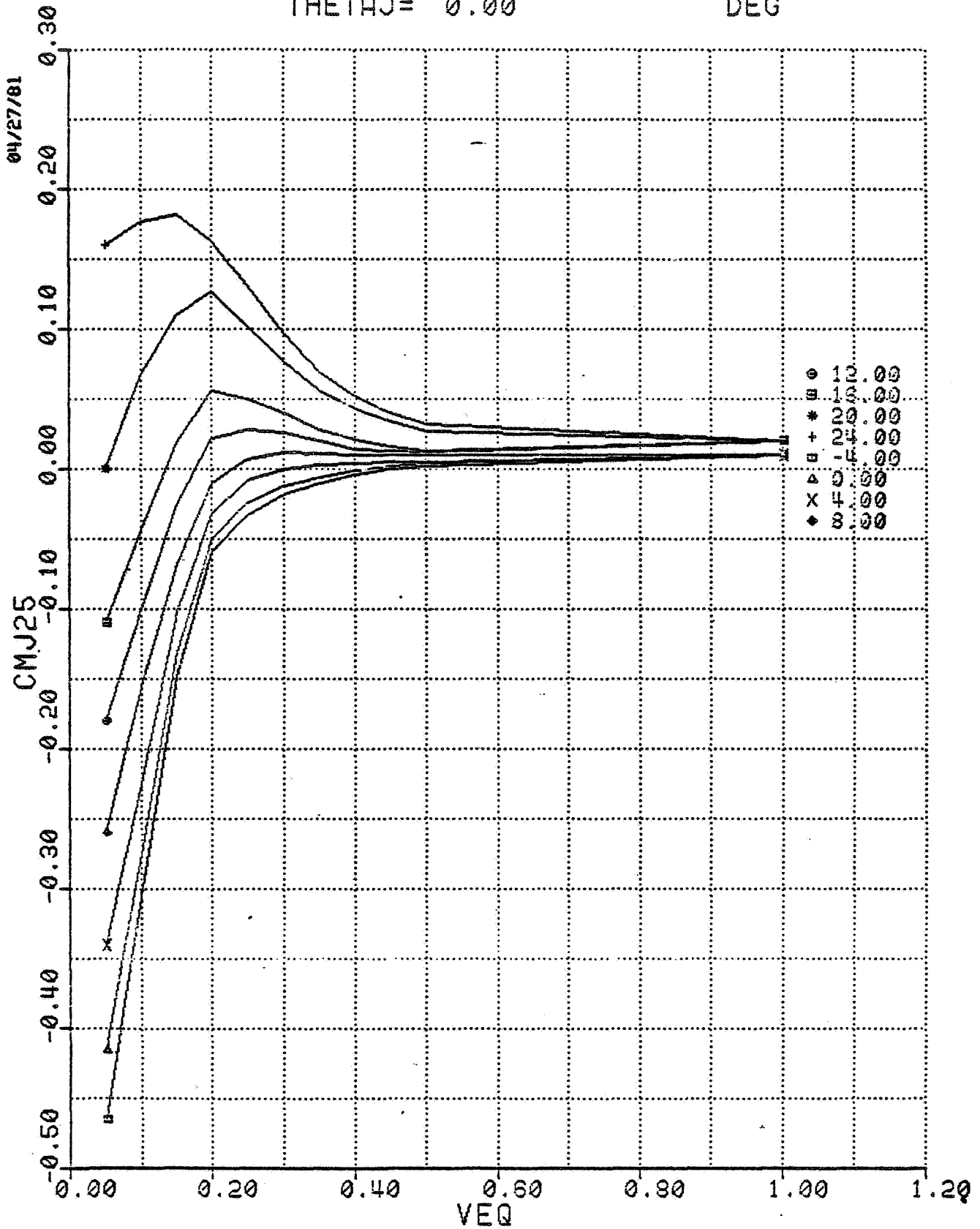
CMGE81 VS THALP
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CMJ25 VS VEQ
FOR VARYING ALPHA
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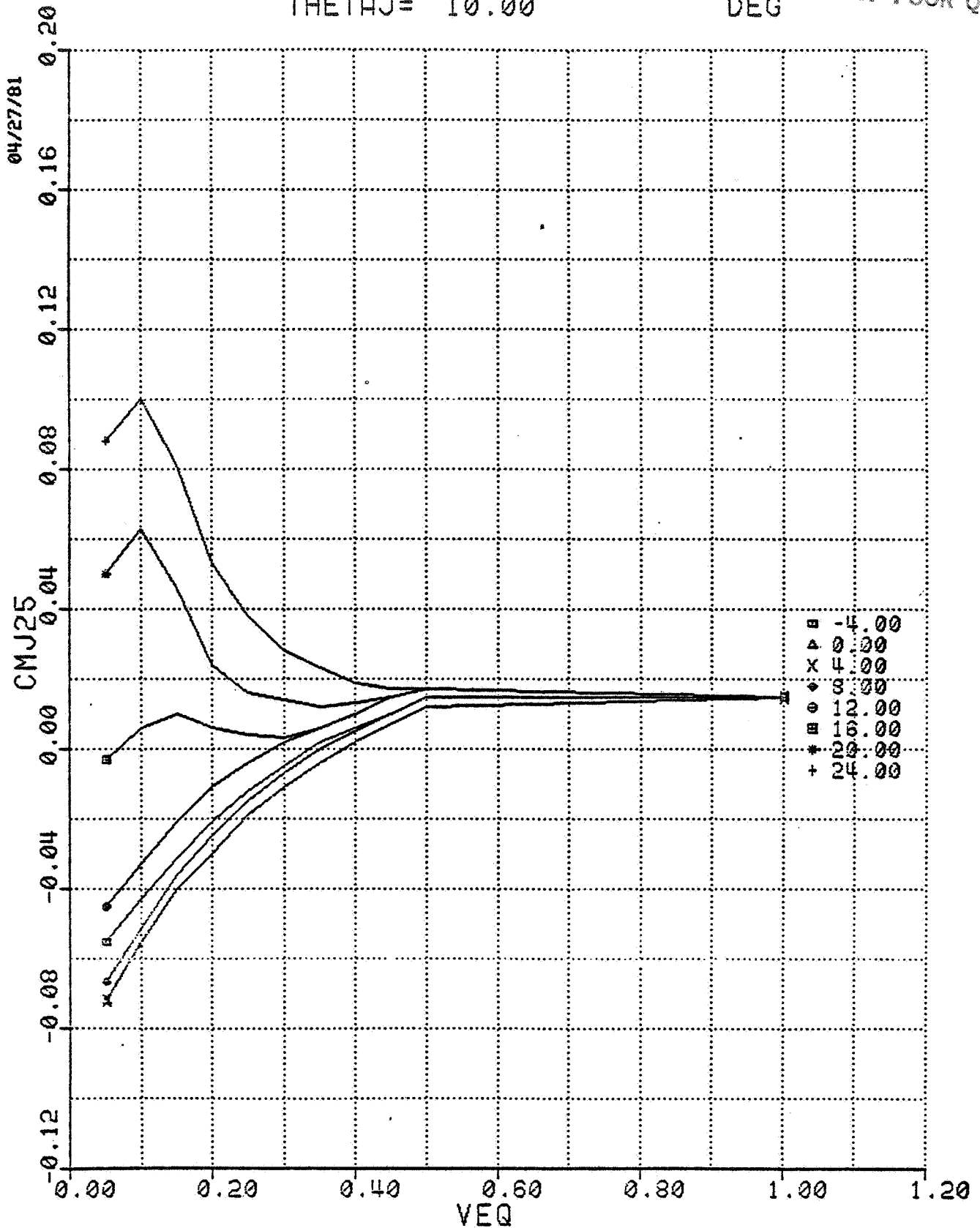
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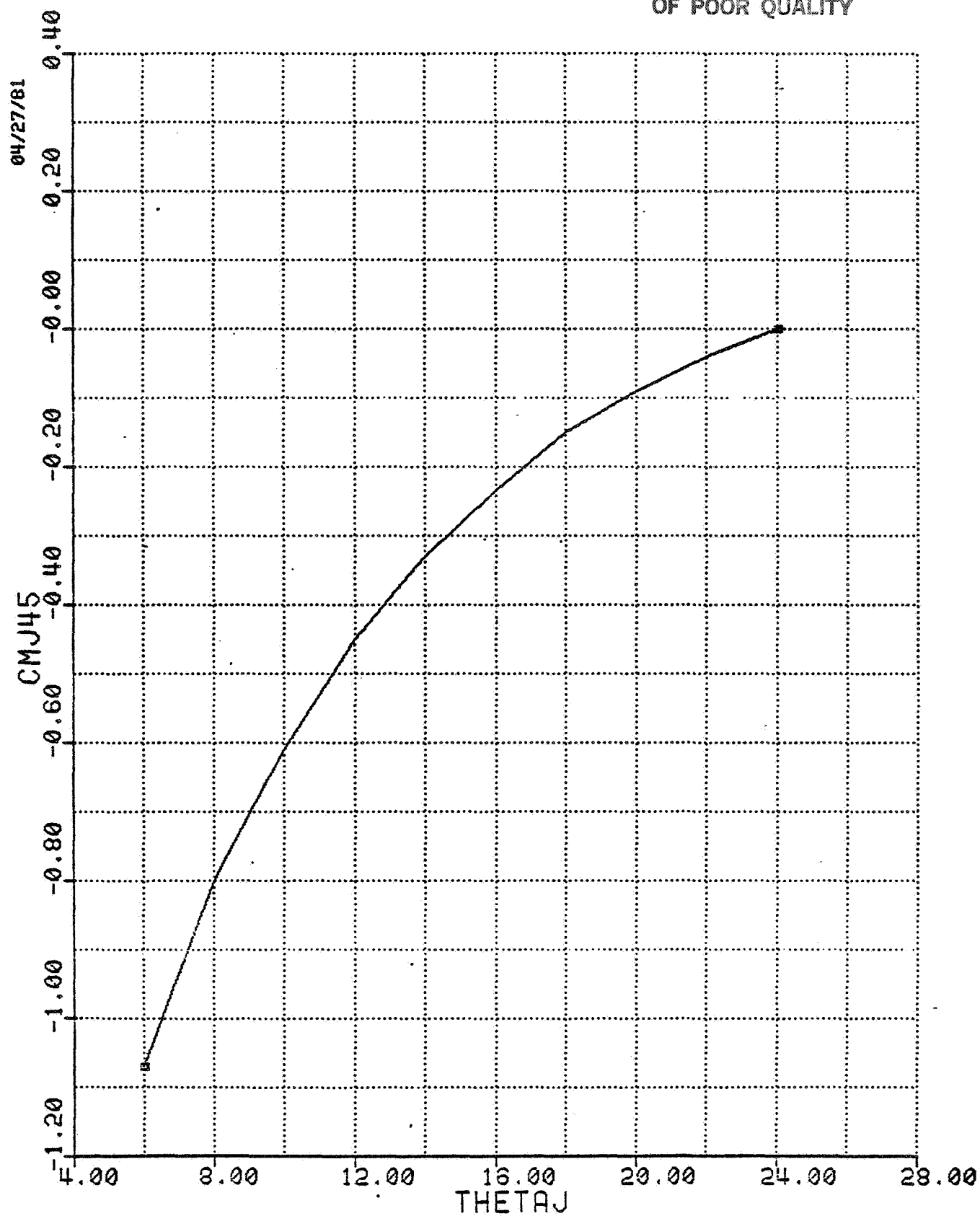
CMJ25 VS VEQ
FOR VARYING ALPHA
THETAJ= 10.00

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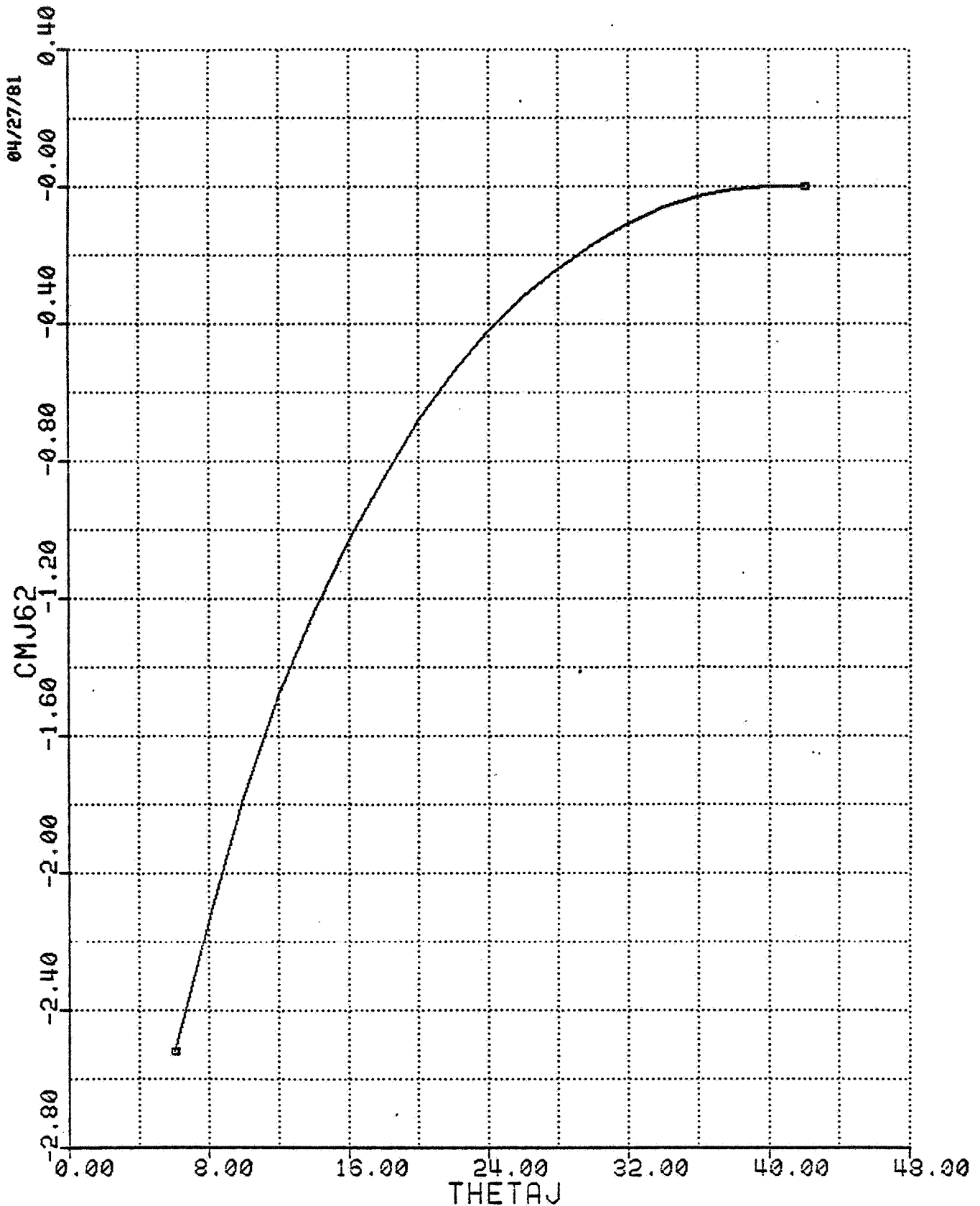
CMJ45 VS THETAJ ORIGINAL PAGE IS
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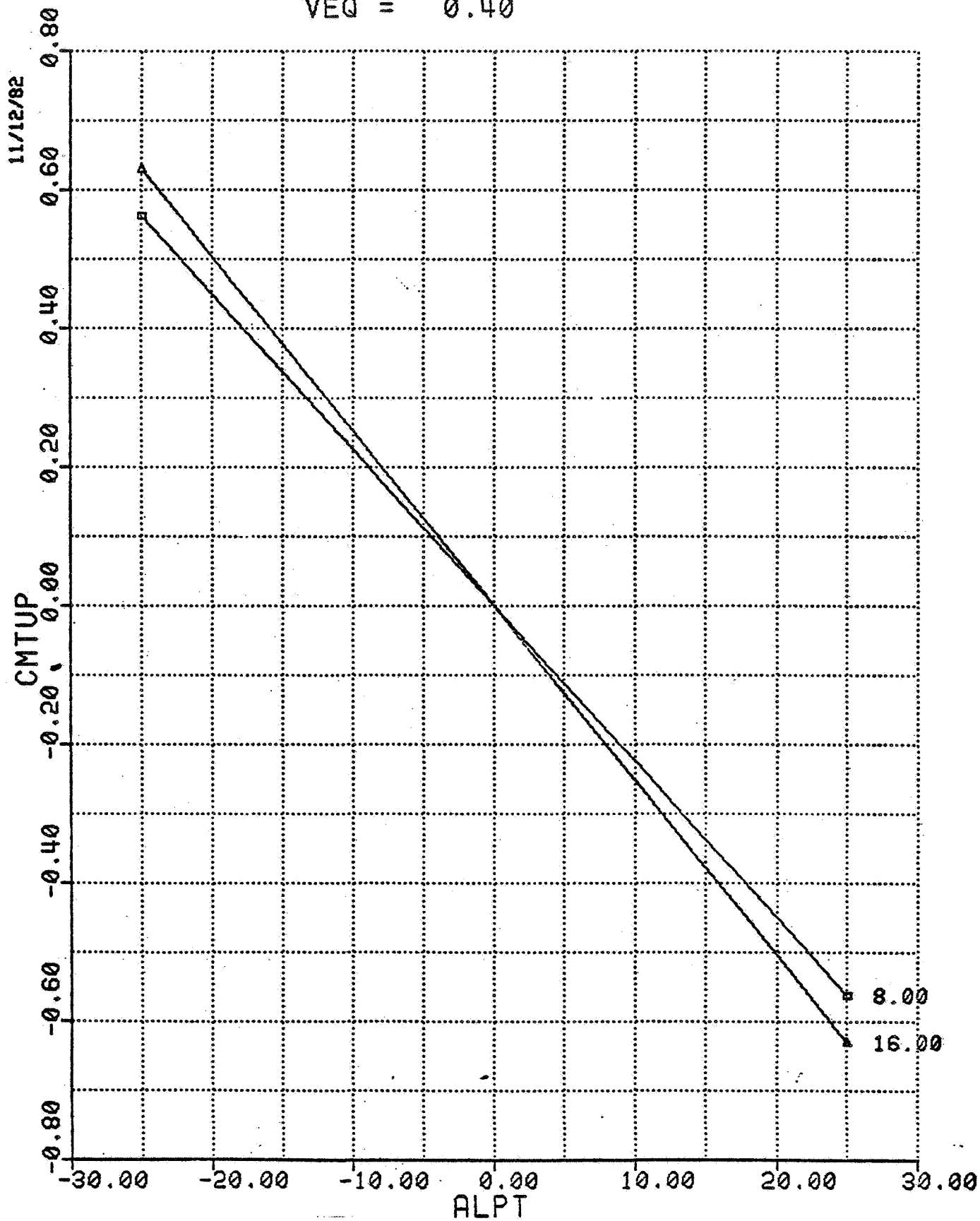
CMJ62 VS THETAJ



- C-5

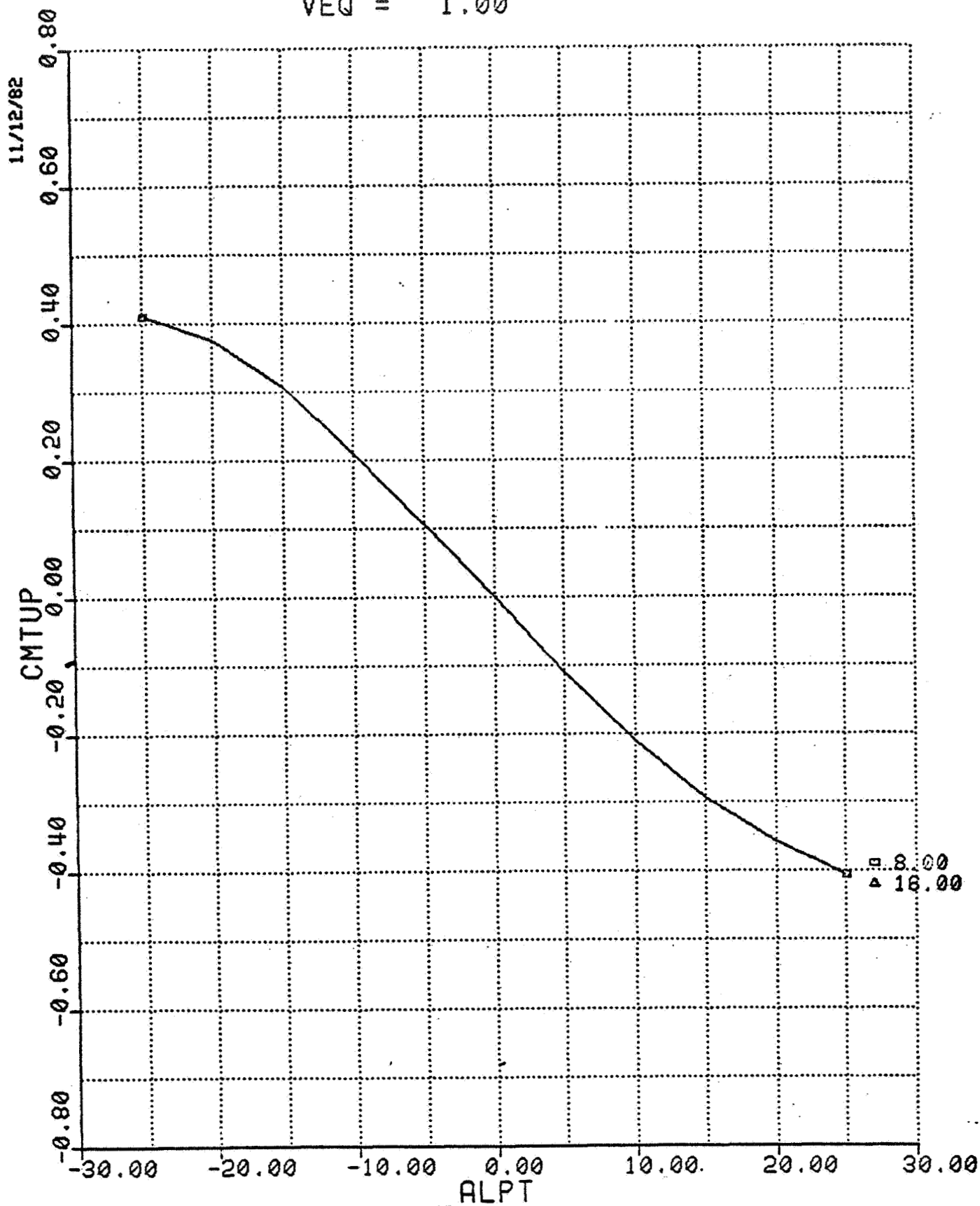
CMTUP VS ALPT
FOR VARYING ALPHA
VEQ = 0.40

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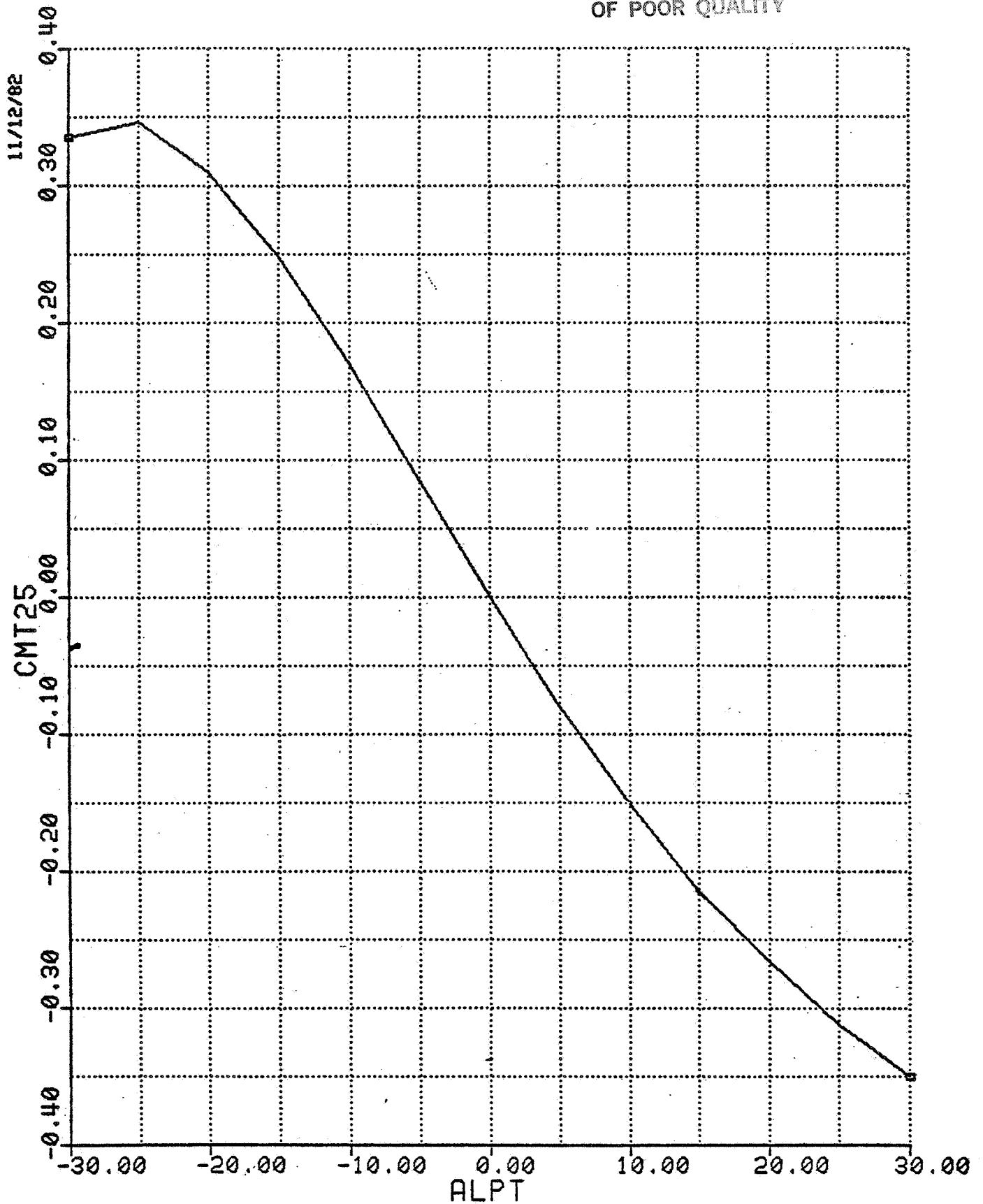


CMTUP VS ALPT
FOR VARYING ALPHA
VEQ = 1.00

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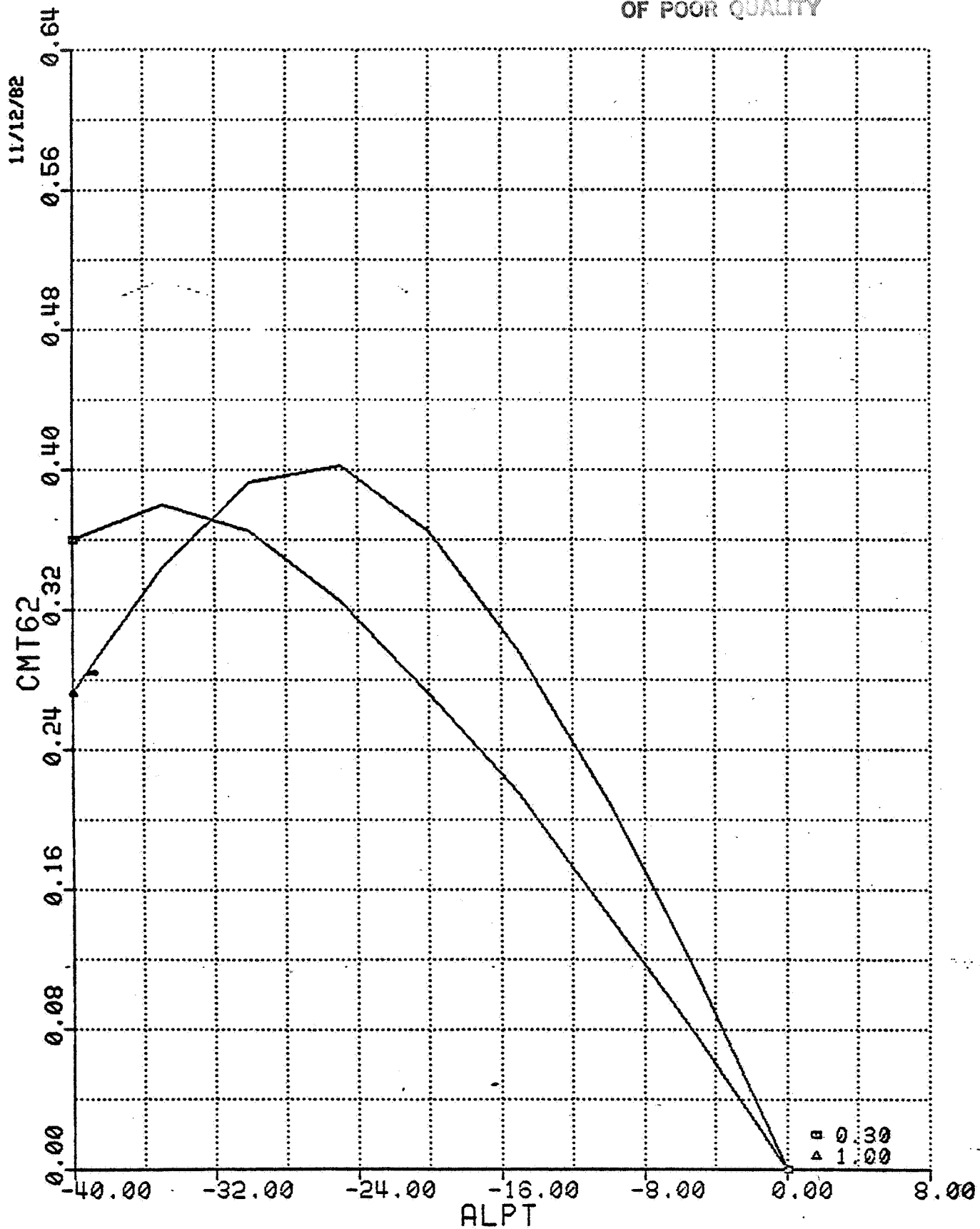


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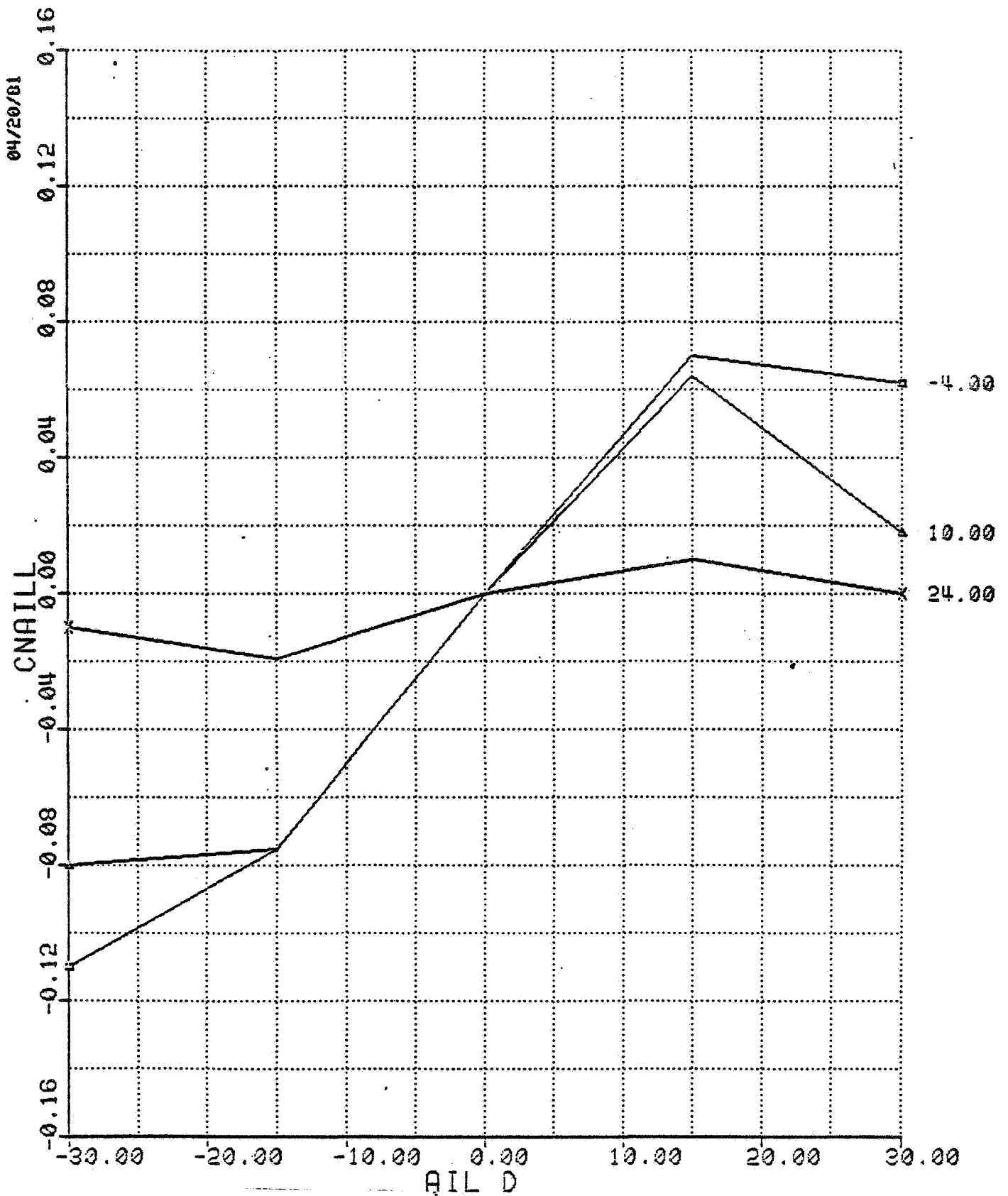
CMT62 VS ALPT
FOR VARYING VEQ

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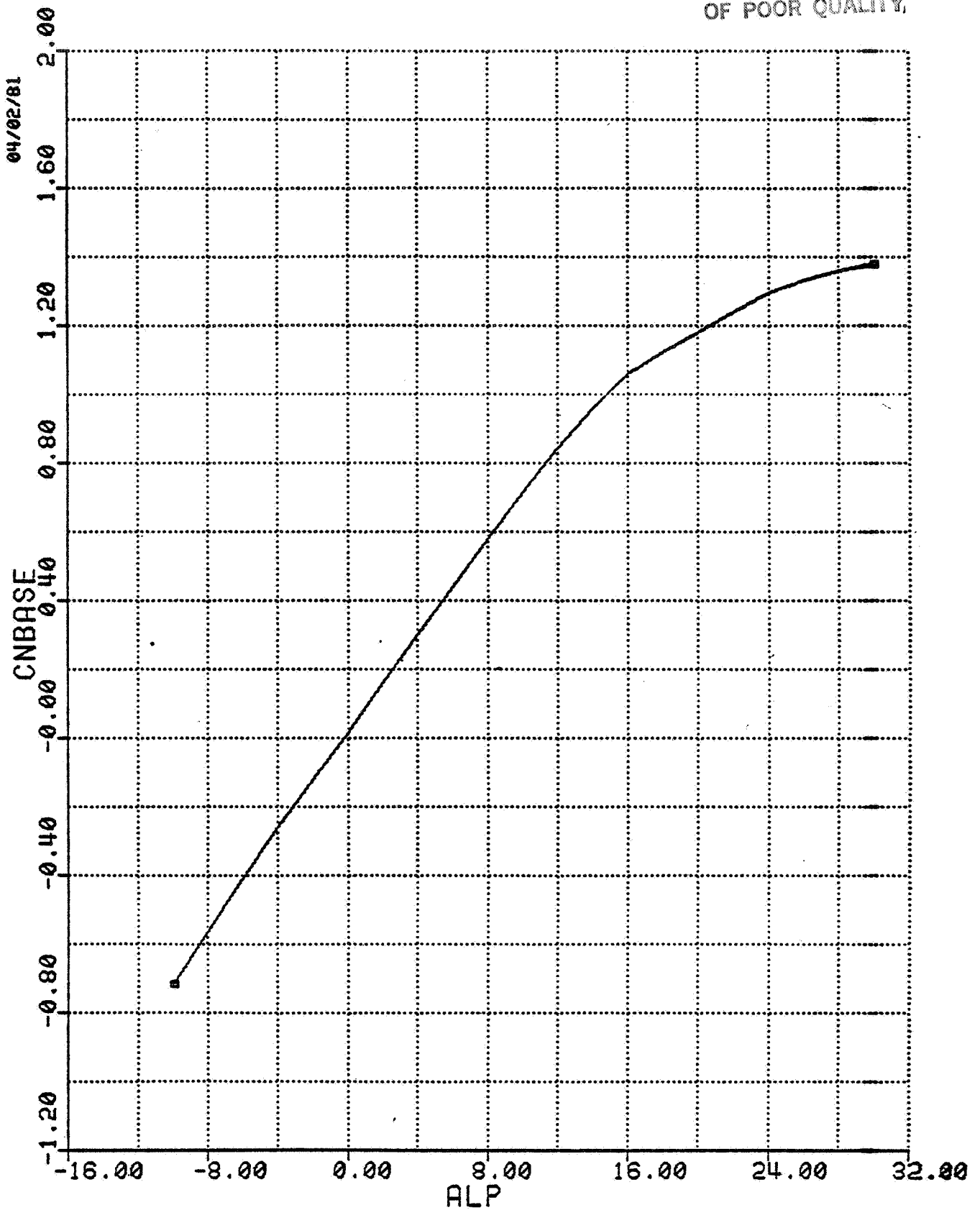
CNAILL VS AIL D
FOR VARYING ALPHA

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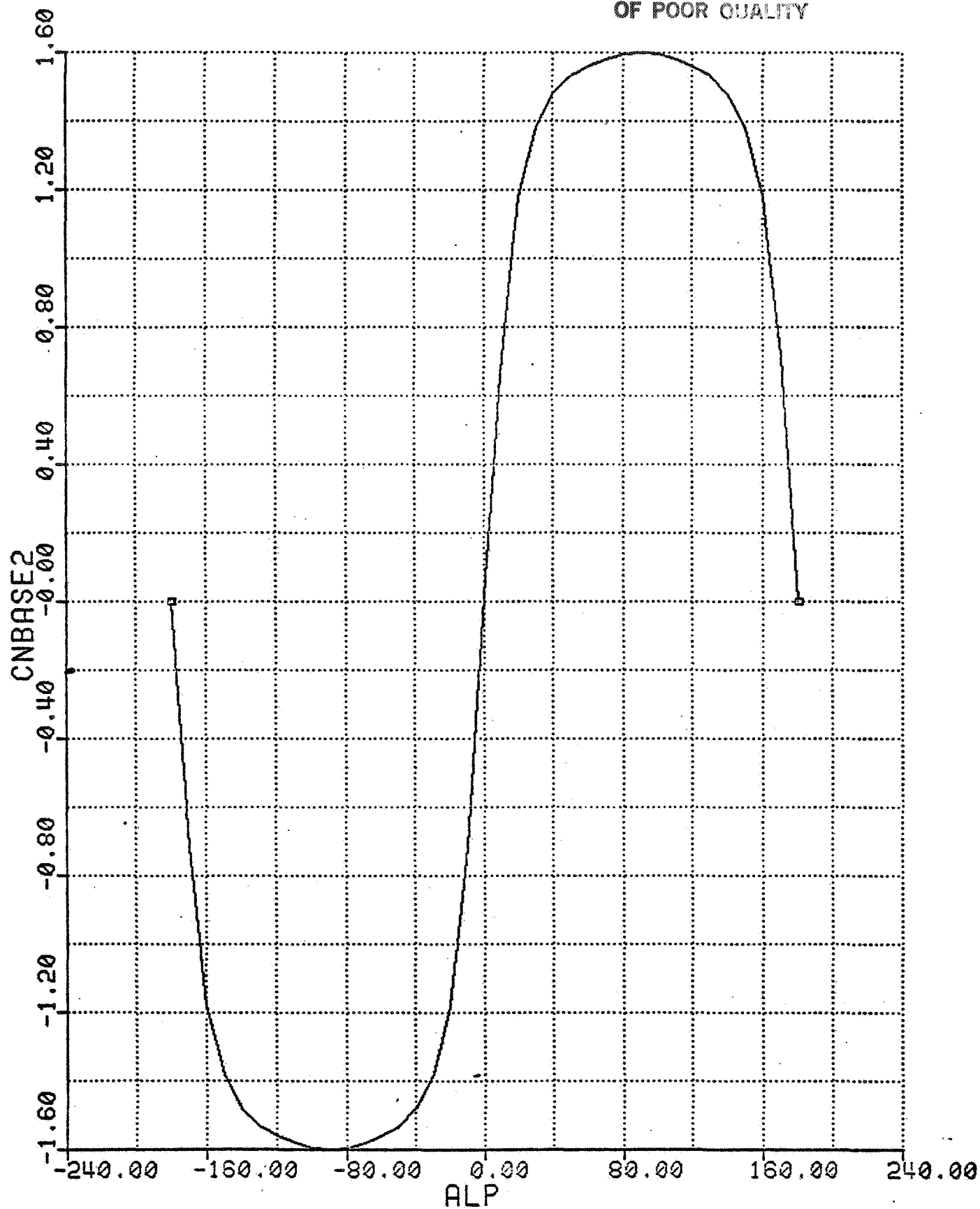
CNBASE VS ALP

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CNBASE2 VS ALP

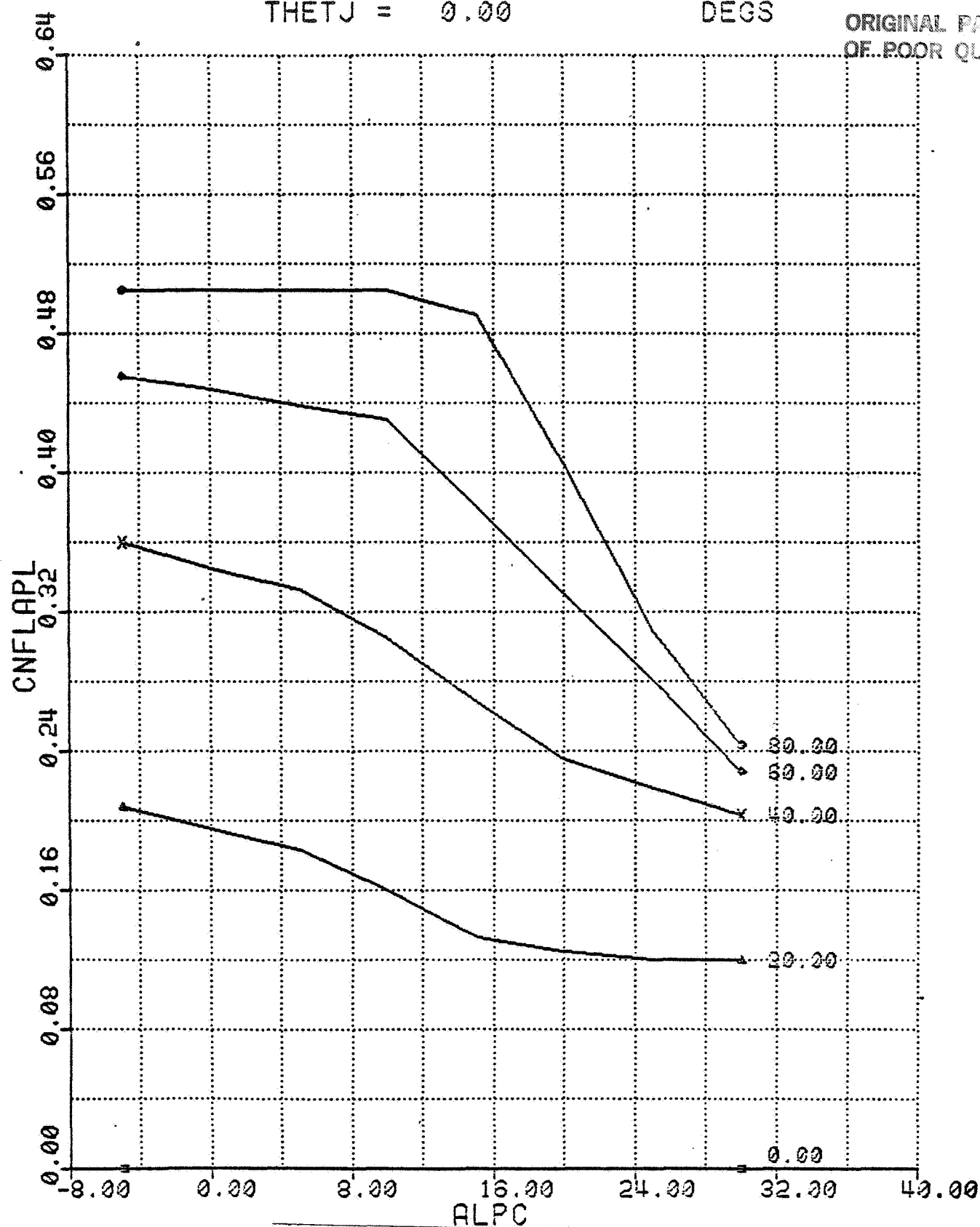
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CNFLAPL VS ALPC
FOR VARYING DFLAPL
THETJ = 0.00

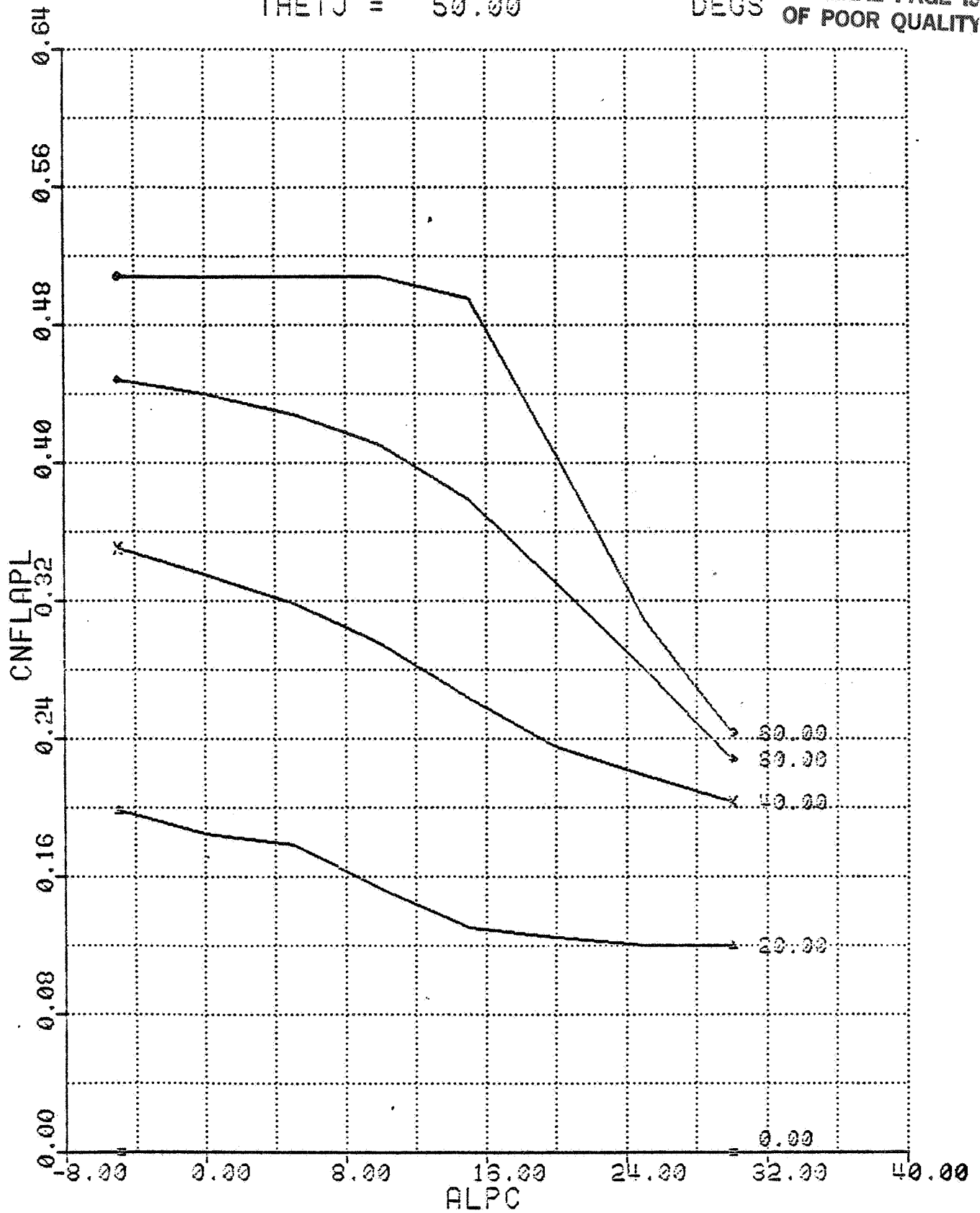
DEGS

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CNFLAPL VS ALPC
FOR VARYING DFLAPL
THETJ = 50.00

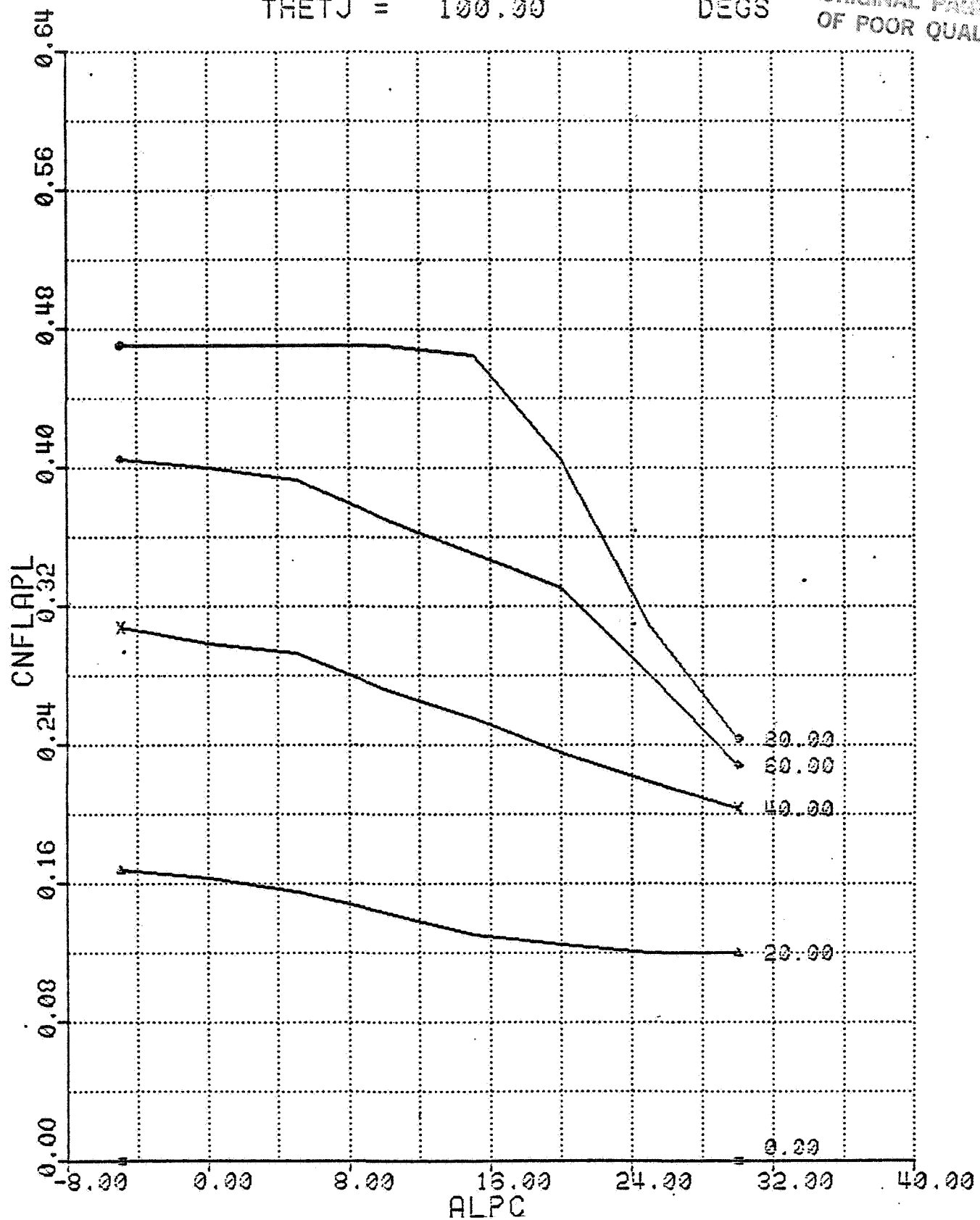
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CNFLAPL VS ALPC
FOR VARYING DFLAPL
THETJ = 100.00

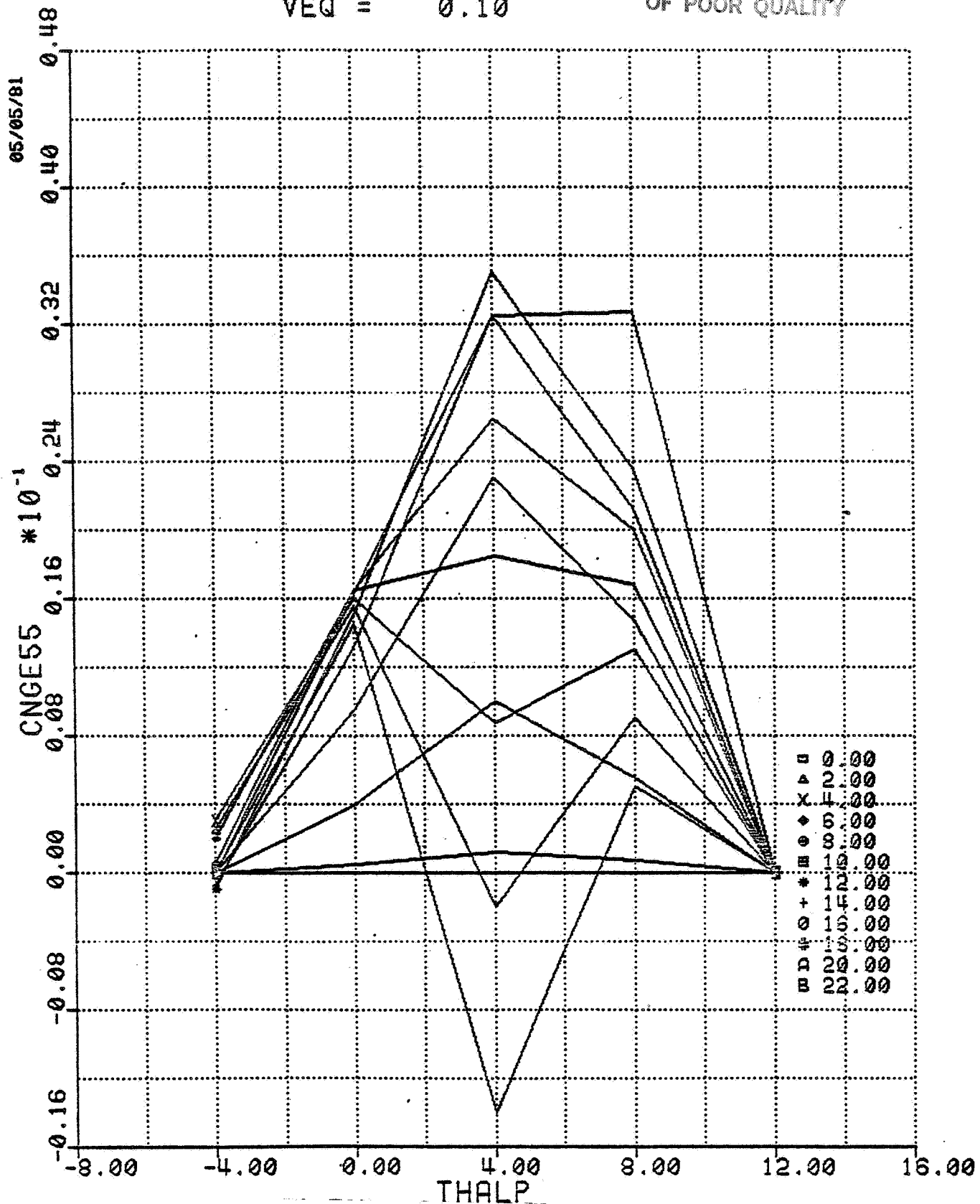
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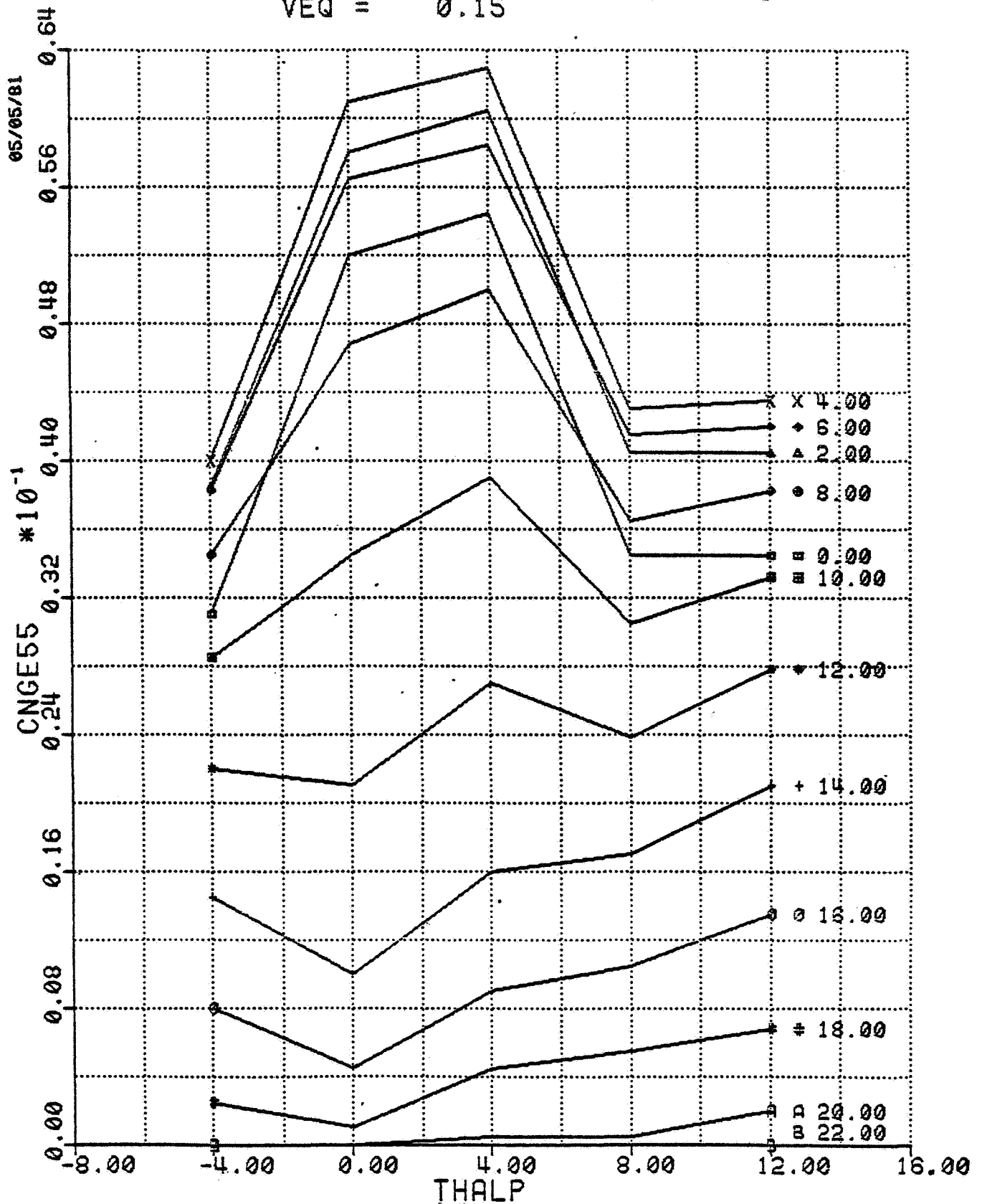
CNGE55 VS THALP
FOR VARYING HP
VEQ = 0.10

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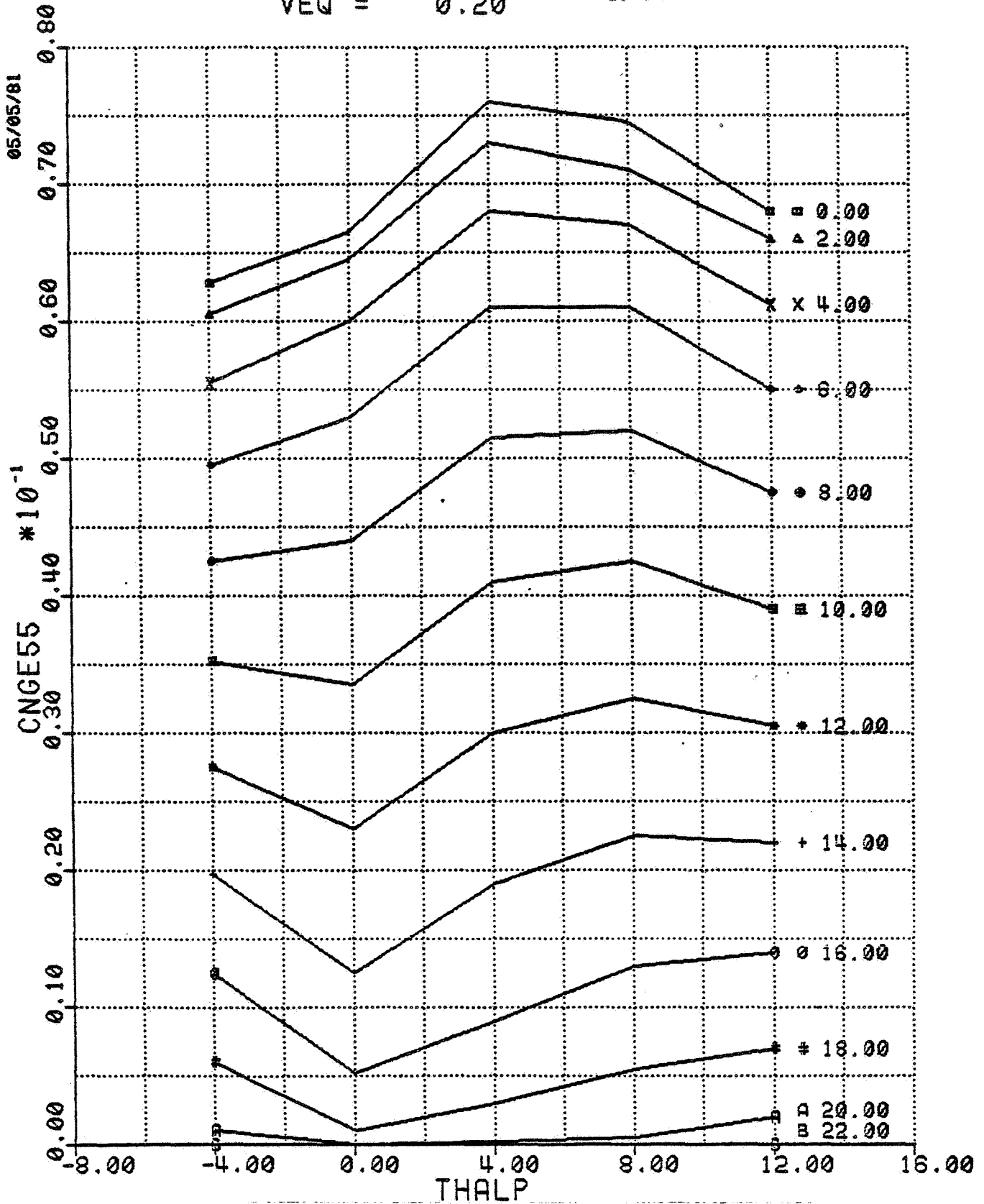
CNGE55 VS THALP
FOR VARYING HP
VEQ = 0.15

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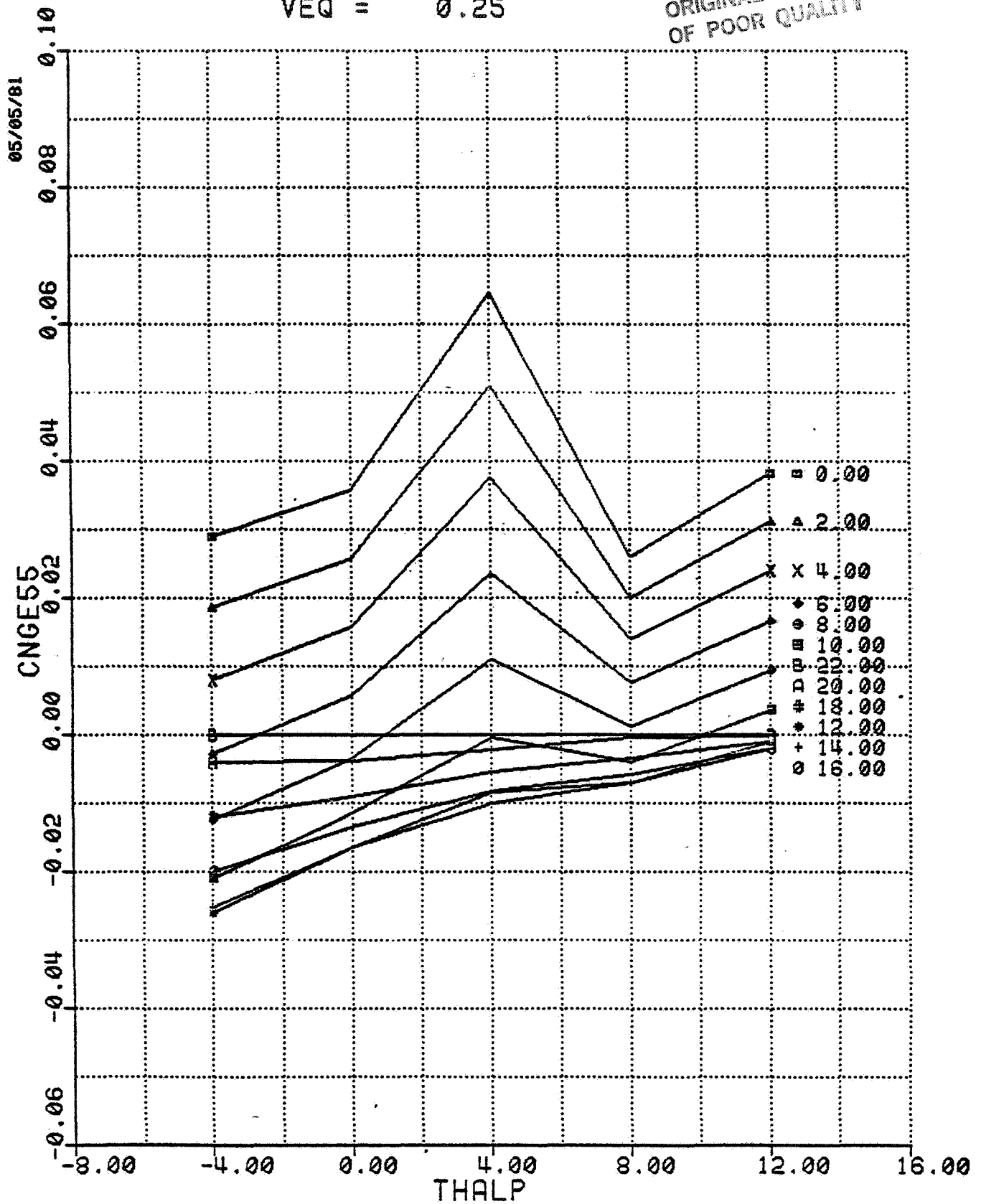
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FOR VARYING HP
VEQ = 0.20

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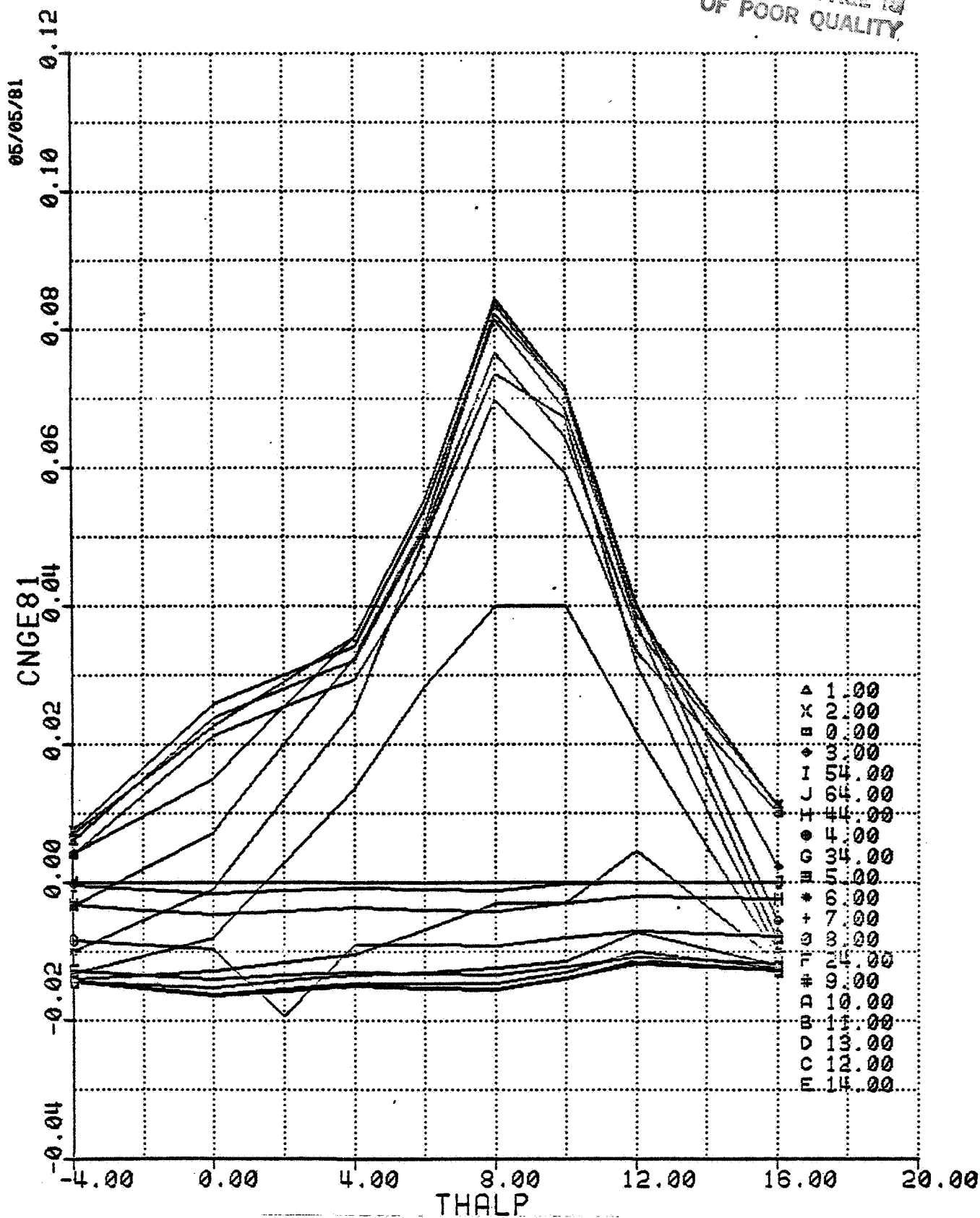
CNGE55 VS THALP
FOR VARYING HP
VEQ = 0.25

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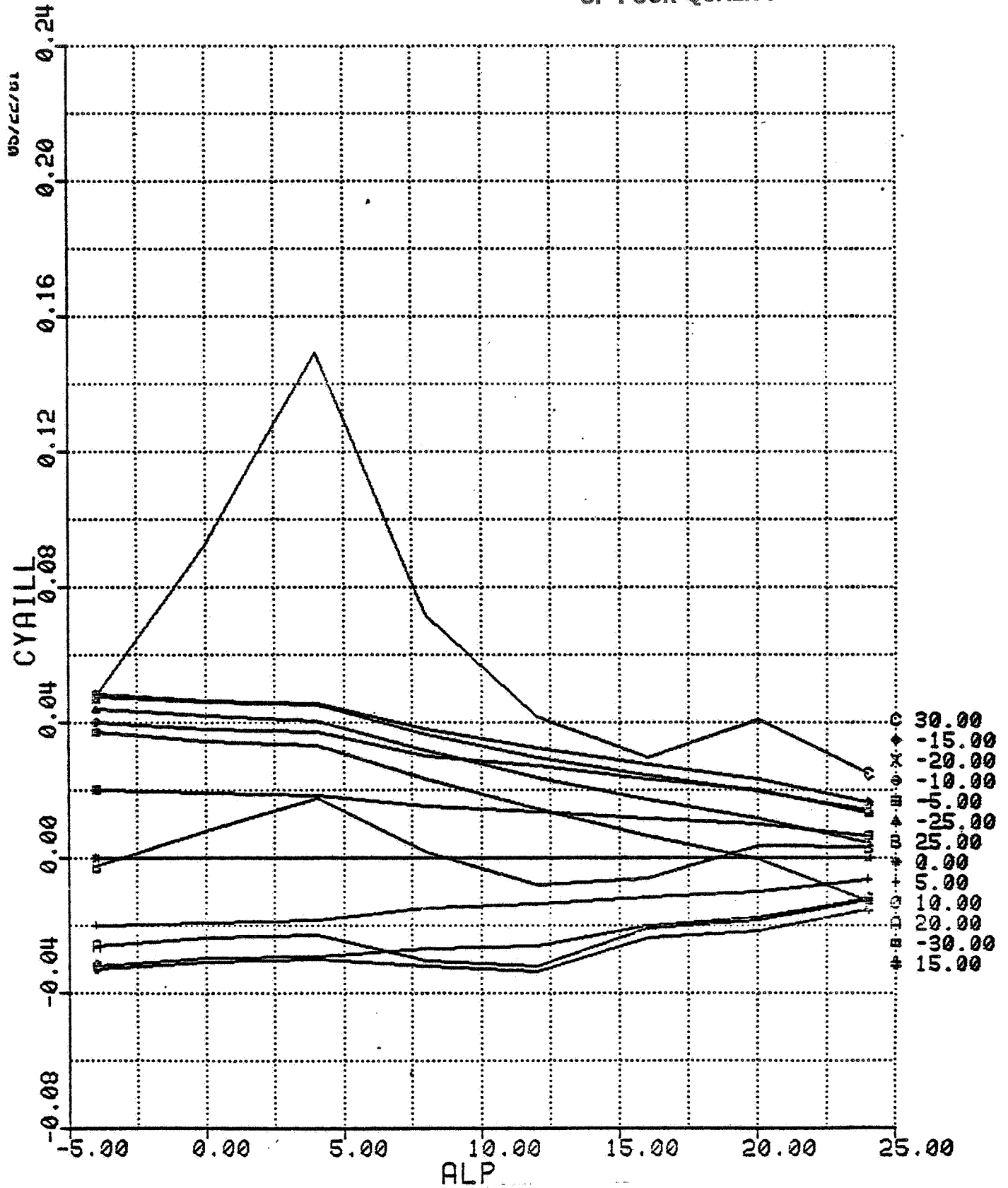


CNGE81 VS THALP
FOR VARYING HP

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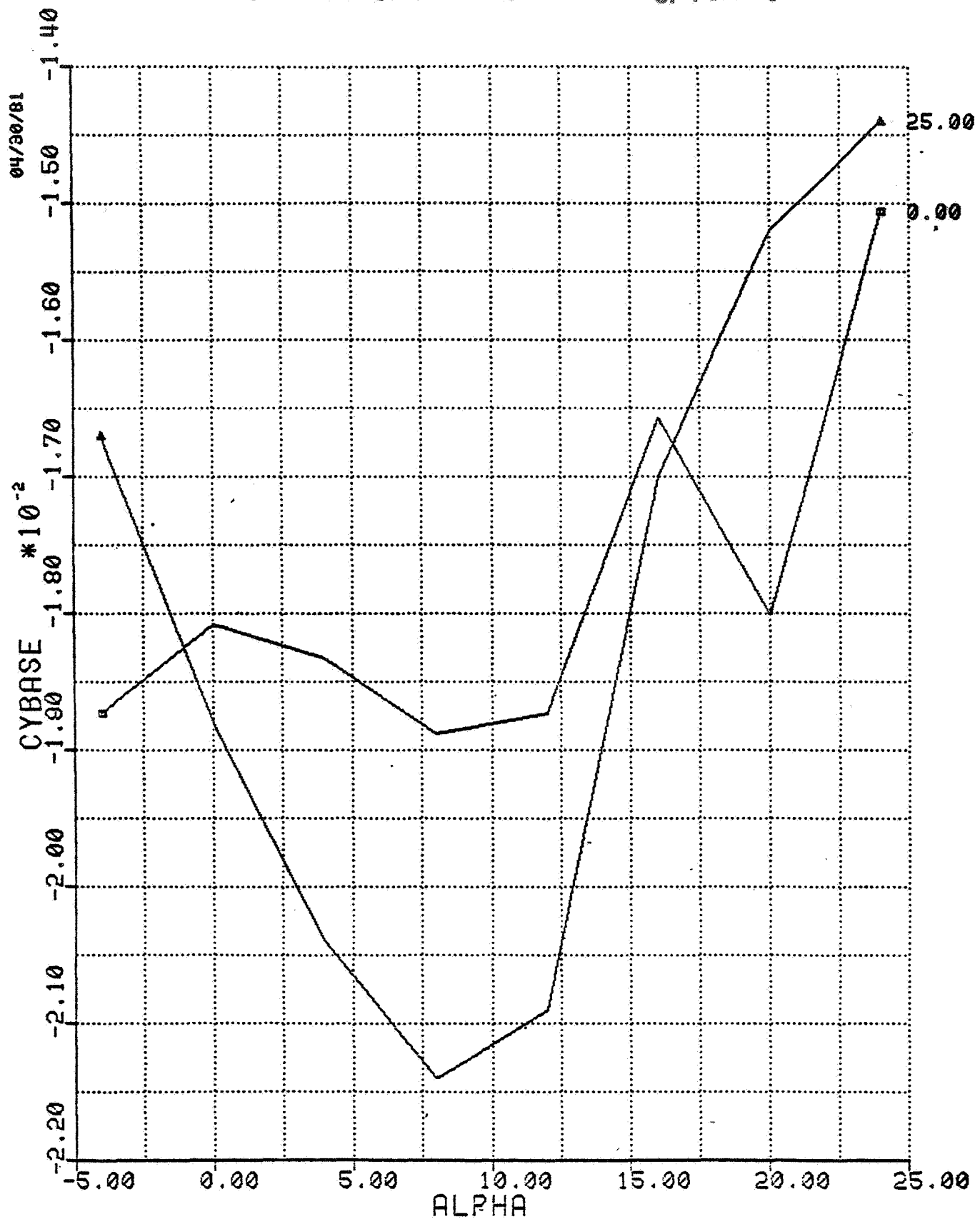


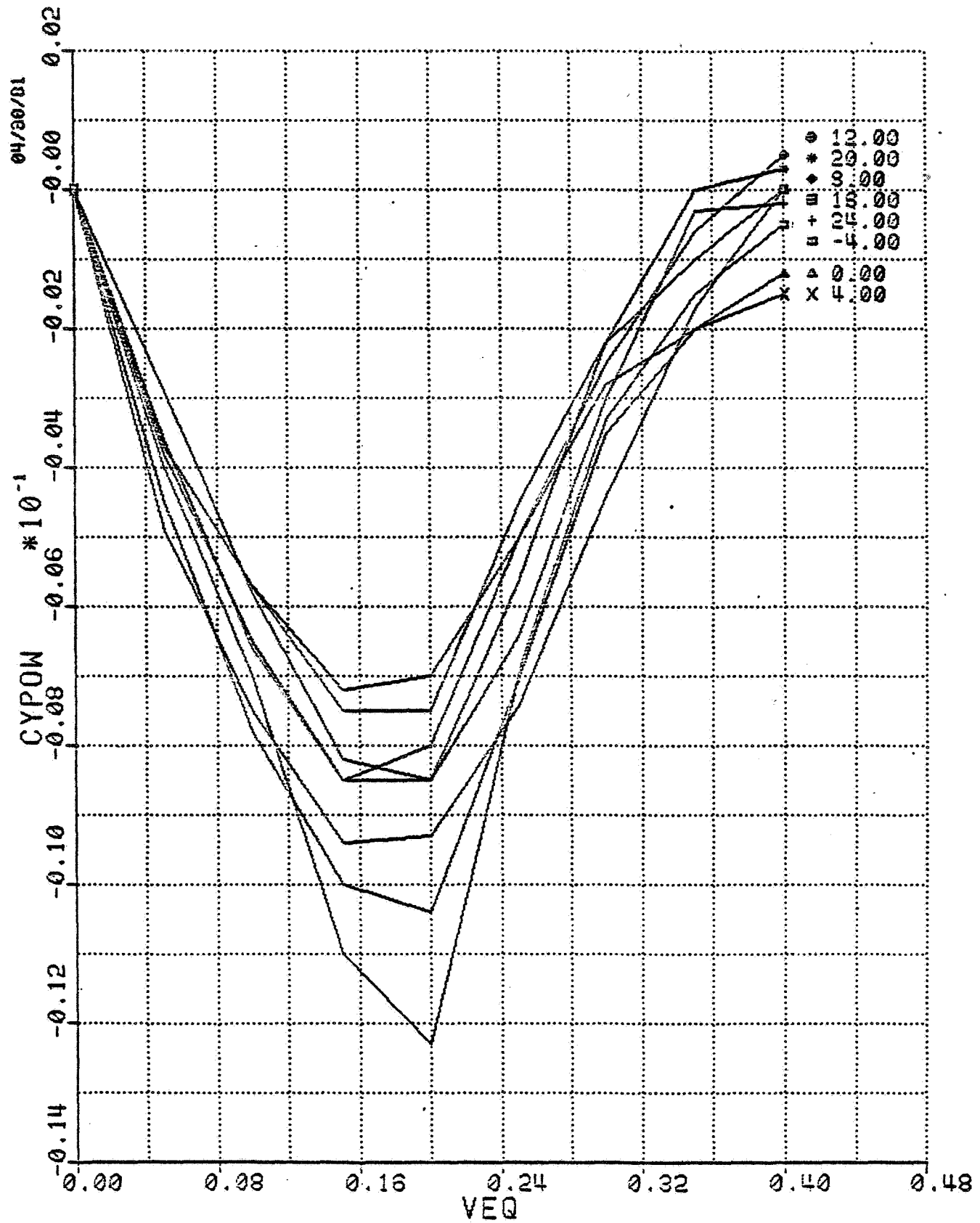
CYAILL VS ALP
FOR VARYING DAL ORIGINAL PAGE 13
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CYBASE VS ALPHA
FOR VARYING FLAP

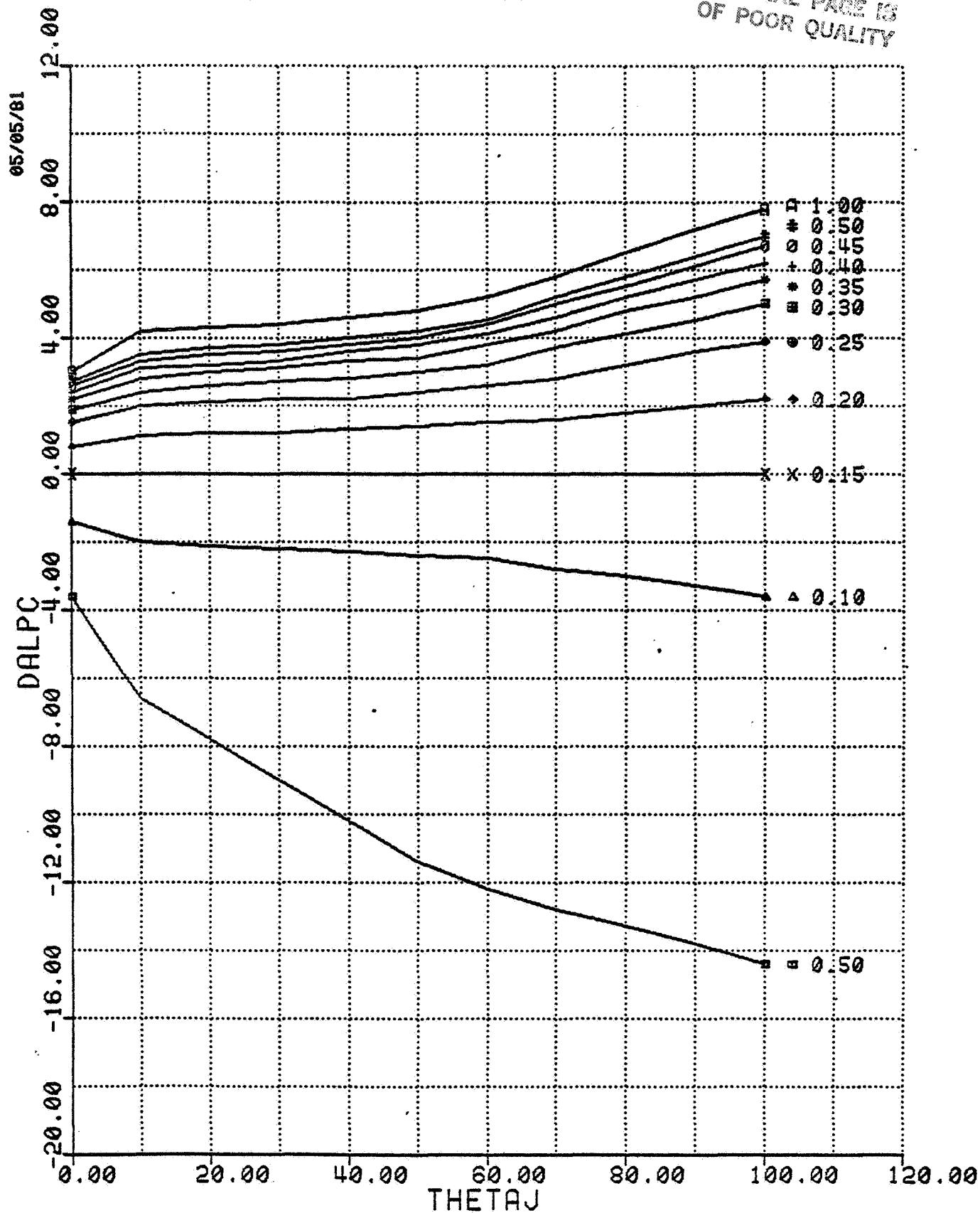
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CYPQW VS VEQ
FOR VARYING ALPHAORIGINAL PAGE IS
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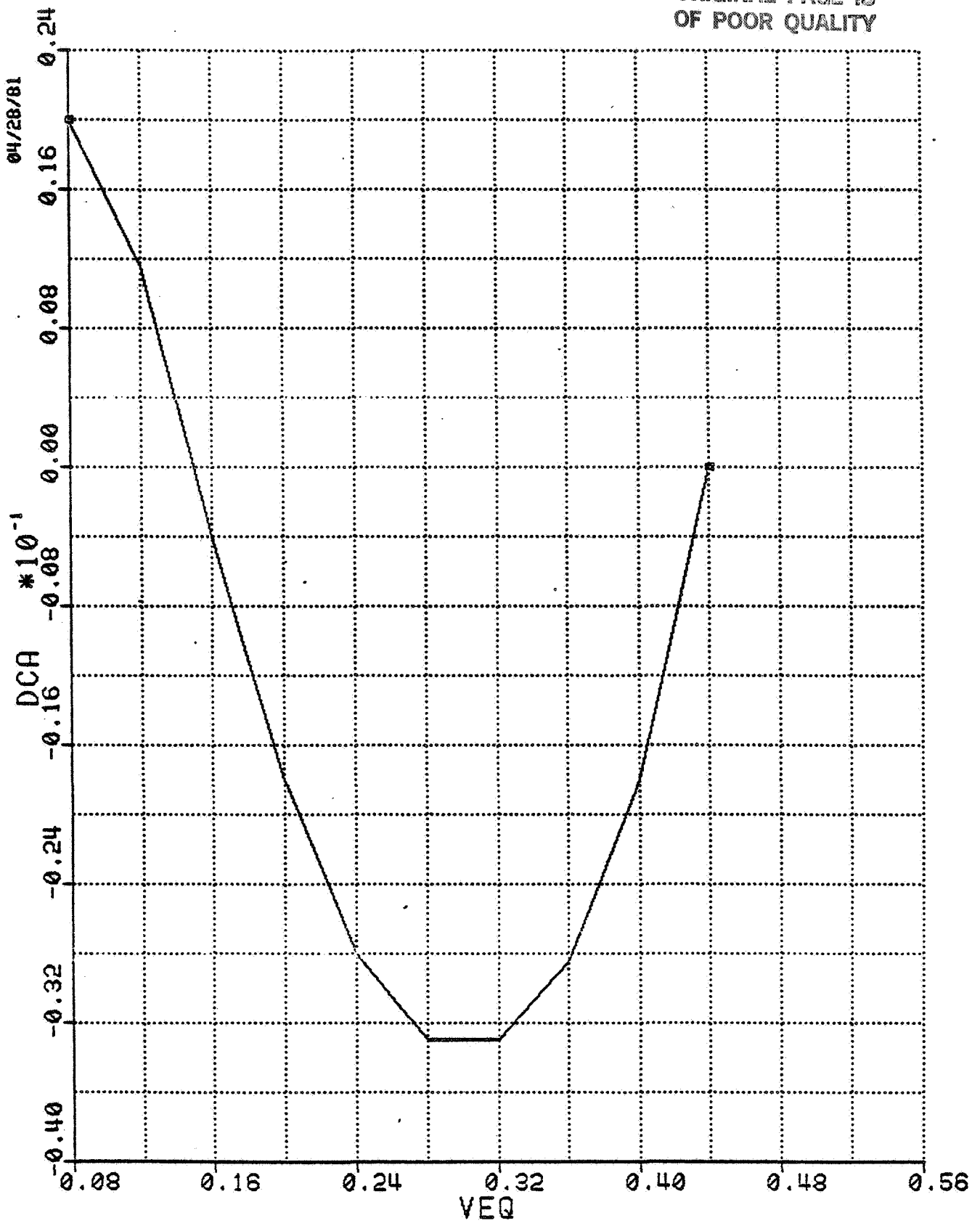
DALPC VS THETAJ FOR VARYING VEQ

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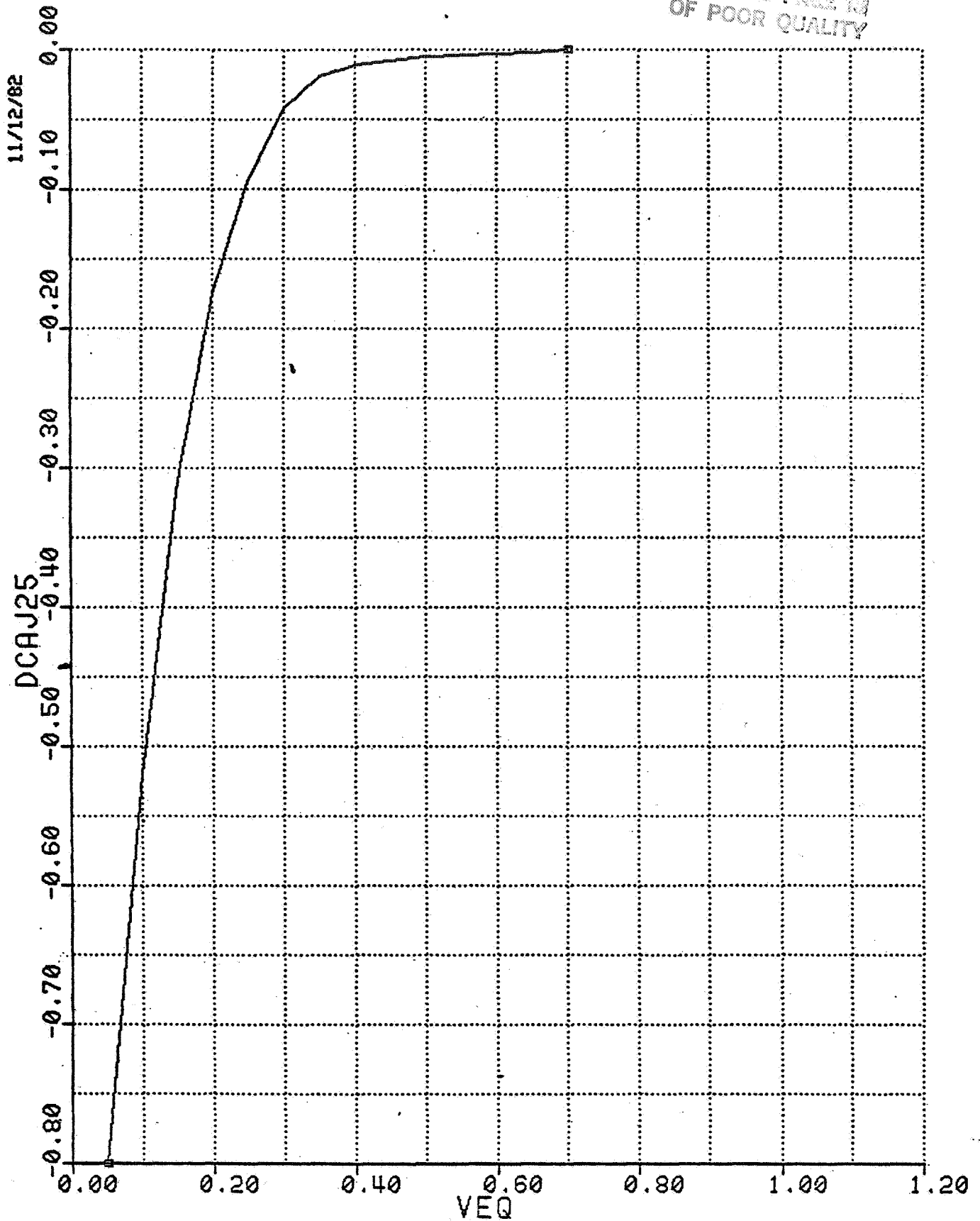
DCA VS VEQ

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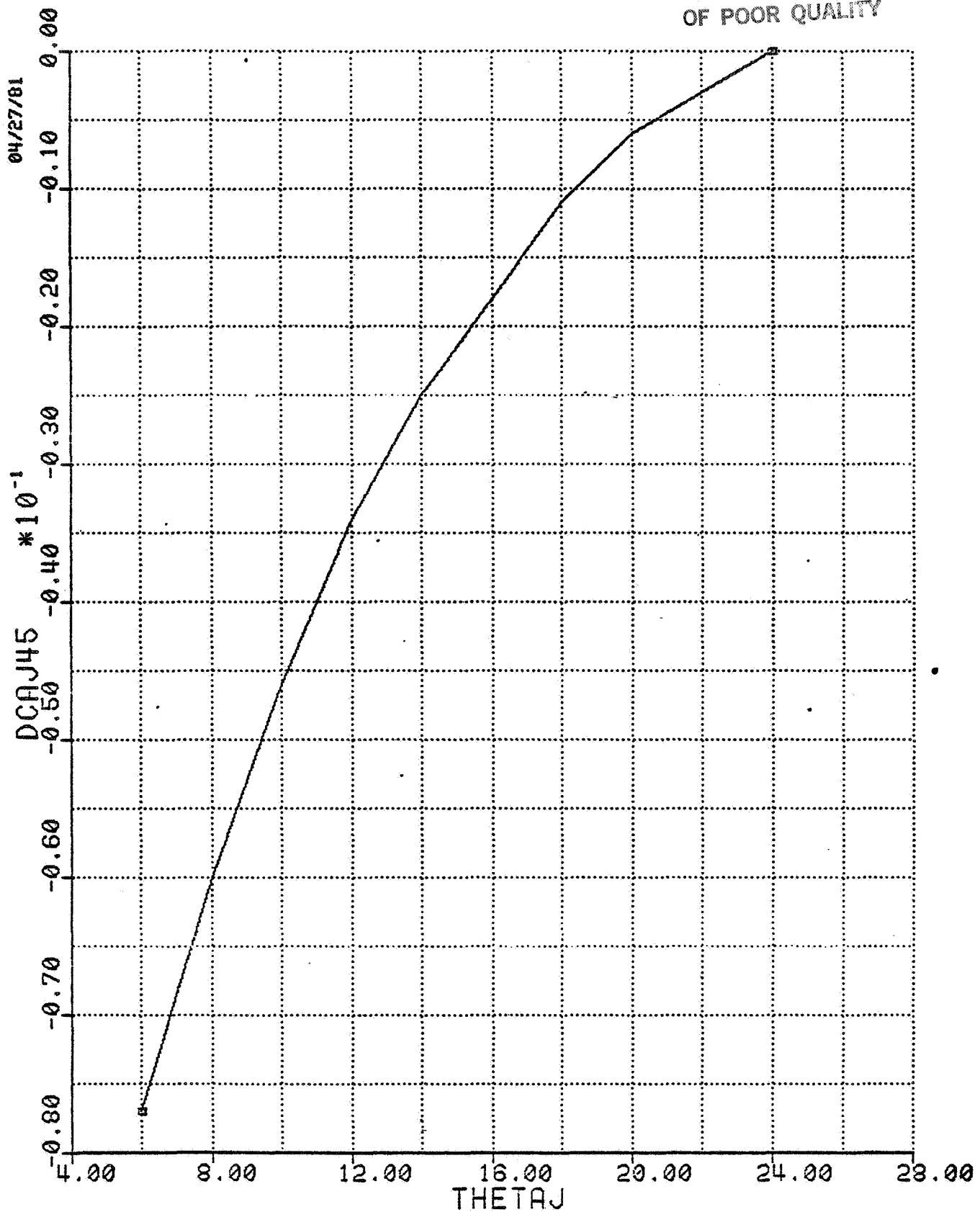
DCAJ25 VS VEQ

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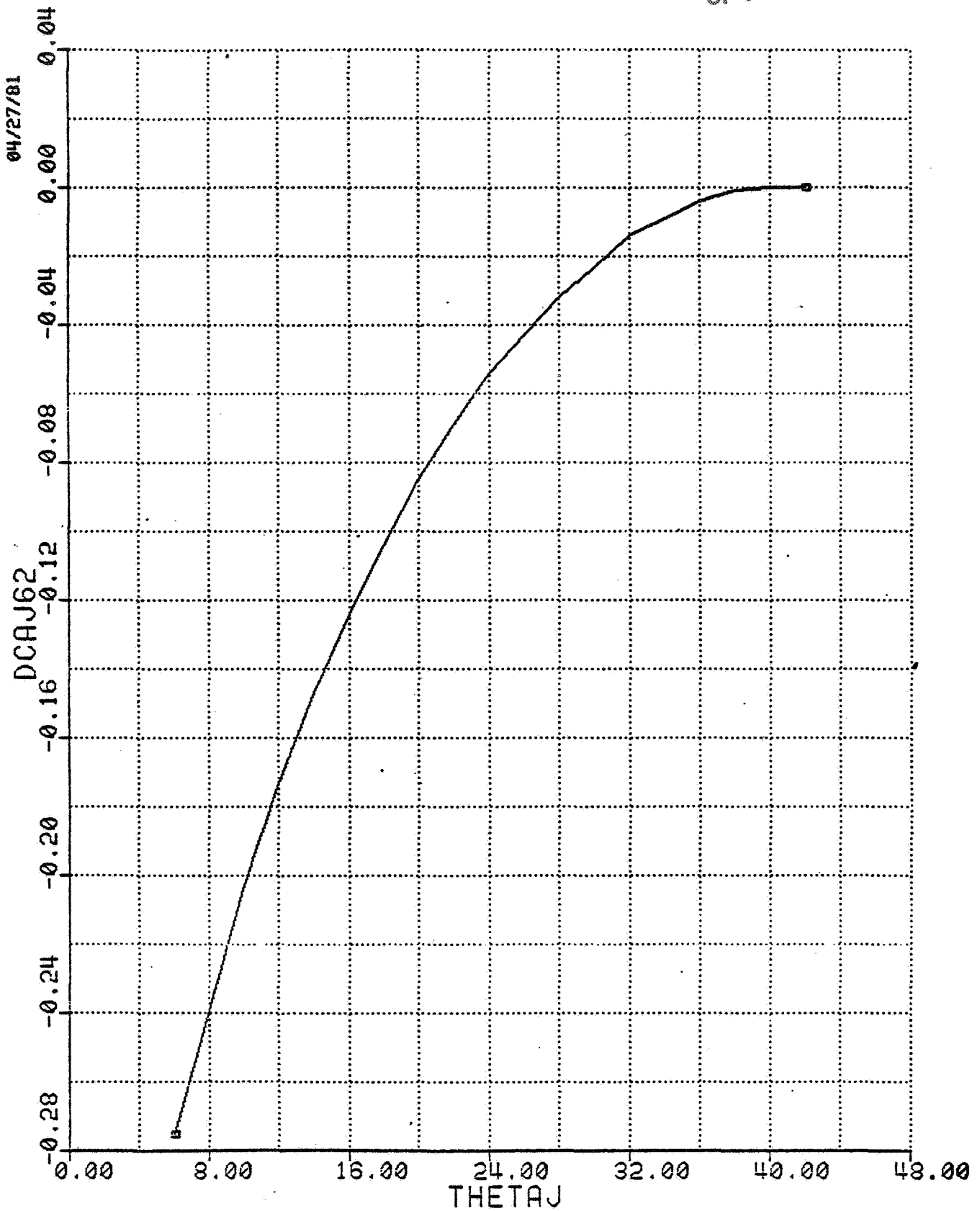


DCAJ45 VS THETAJ

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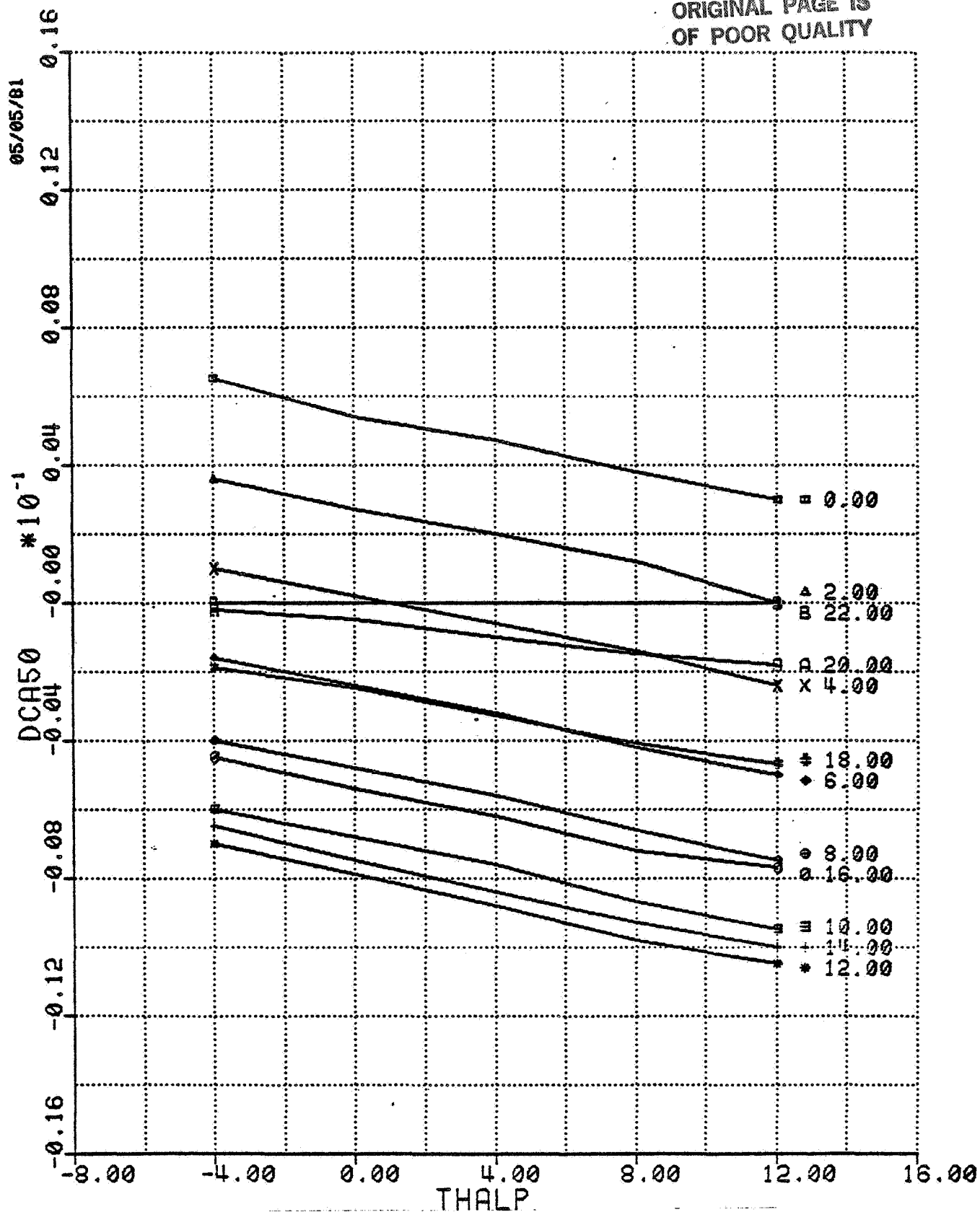


DCAJ62 VS THETAJ

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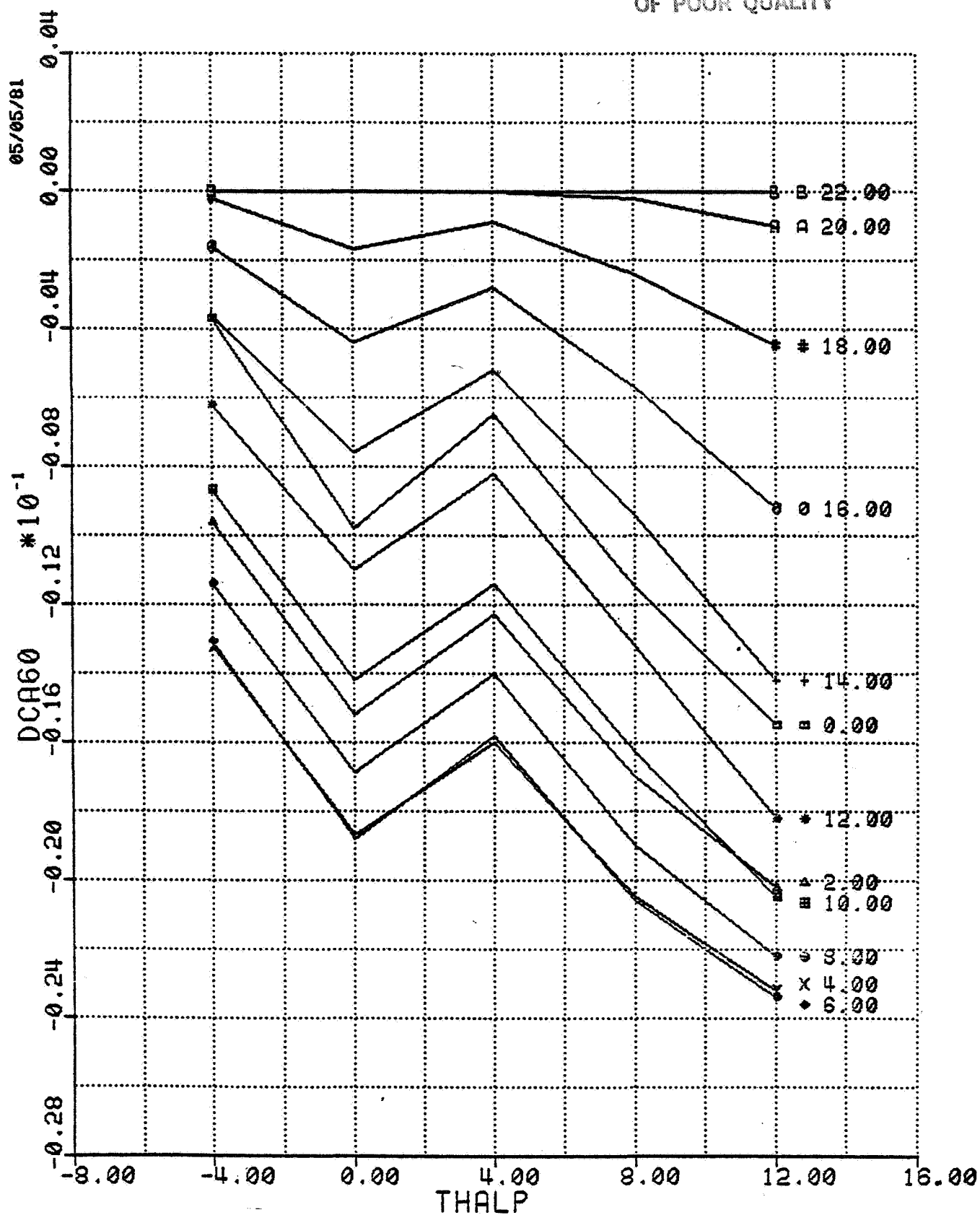
DCA50 VS THALP FOR VARYING HP

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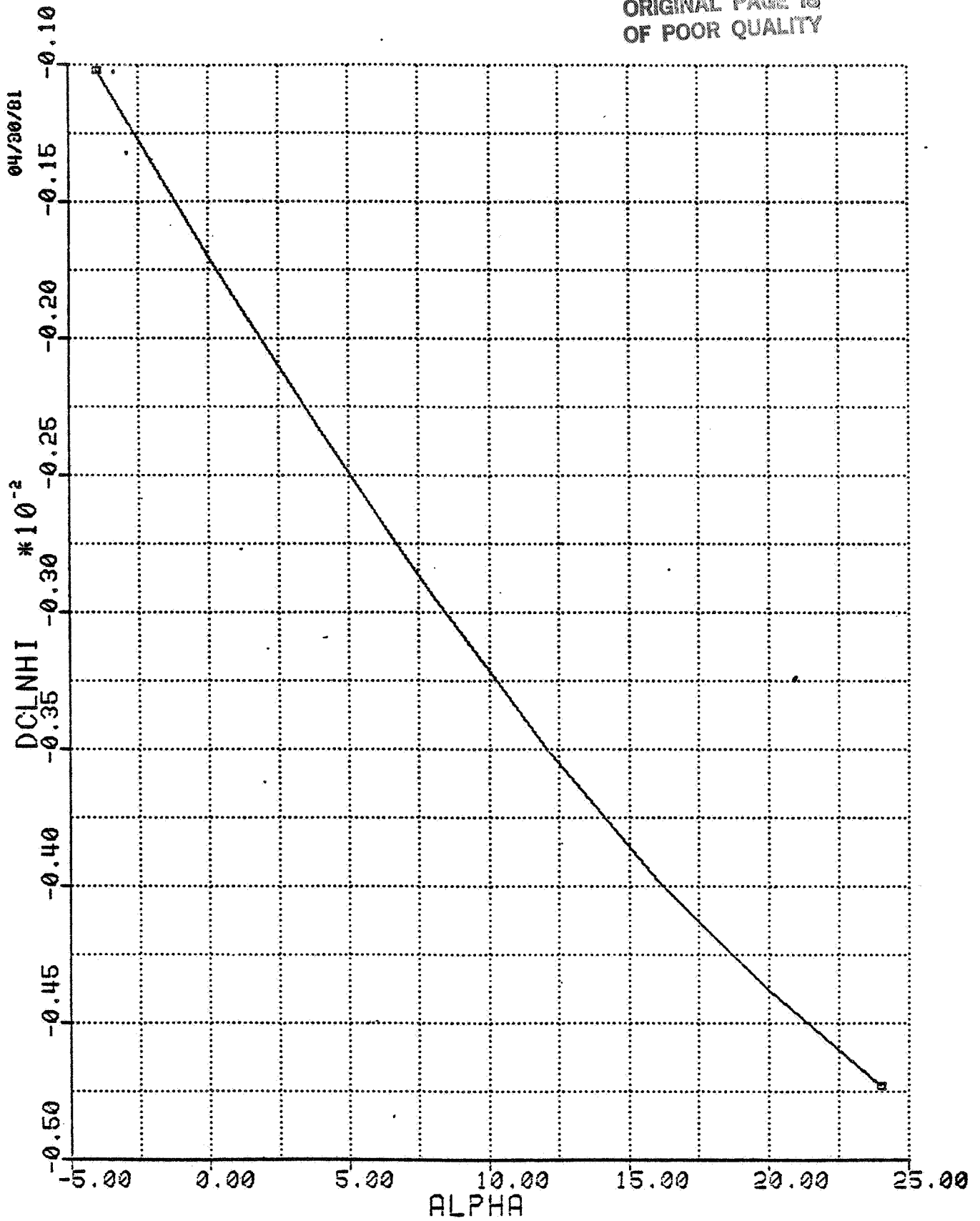
DCA60 VS THALP
FOR VARYING HP

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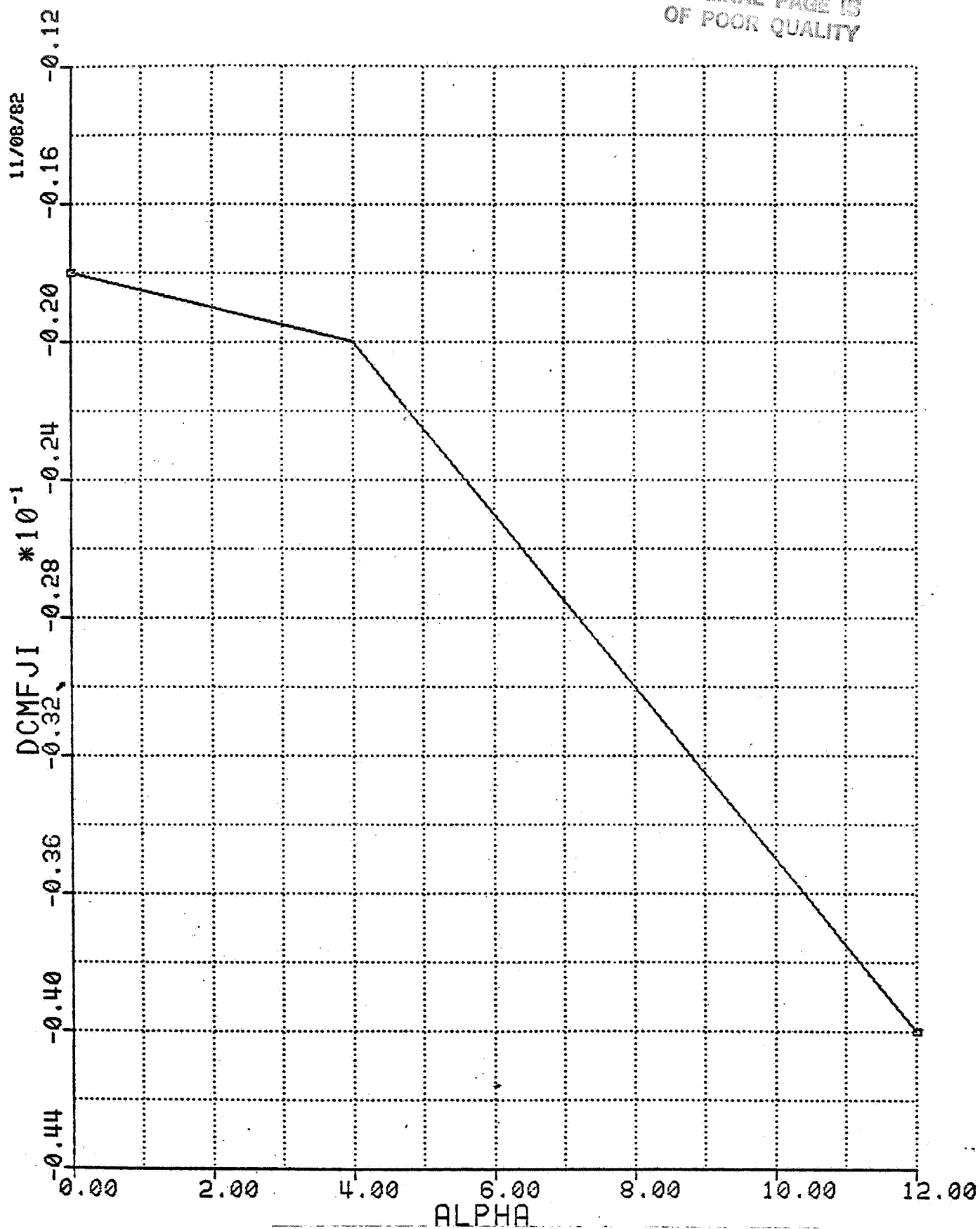
DCLNHI VS ALPHA

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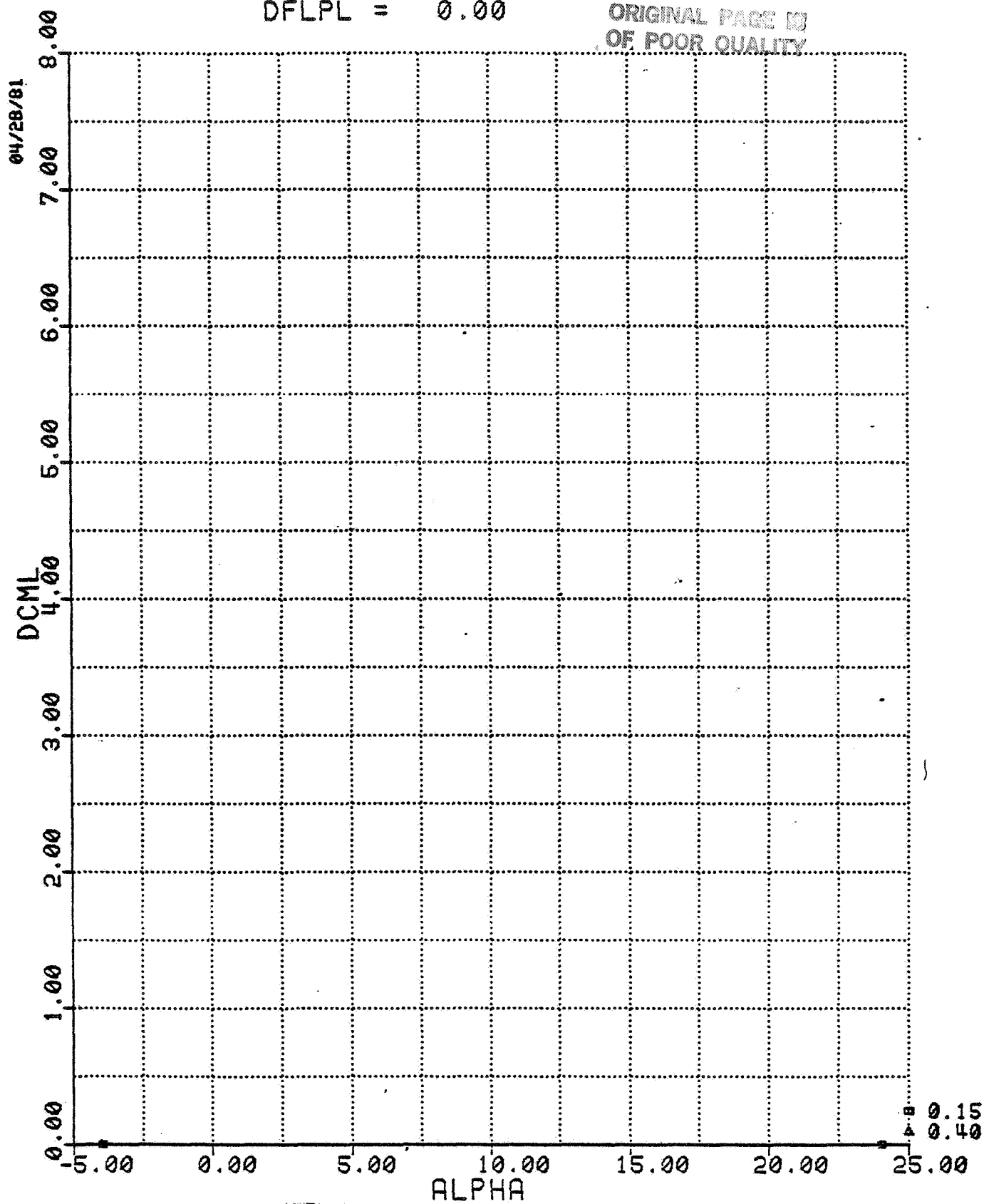
DCMFJI VS ALPHA

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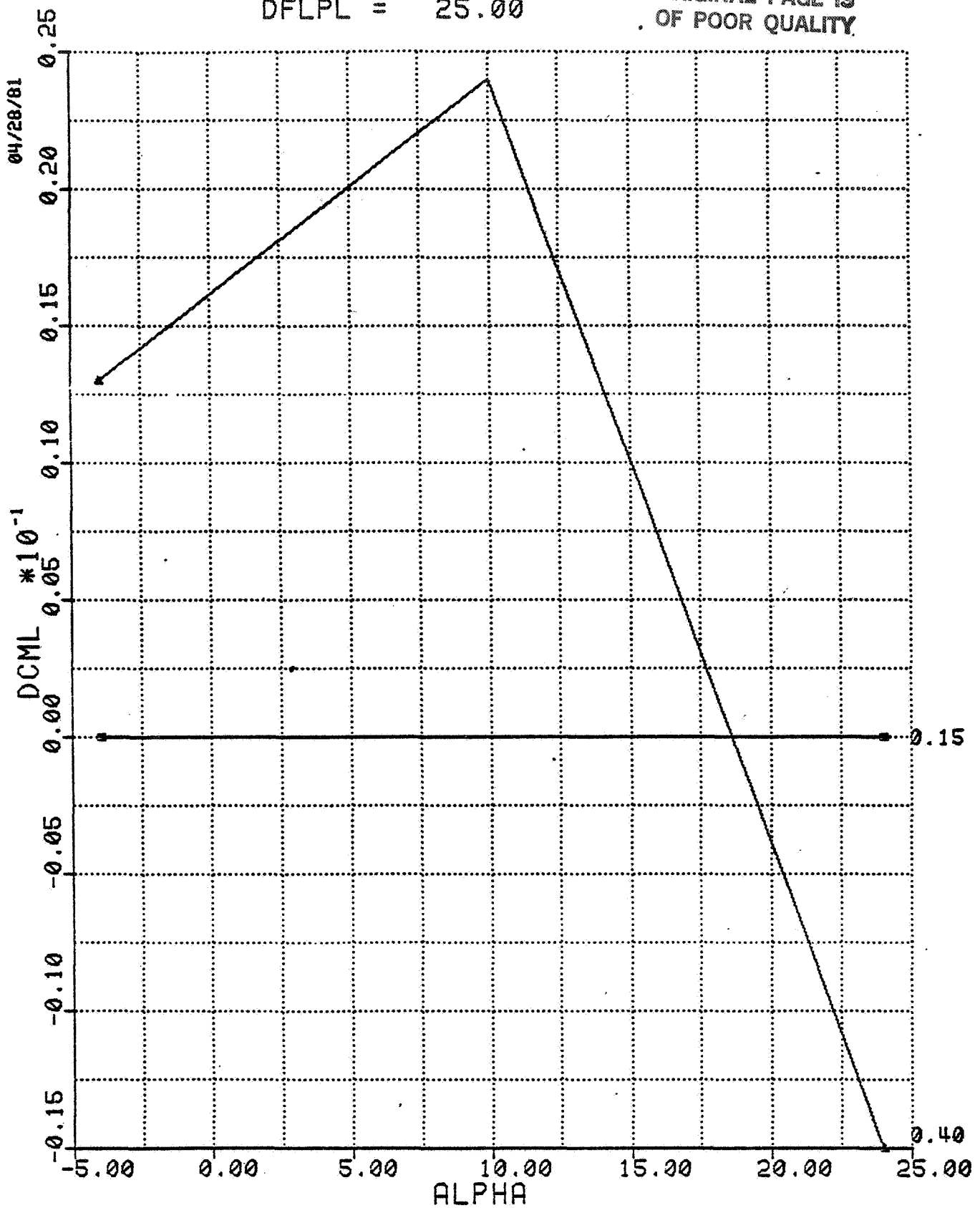
DCML VS ALPHA
FOR VARYING VEQ
DFLPL = 0.00

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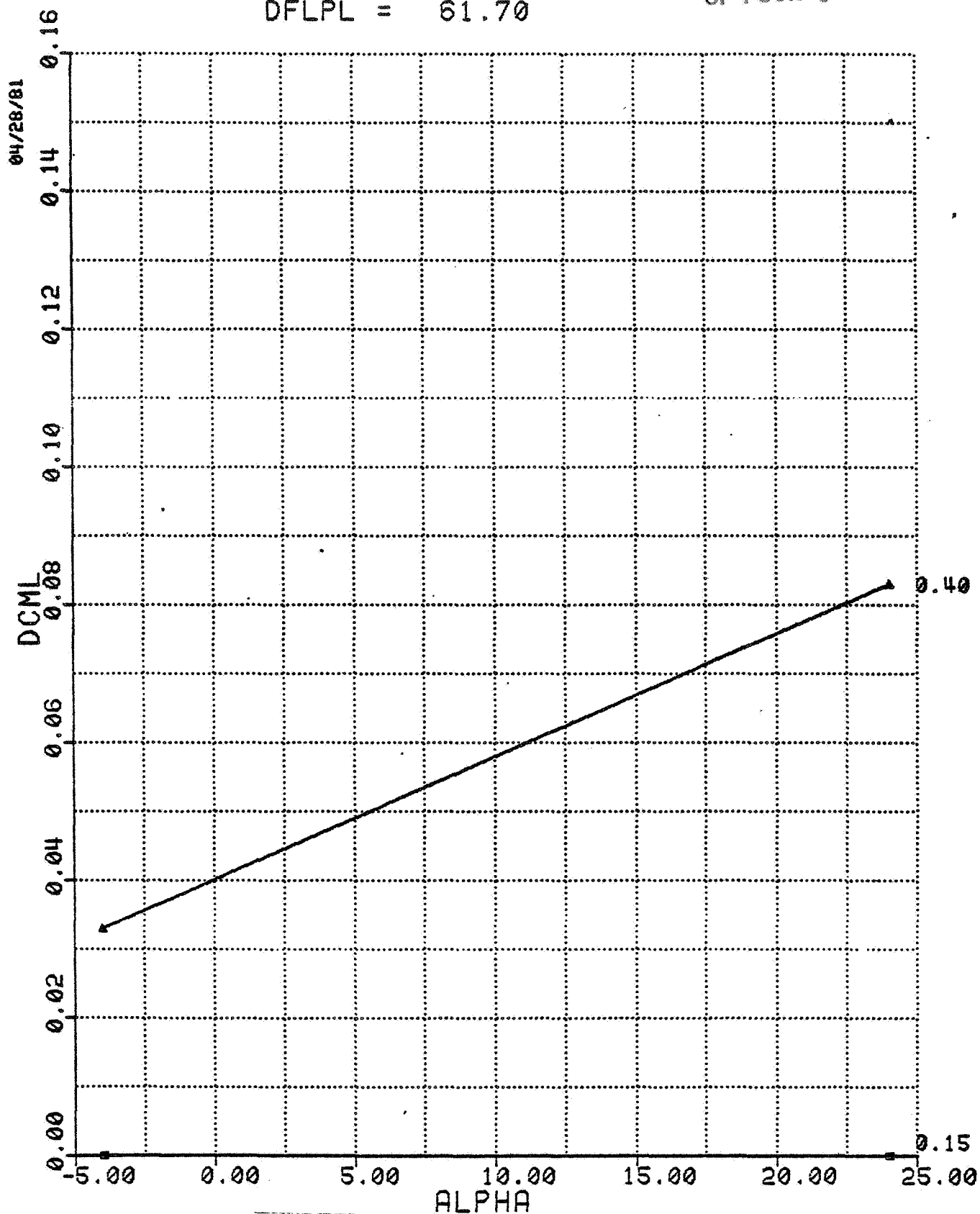
DCML VS ALPHA
FOR VARYING VEQ
DFLPL = 25.00

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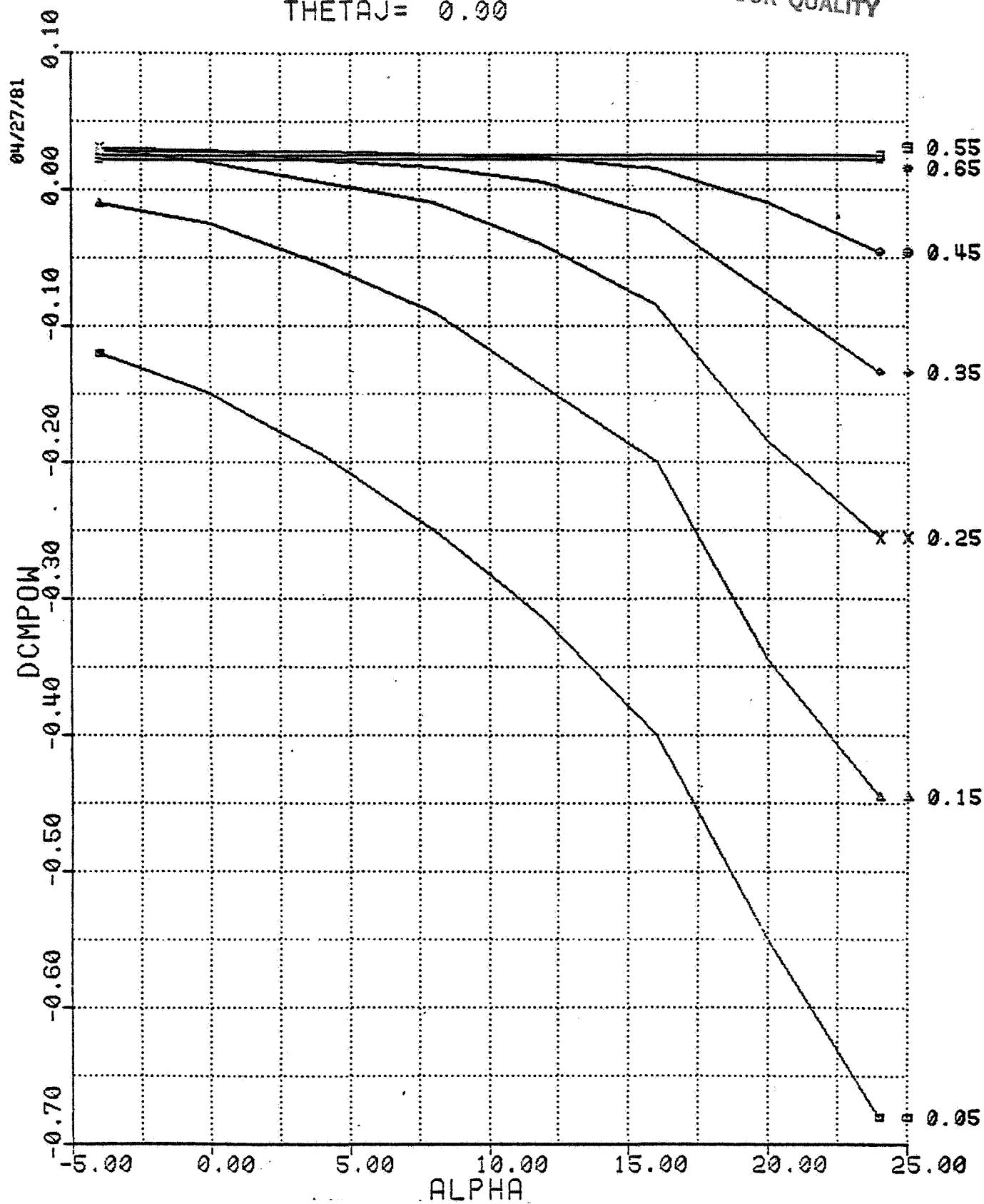
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FOR VARYING VEQ
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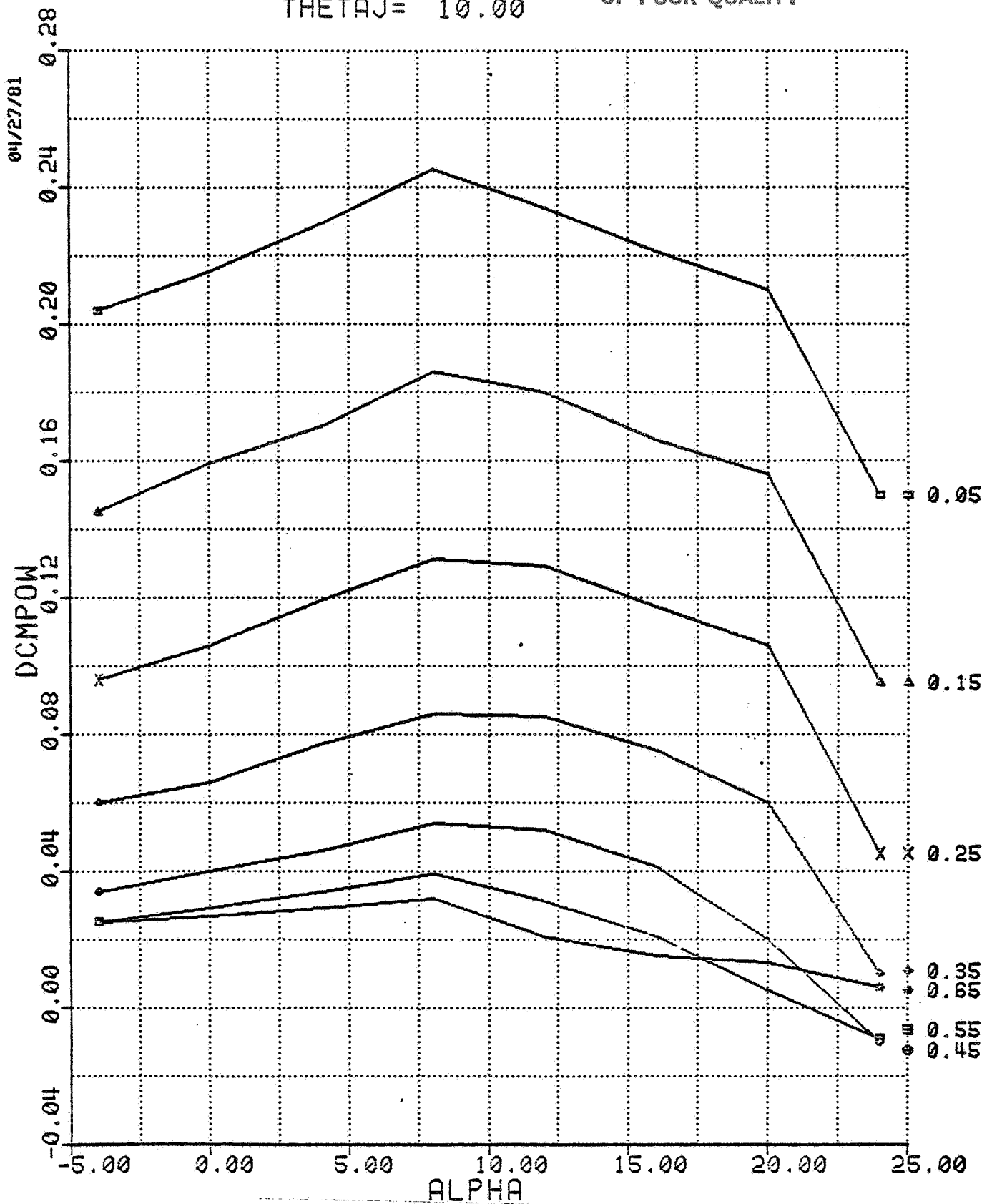
DCMPOW VS ALPHA
FOR VARYING VEQ
THETAJ = 0.00

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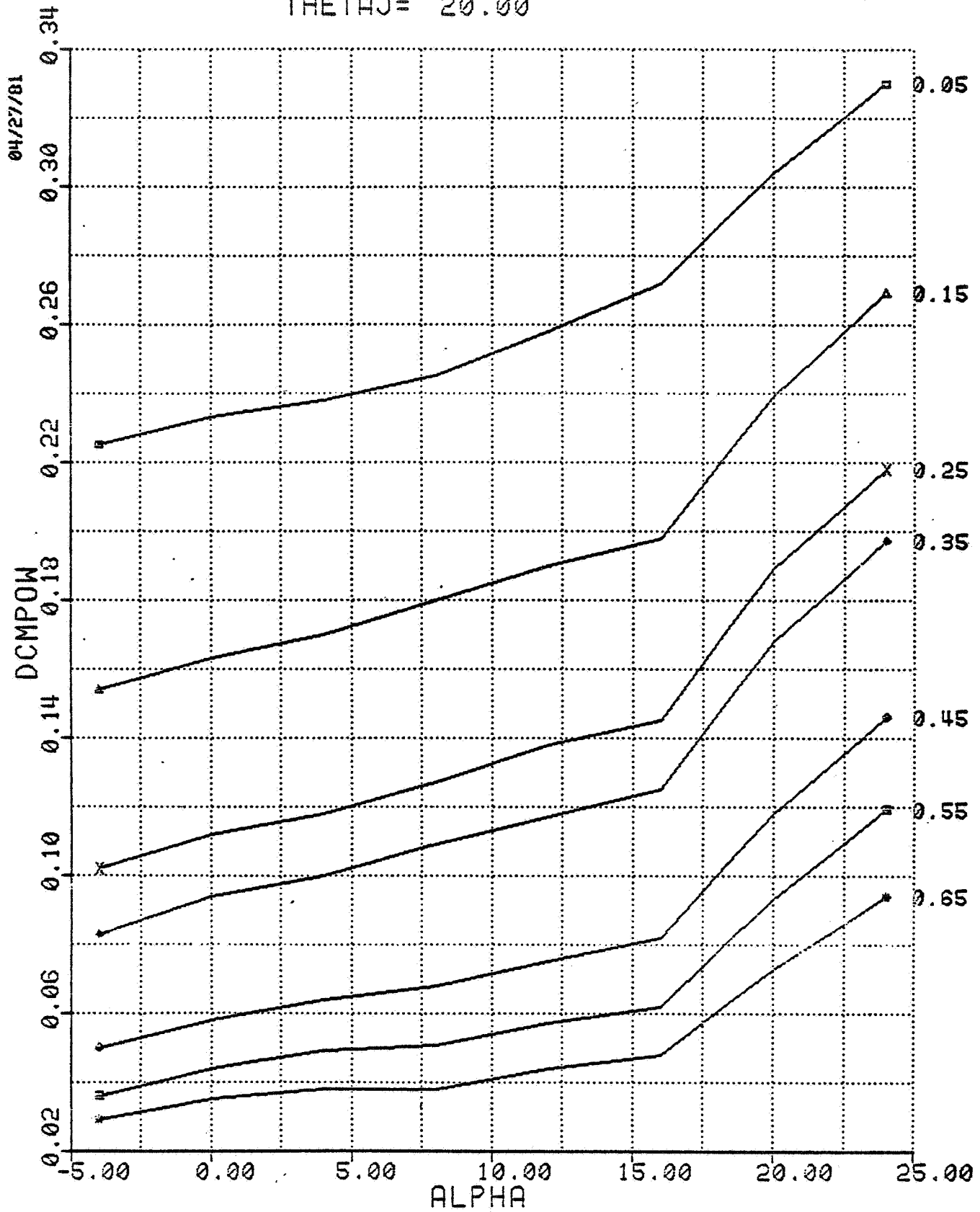
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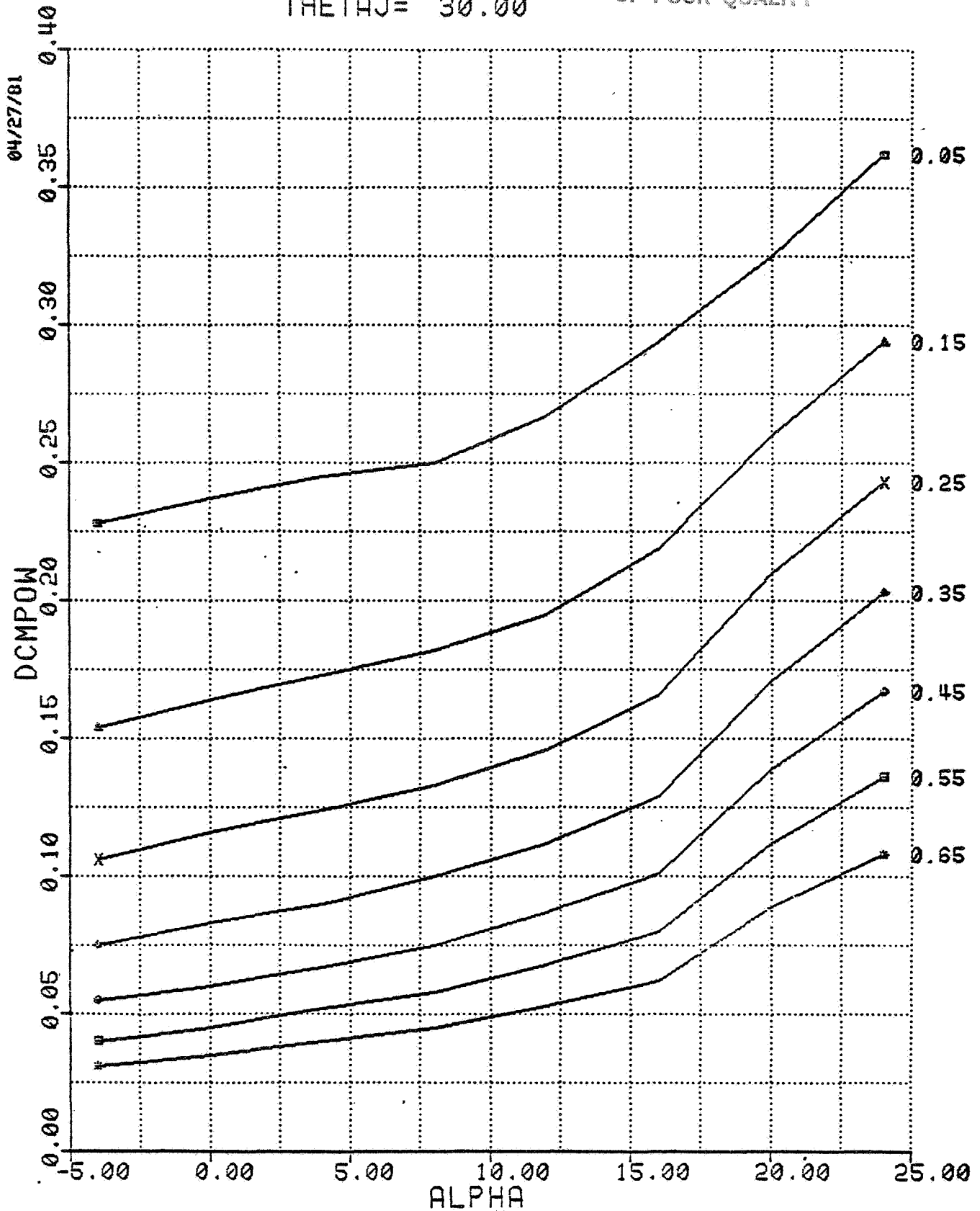
DCMPOW VS ALPHA
FOR VARYING VEQ
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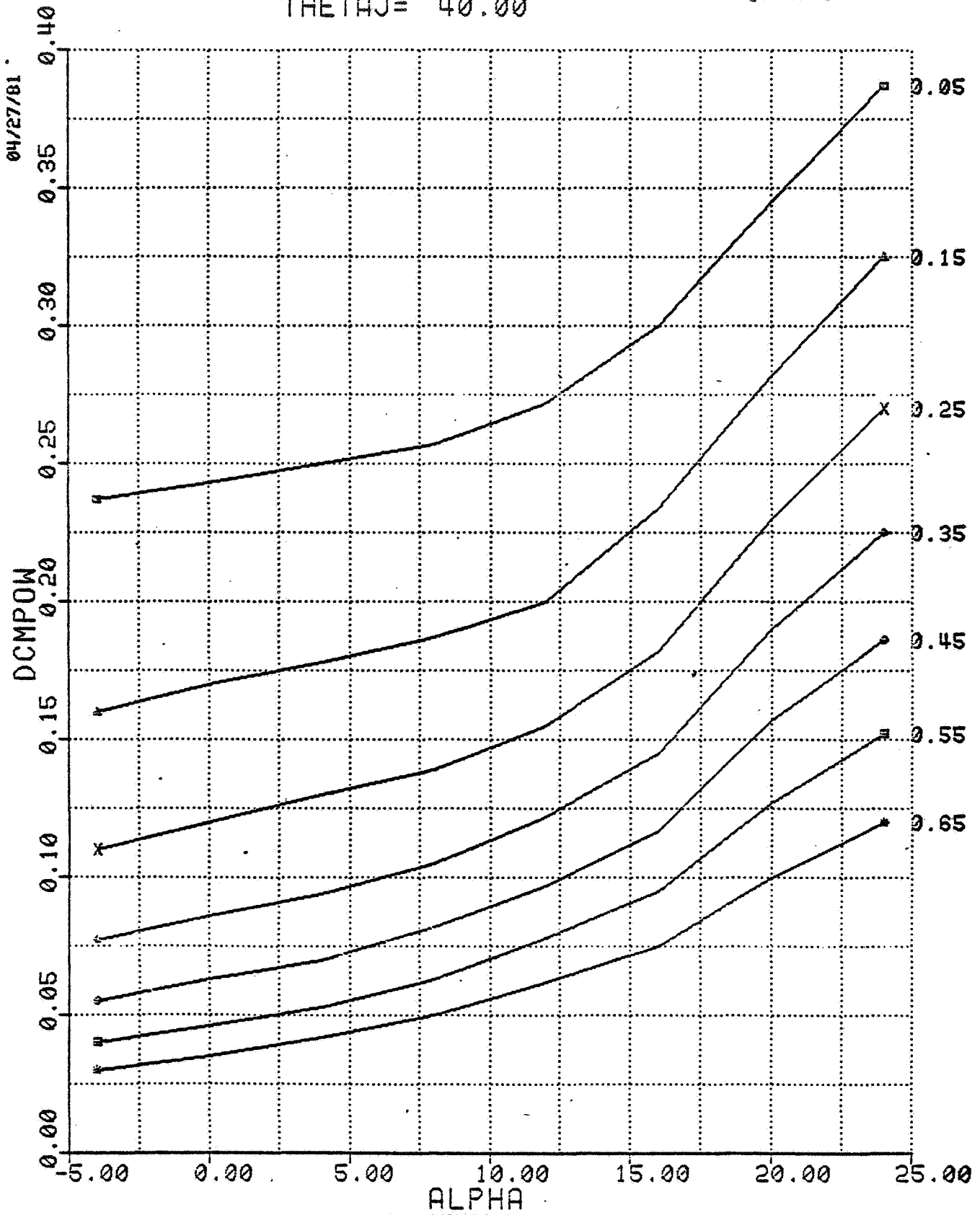
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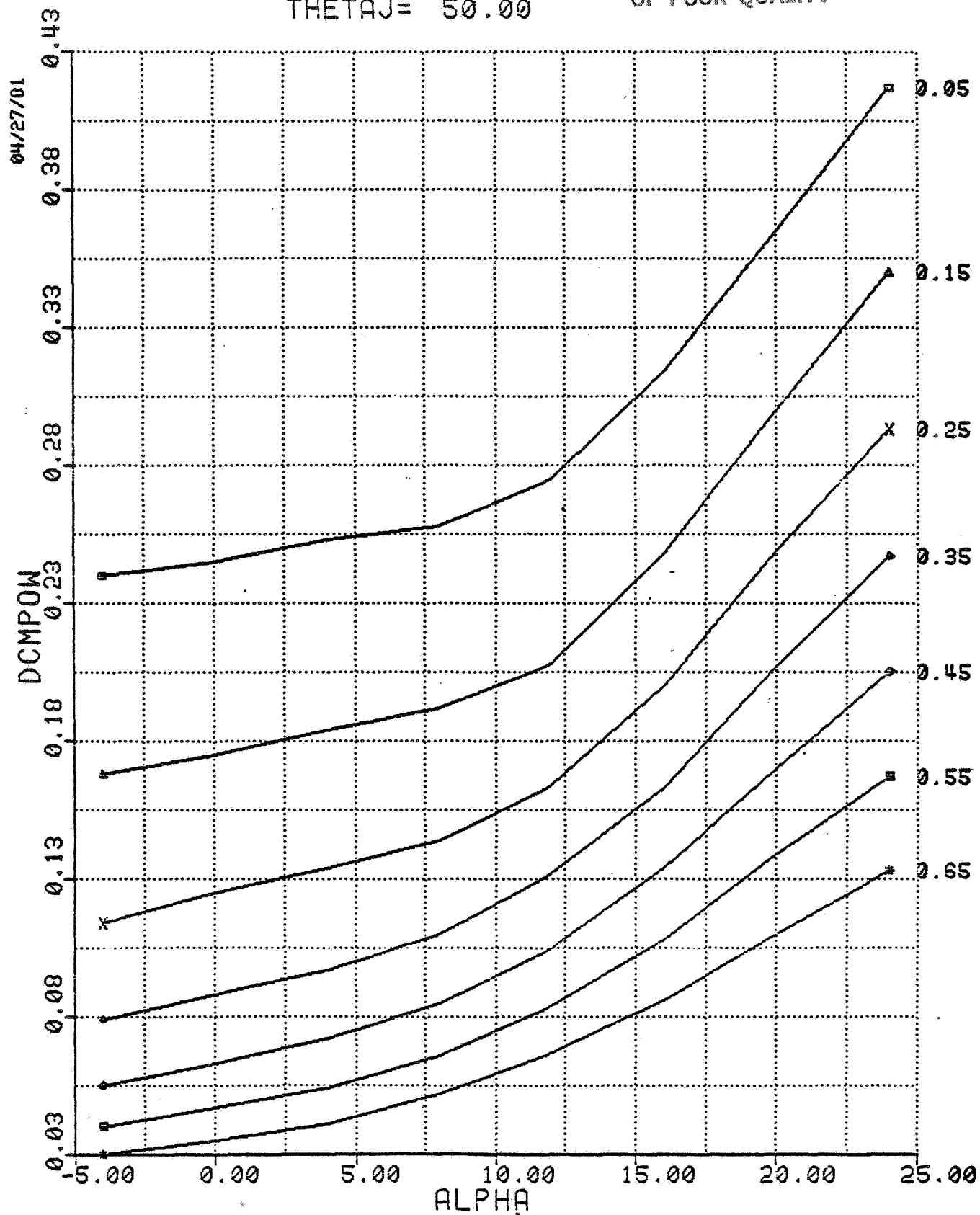
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FOR VARYING VEQ
THETAJ= 40.00

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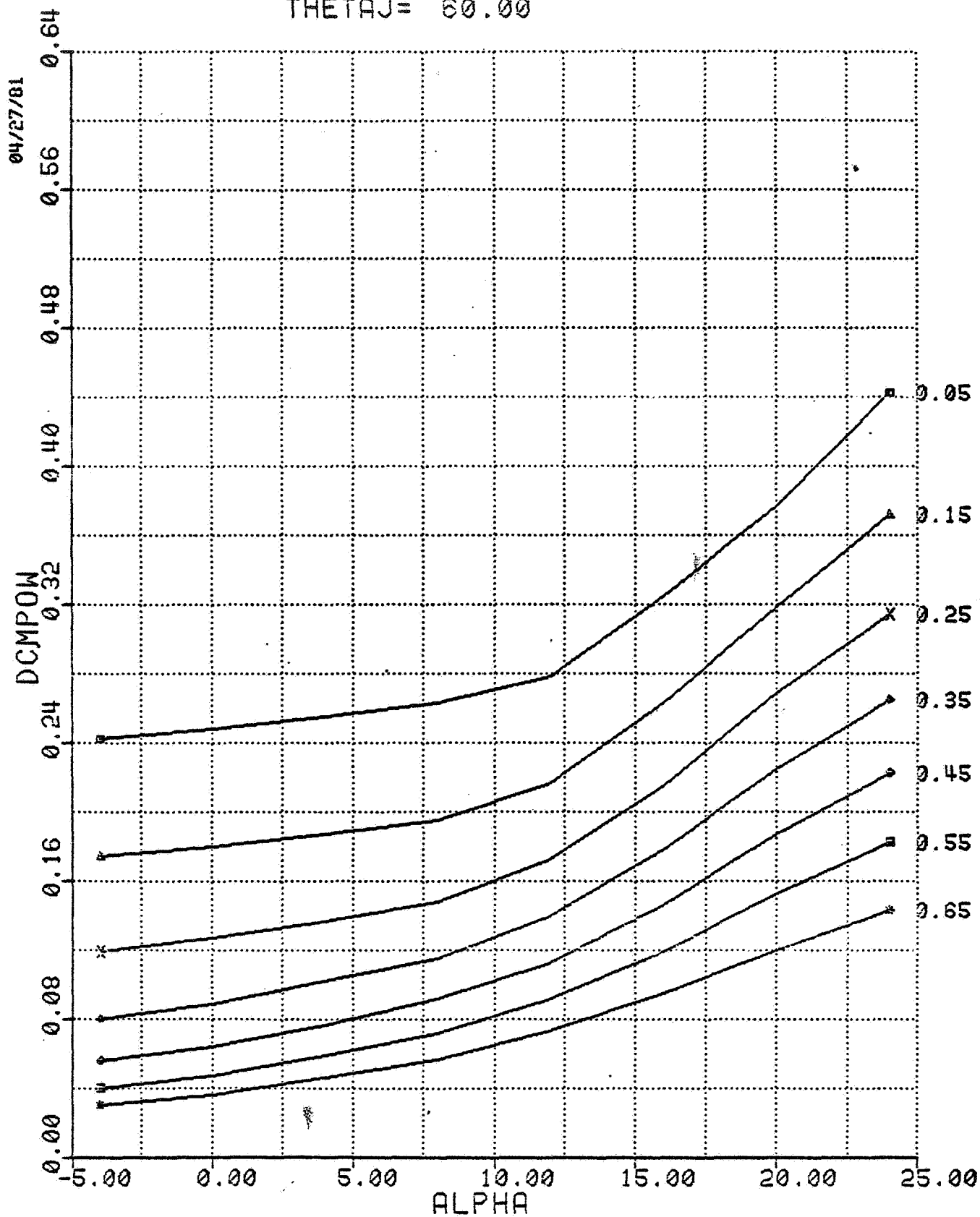
DCMPOW VS ALPHA
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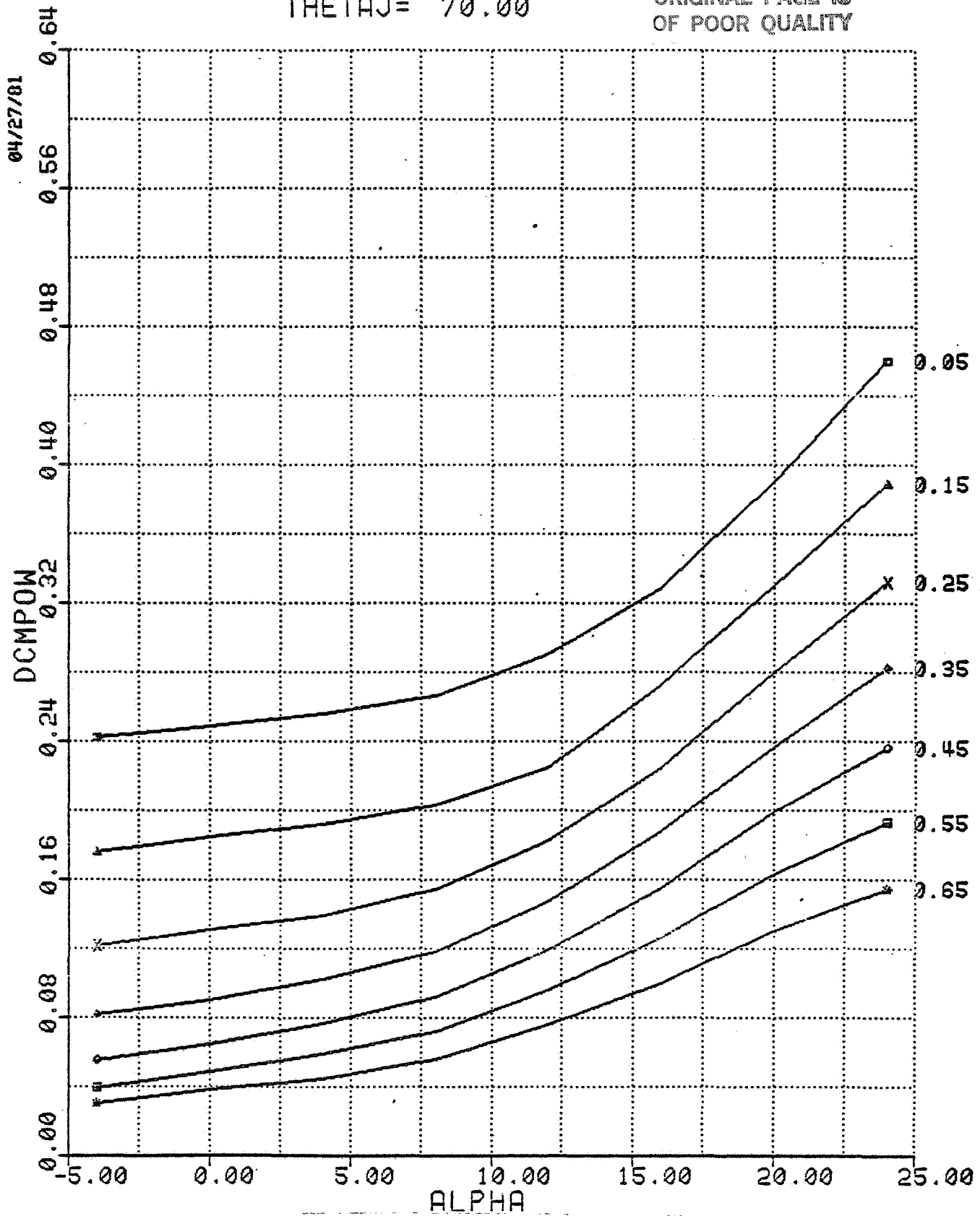
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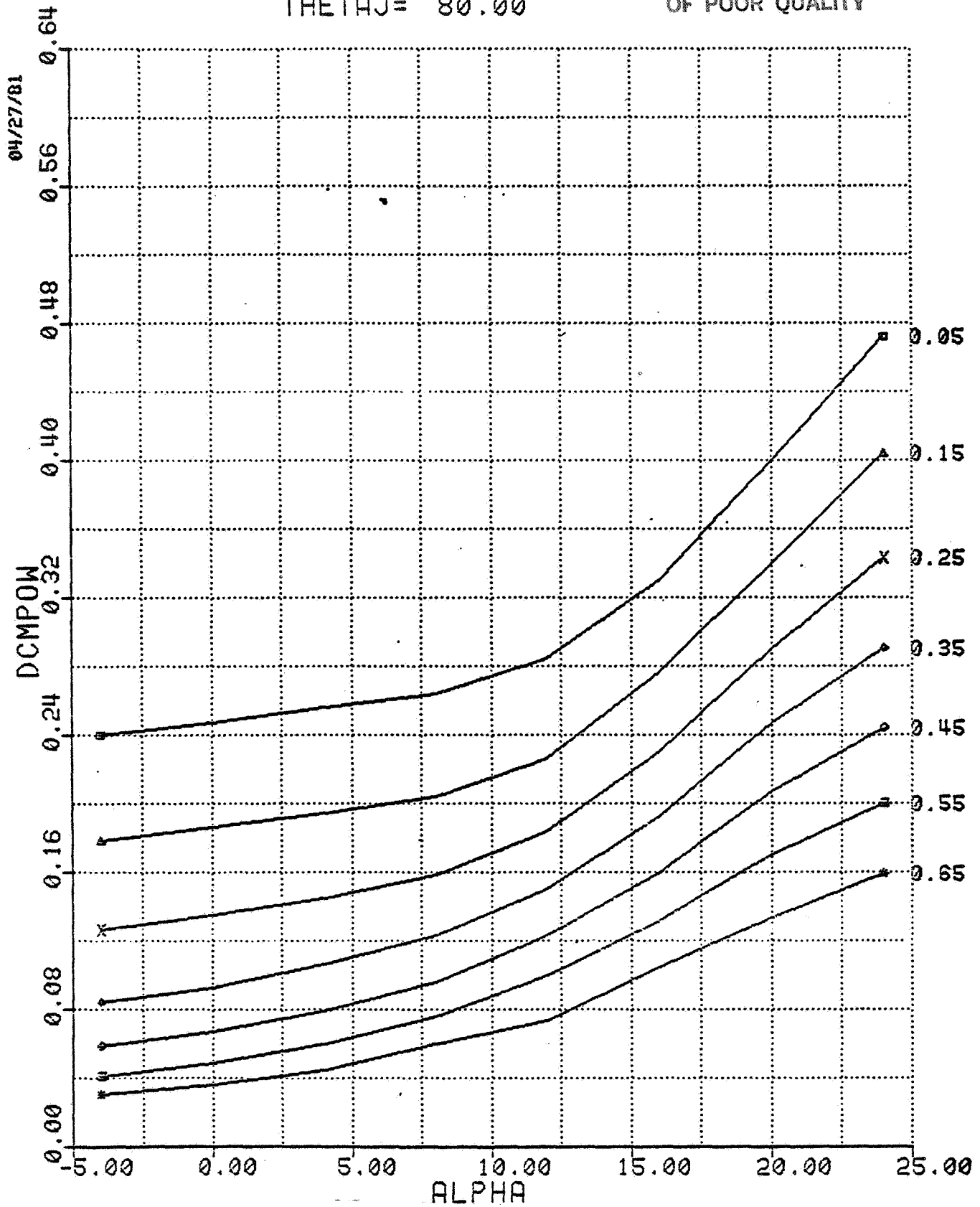
DCMPOW VS ALPHA
FOR VARYING VEQ
THETAJ = 70.00

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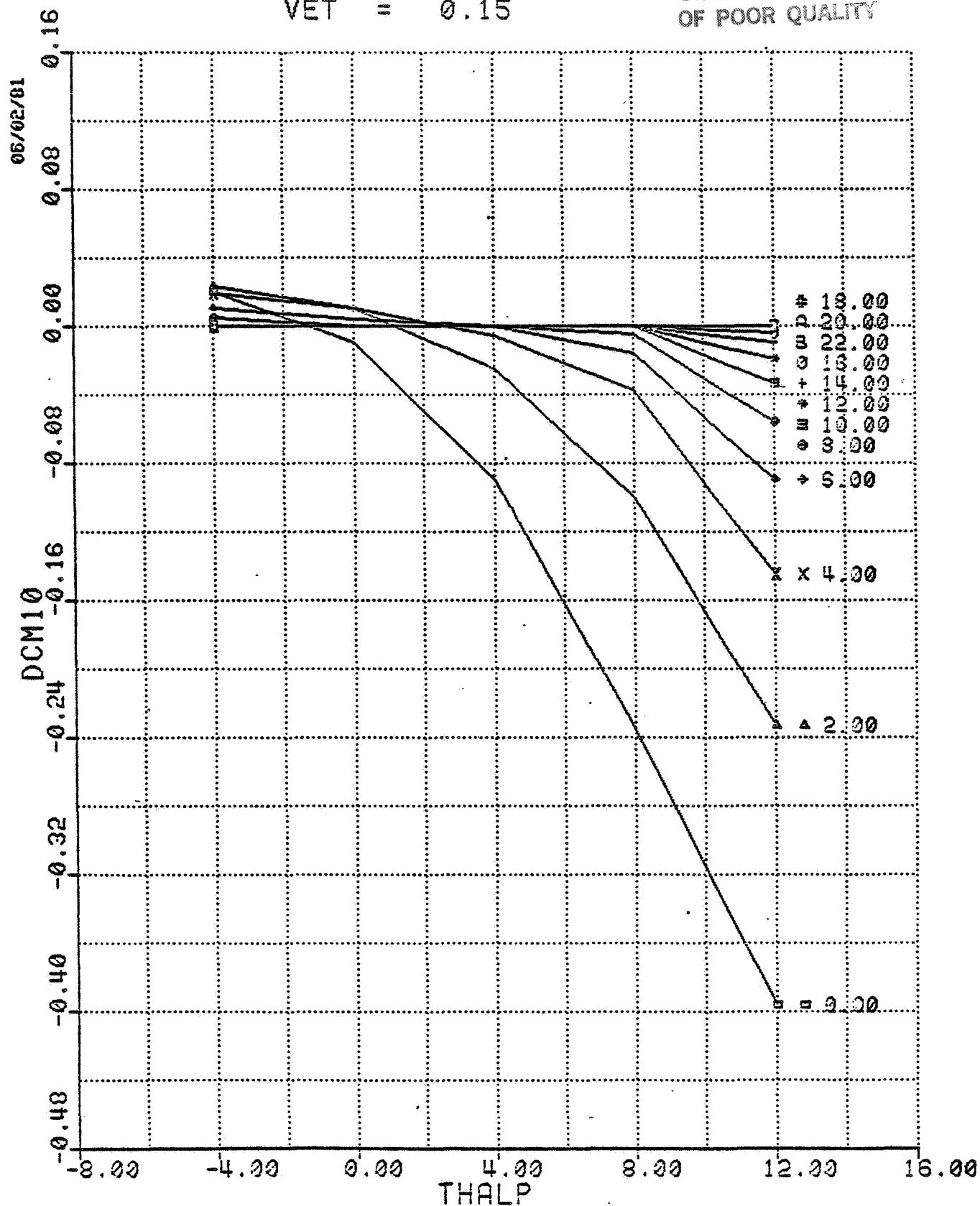
DCMPOW VS ALPHA
FOR VARYING VEQ
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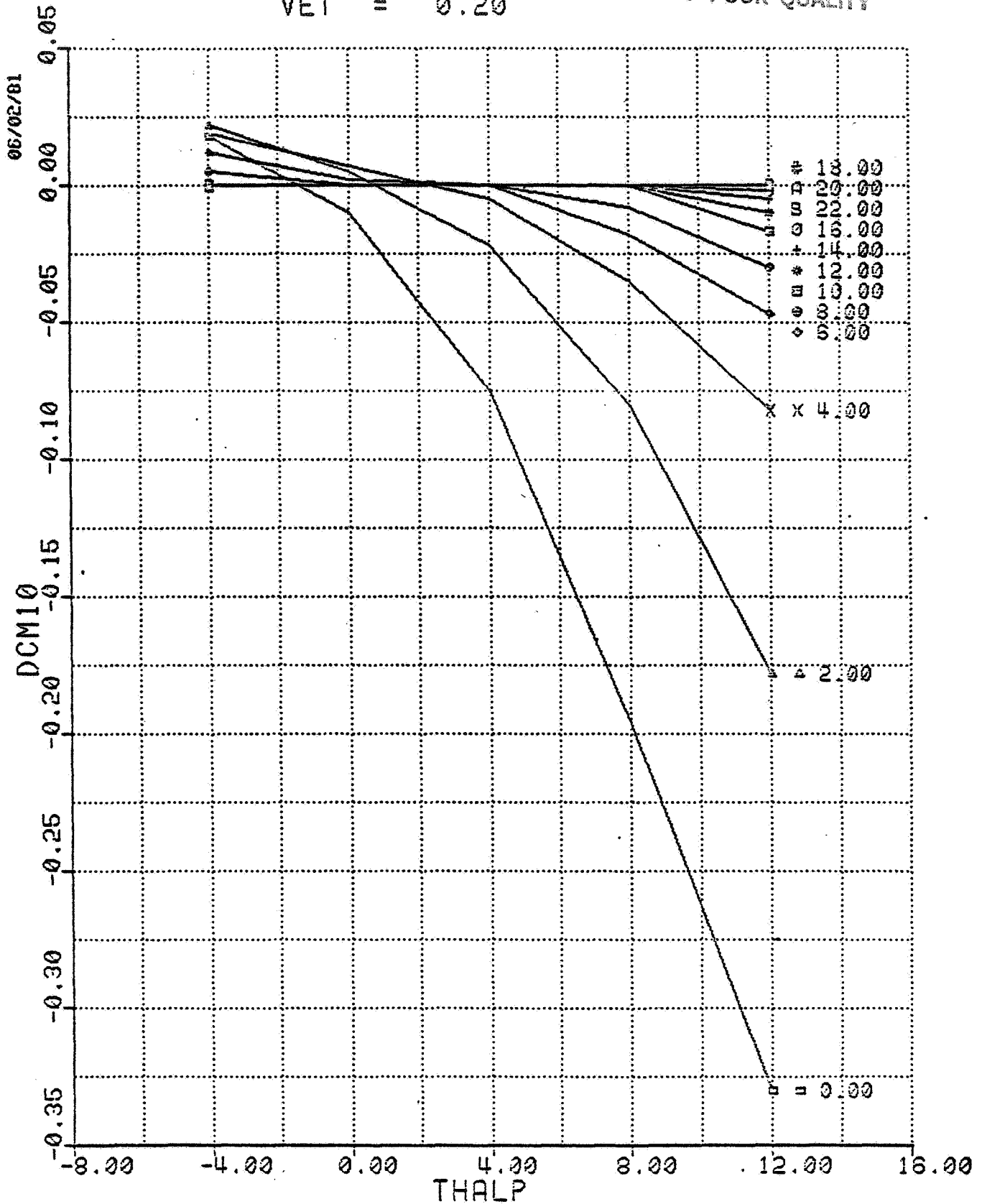
DCM10 VS THALP
FOR VARYING ALTITUDE
VET = 0.15

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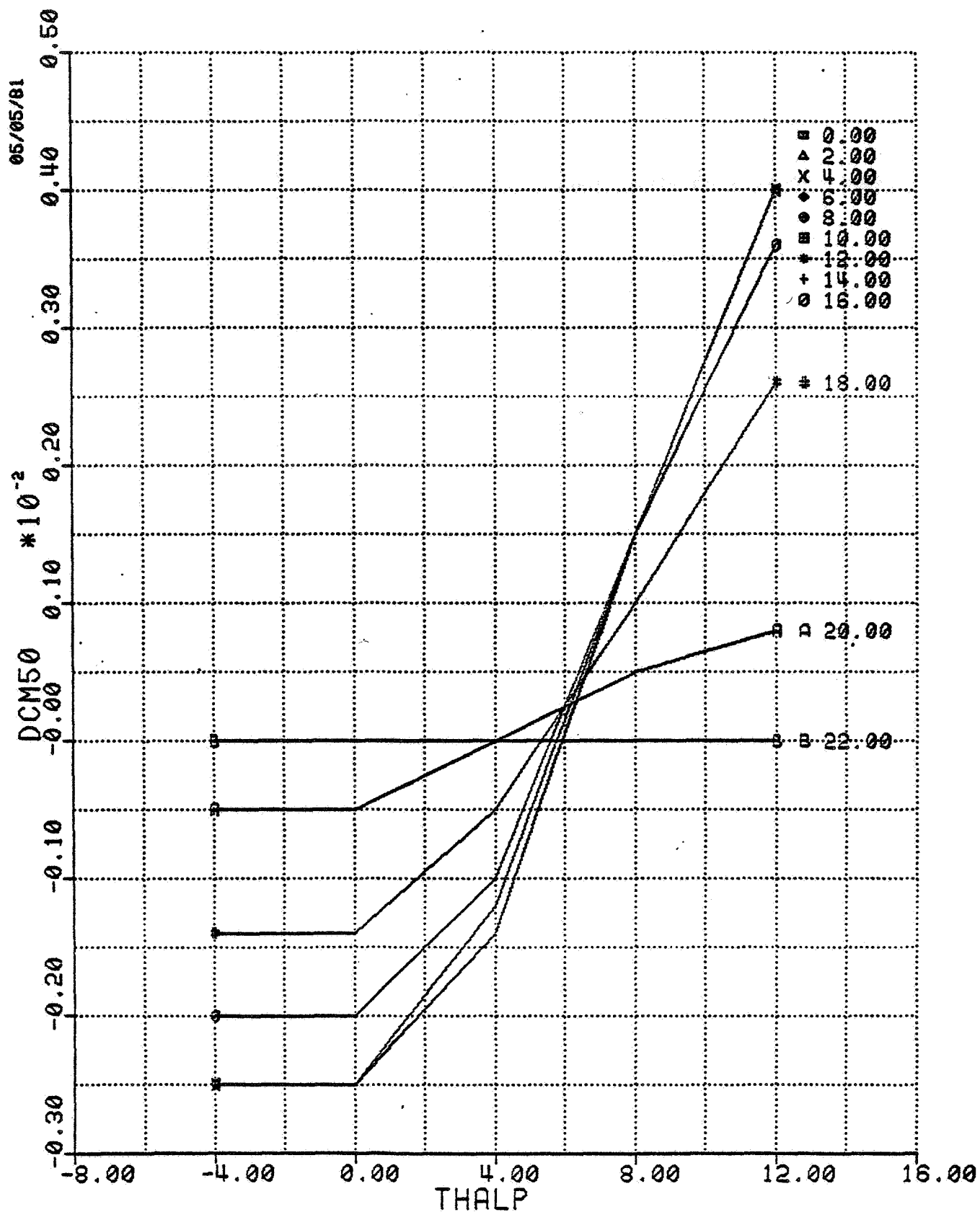
DCM10 VS THALP
FOR VARYING ALTITUDE
VET = 0.20

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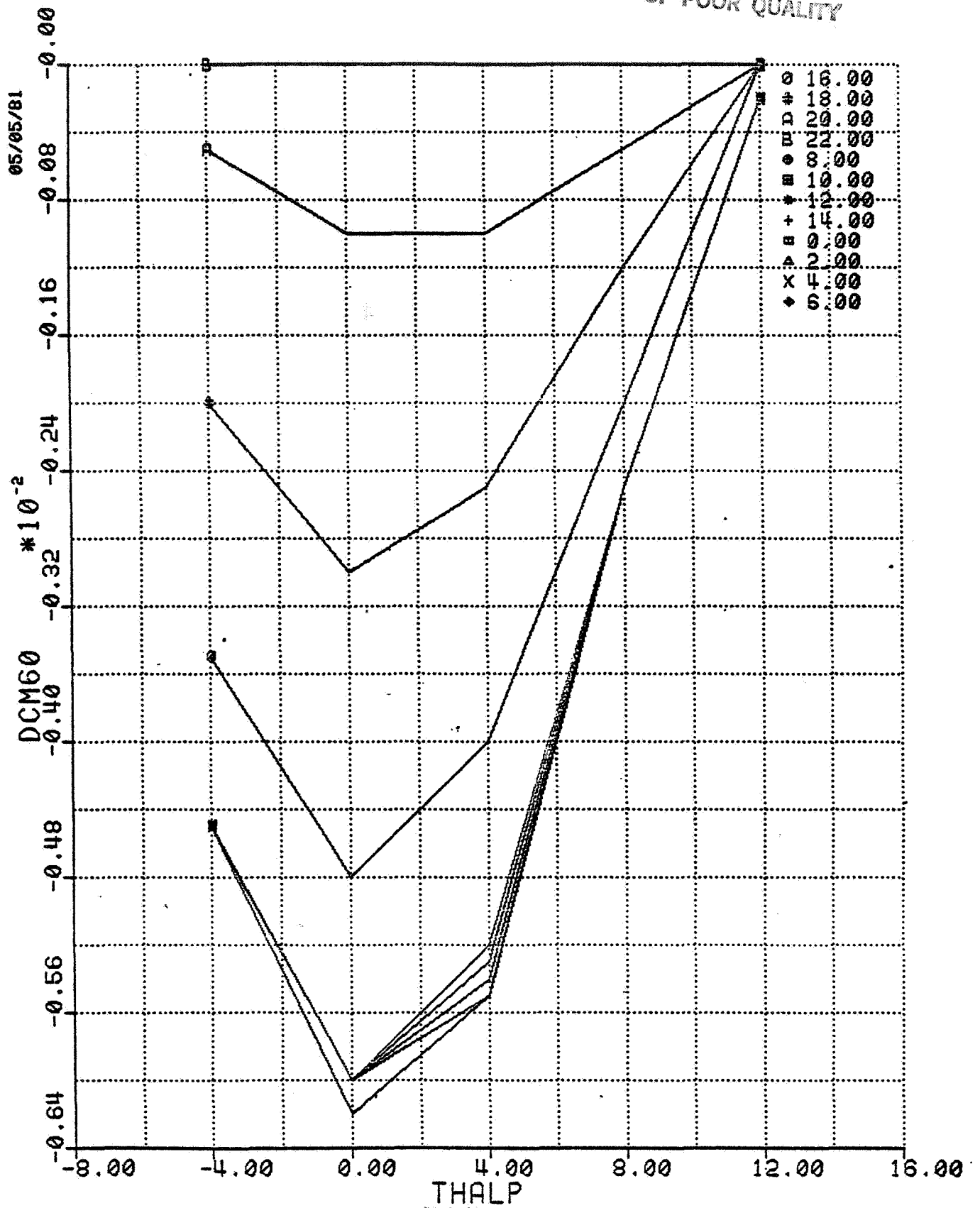
DCM50 VS THALP FOR VARYING HP

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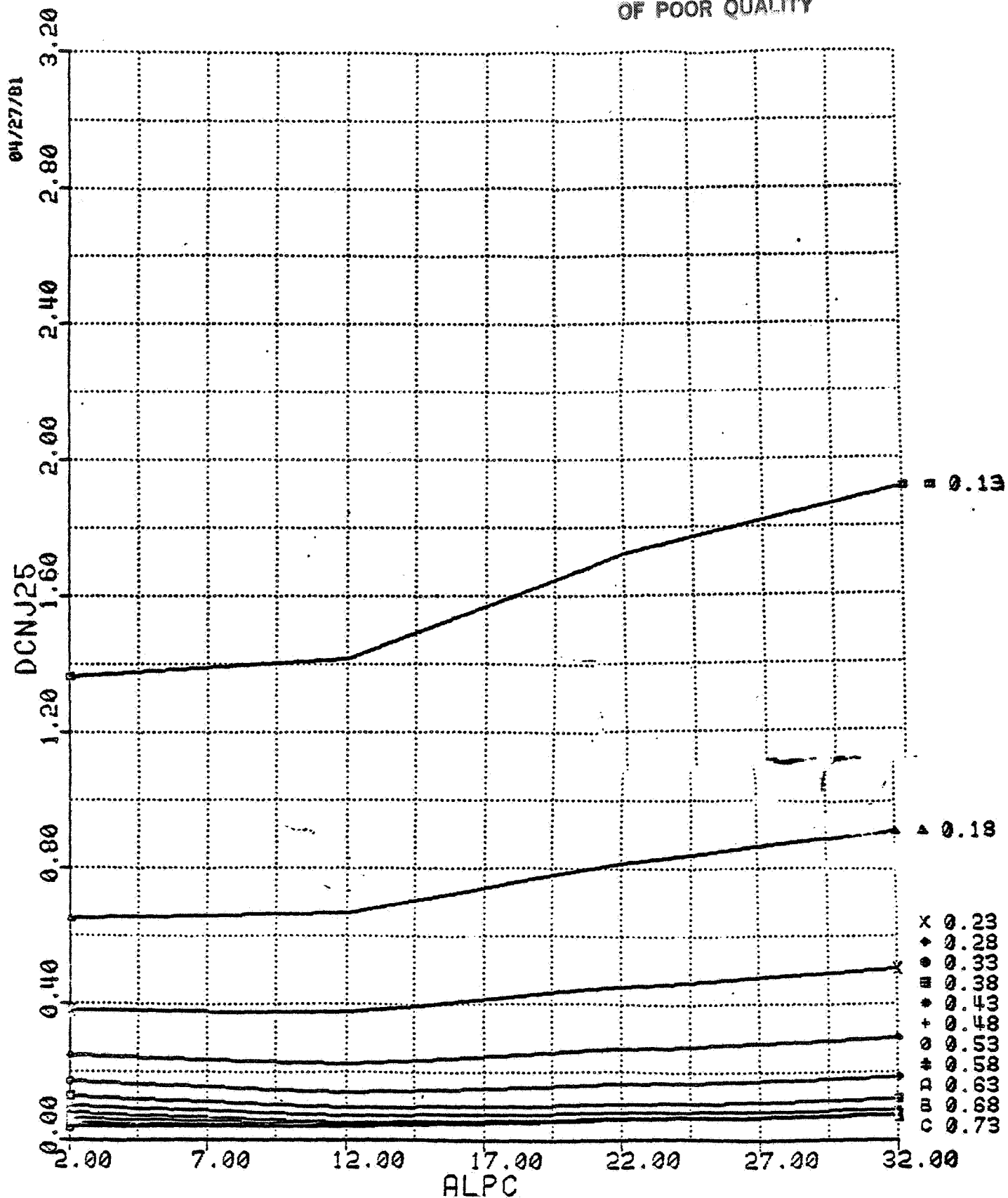
DCM60 VS THALP
FOR VARYING HP

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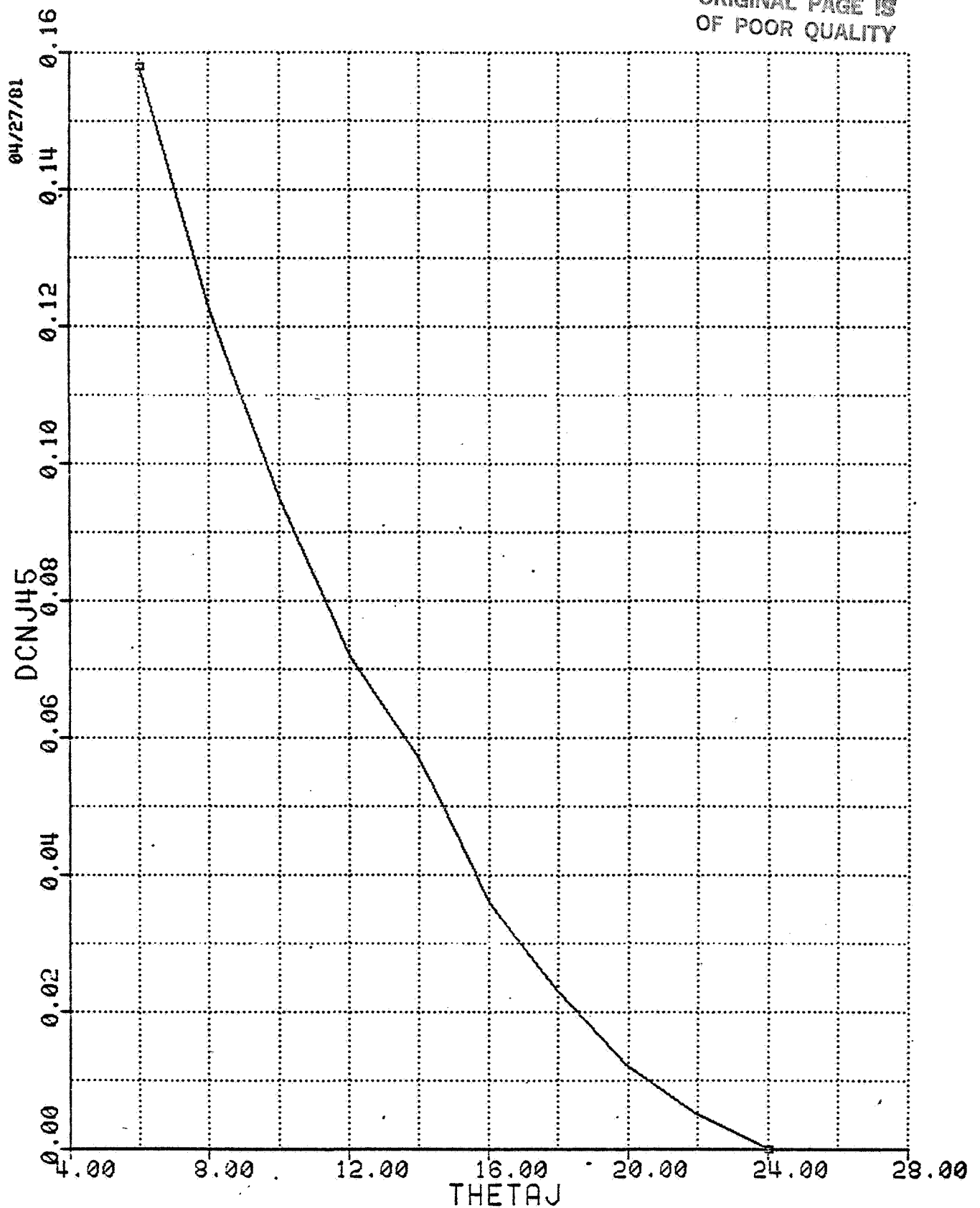
DCNJ25 VS ALPC FOR VARYING VEG

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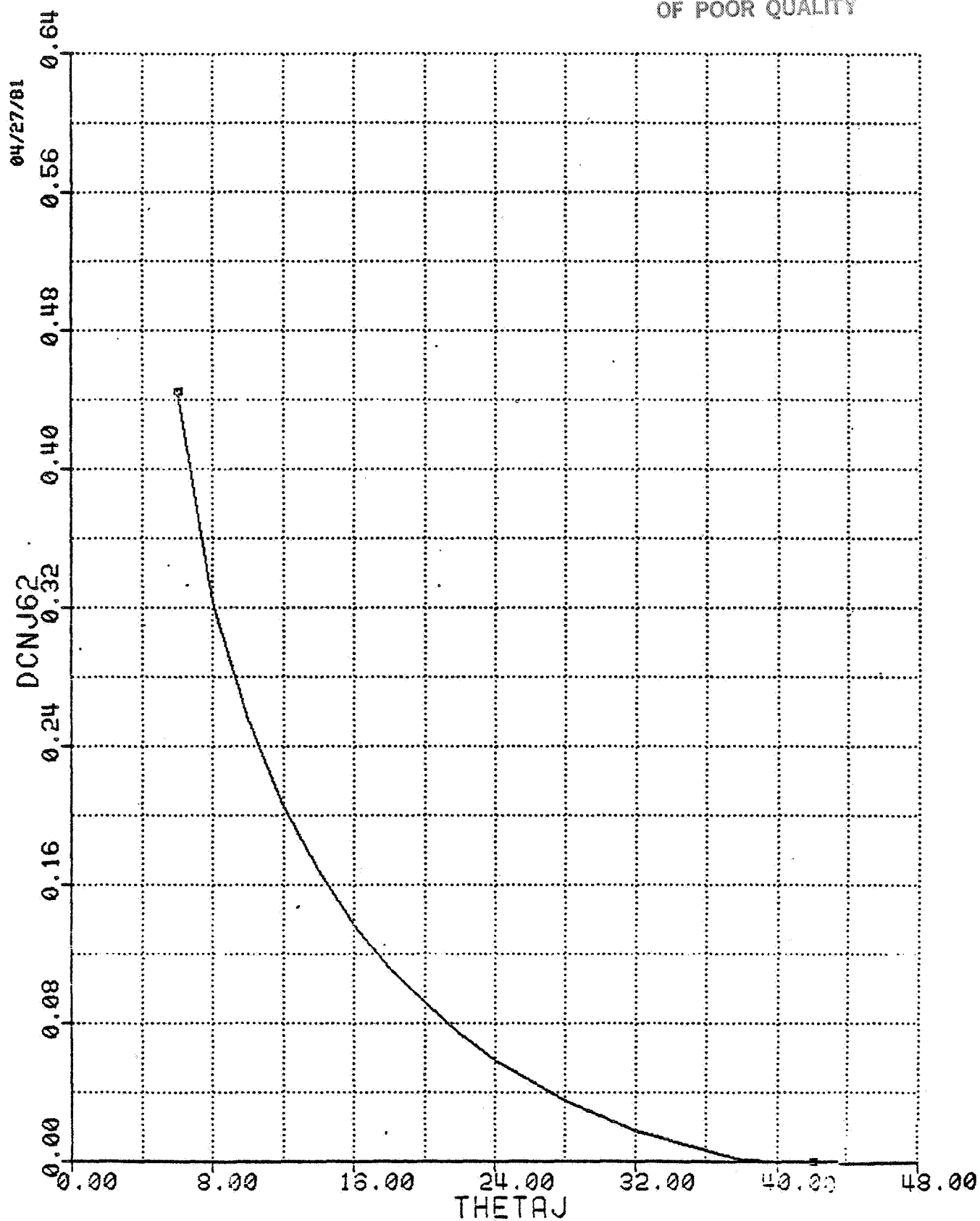


DCNJ45 VS THETAJ

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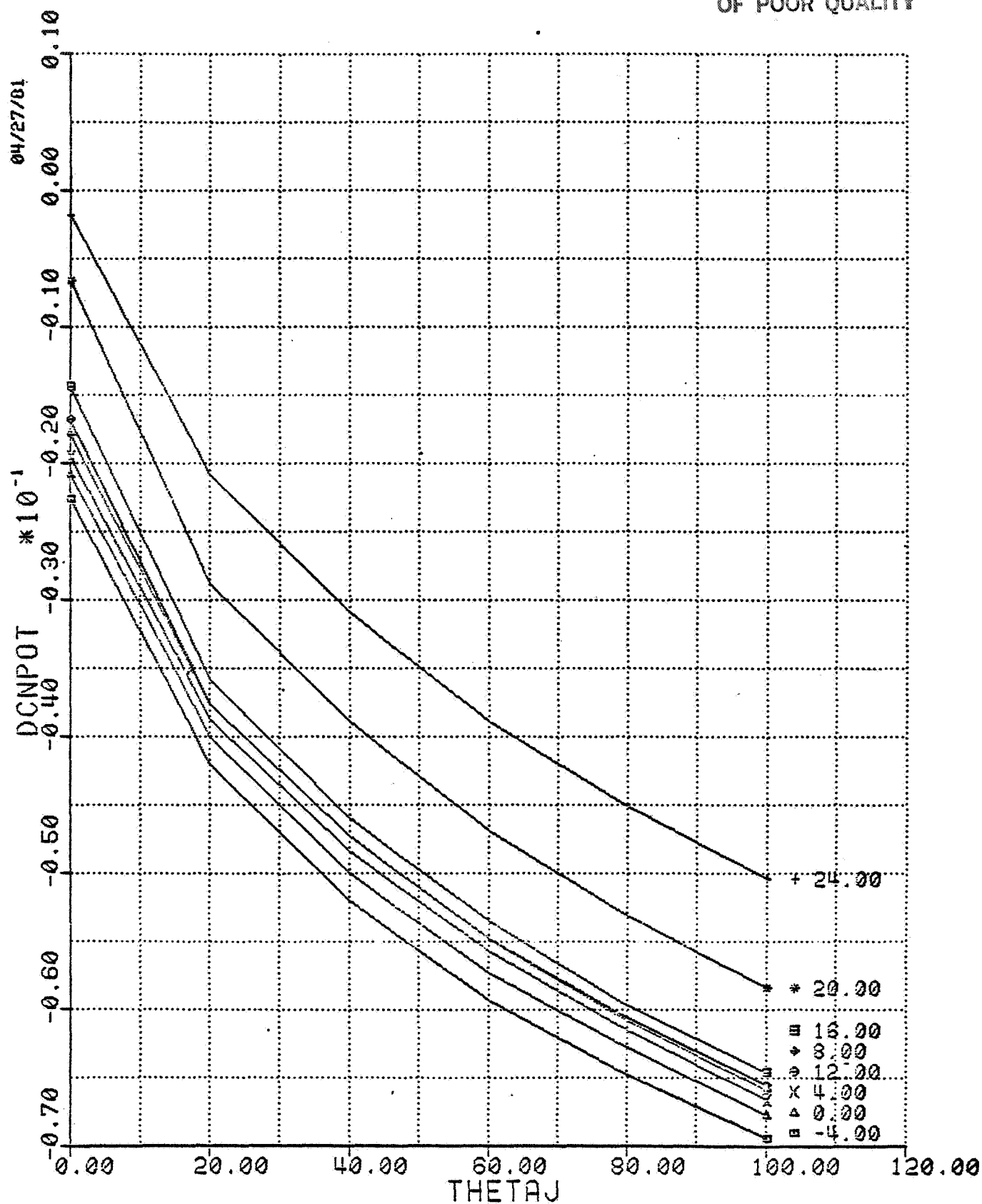


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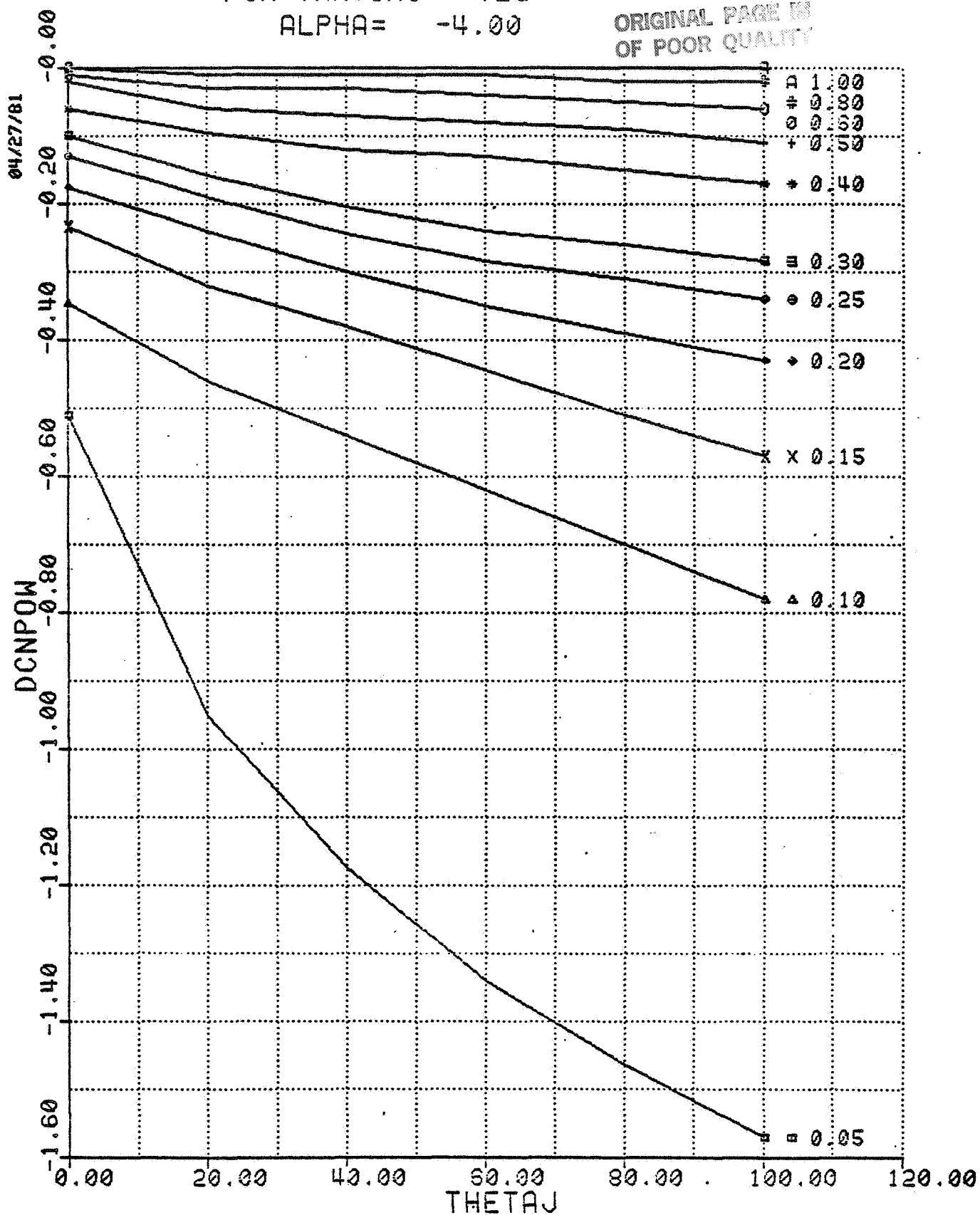
DCNPOT VS THETAJ
FOR VARYING ALPHA

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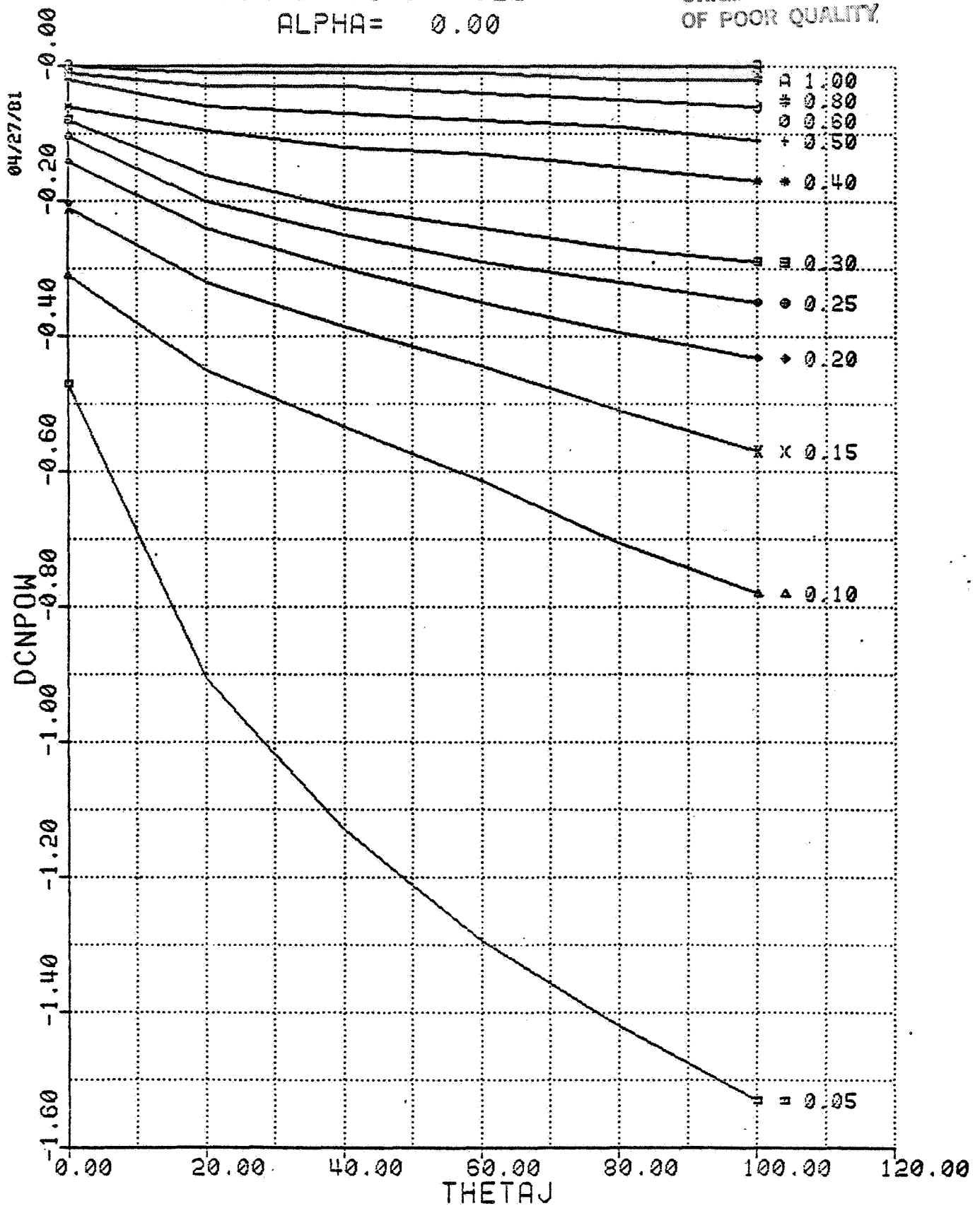
DCNPOW VS THETAJ
FOR VARYING VEQ
ALPHA= -4.00

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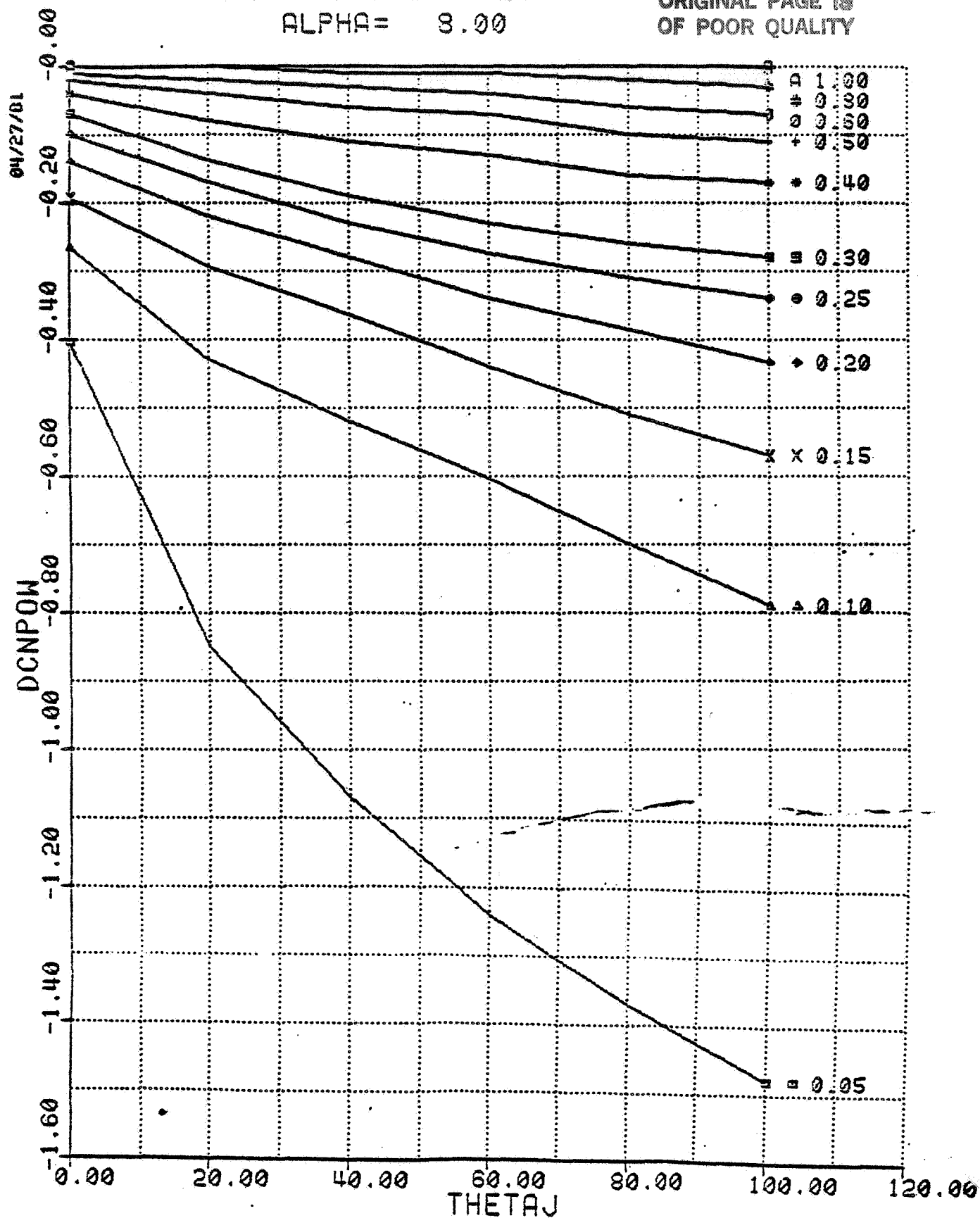
DCNPOW VS THETAJ
FOR VARYING VEQ
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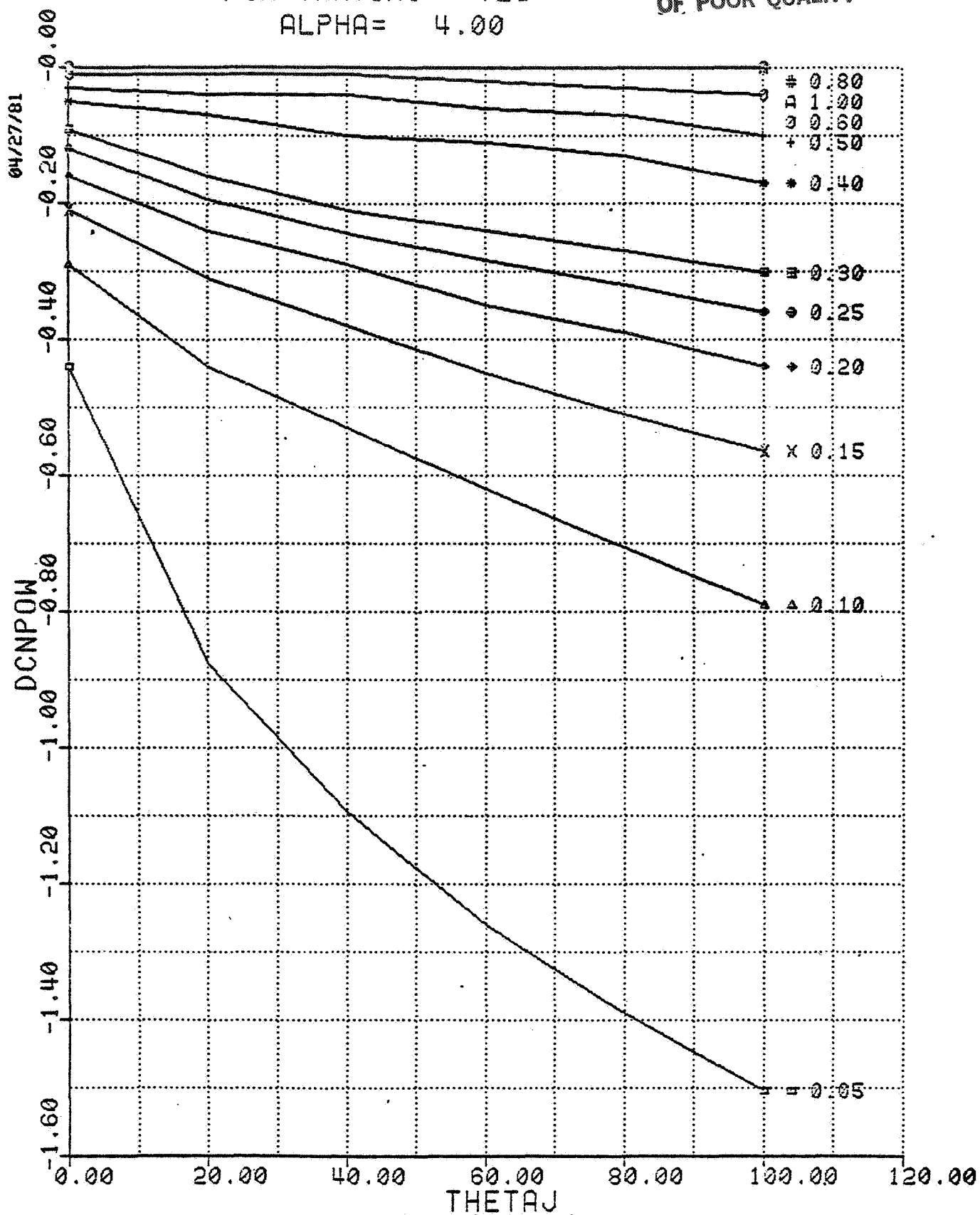
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FOR VARYING VEQ
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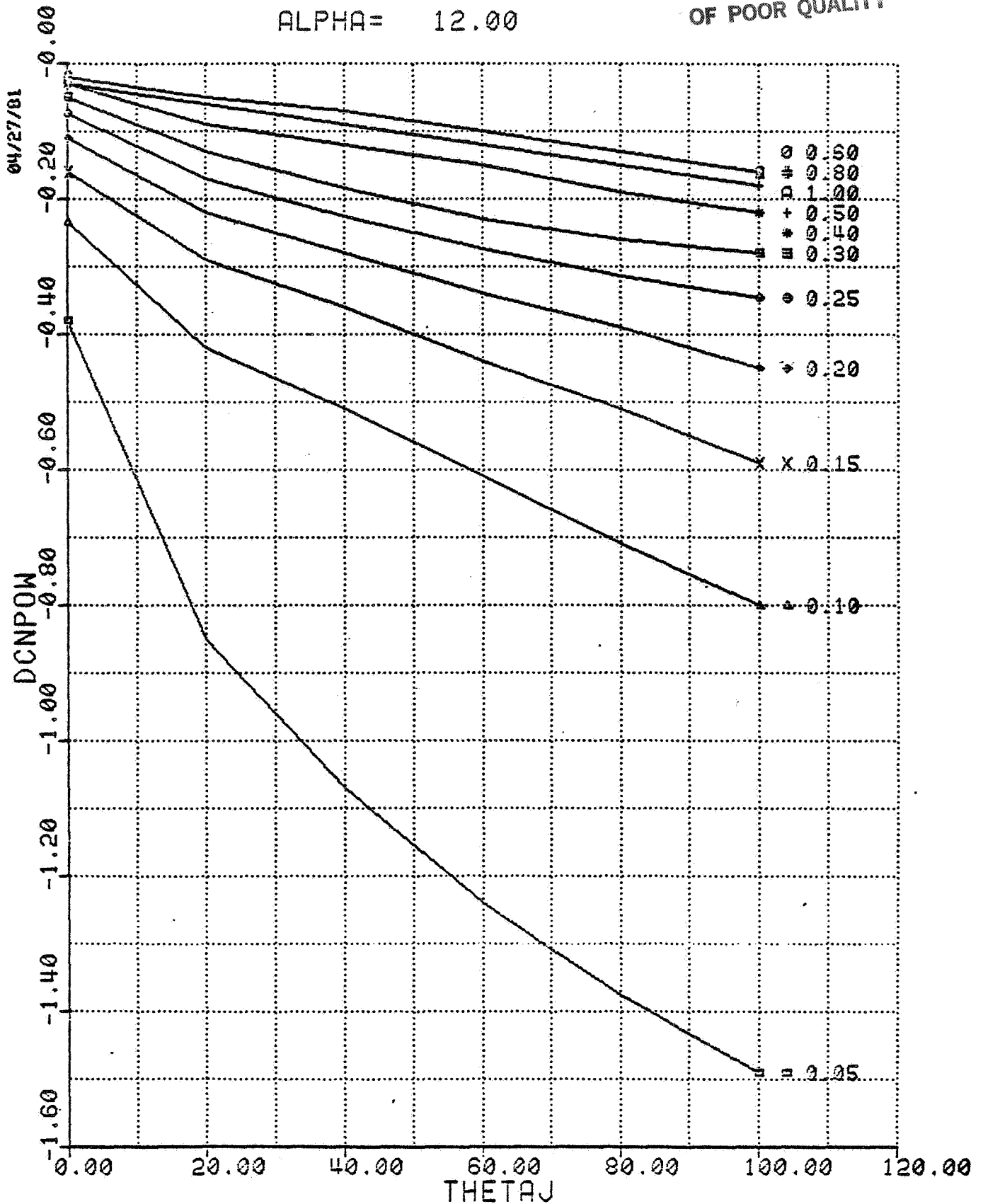
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FOR VARYING VEQ
ALPHA= 4.00

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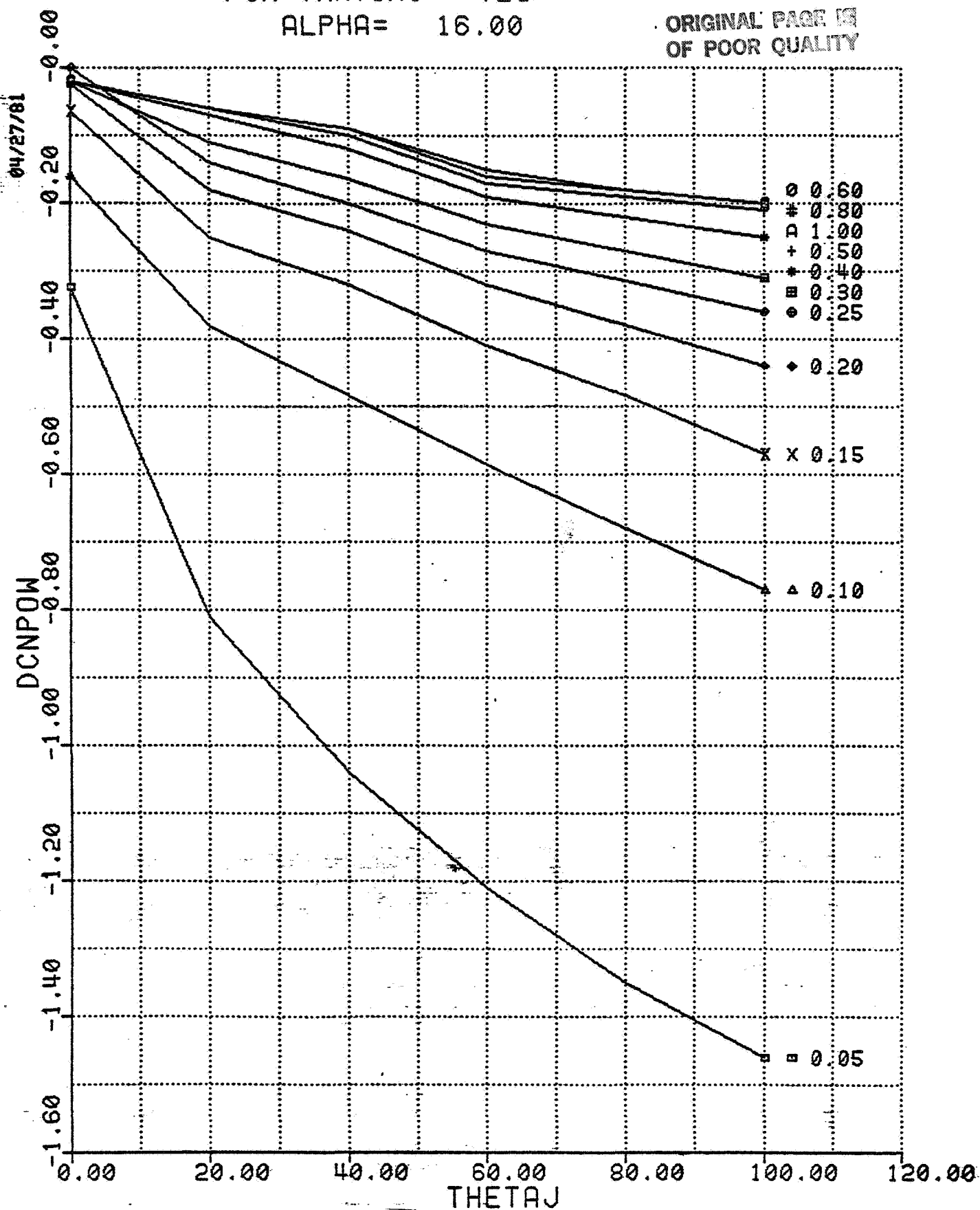
DCNPOW VS THETAJ
FOR VARYING VEQ
ALPHA= 12.00

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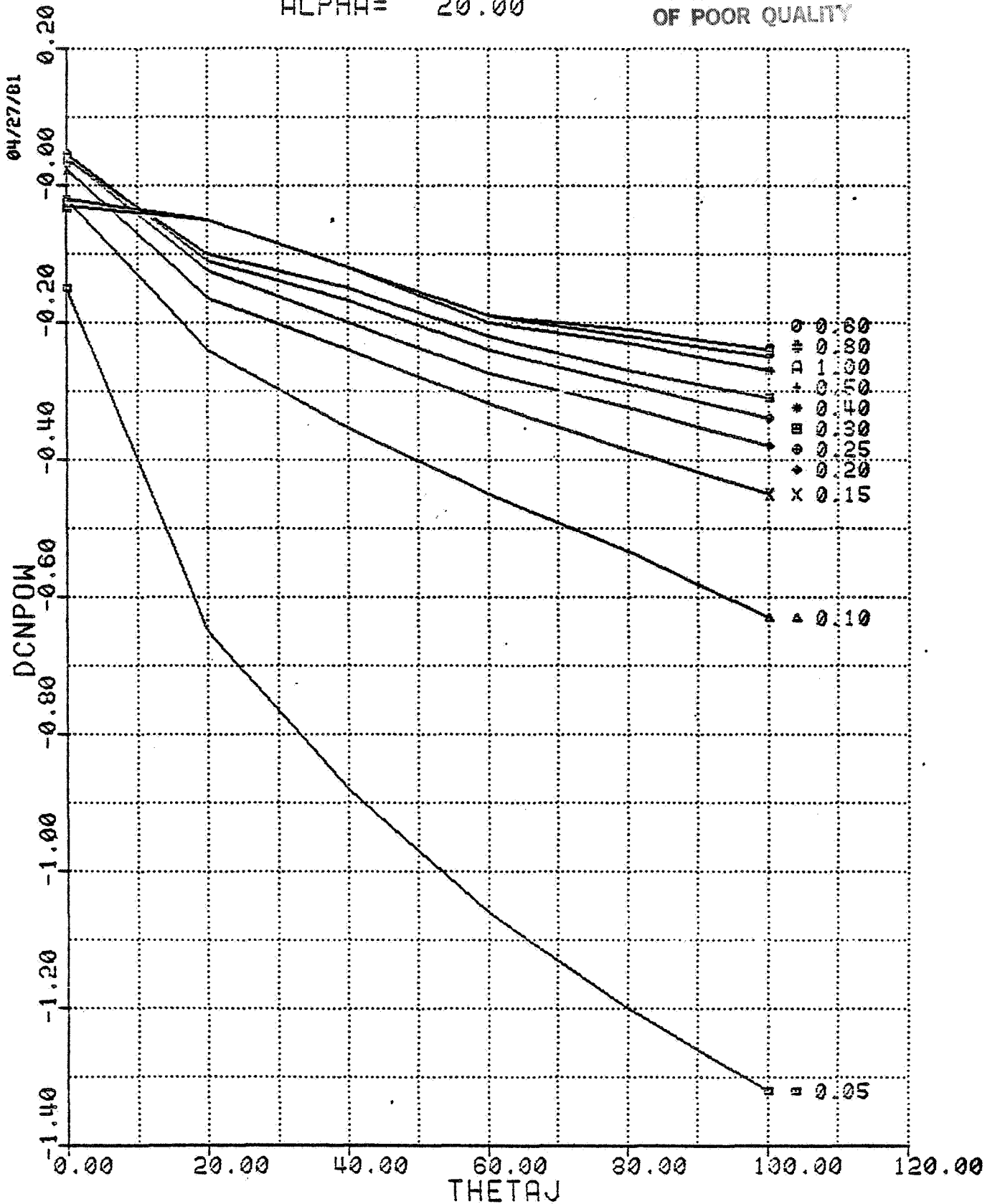
DCNPOW VS THETAJ
FOR VARYING VEQ
ALPHA= 16.00

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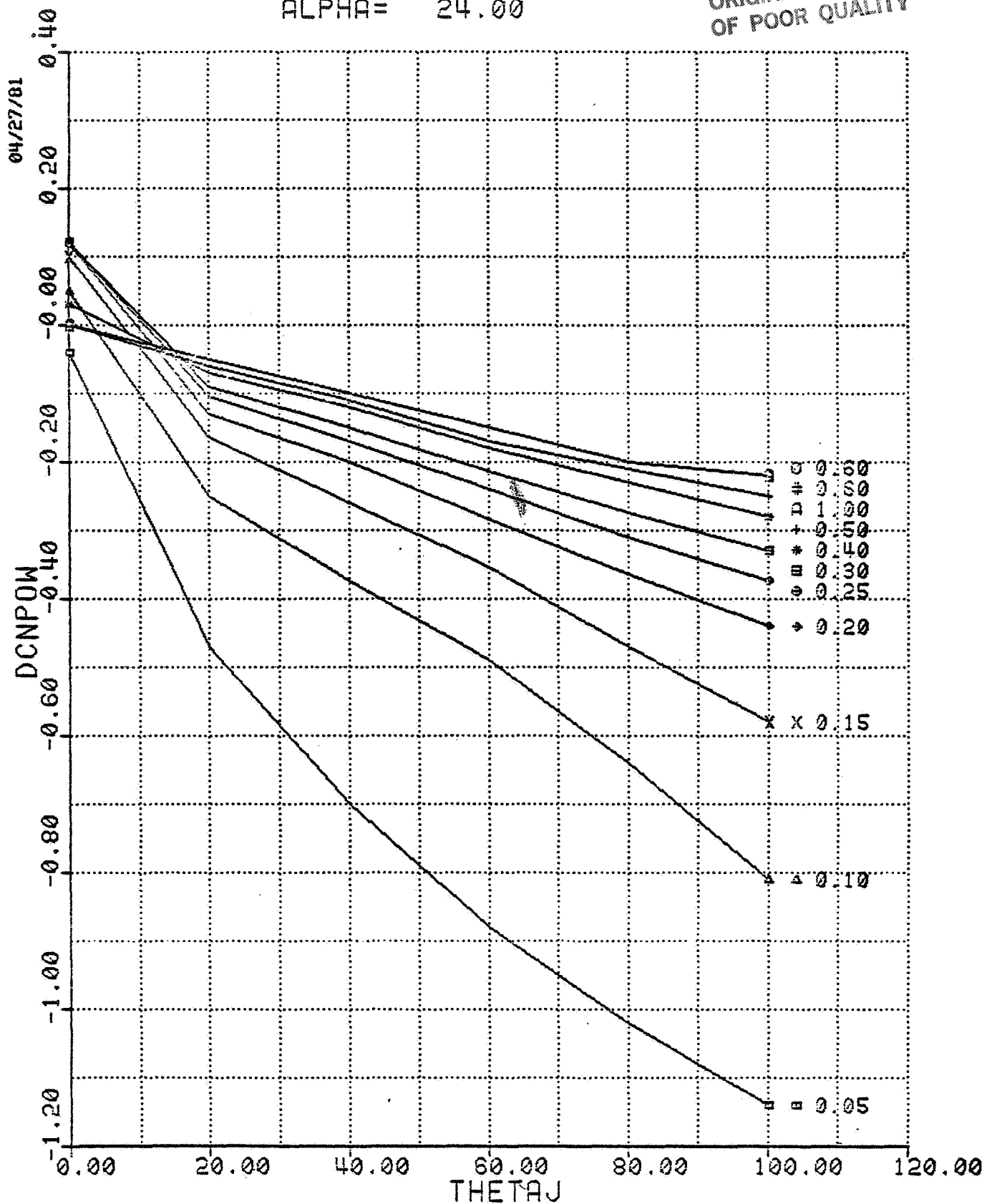
DCNPOW VS THETAJ
FOR VARYING VEQ
ALPHA= 20.00

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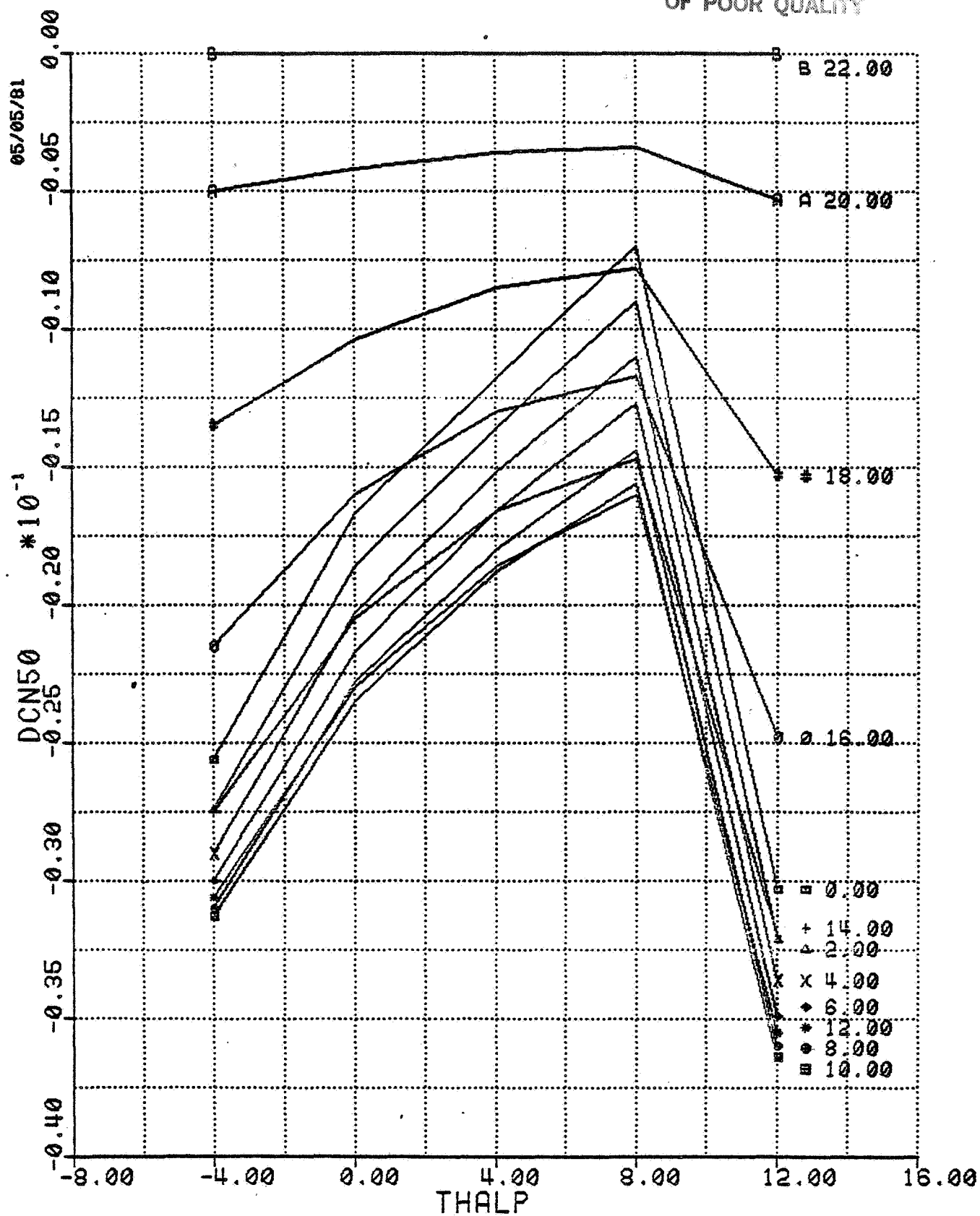
DCNPOW VS THETAJ
FOR VARYING VEQ
ALPHA= 24.00

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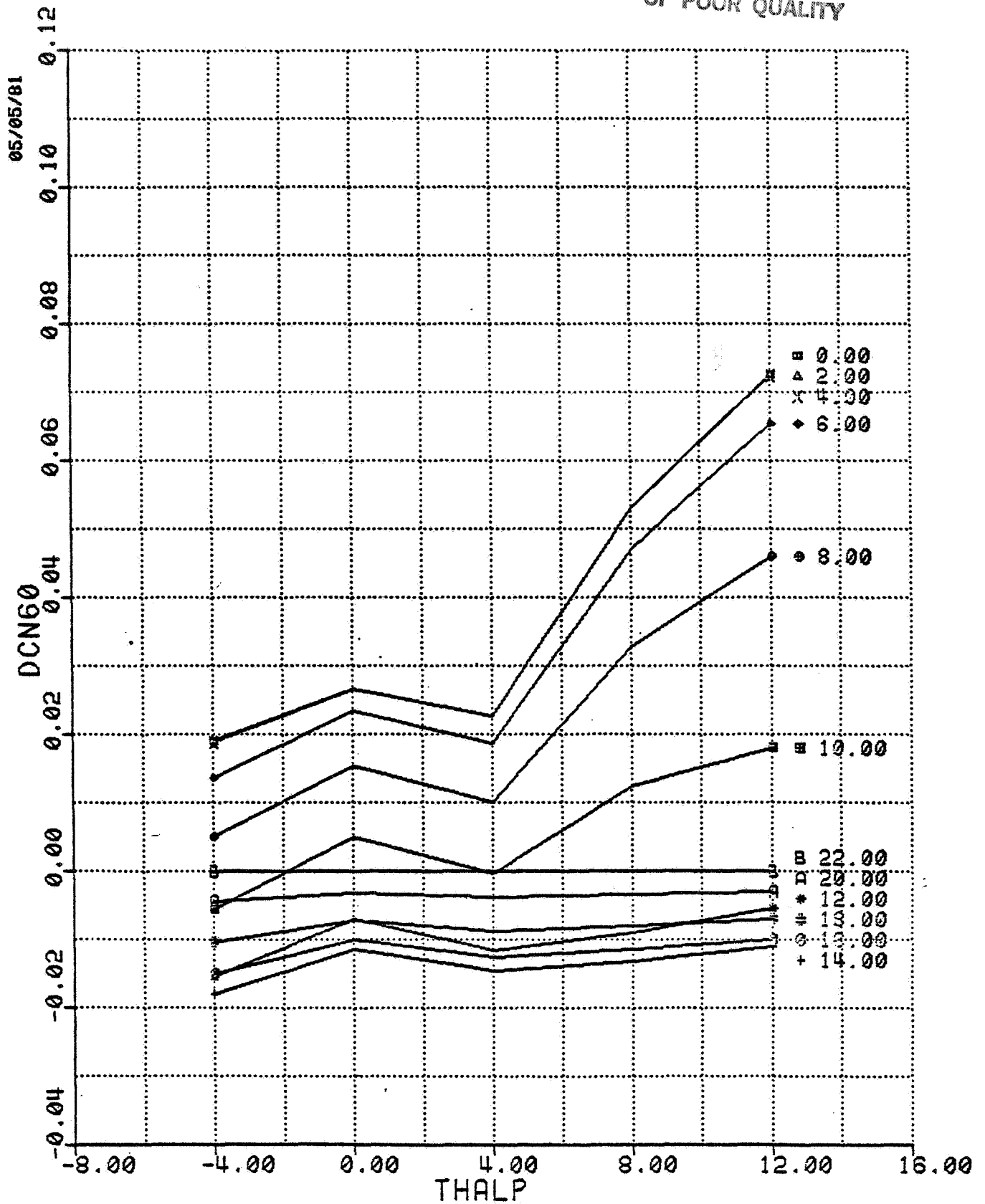
DCN50 VS THALP
FOR VARYING HP

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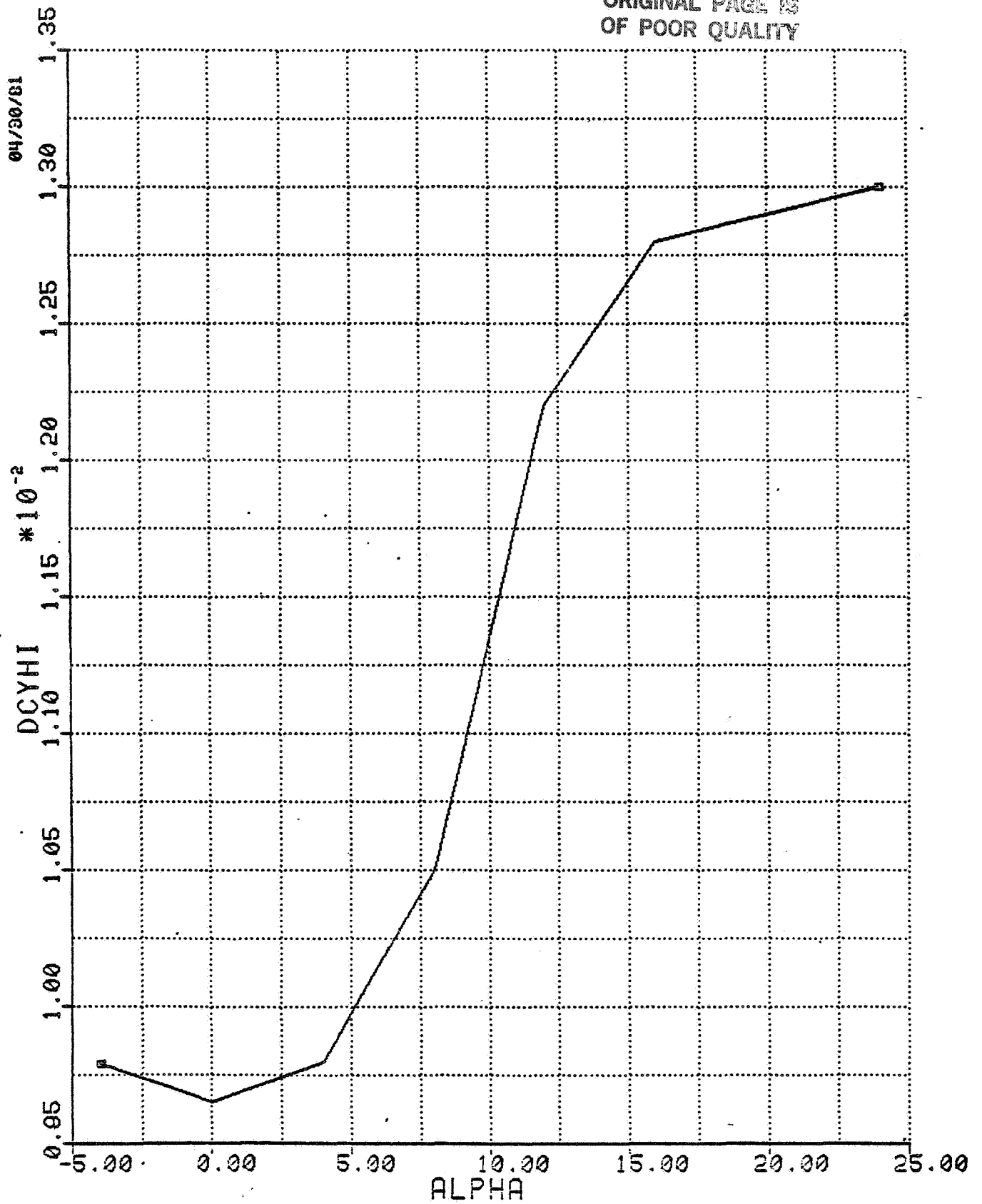
DCN60 VS THALP
FOR VARYING HP

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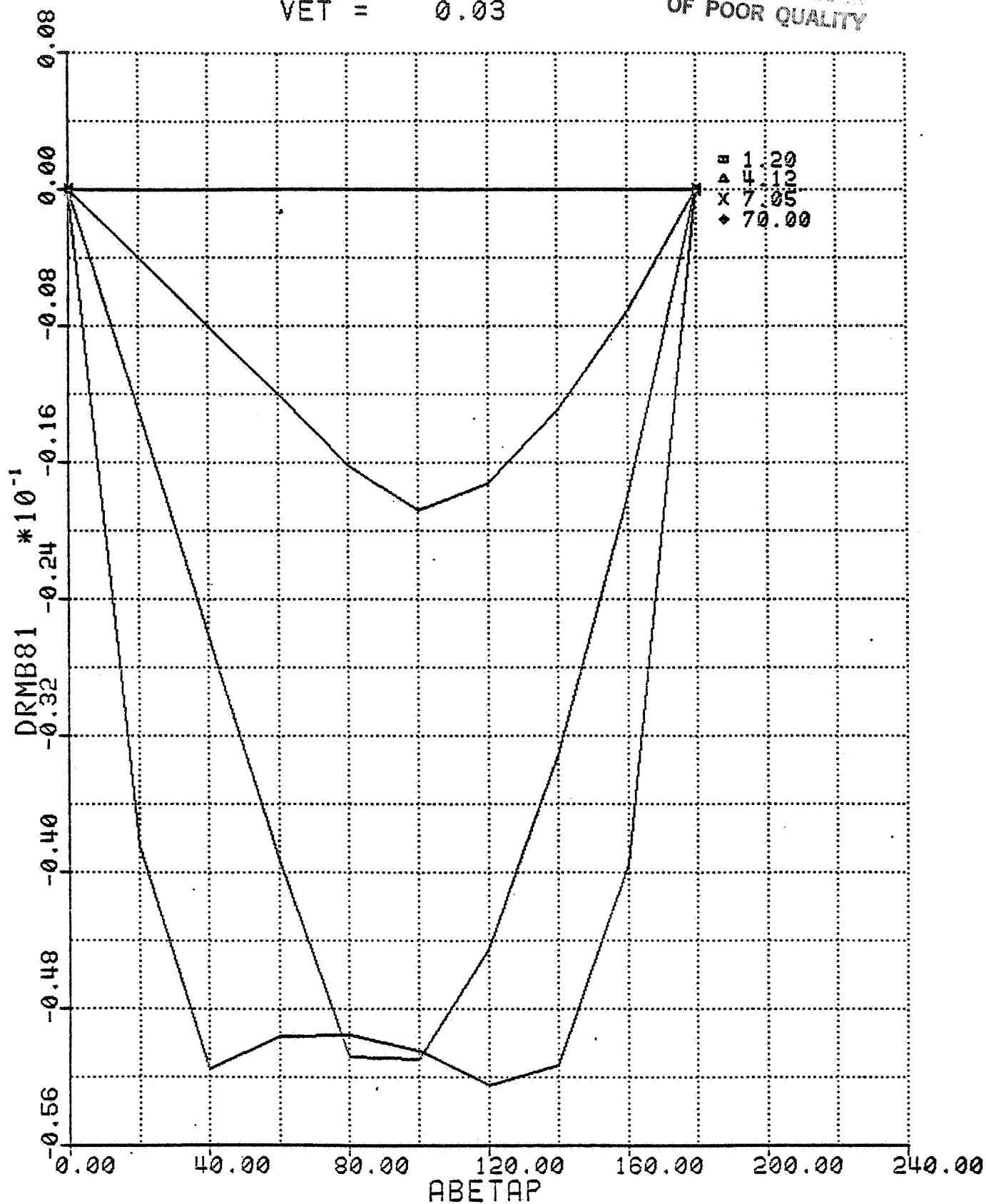
DCYHI VS ALPHA

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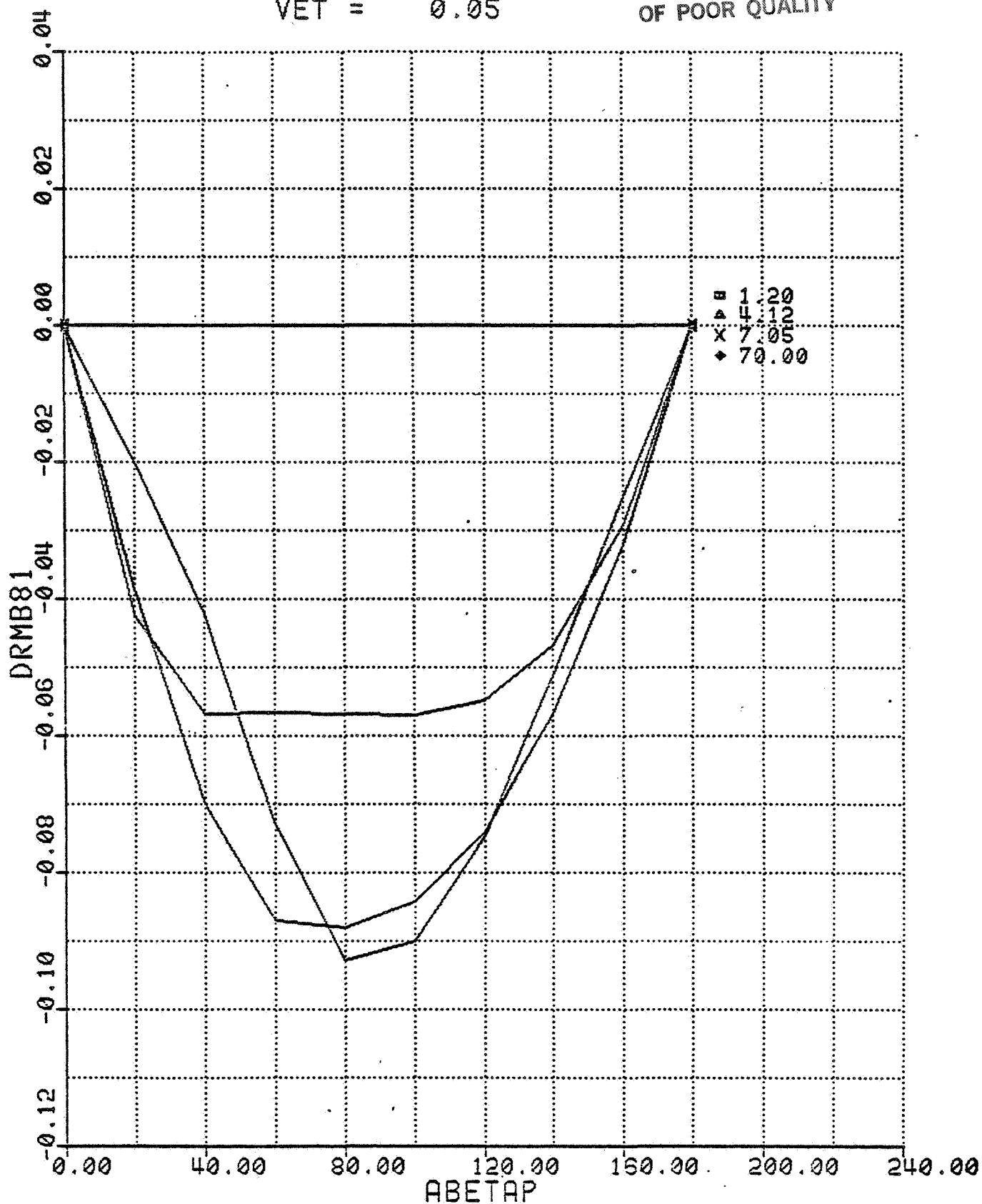
DRMB81 VS ABETAP
FOR VARYING HP
VET = 0.03

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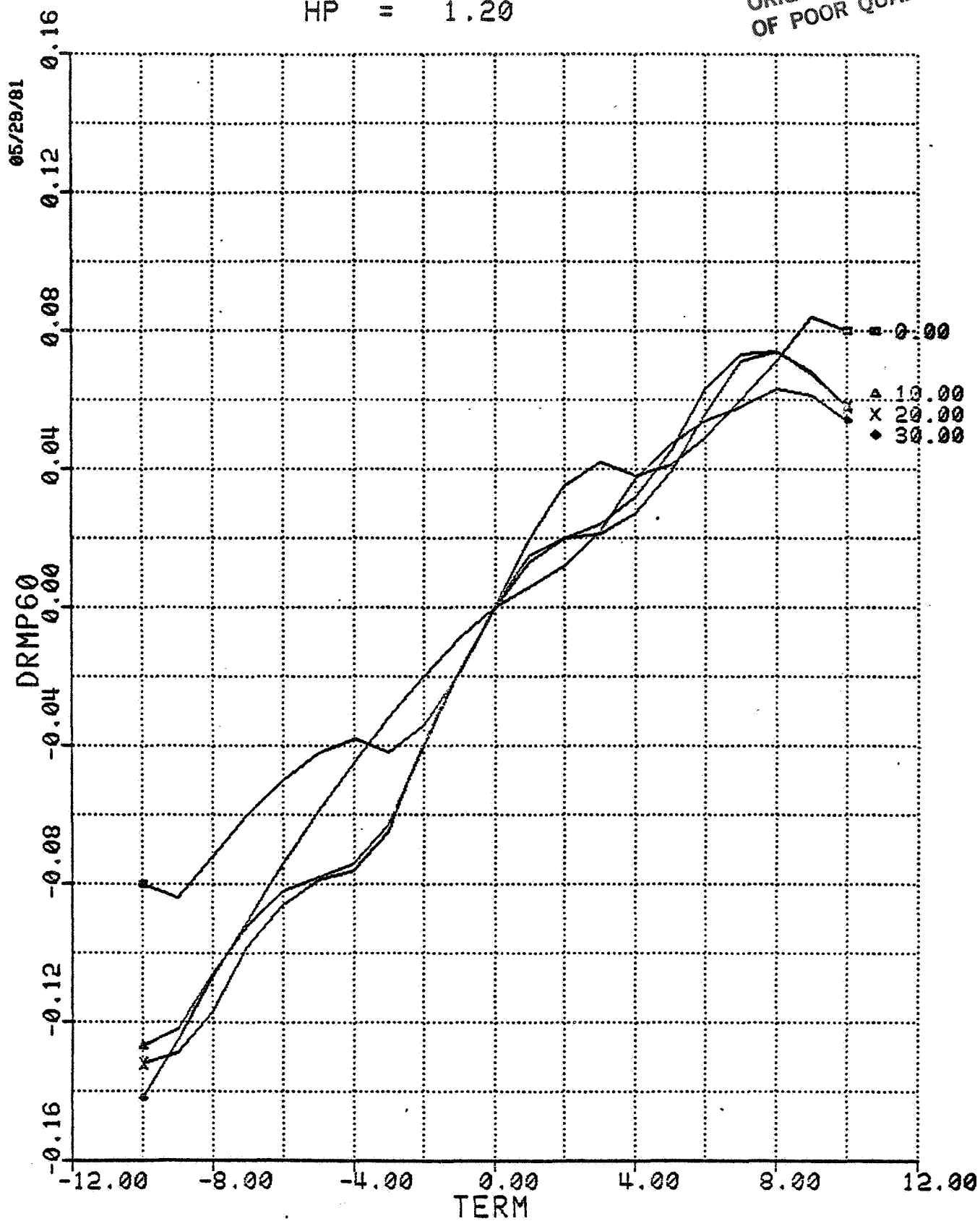
DRMB81 VS ABETAP
FOR VARYING HP
VET = 0.05

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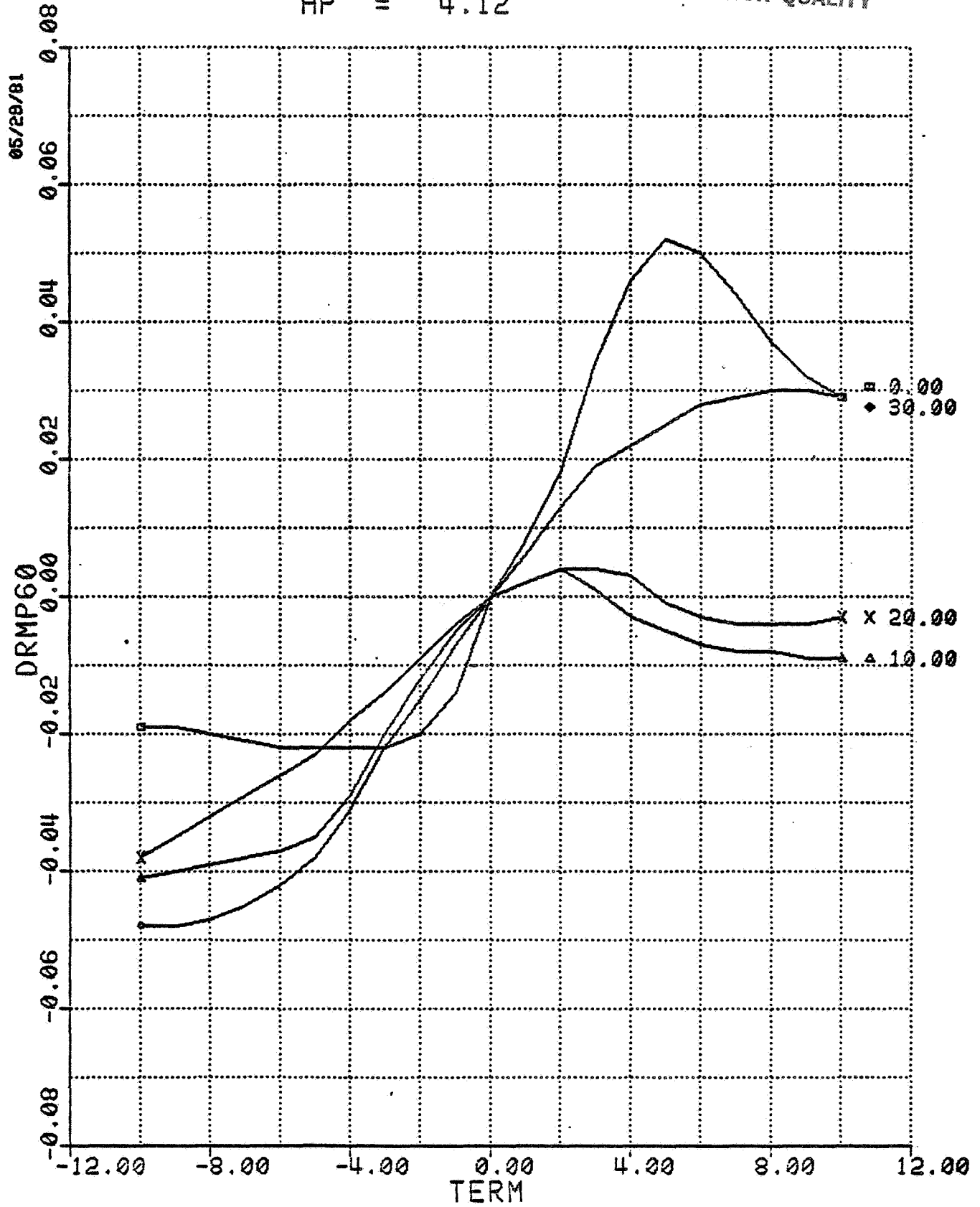
DRMP60 VS TERM
FOR VARYING ABETAP
HP = 1.20

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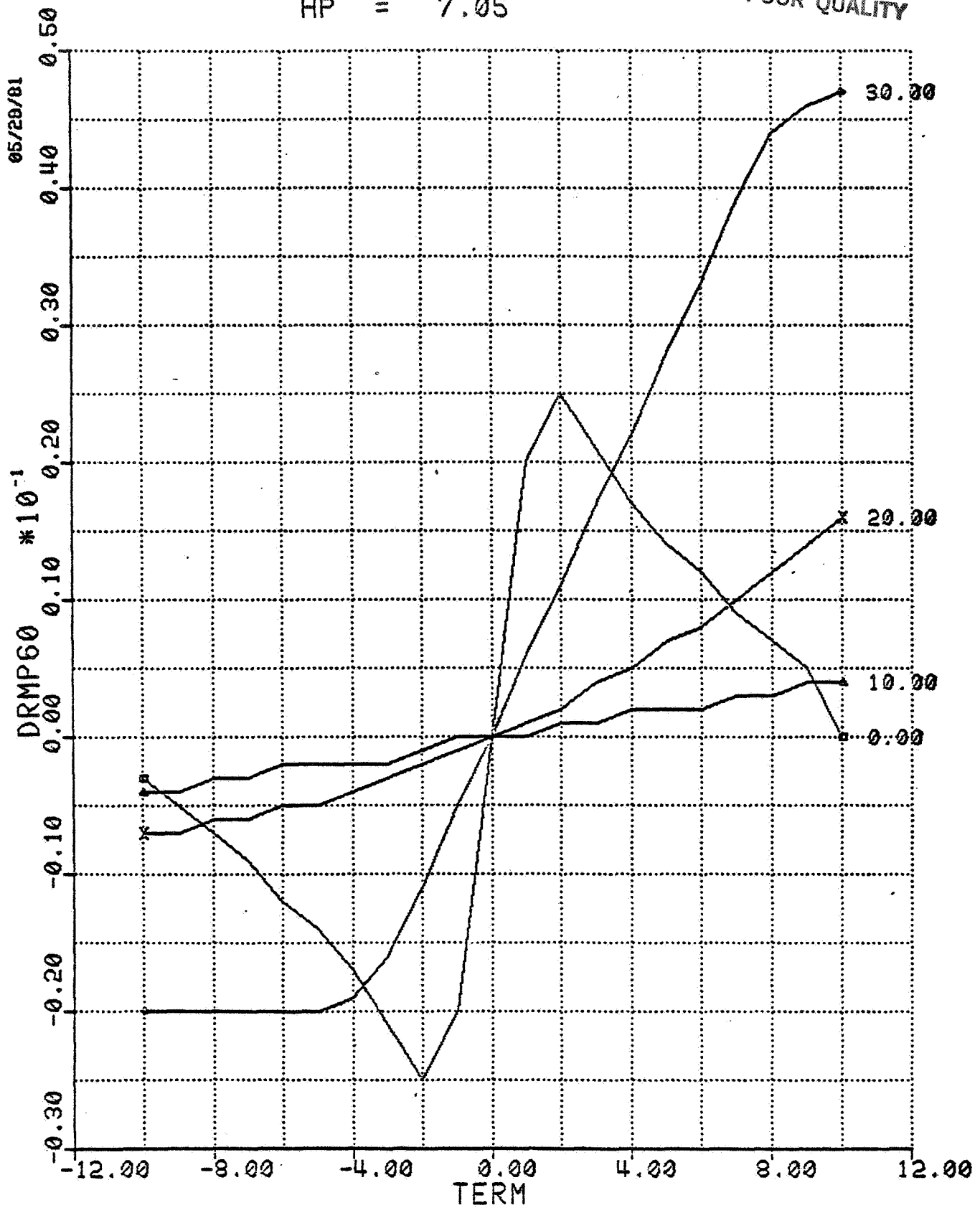
DRMP60 VS TERM
FOR VARYING ABETAP
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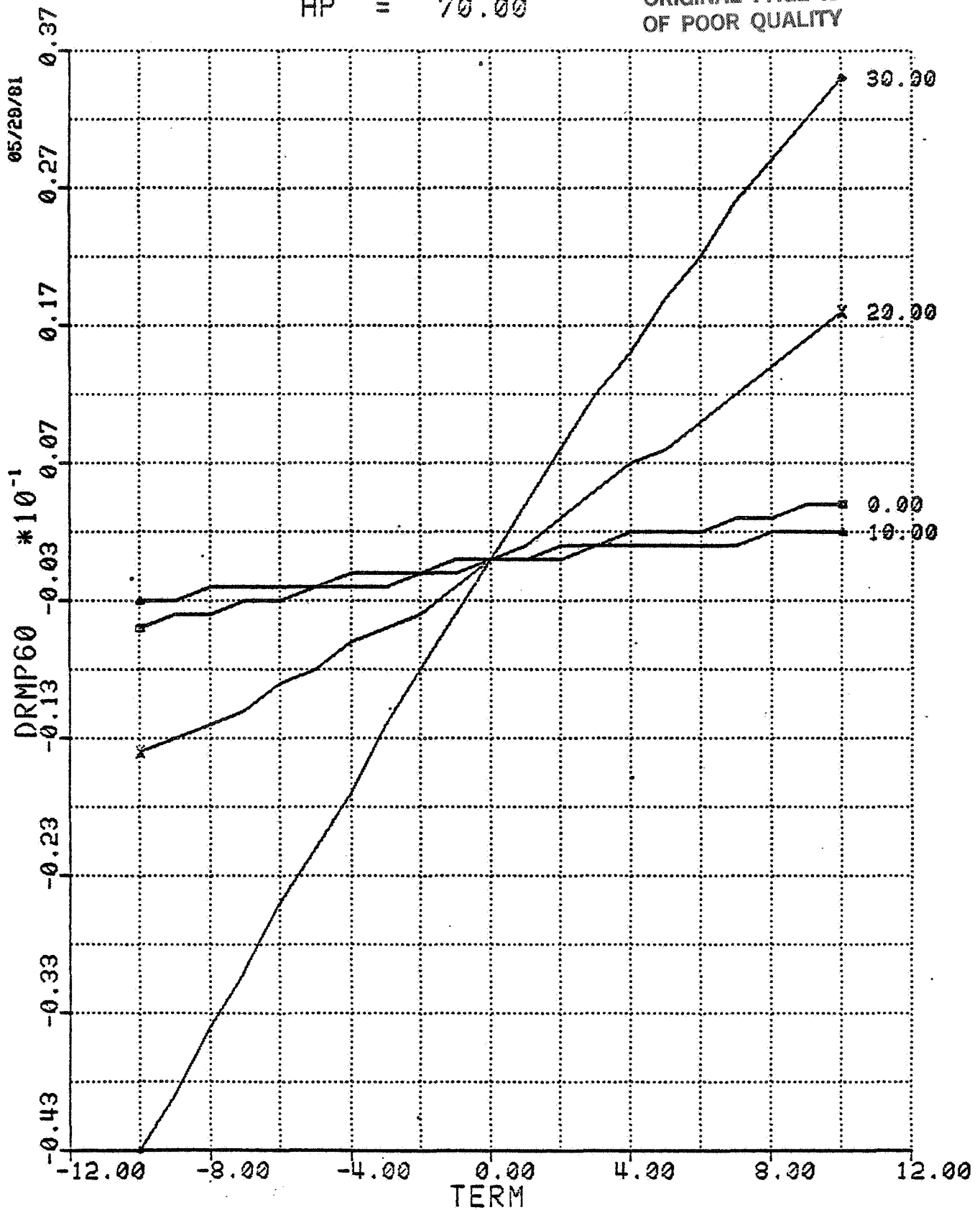
DRMP60 VS TERM
FOR VARYING ABETAP
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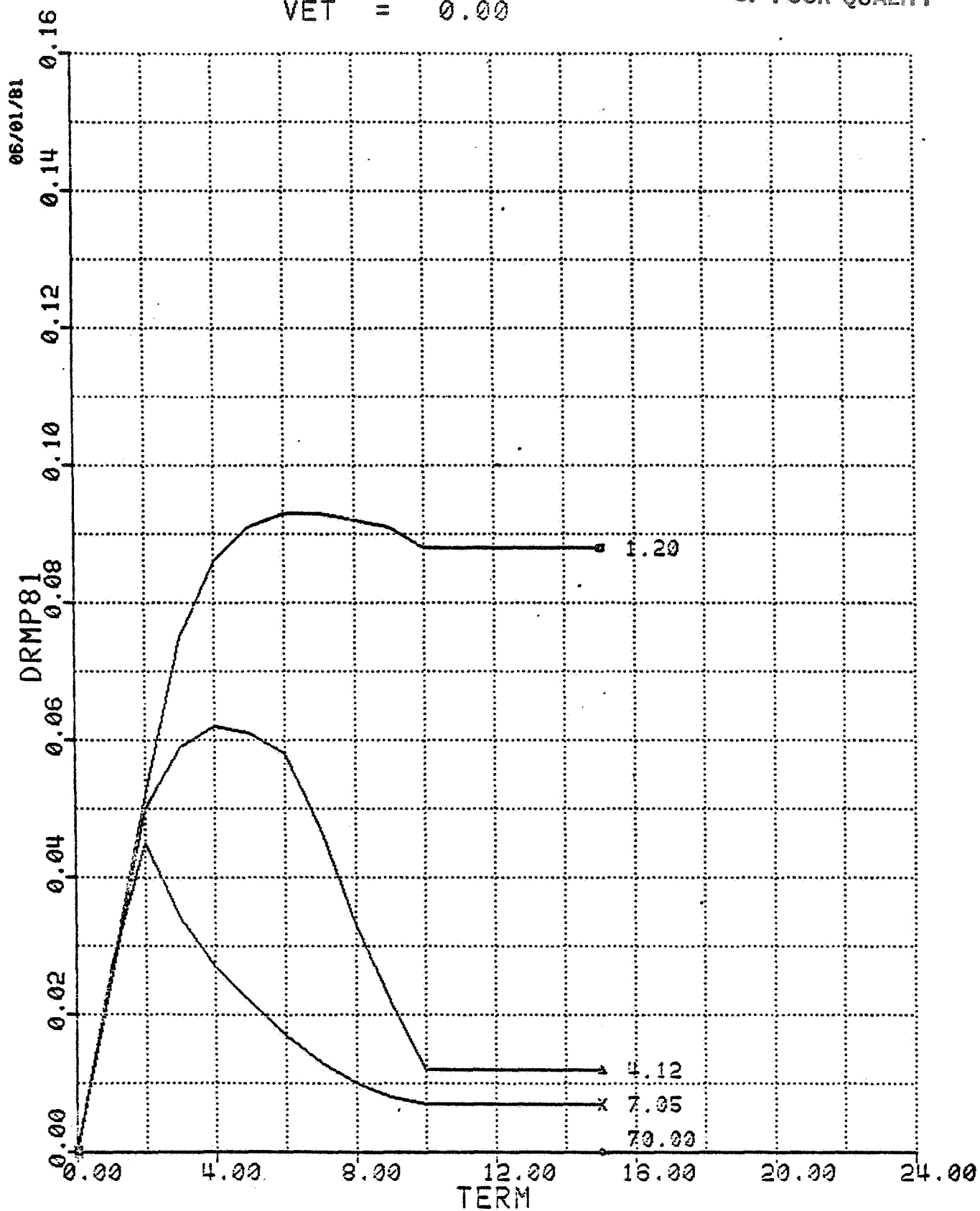
DRMP60 VS TERM
FOR VARYING ABETAP
HP = 70.00

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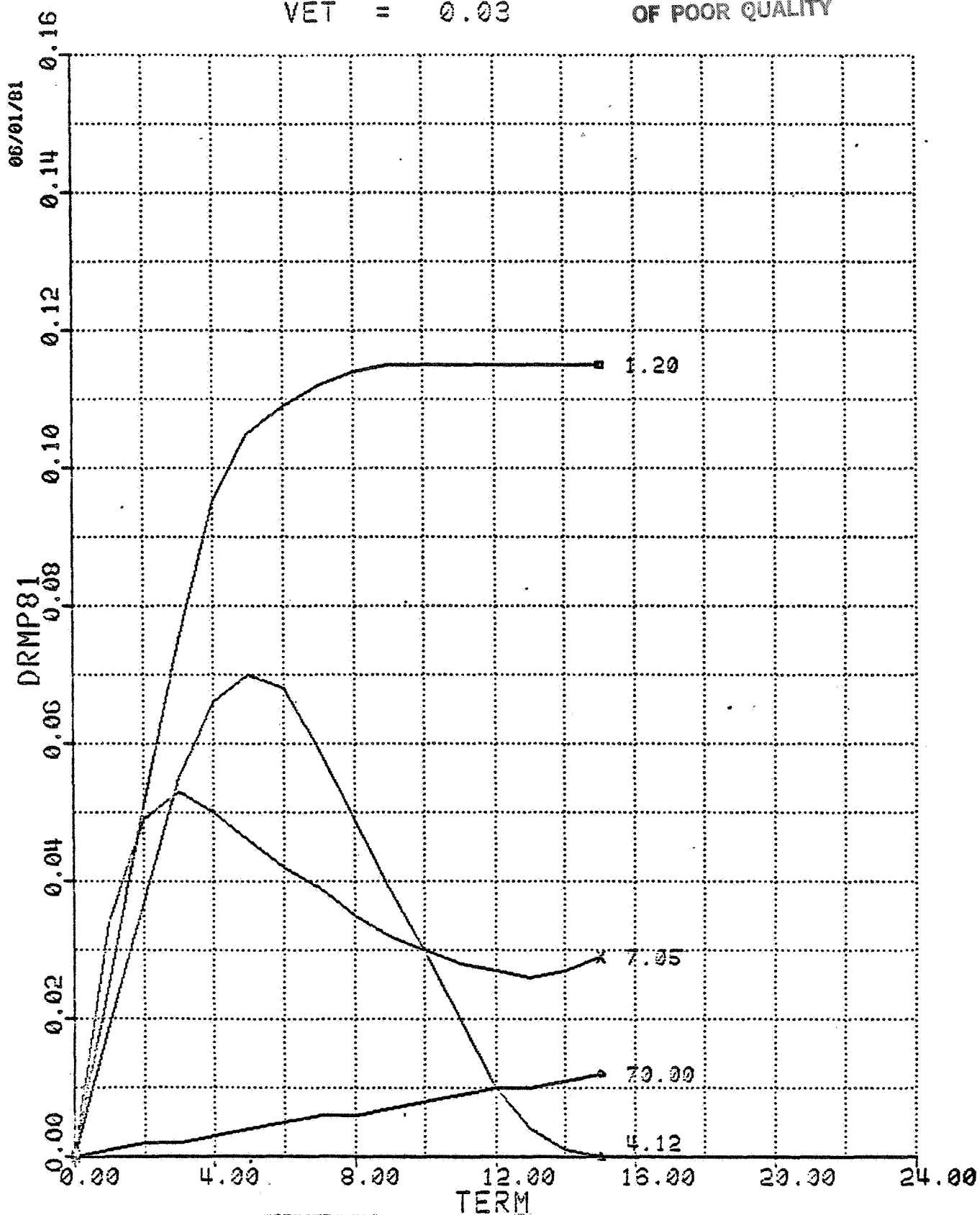
DRMP81 VS TERM
FOR VARYING HP
VET = 0.00

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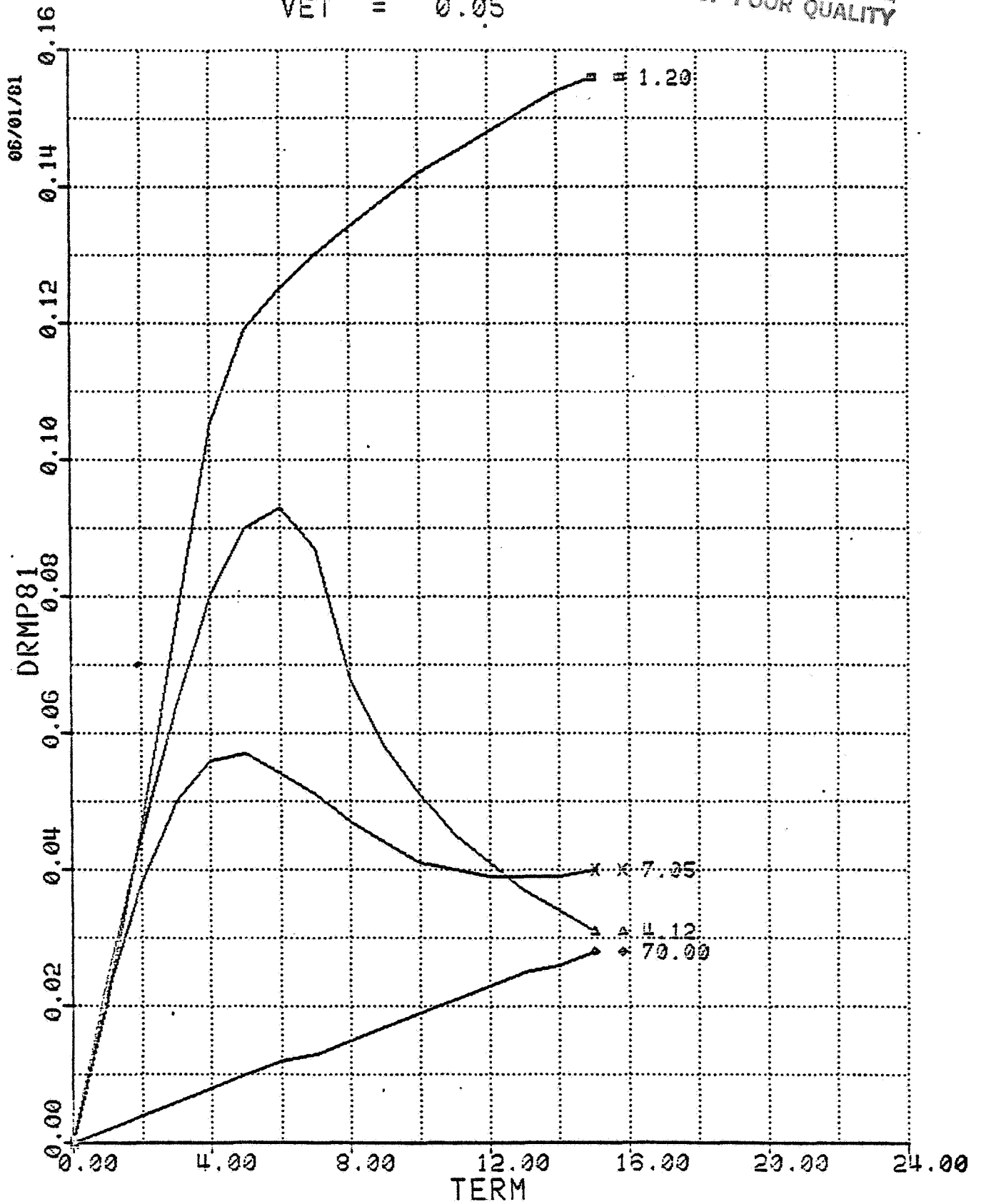
DRMP81 VS TERM
FOR VARYING HP
VET = 0.03

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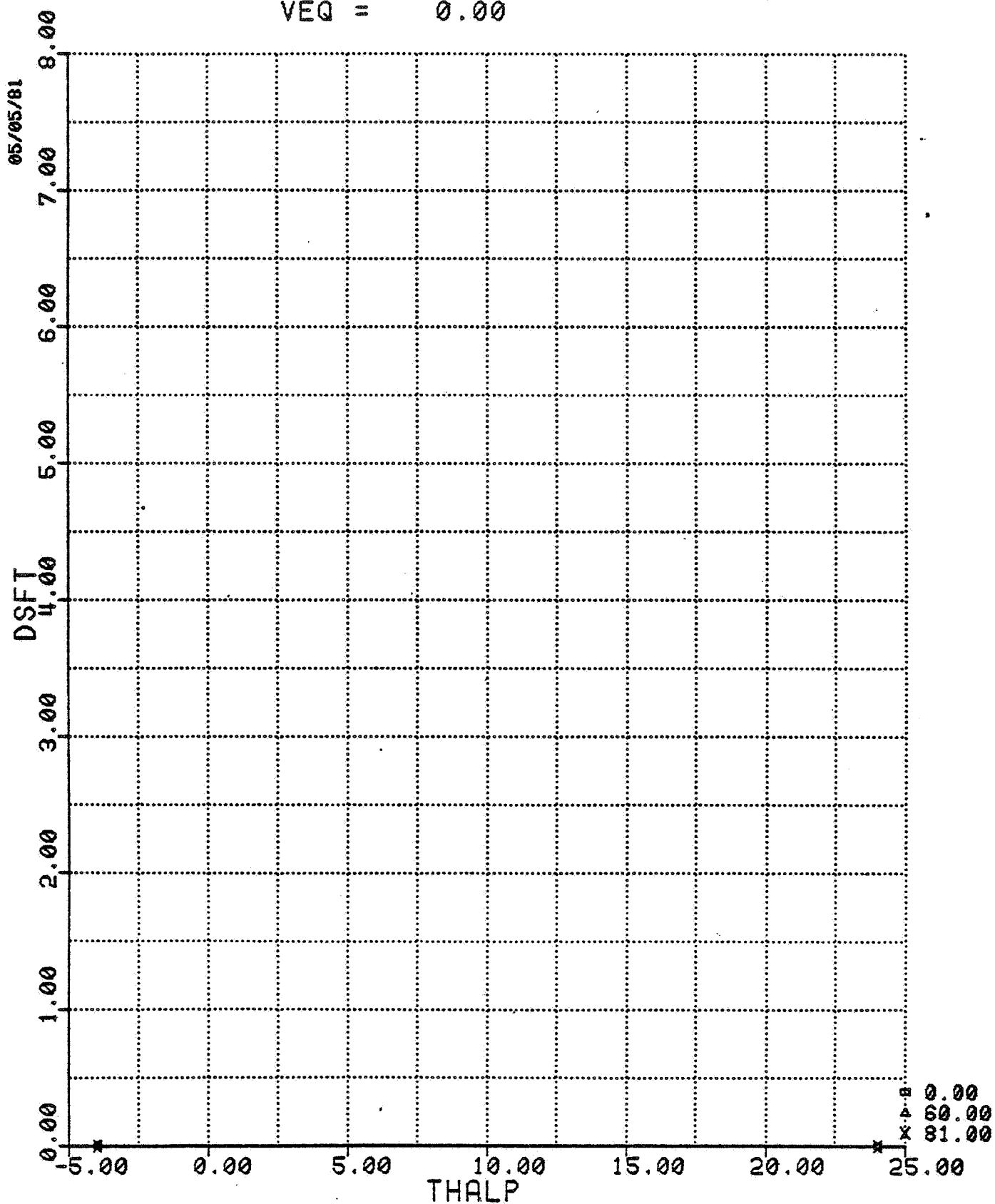
DRMP81 VS TERM
FOR VARYING HP
VET = 0.05

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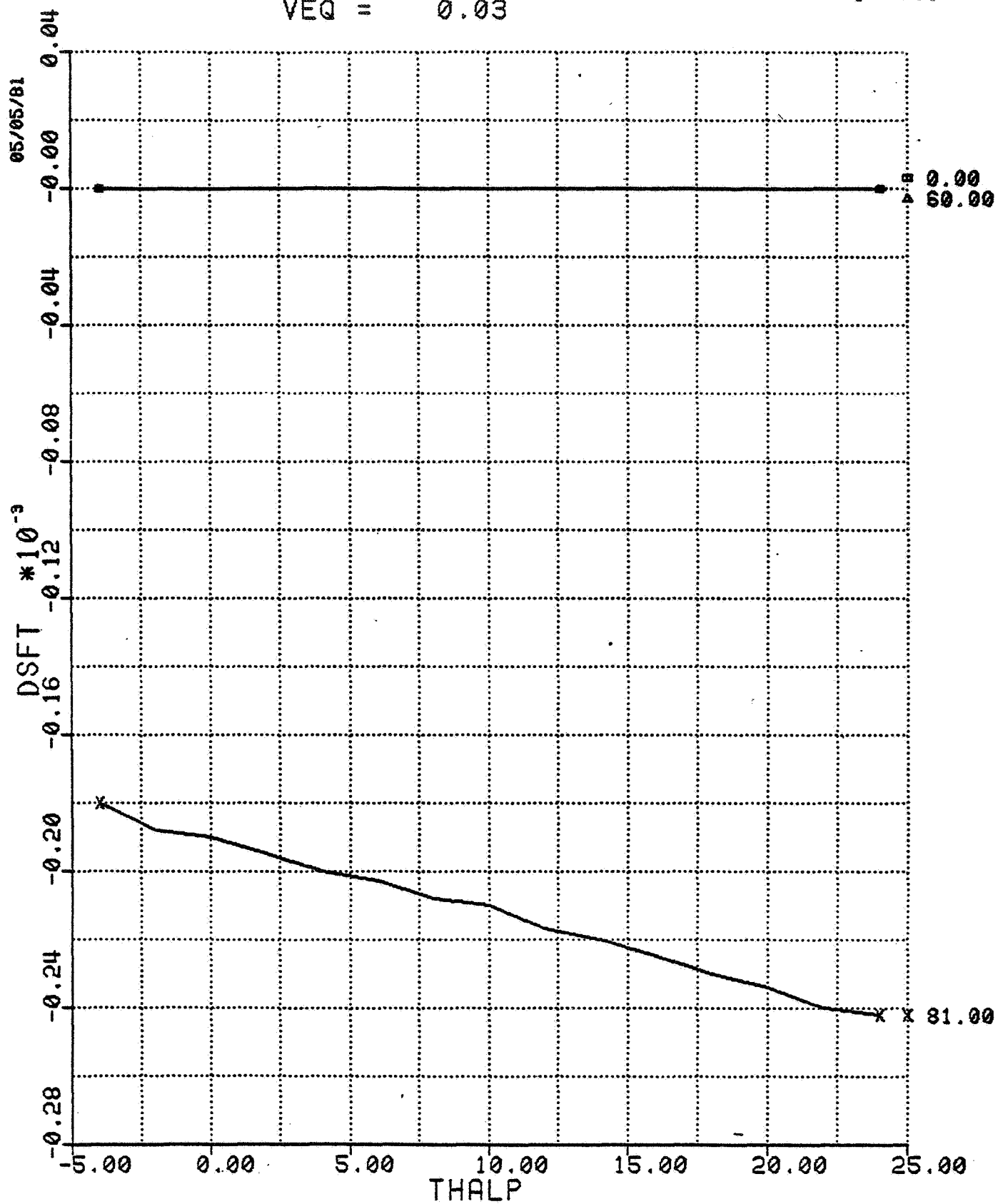
DSFT VS THALP
FOR VARYING THETAJ
VEQ = 0.00

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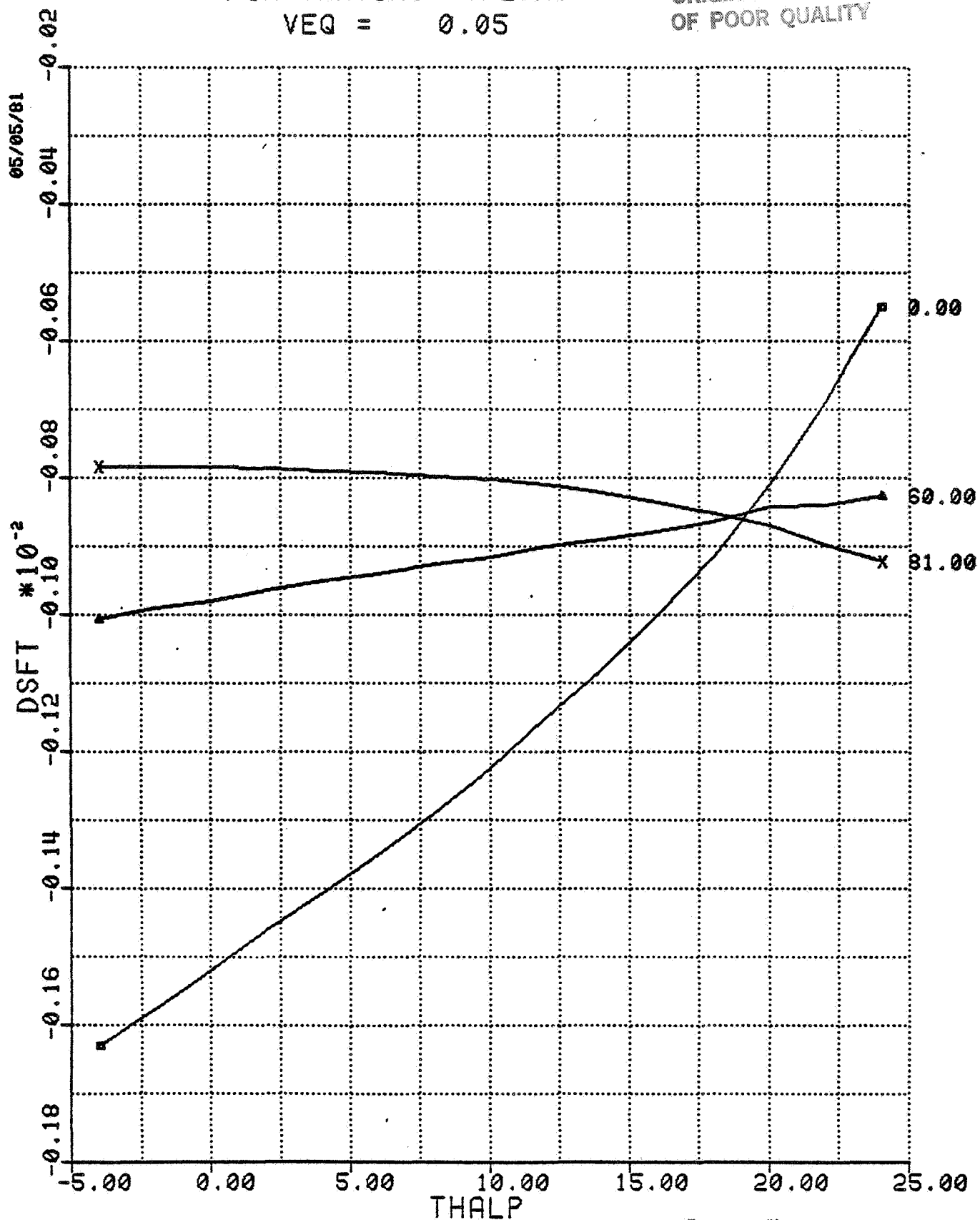
DSFT VS THALP
FOR VARYING THETAJ
VEQ = 0.03

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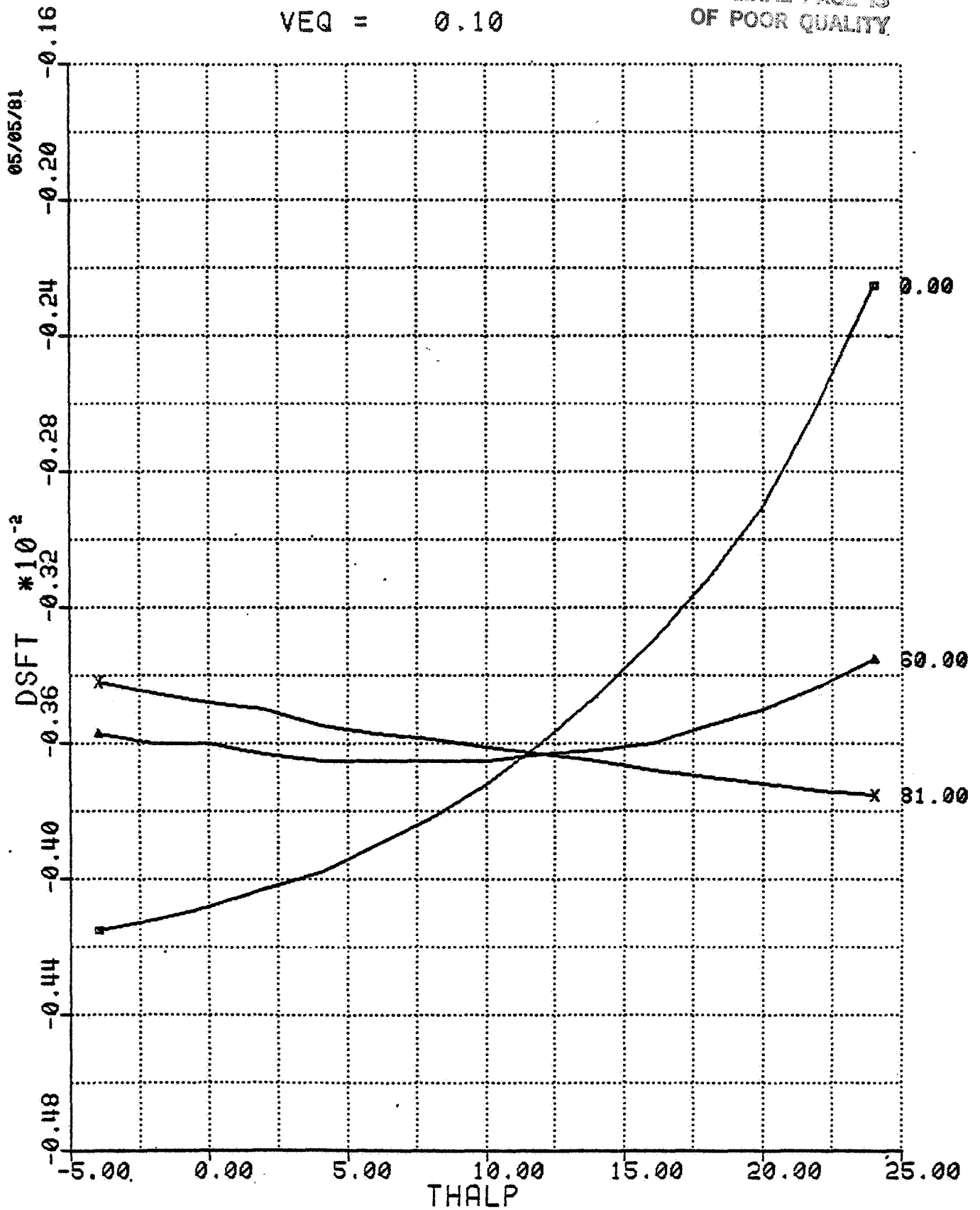
DSFT VS THALP
FOR VARYING THETAJ
VEQ = 0.05

ORIGINAL PAGE 18
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DSFT VS THALP
FOR VARYING THETAJ
VEQ = 0.10

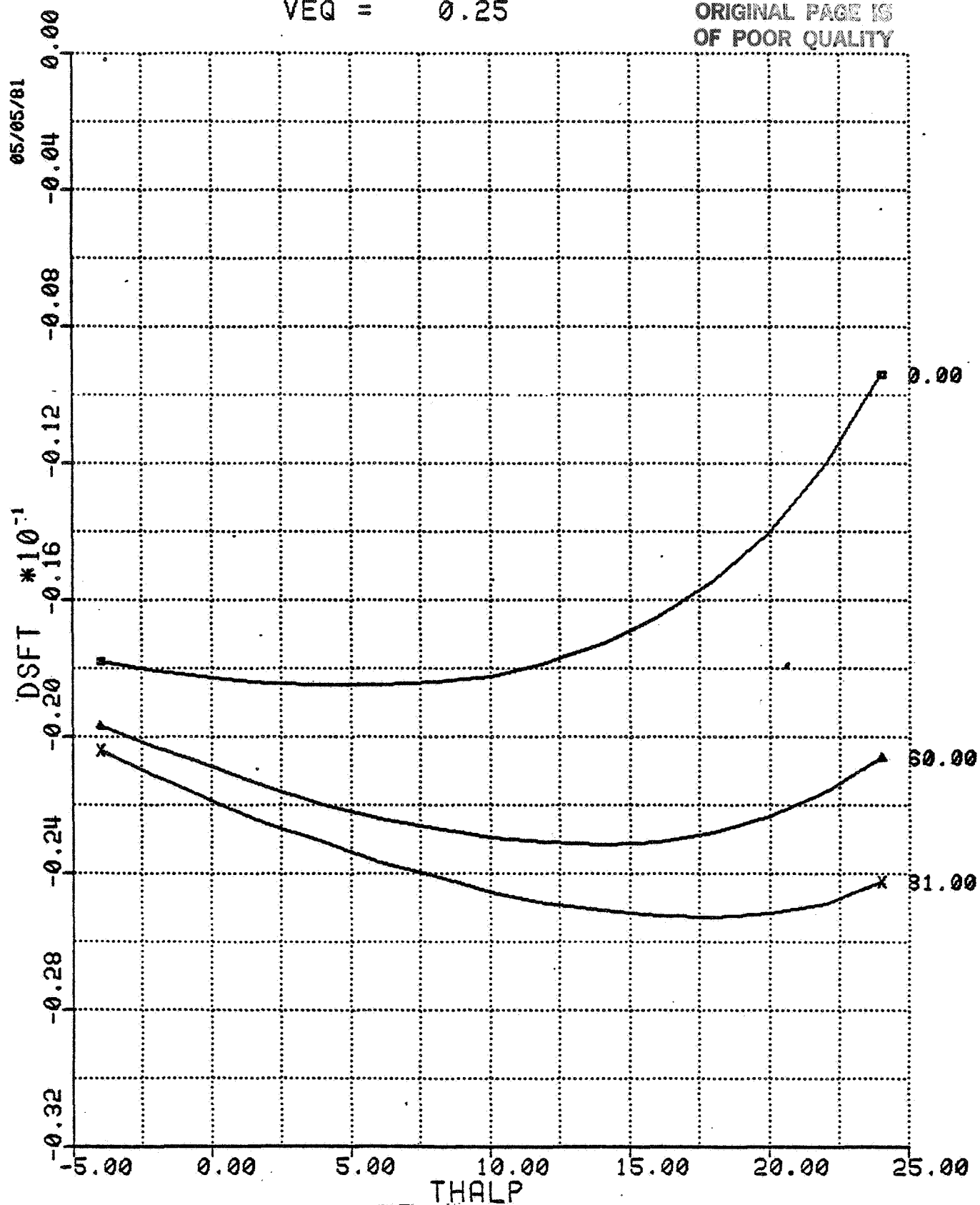
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DSFT VS THALP
FOR VARYING THETAJ

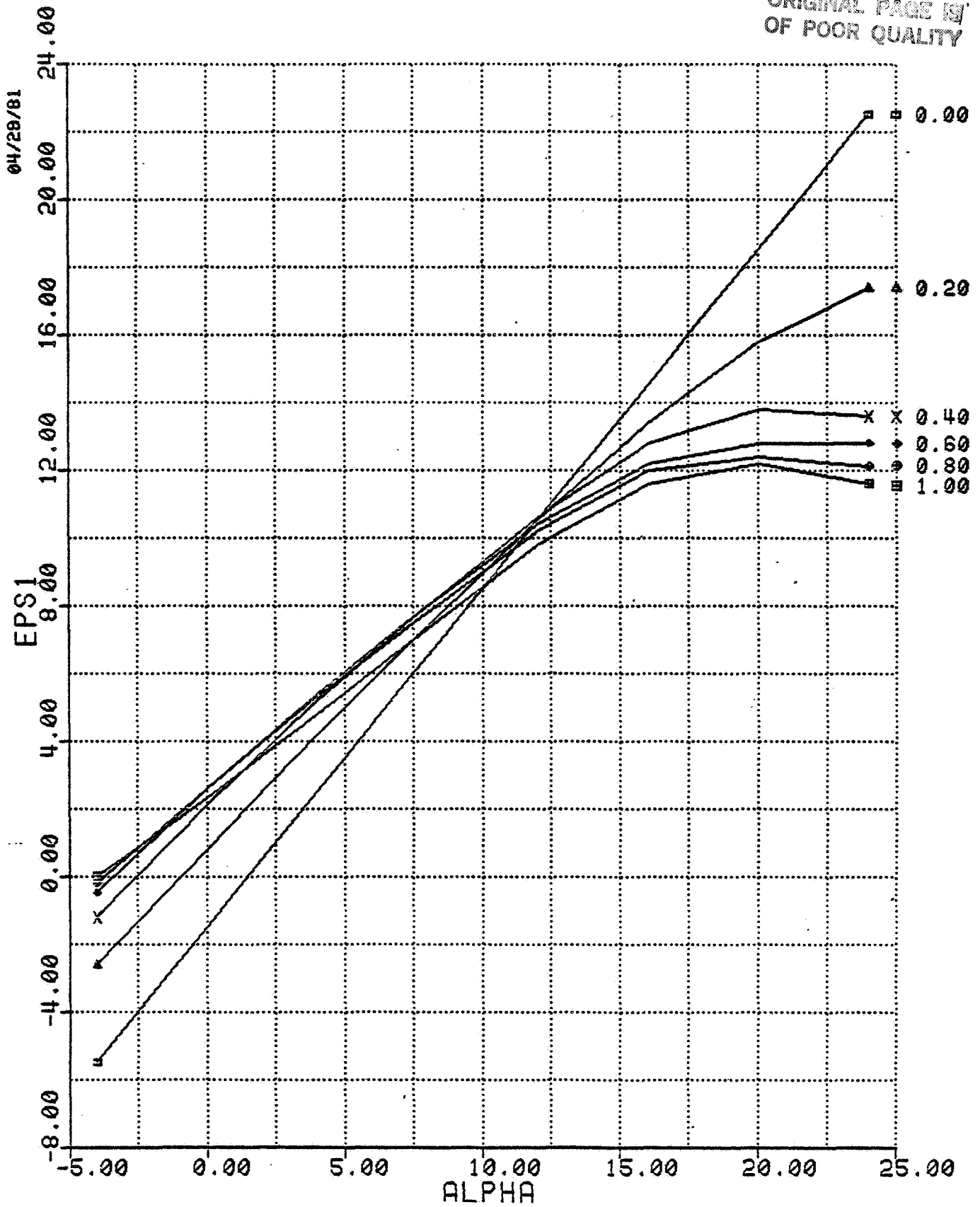
VEQ = 0.25

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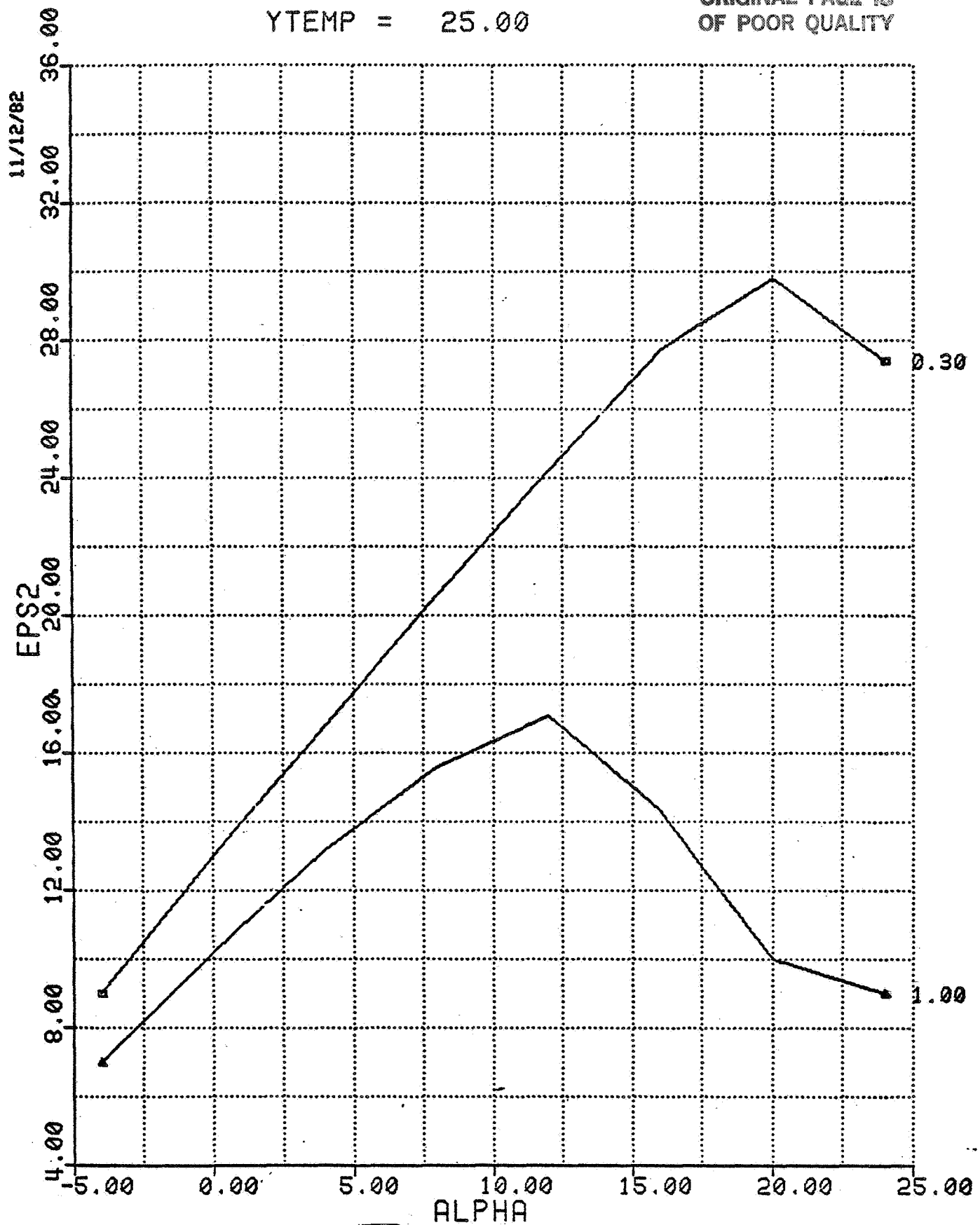
EPS1 VS ALPHA
FOR VARYING VEQ

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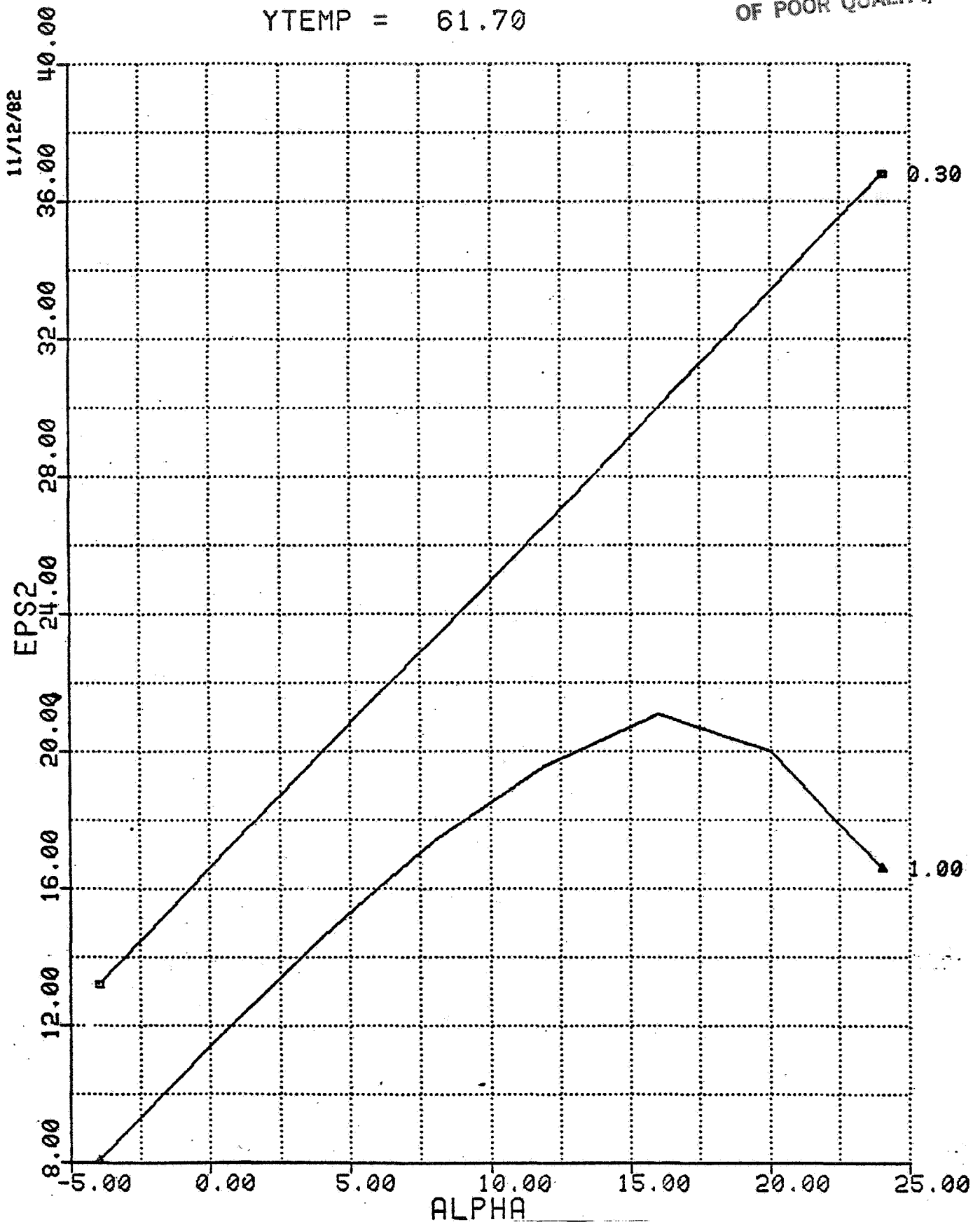
EPS2 VS ALPHA
FOR VARYING VEQ
YTEMP = 25.00

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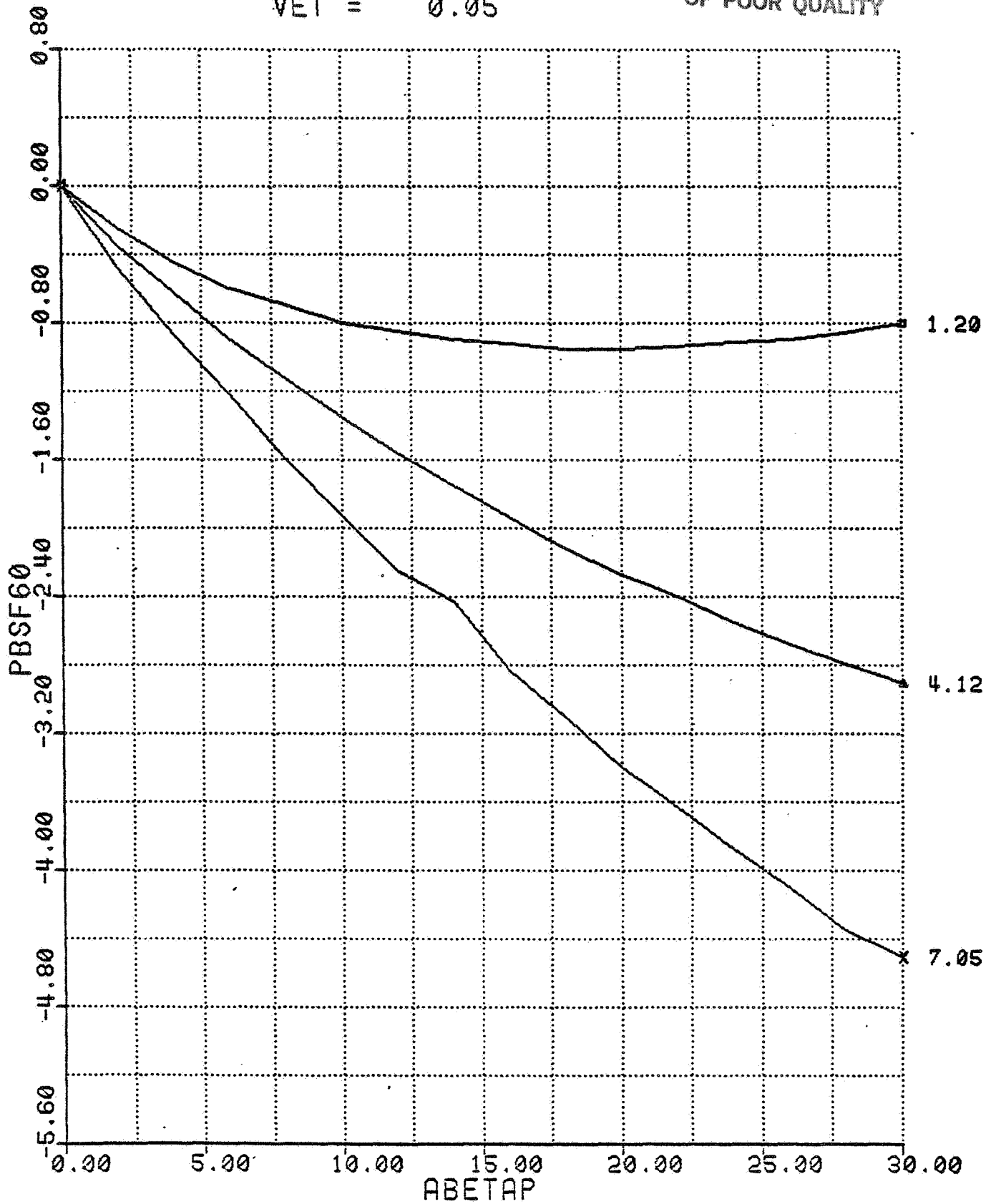
EPS2 VS ALPHA
FOR VARYING VEQ
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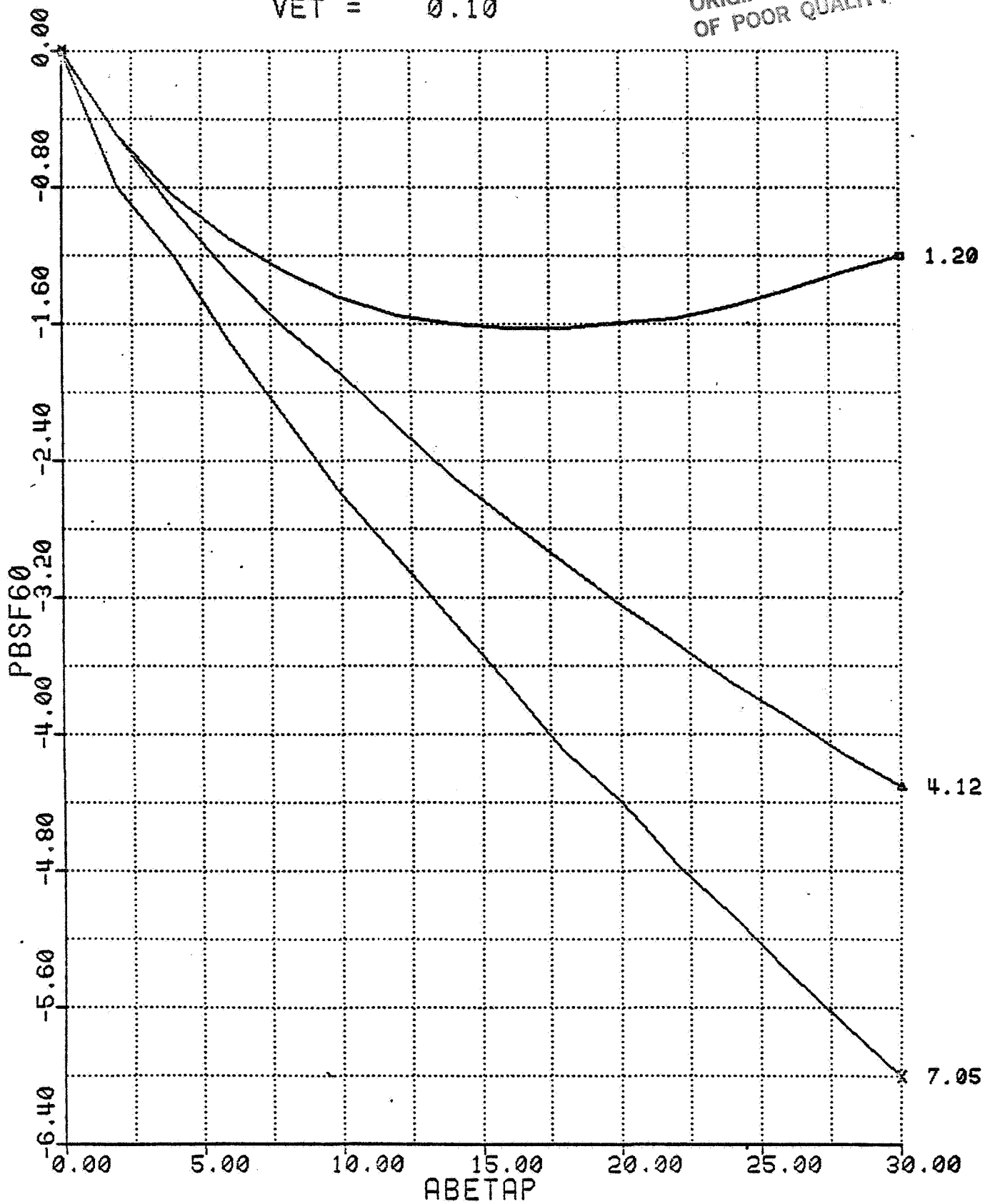
PBSF60 VS ABETAP
FOR VARYING HP
VET = 0.05

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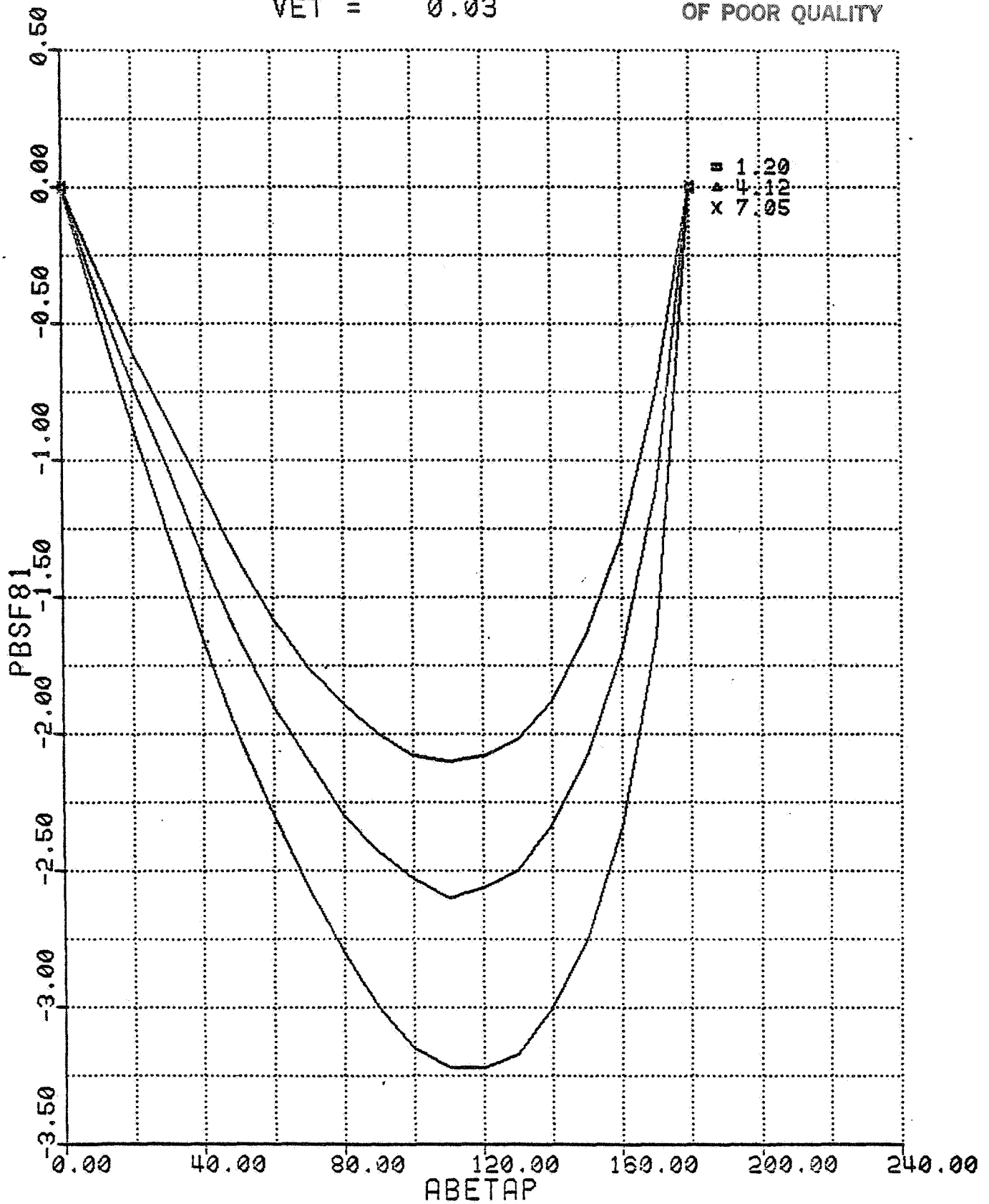
PBSF60 VS ABETAP
FOR VARYING HP
VET = 0.10

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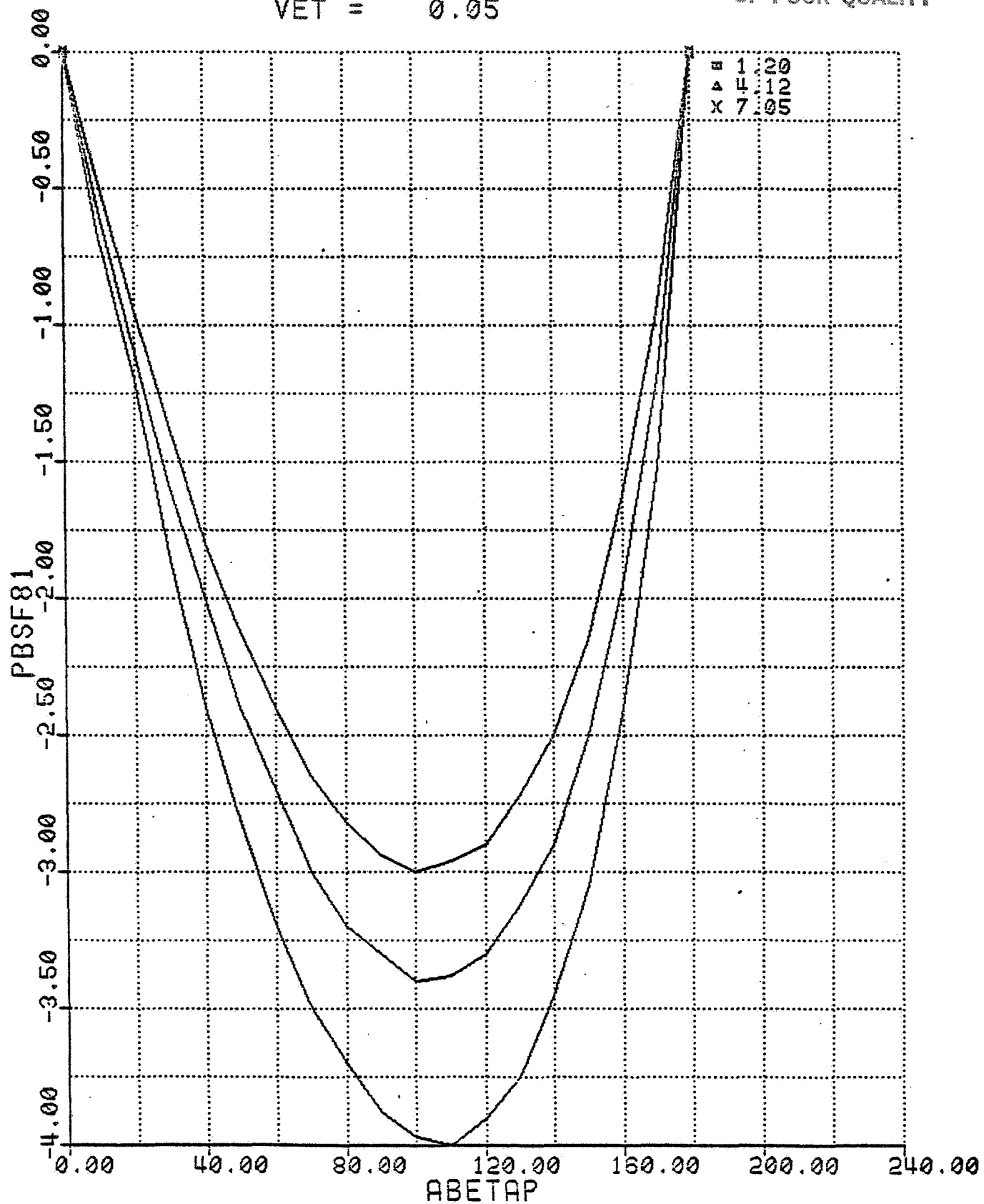
PBSF81 VS ABETAP
FOR VARYING HP
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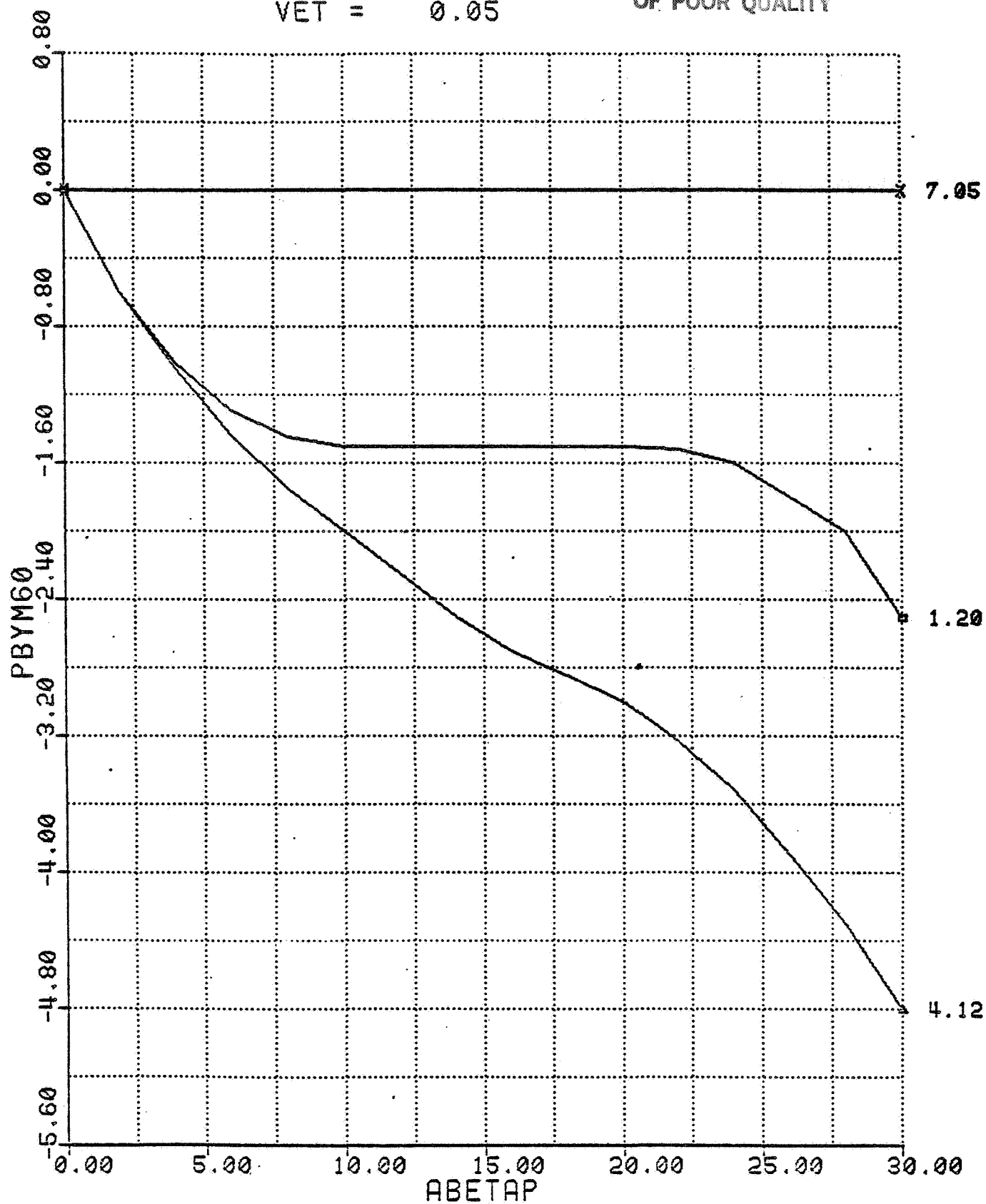
PBSF81 VS ABETAP
FOR VARYING HP
VET = 0.05

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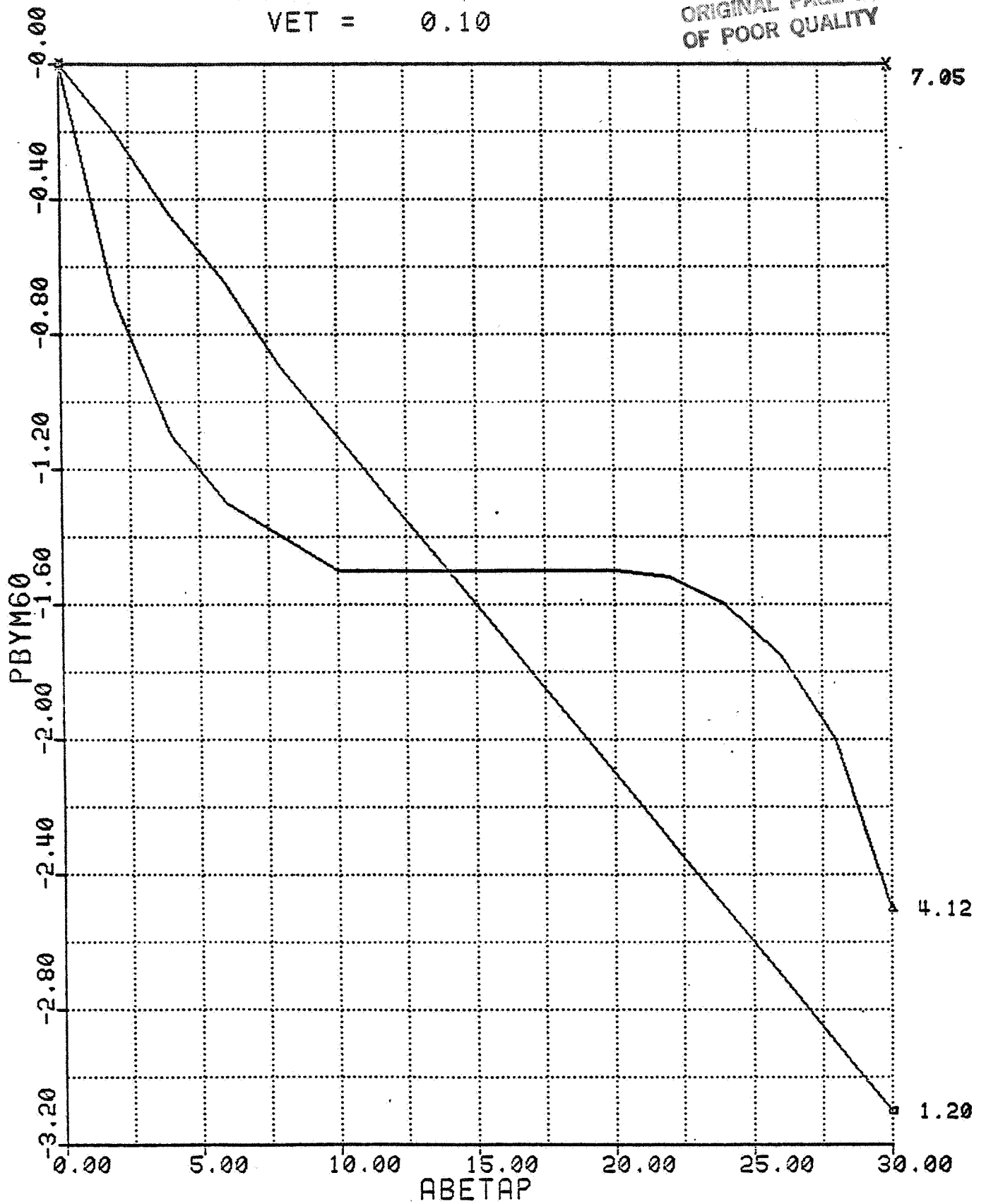
PBYM60 VS ABETAP
FOR VARYING HP
VET = 0.05

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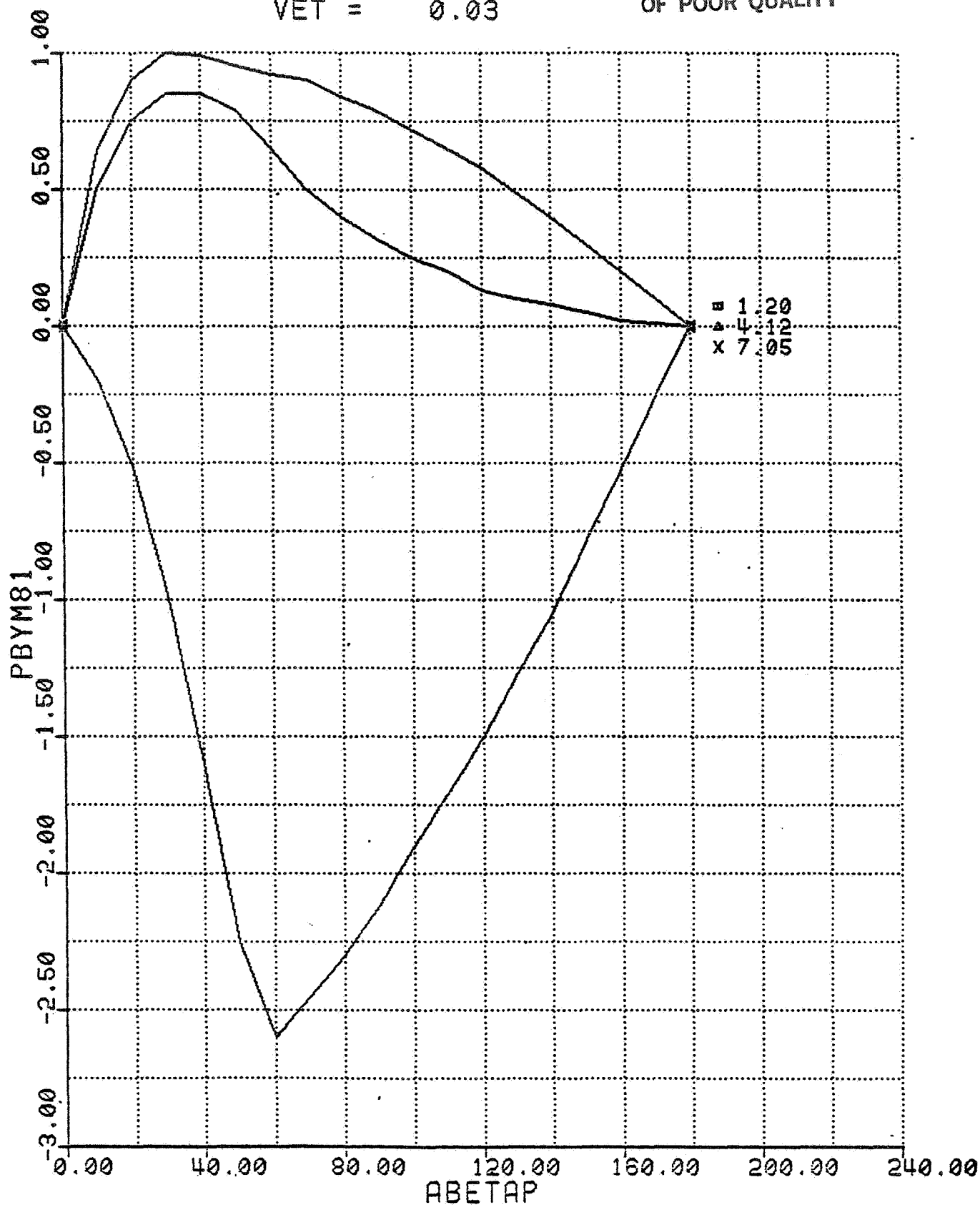
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PBYM81 VS ABETAP
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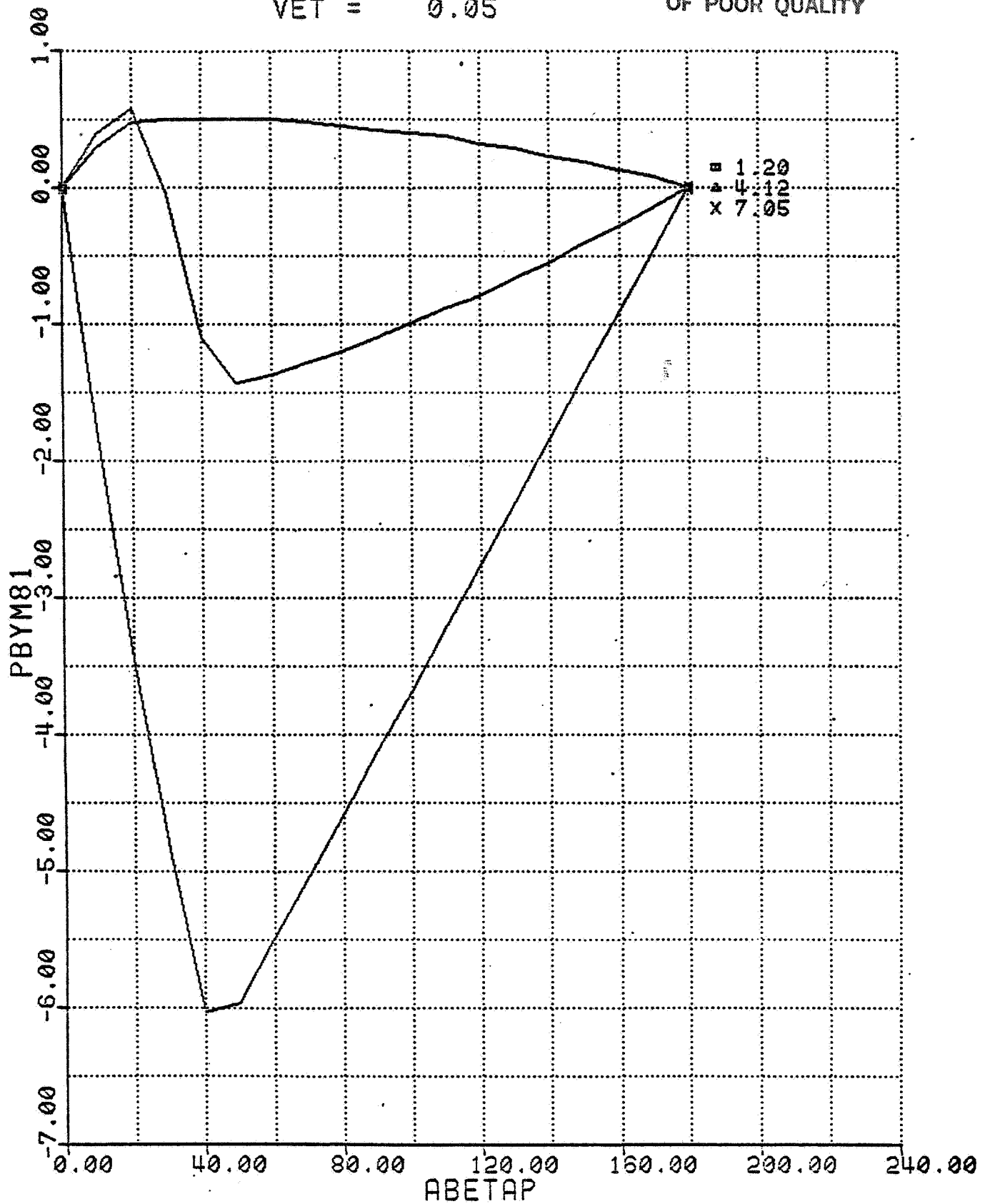
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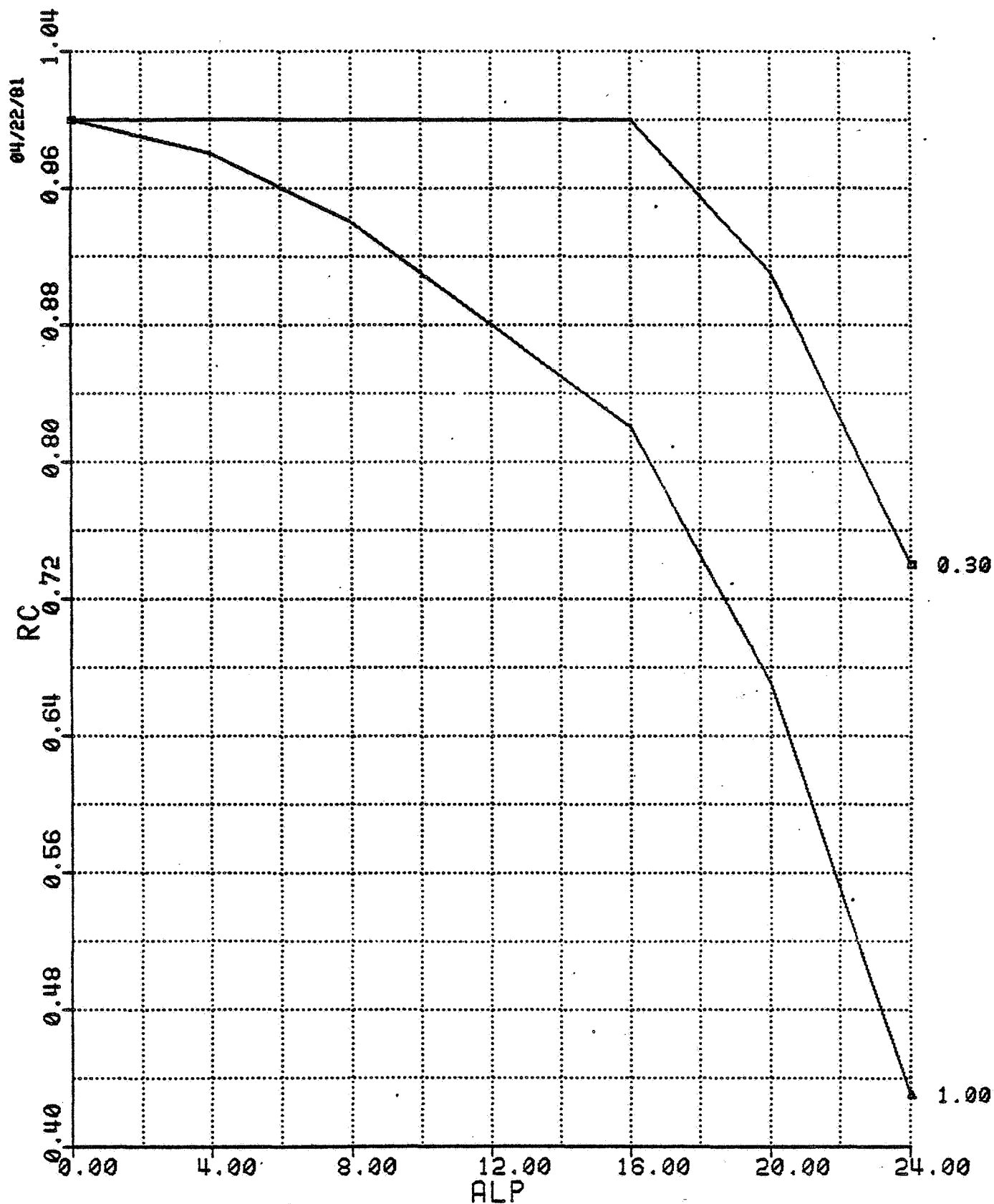
MCDONNELL DOUGLAS

PBYM81 VS ABETAP
FOR VARYING HP
VET = 0.05

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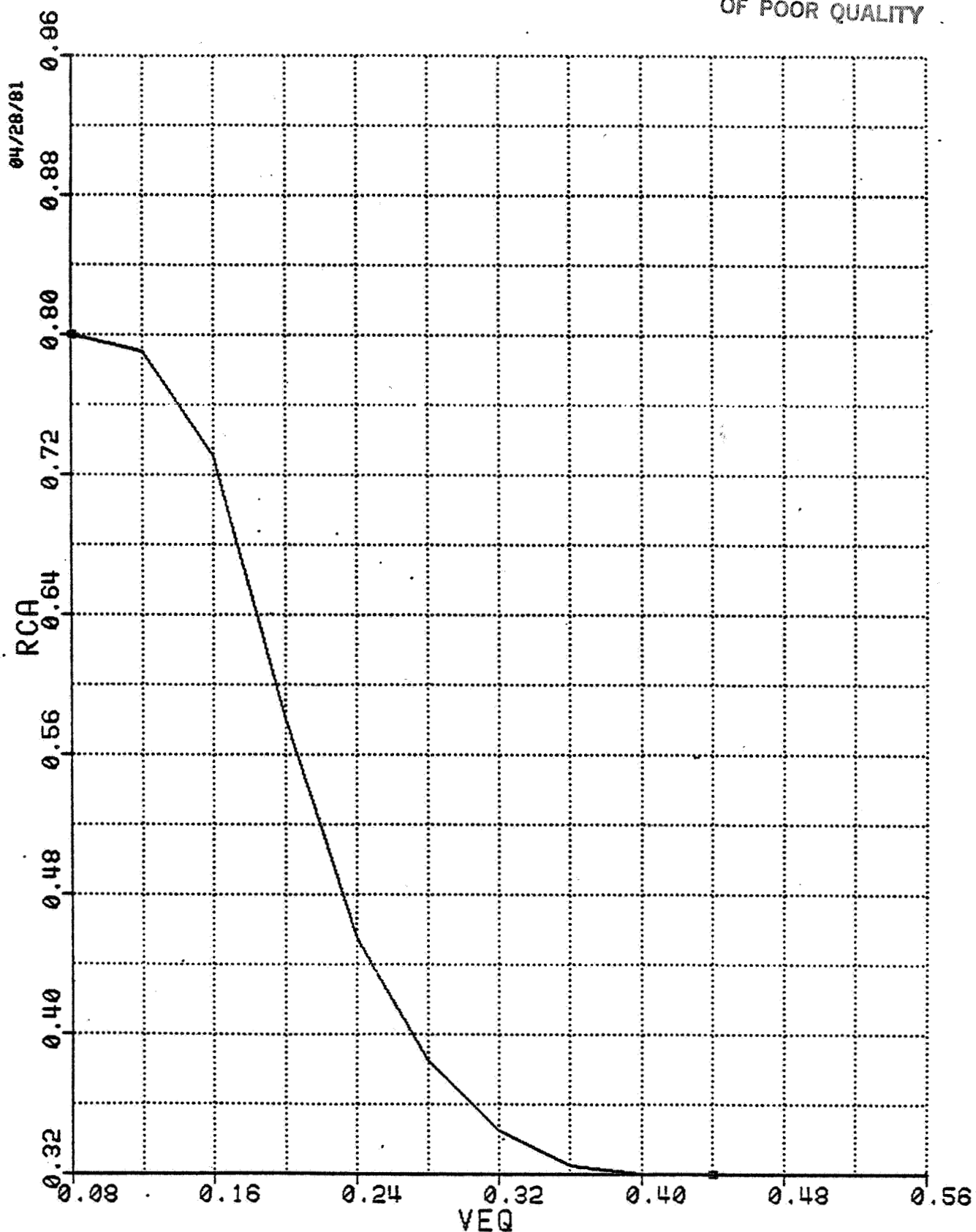


RC VS ALP ORIGINAL PAGE IS
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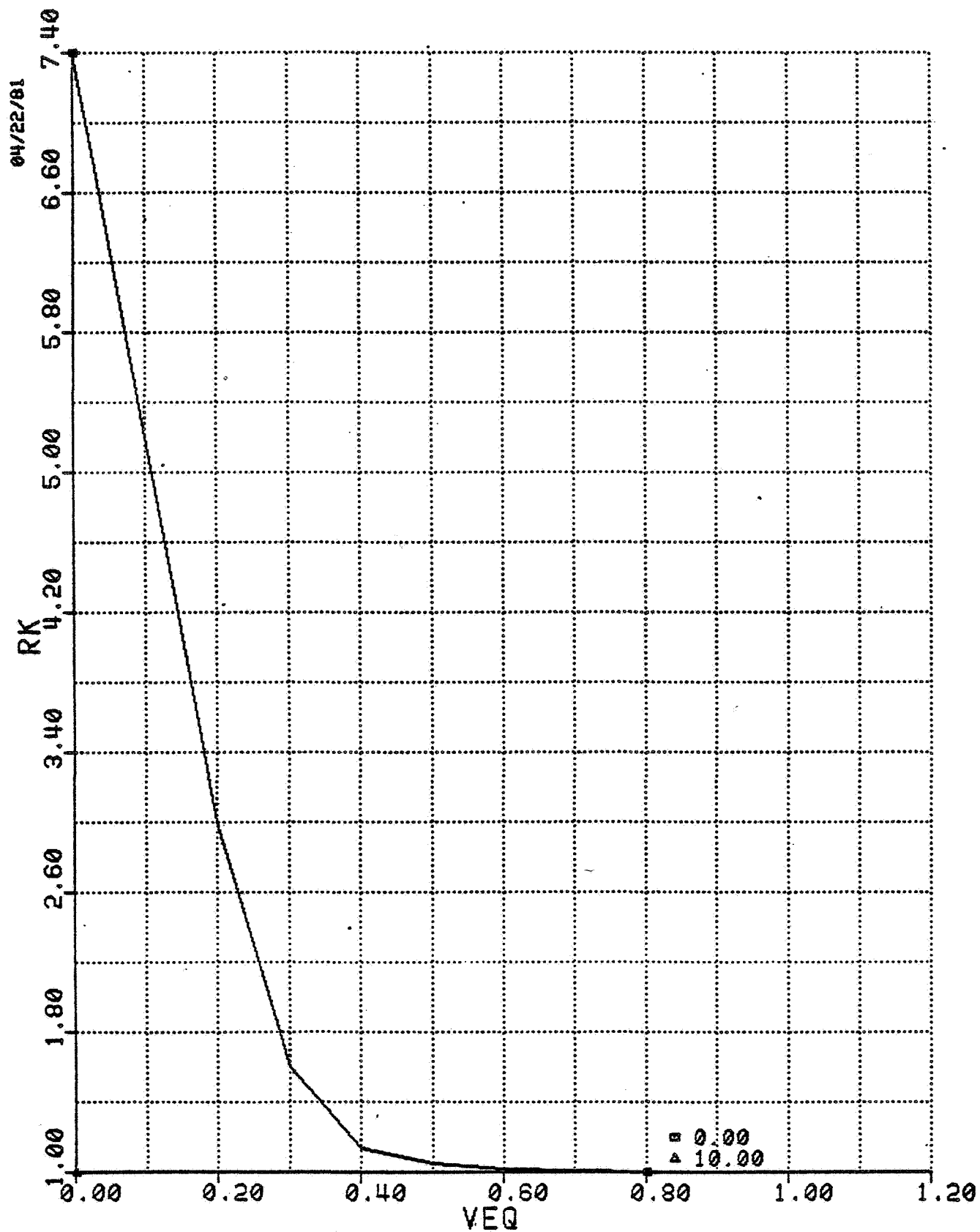
RCA VS VEQ

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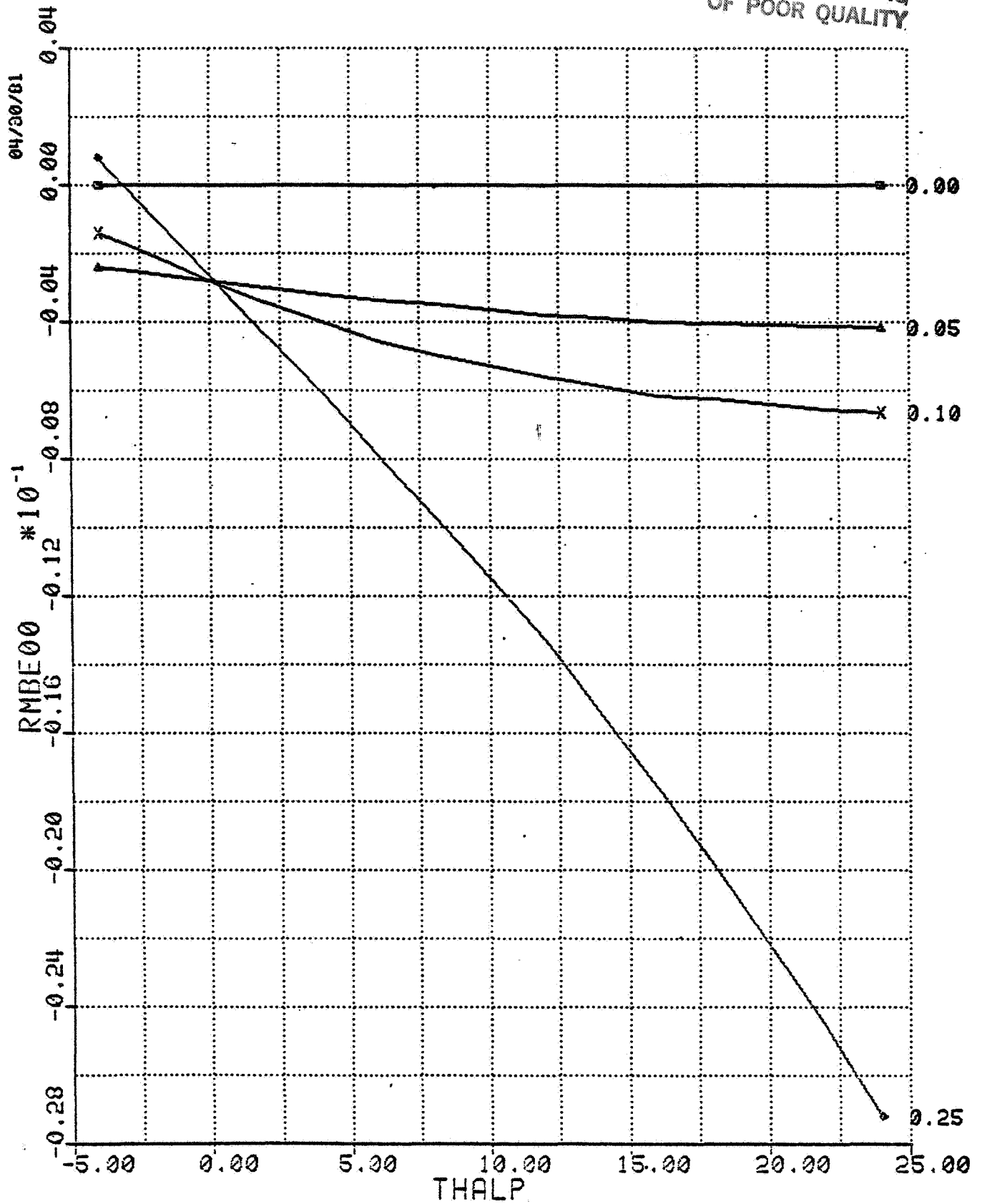
RK VS VEQ
FOR VARYING THETAJ

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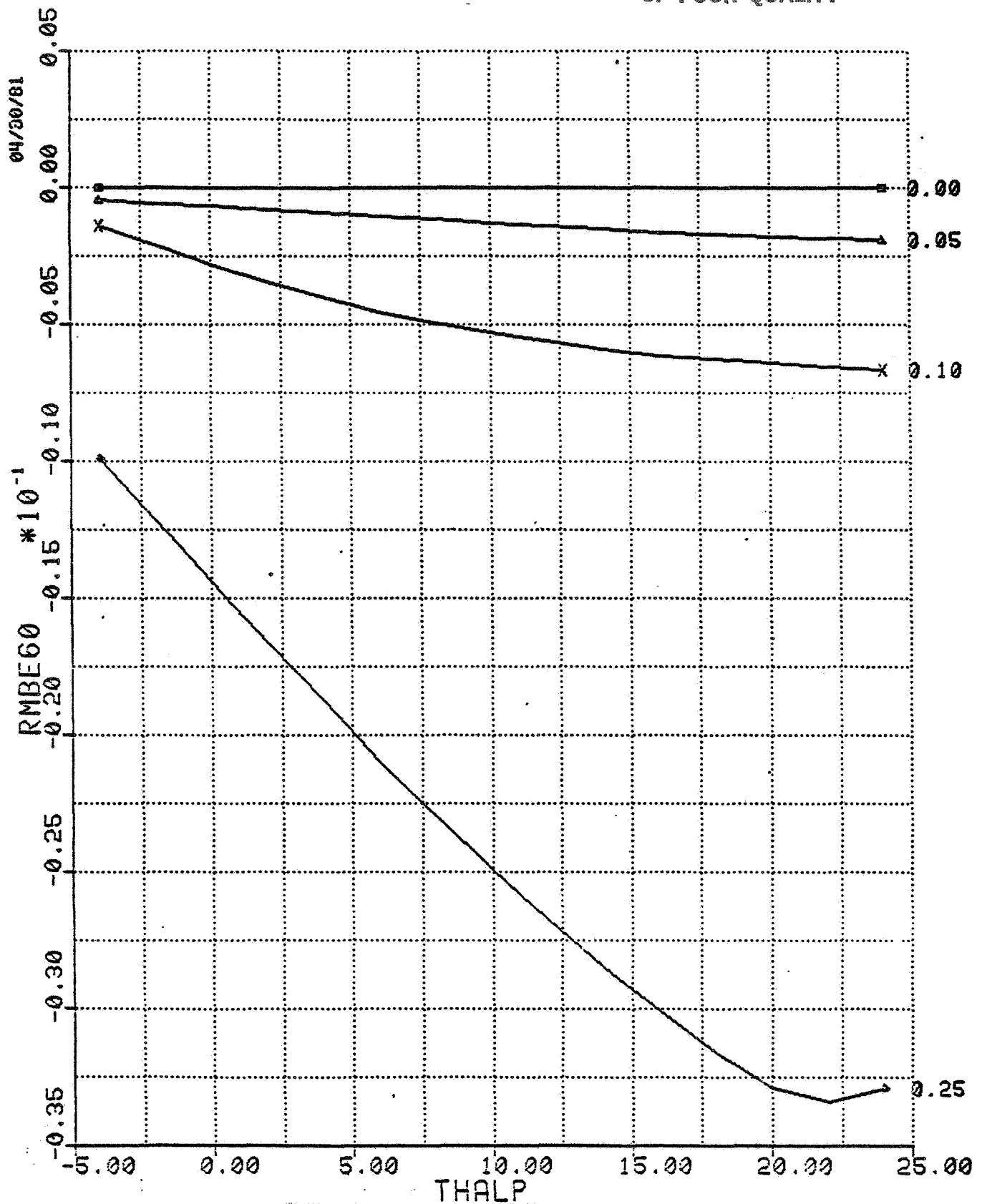
RMBE00 VS THALP
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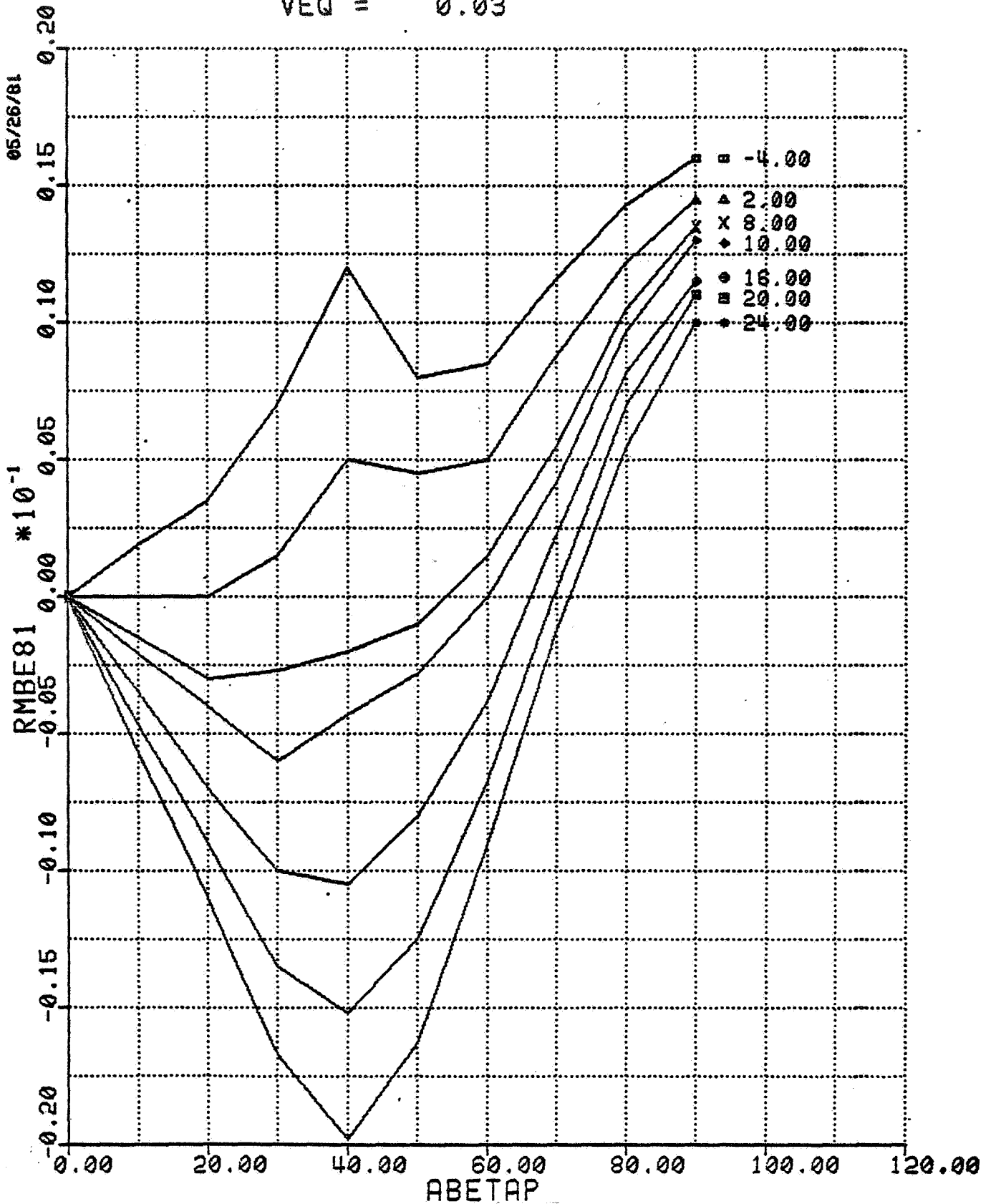
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FOR VARYING VEQ

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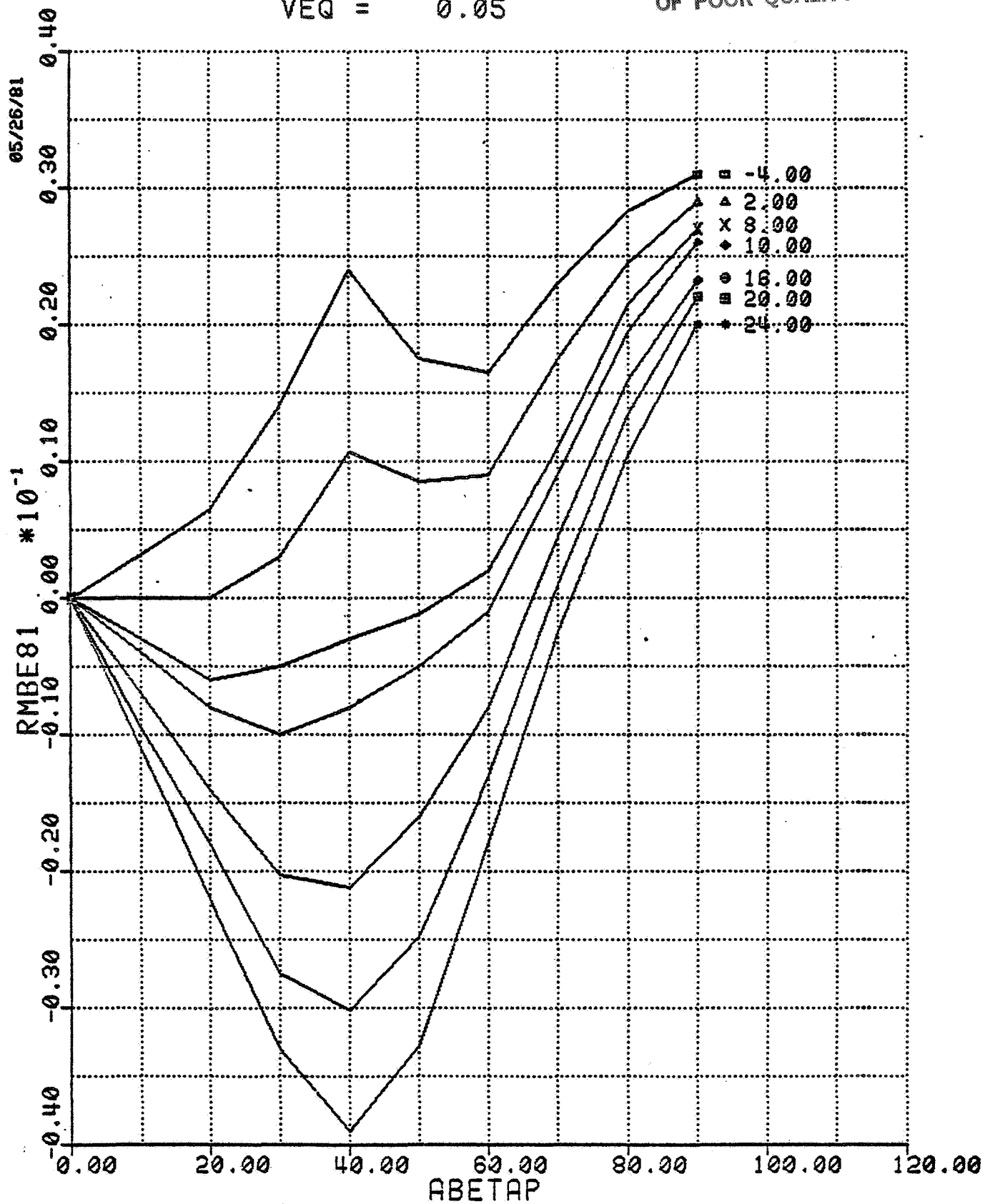
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FOR VARYING THALP
VEQ = 0.03

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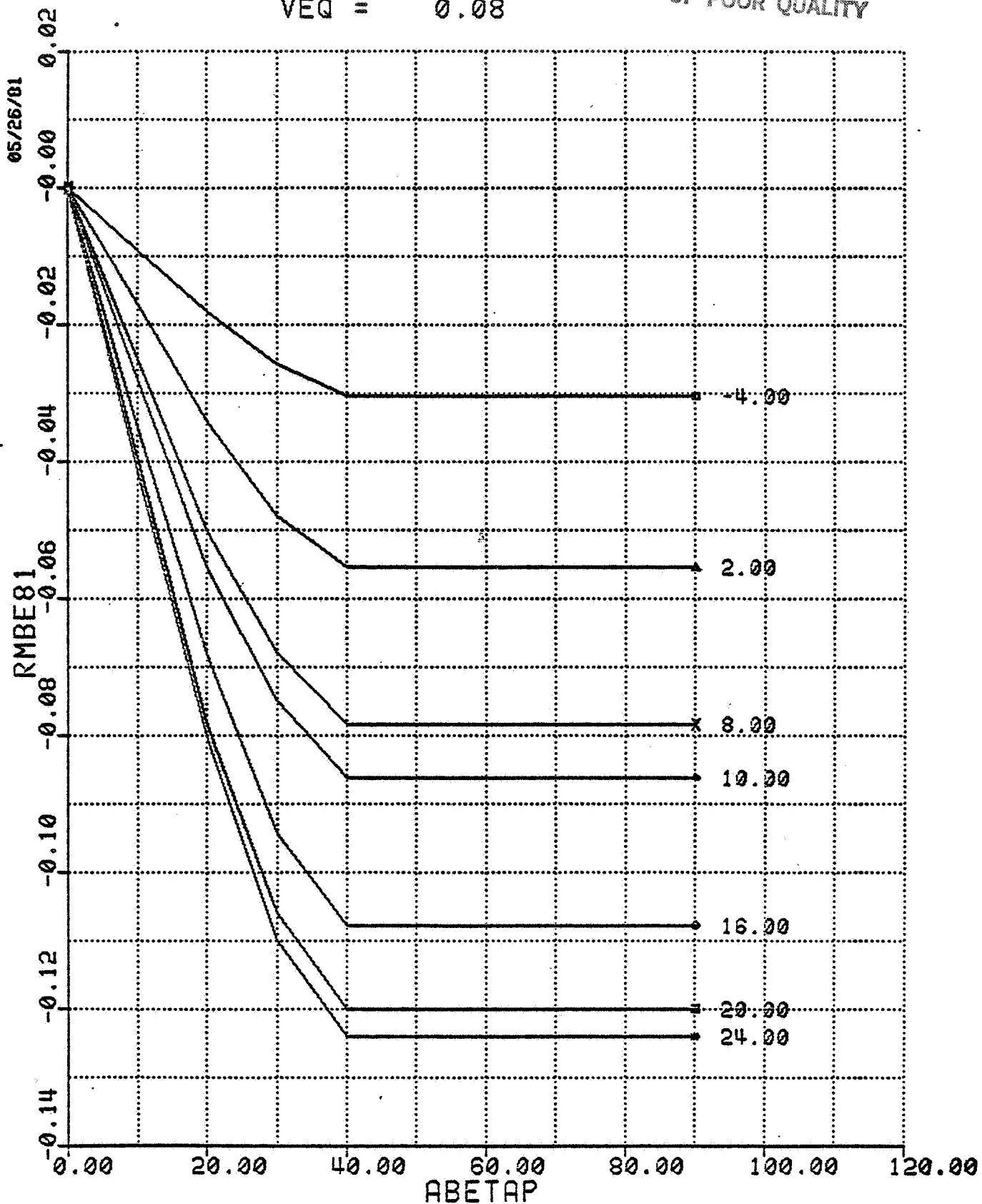
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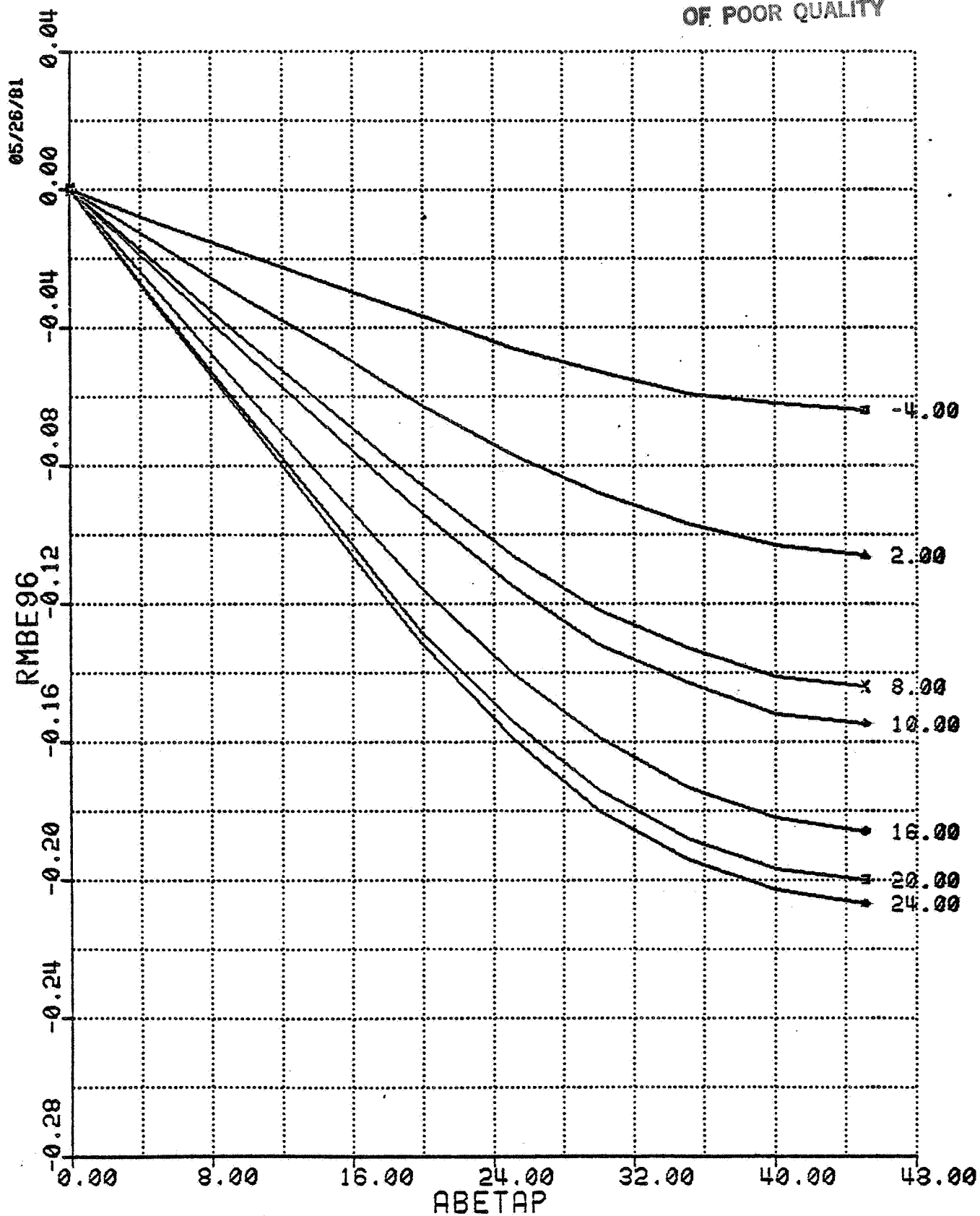
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FOR VARYING THALP
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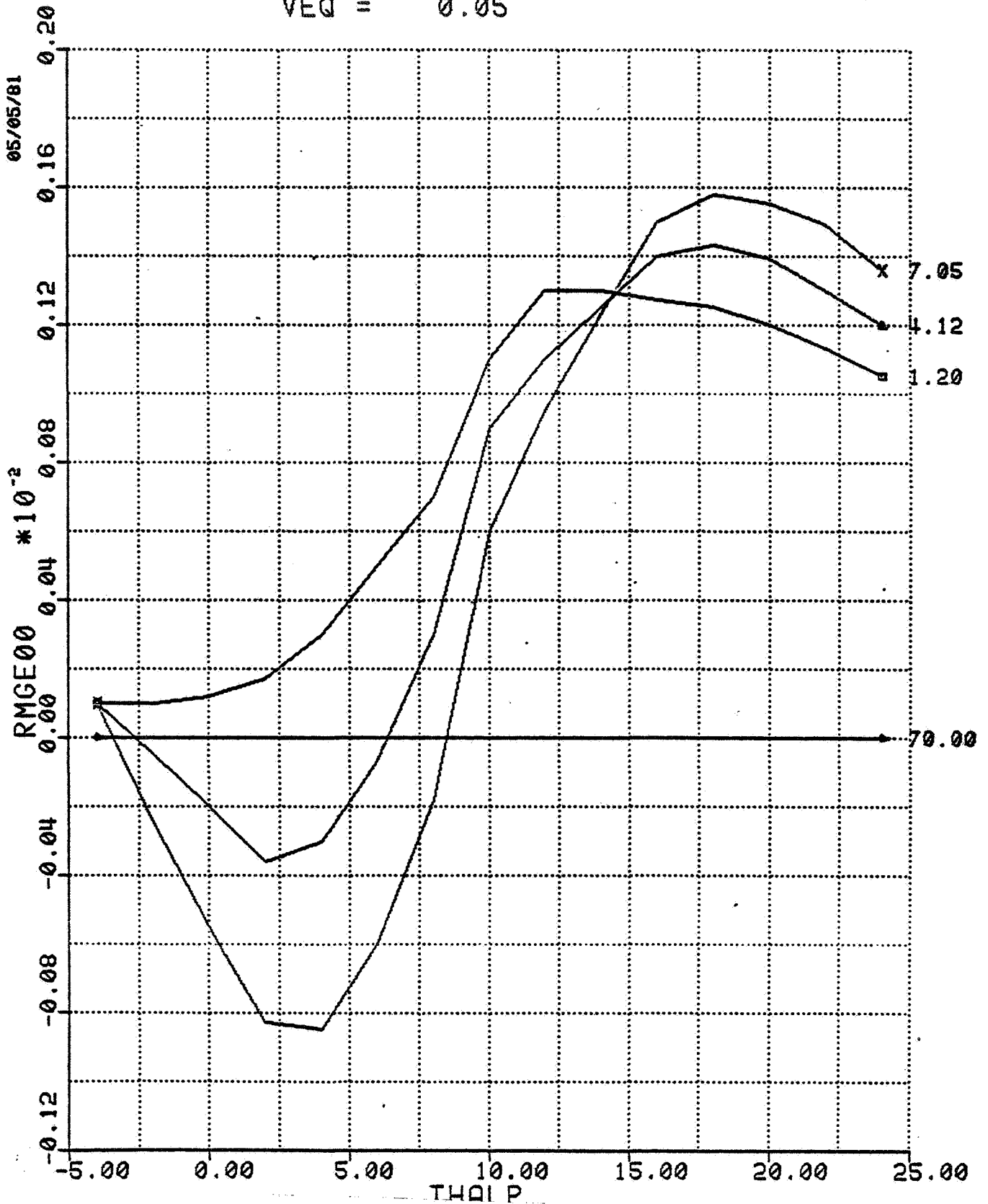
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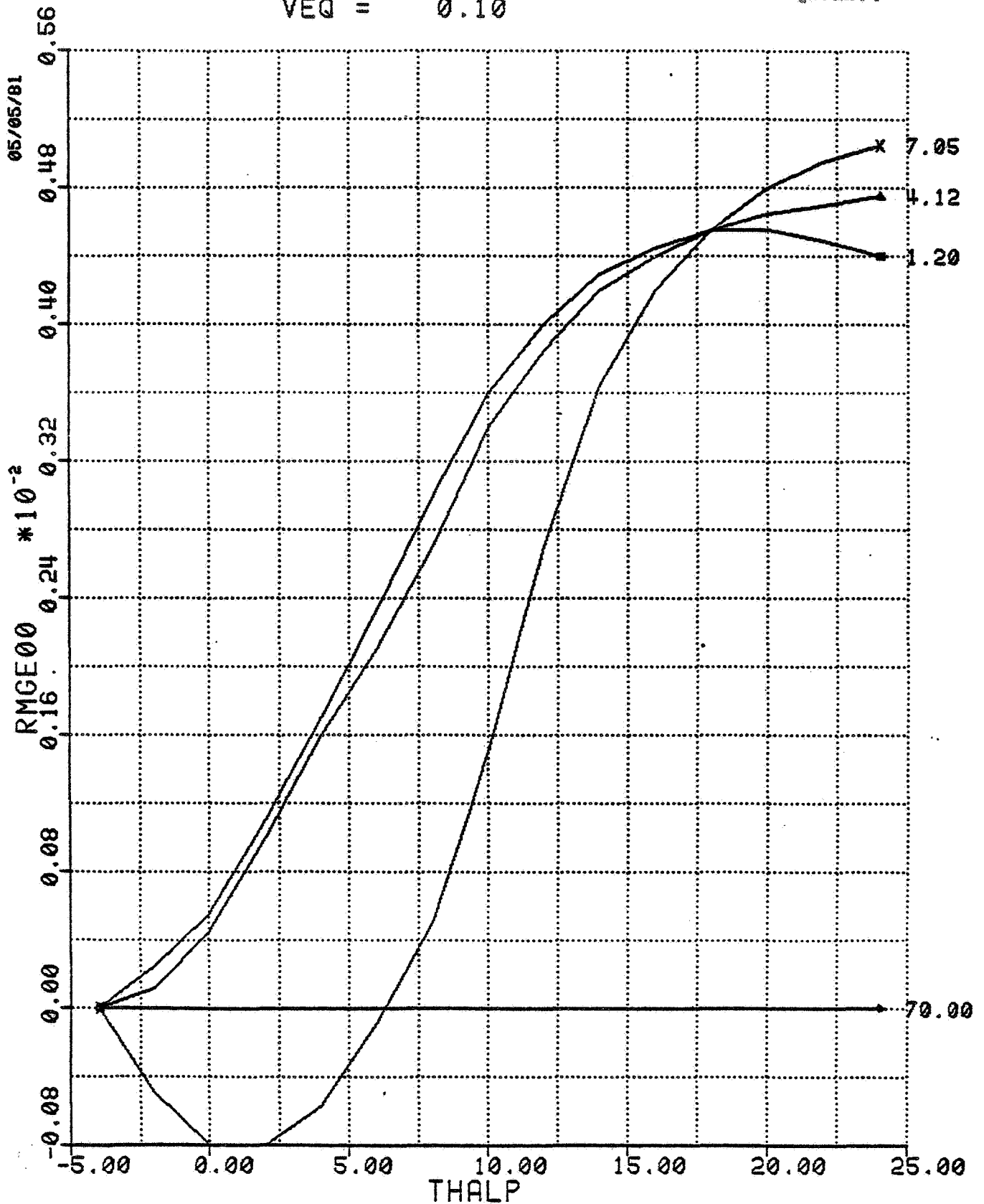
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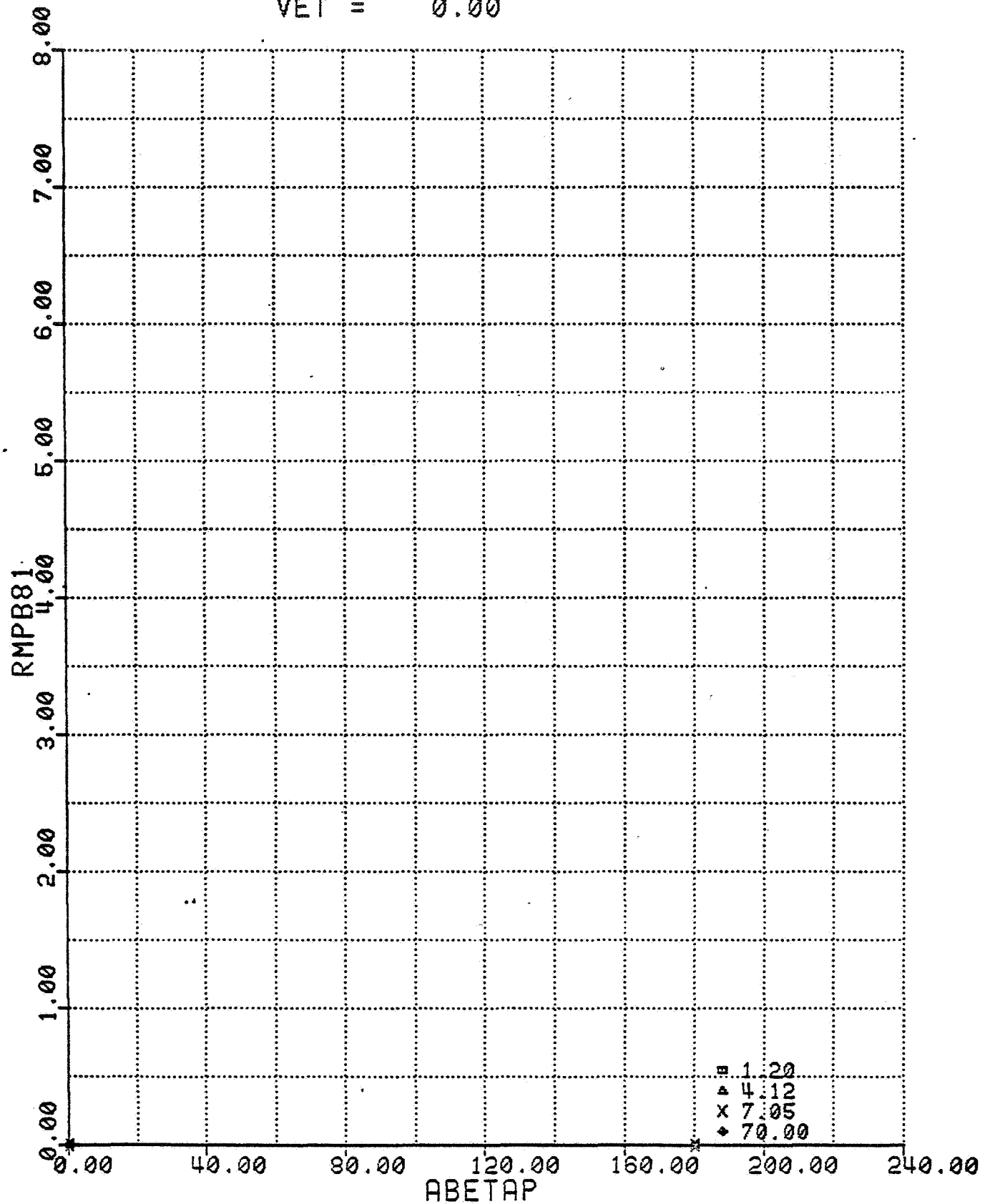
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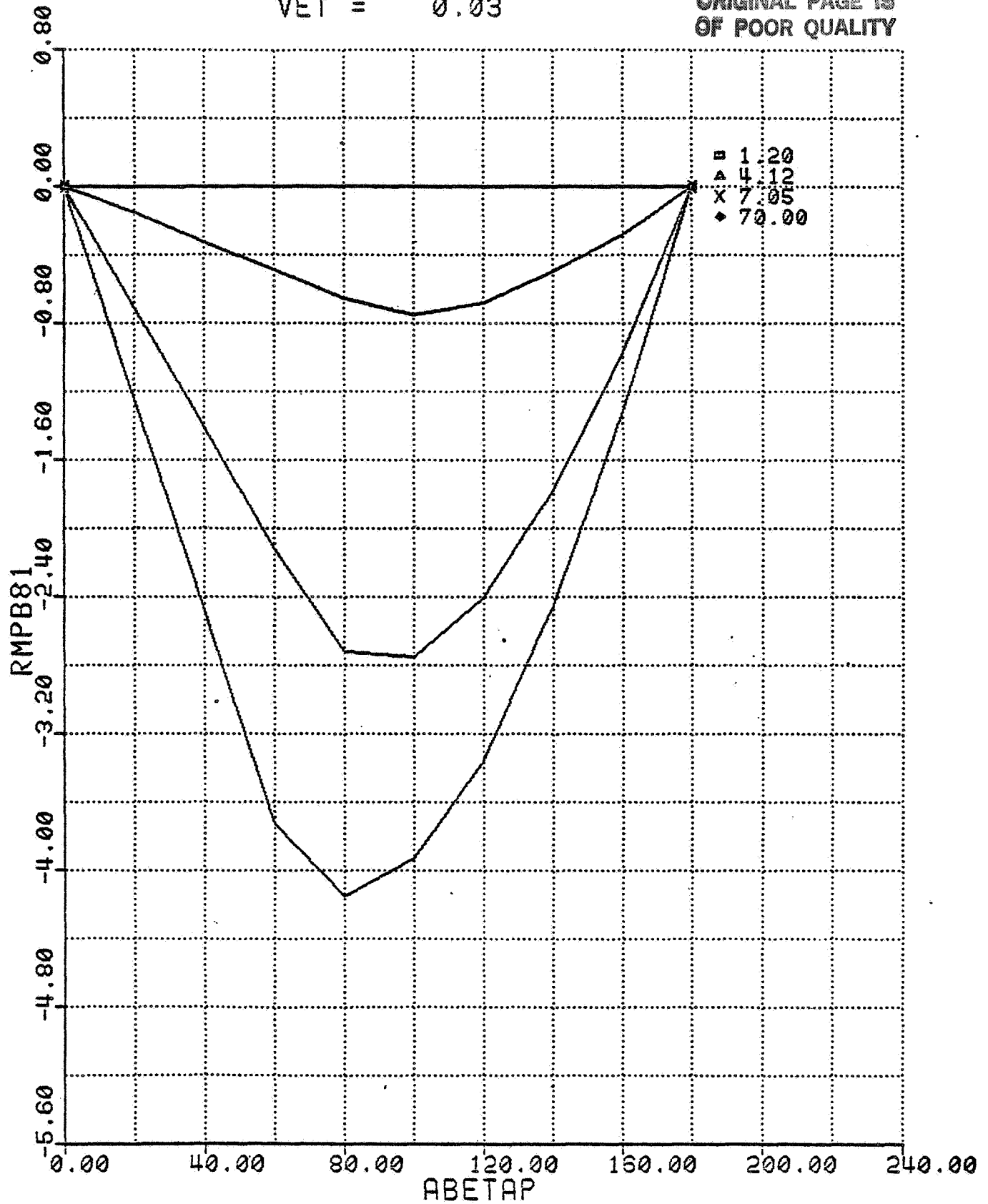
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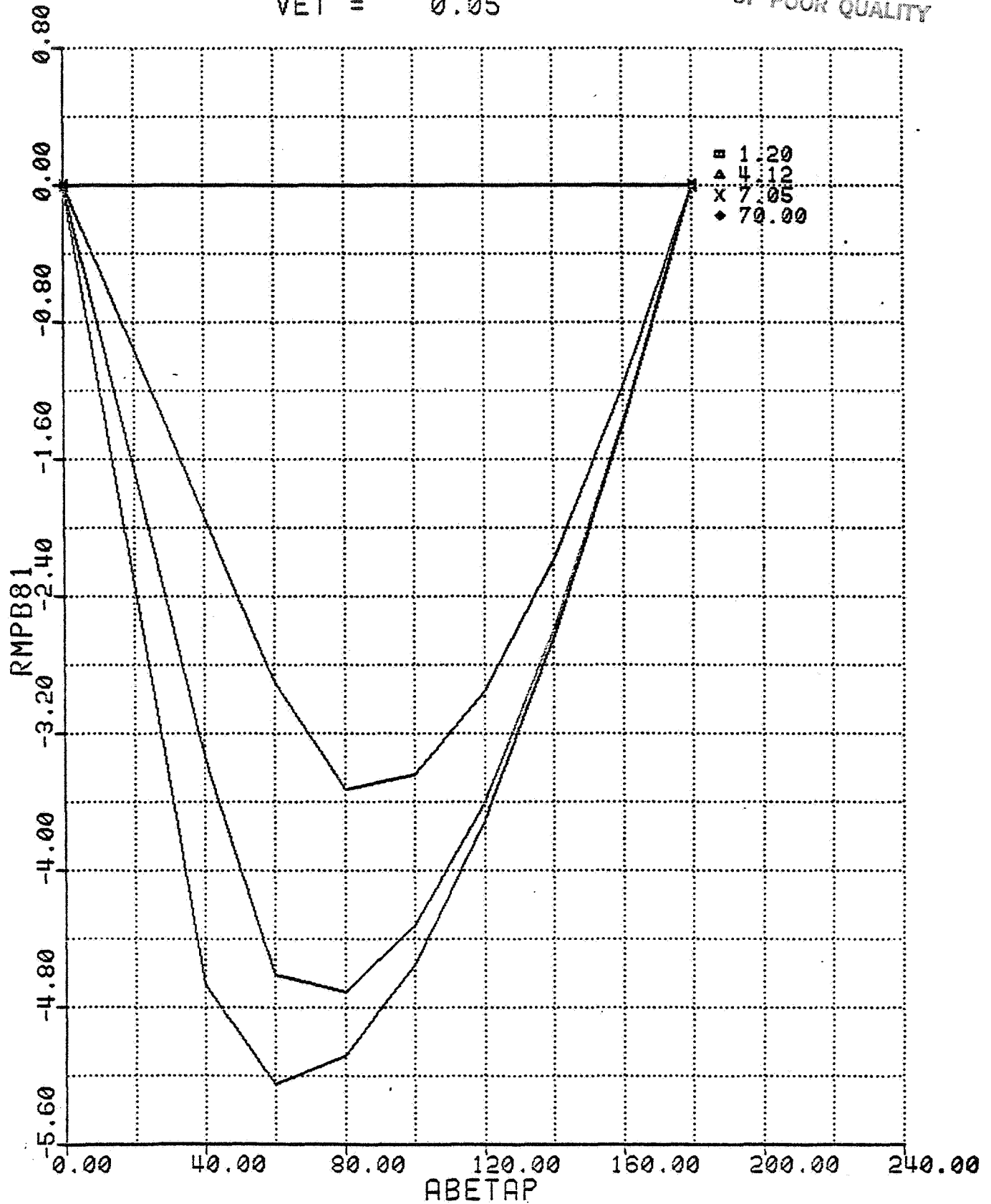
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RMPB81 VS ABETAP
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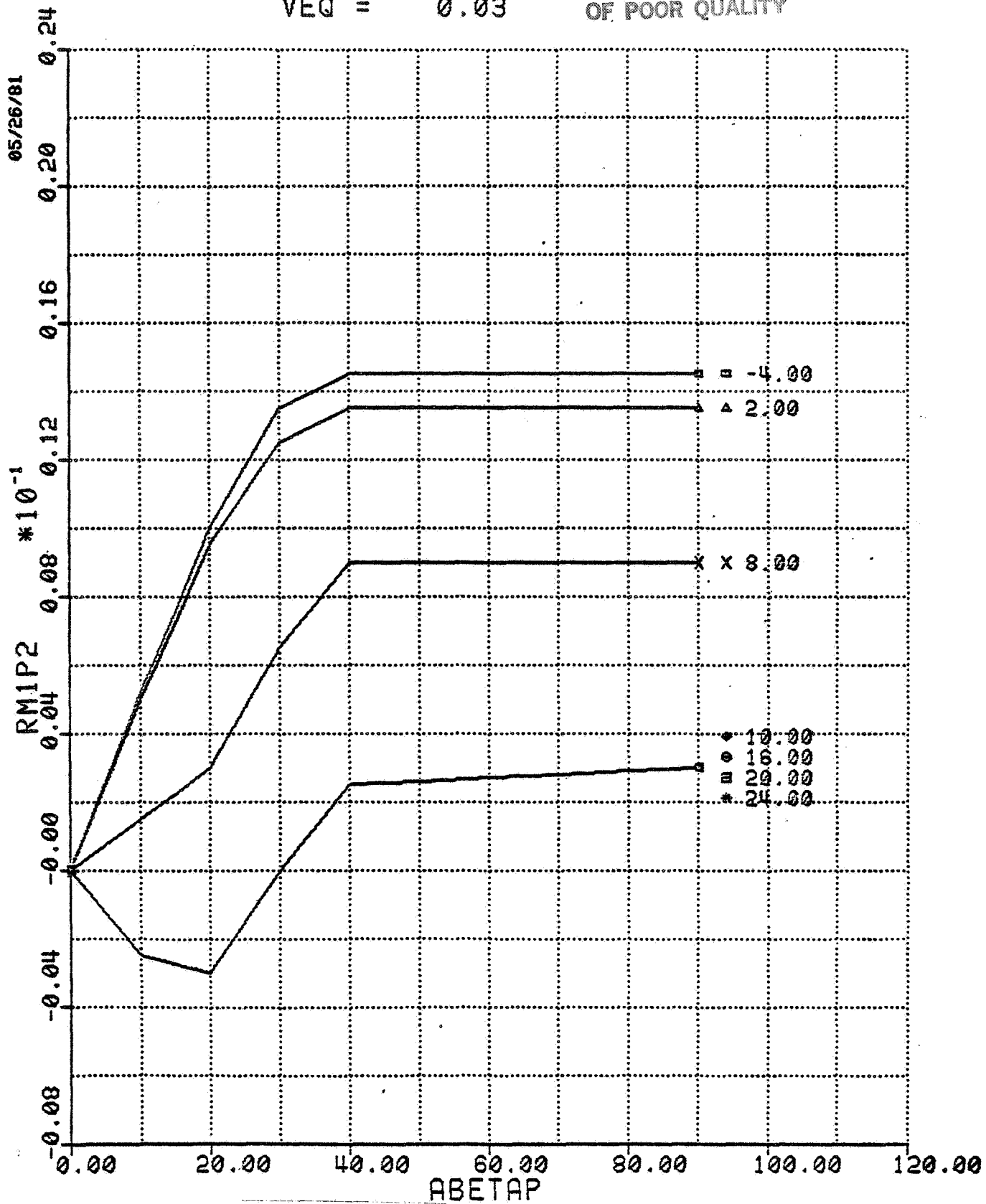
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C-6

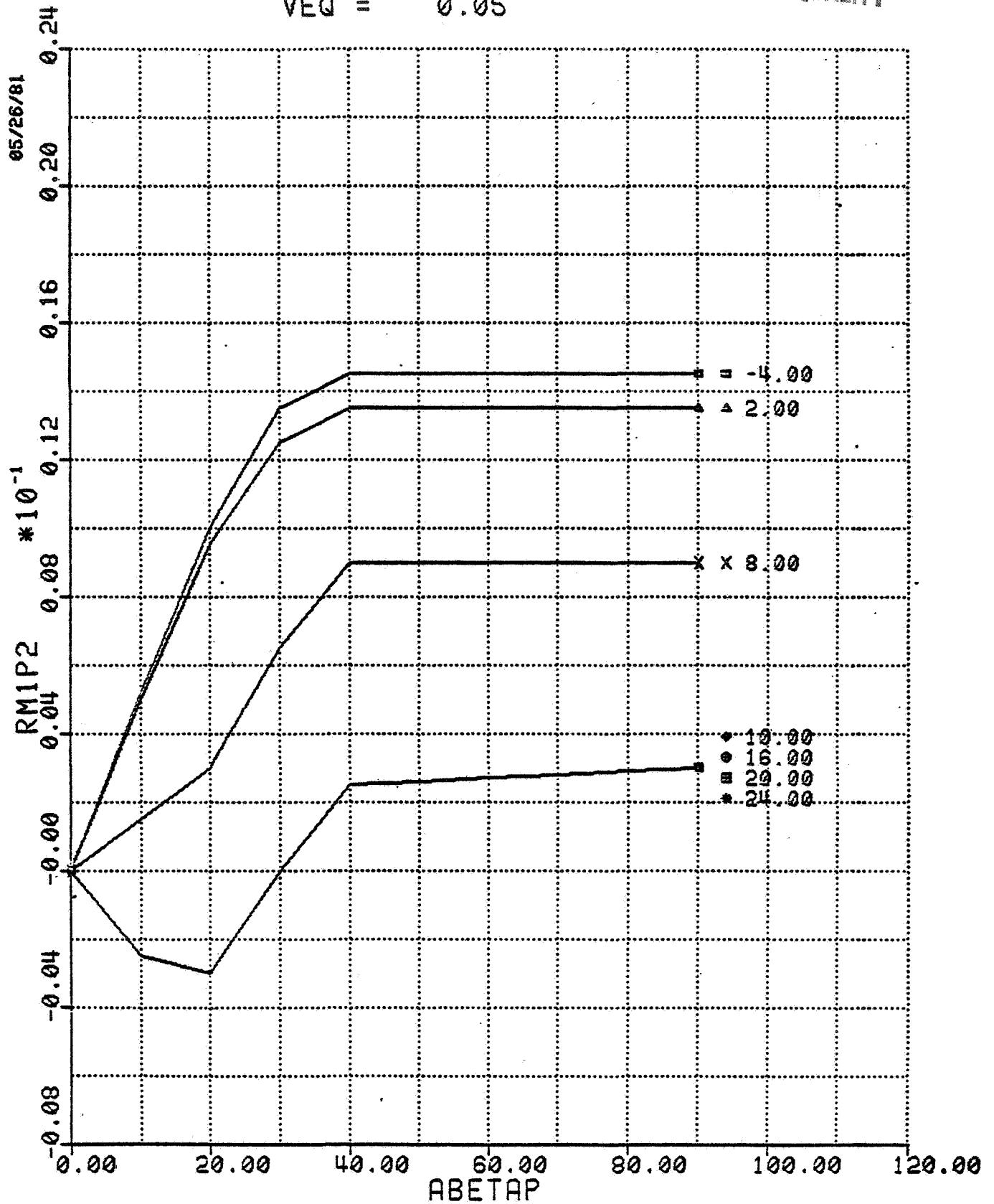
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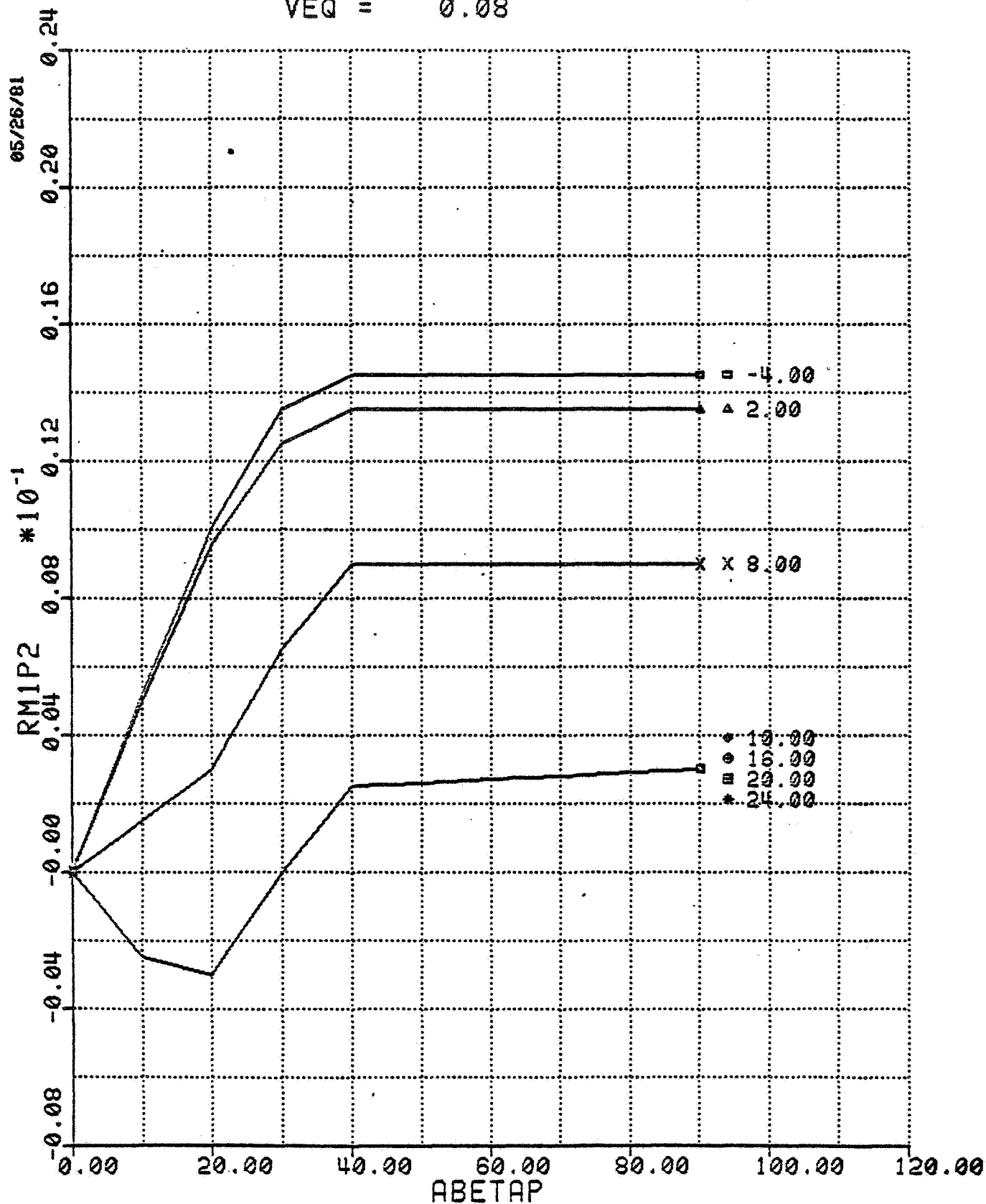
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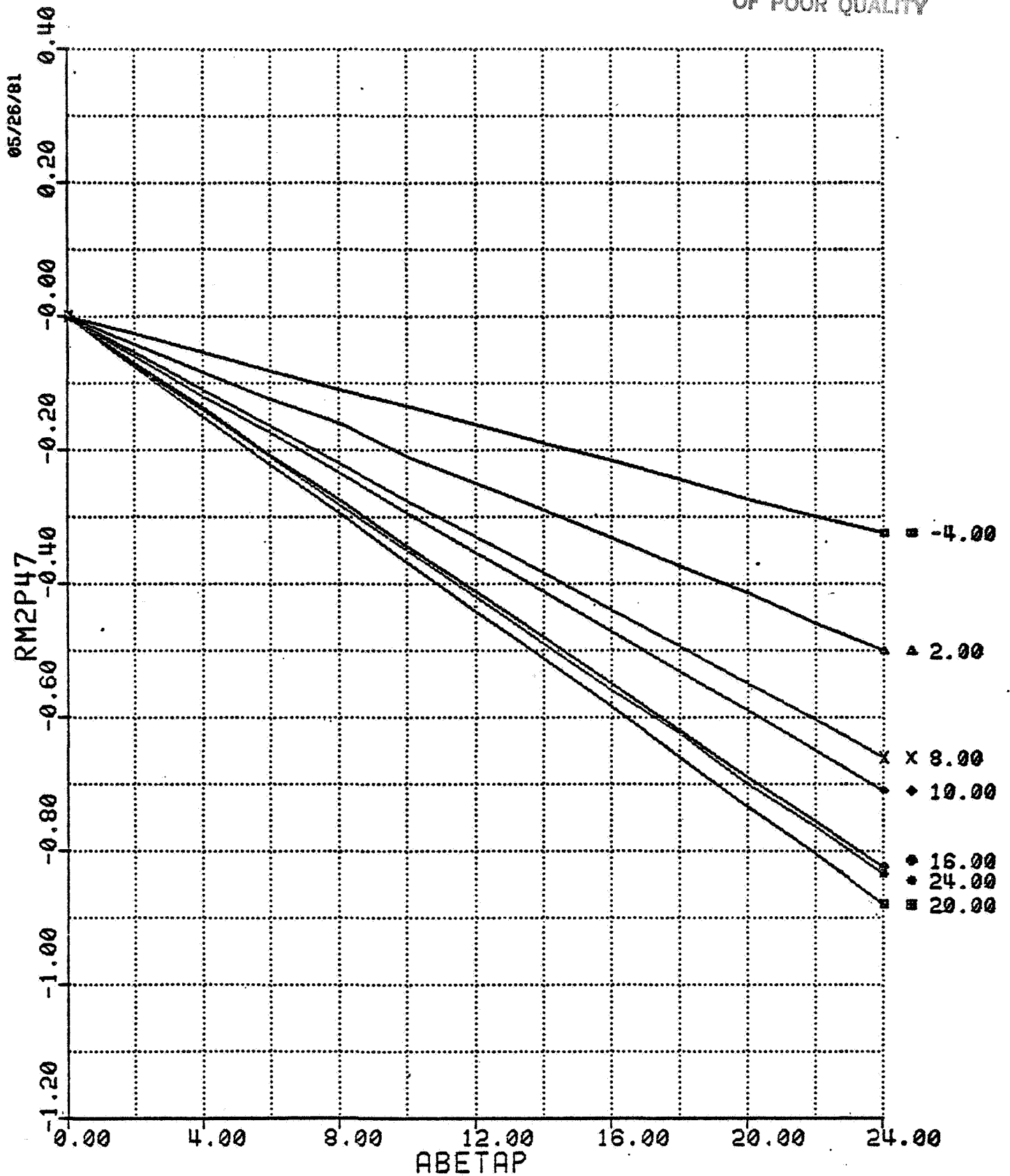
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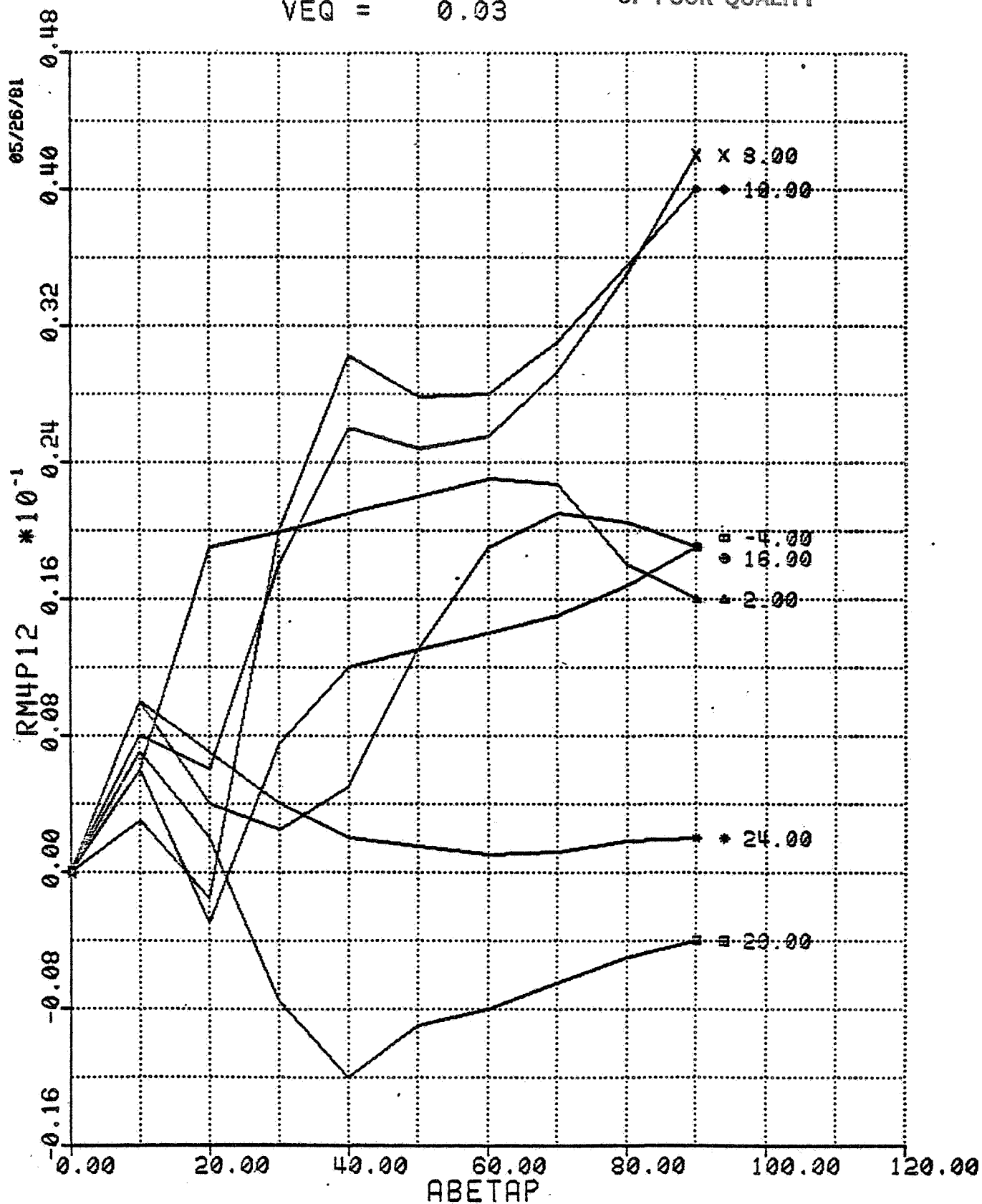
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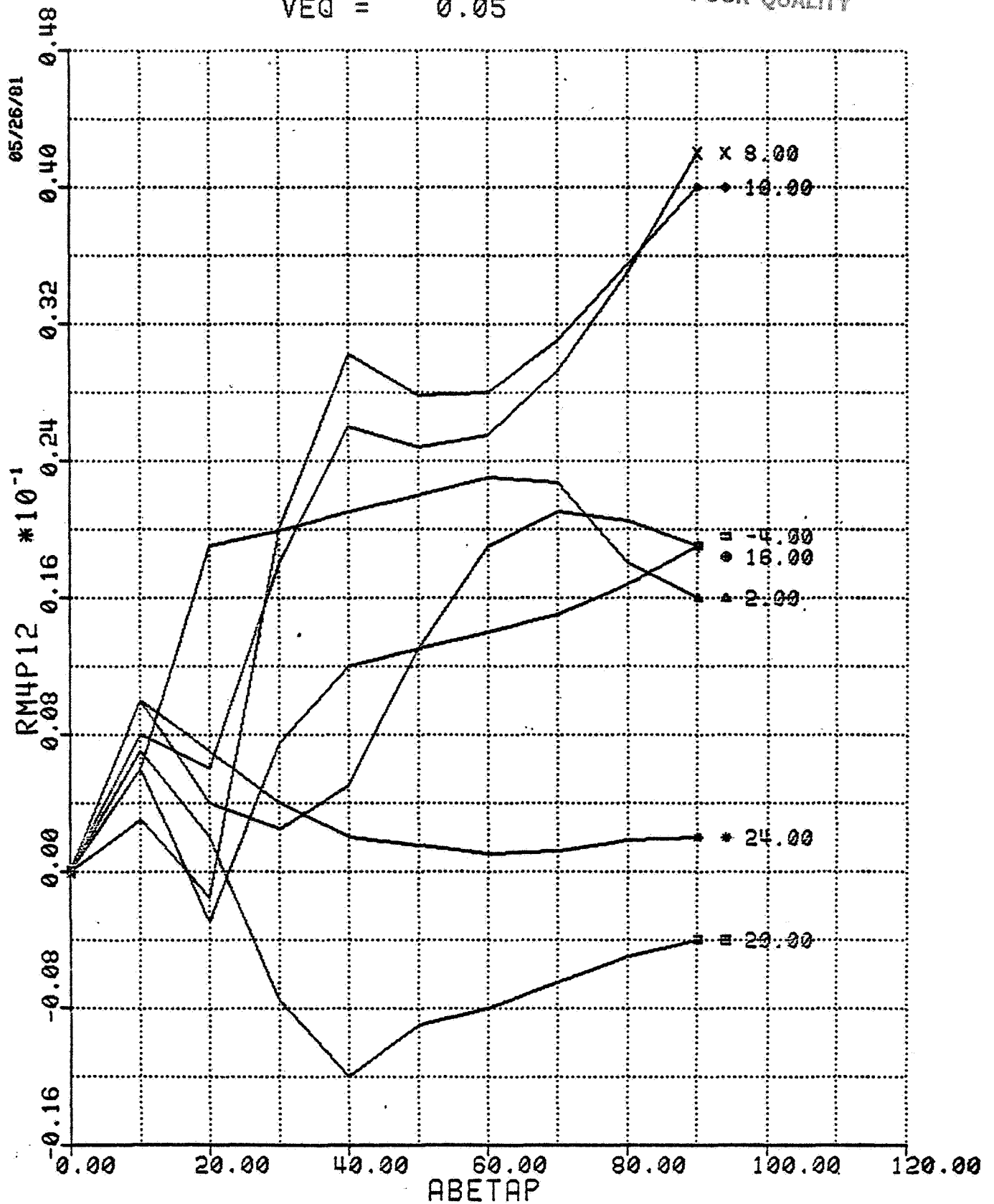
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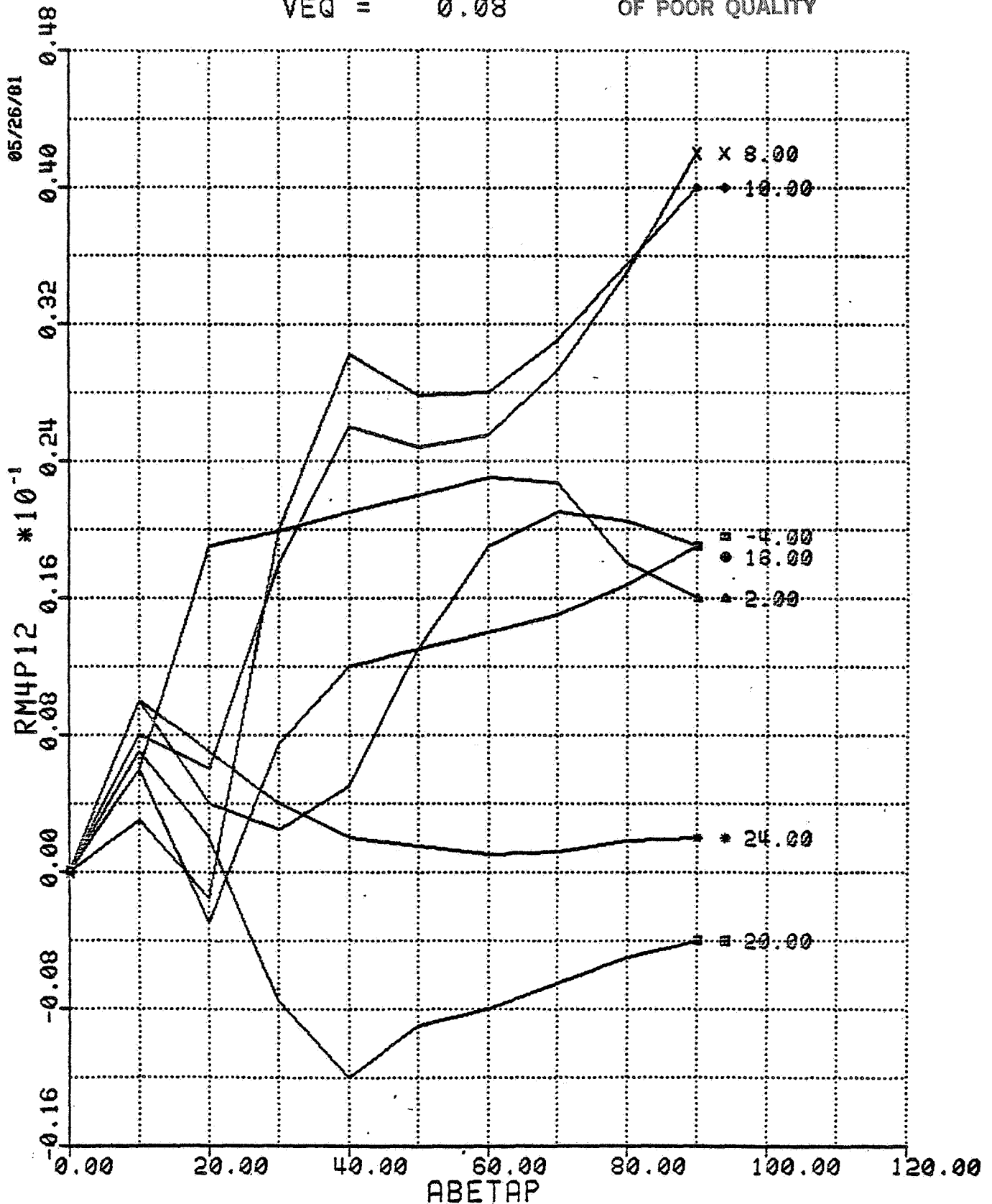
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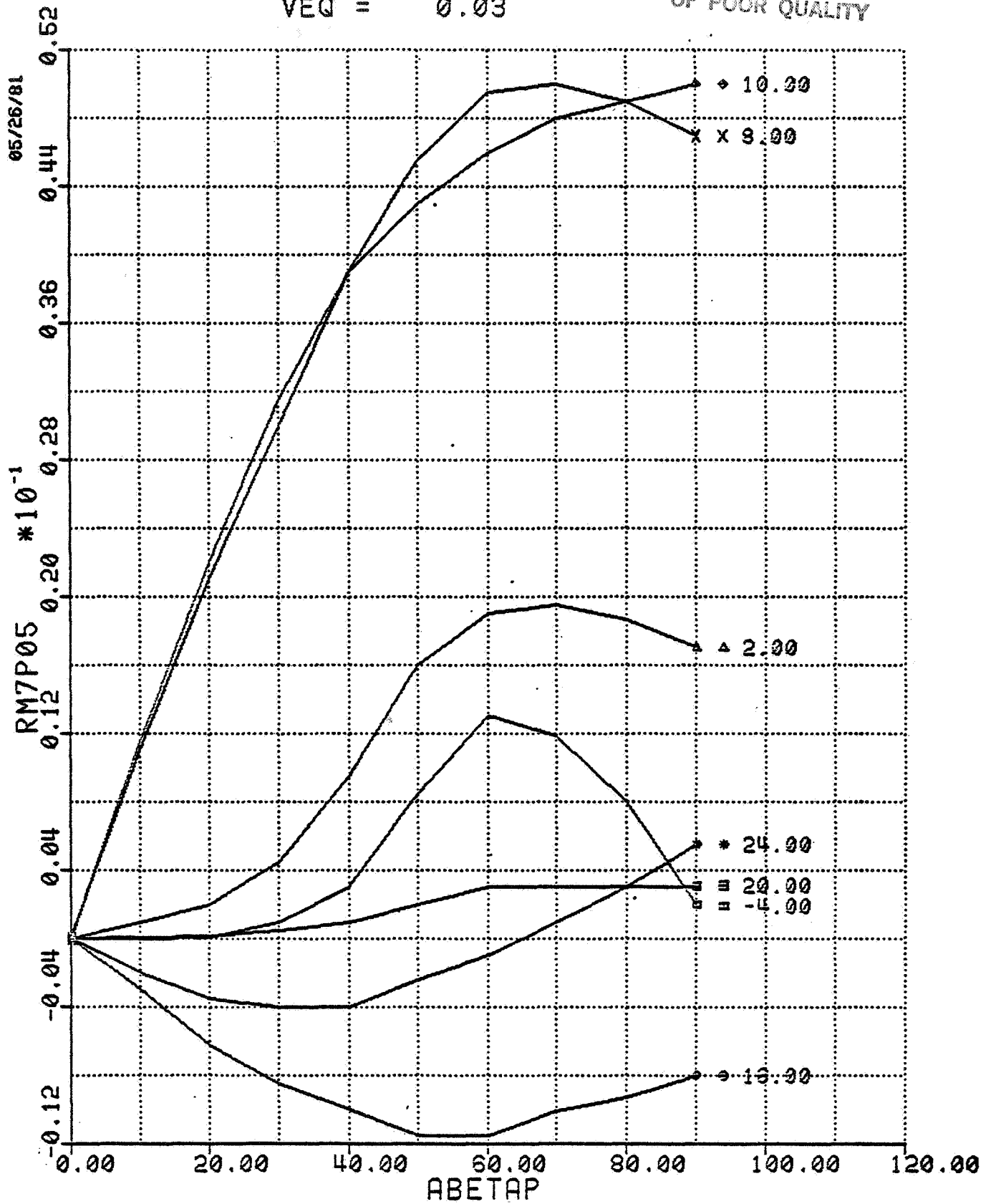
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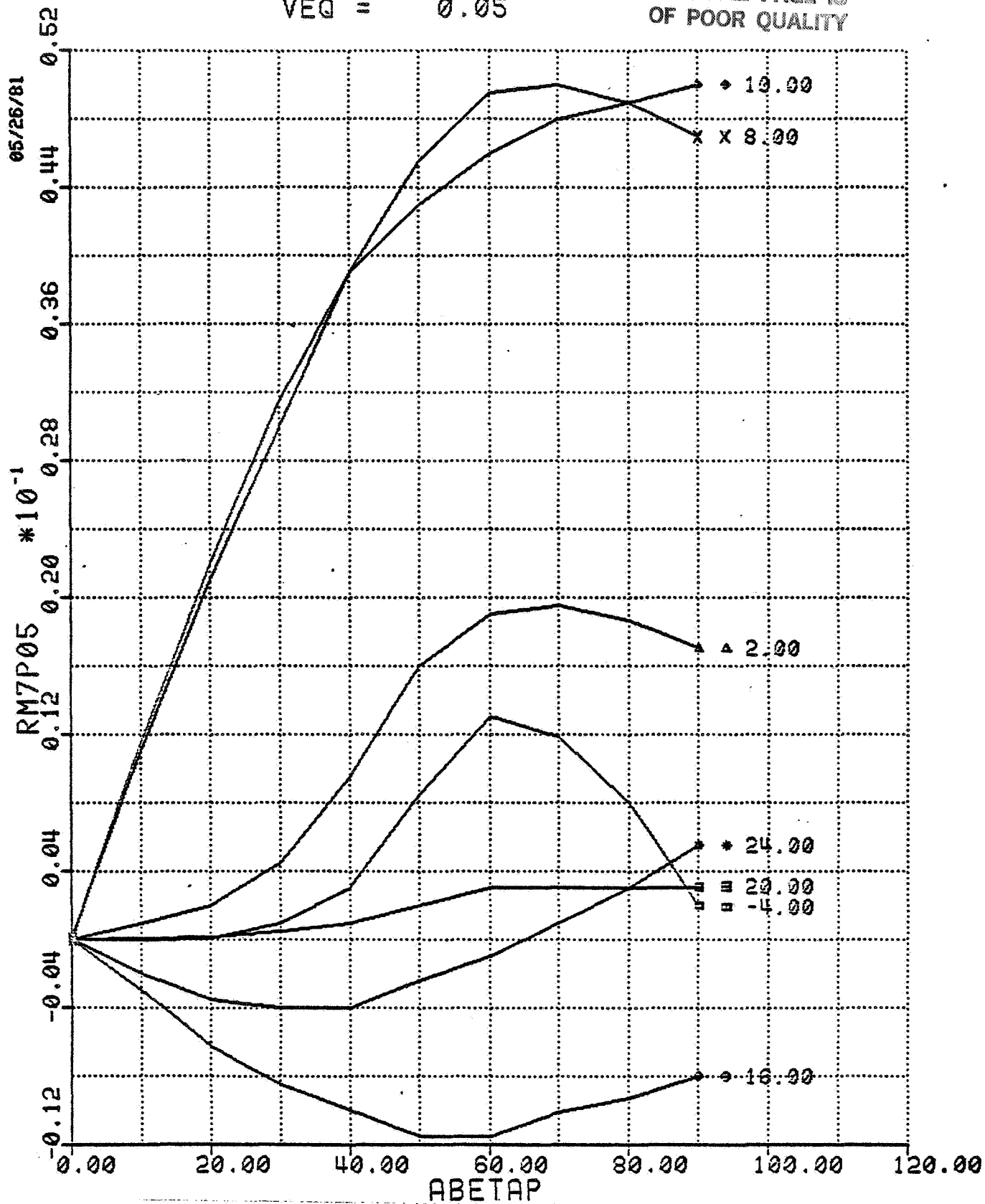
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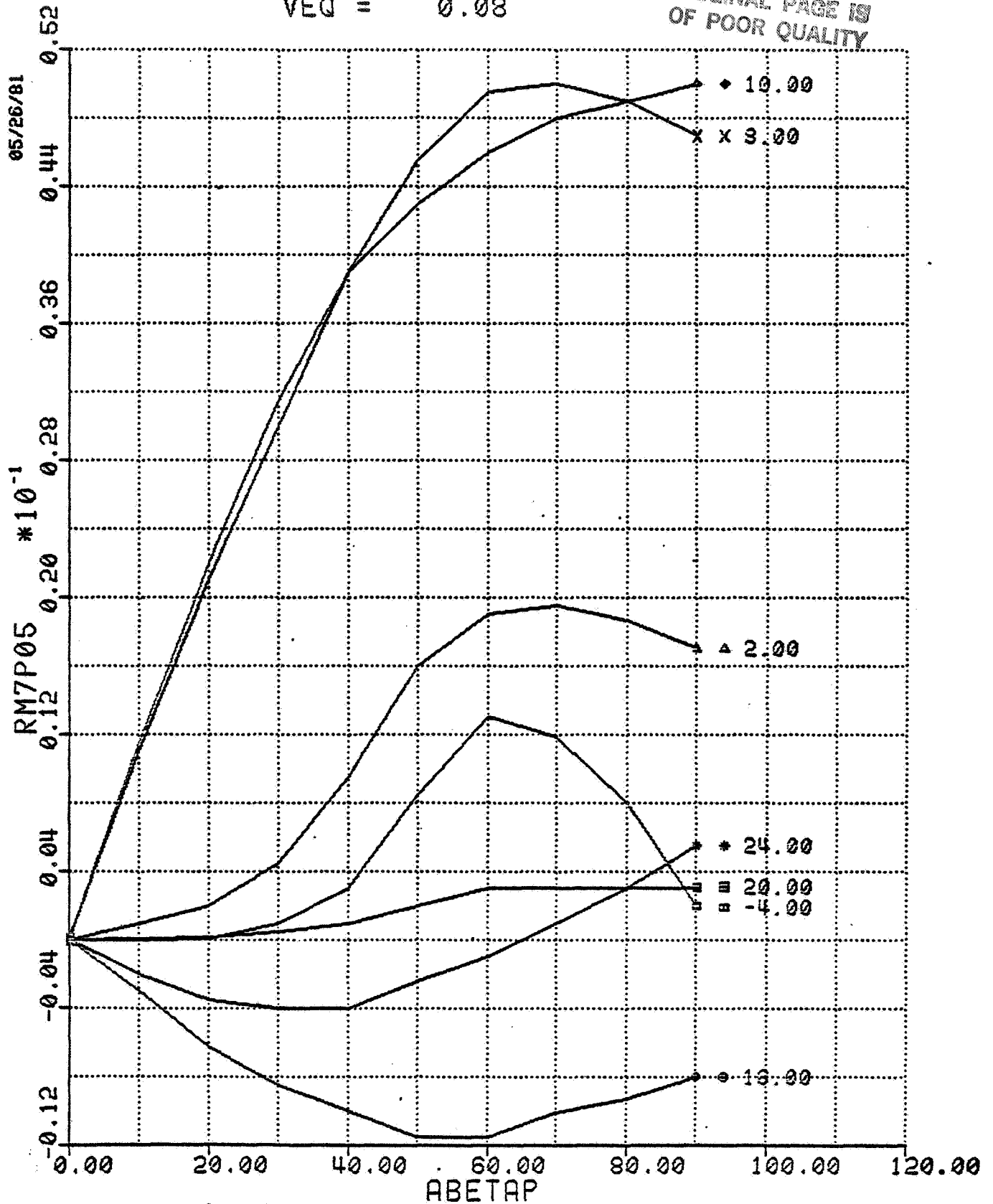
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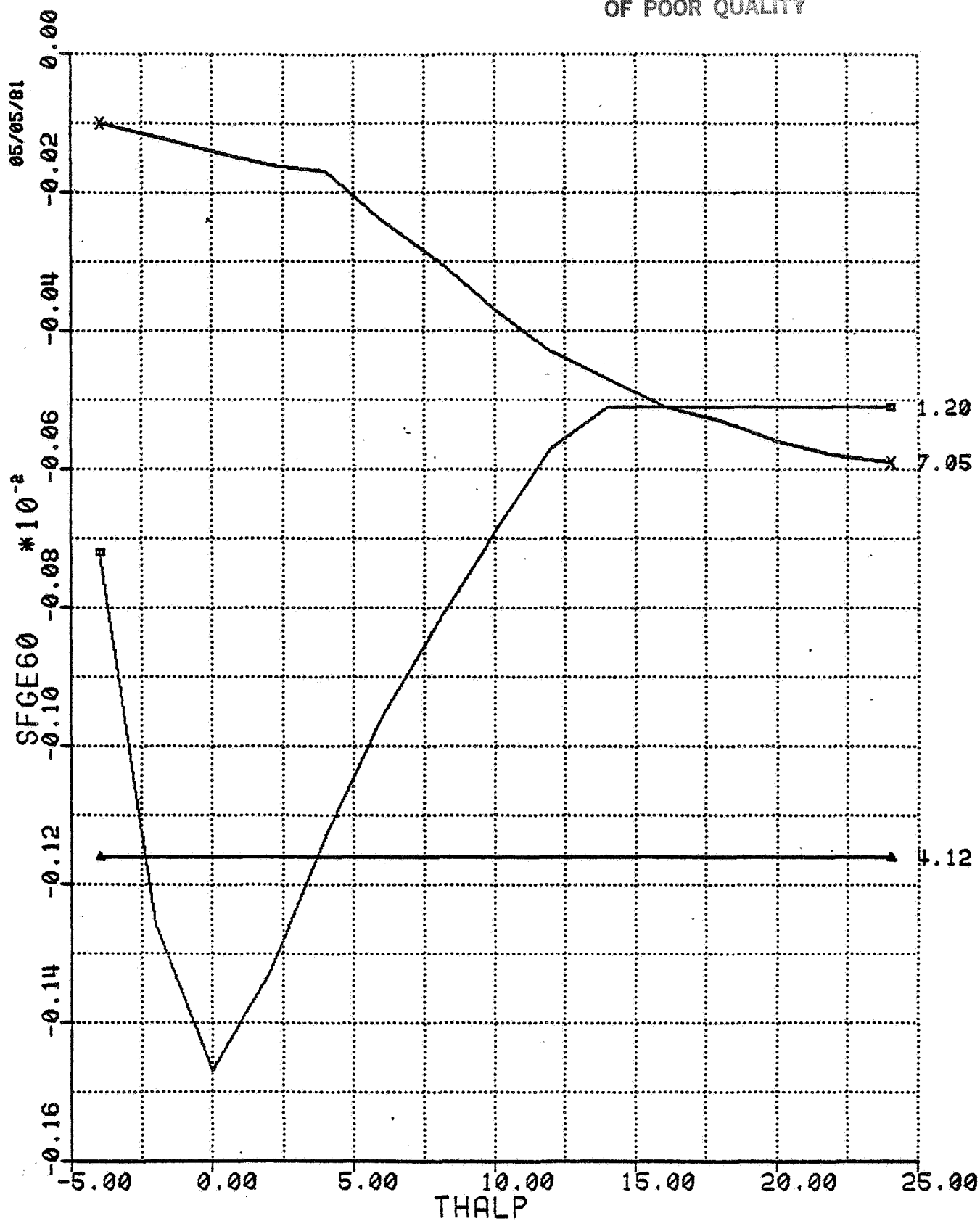
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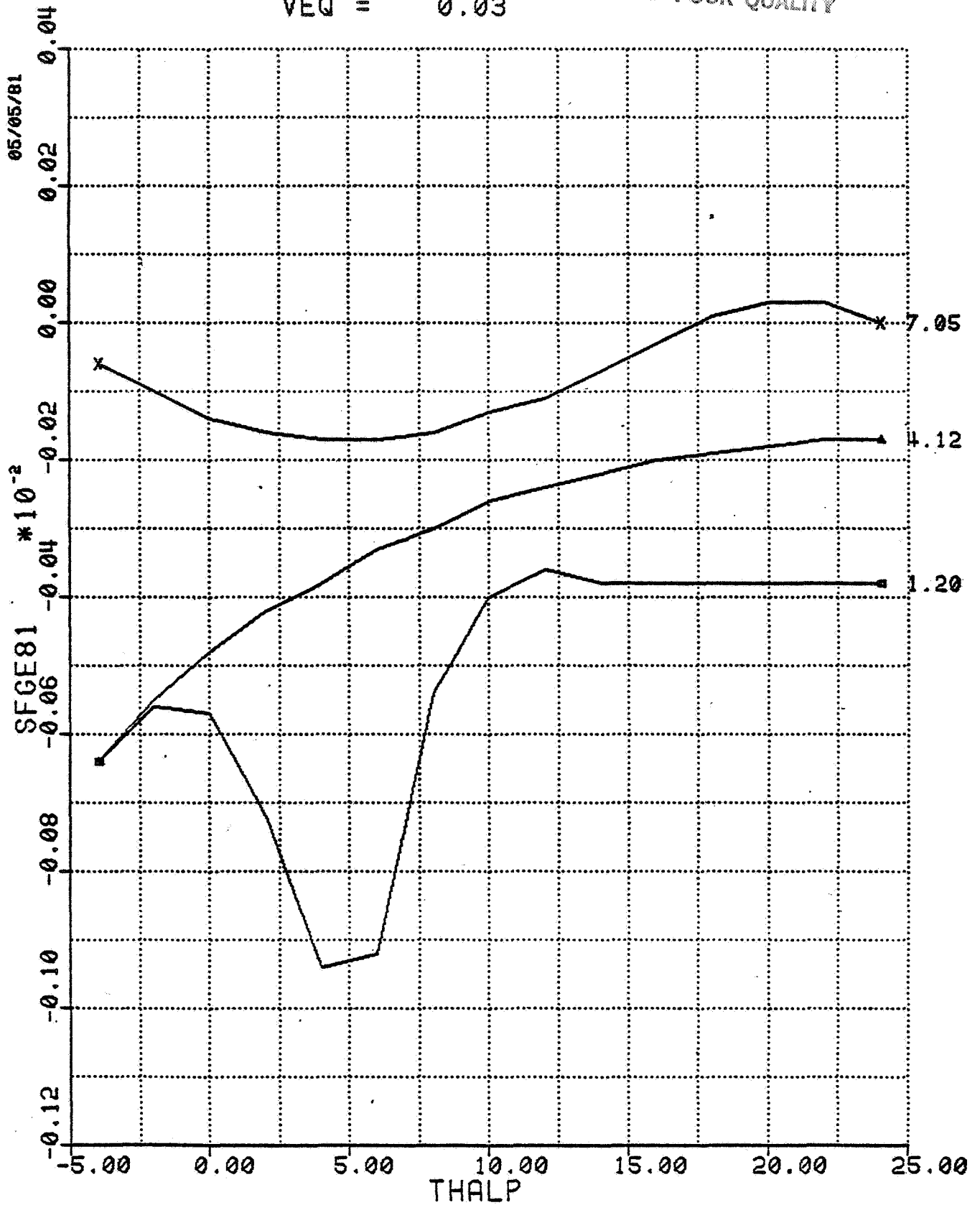
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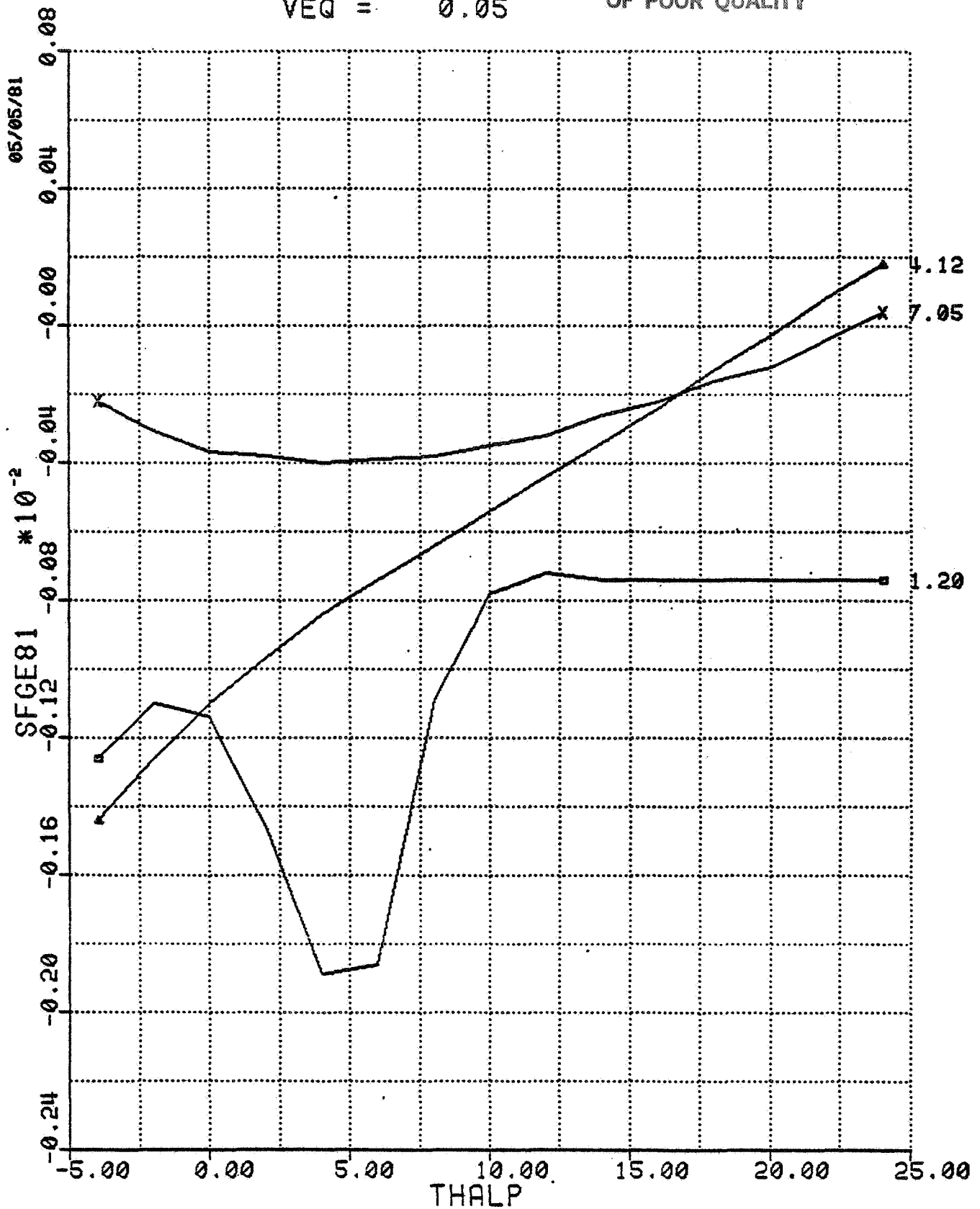
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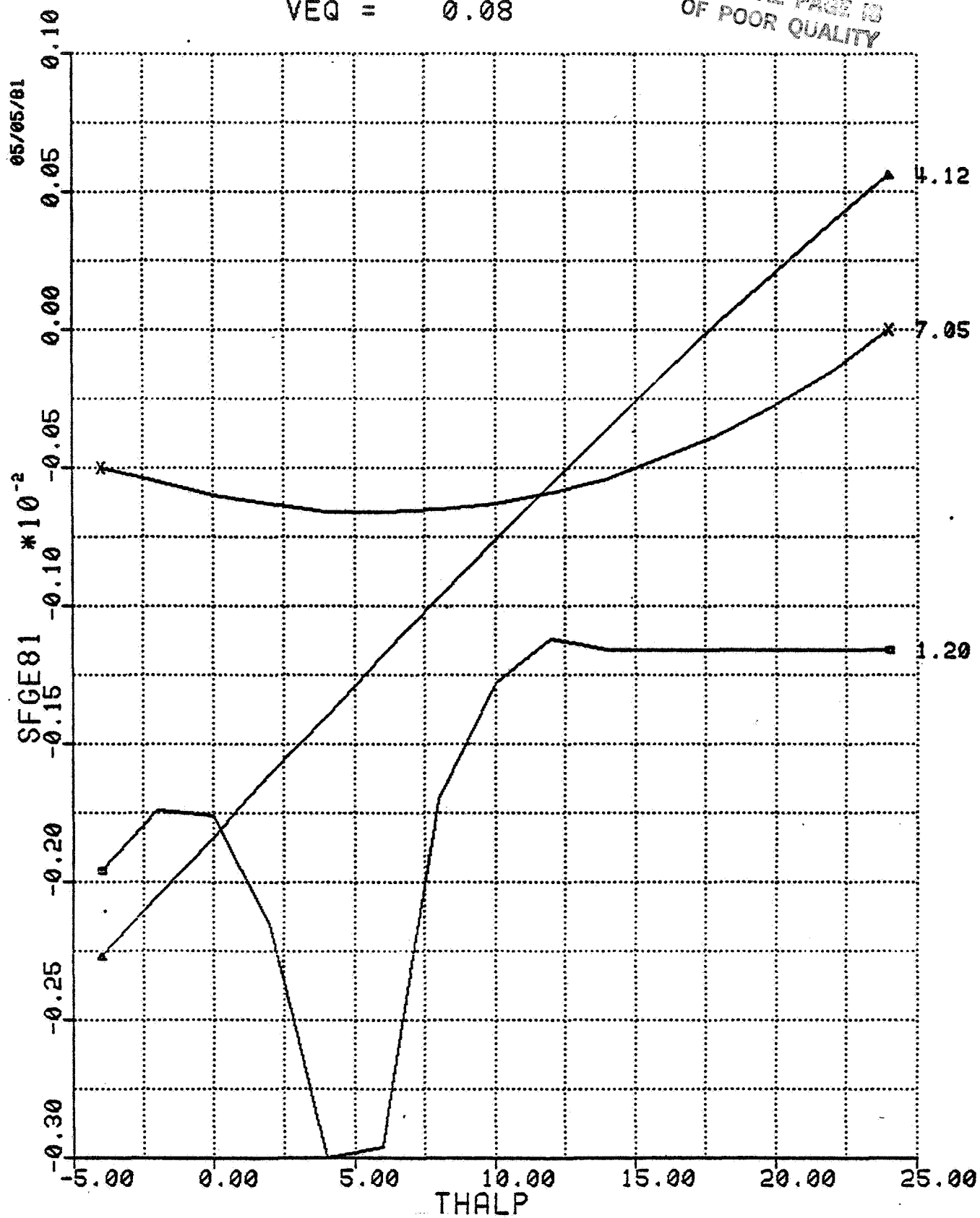
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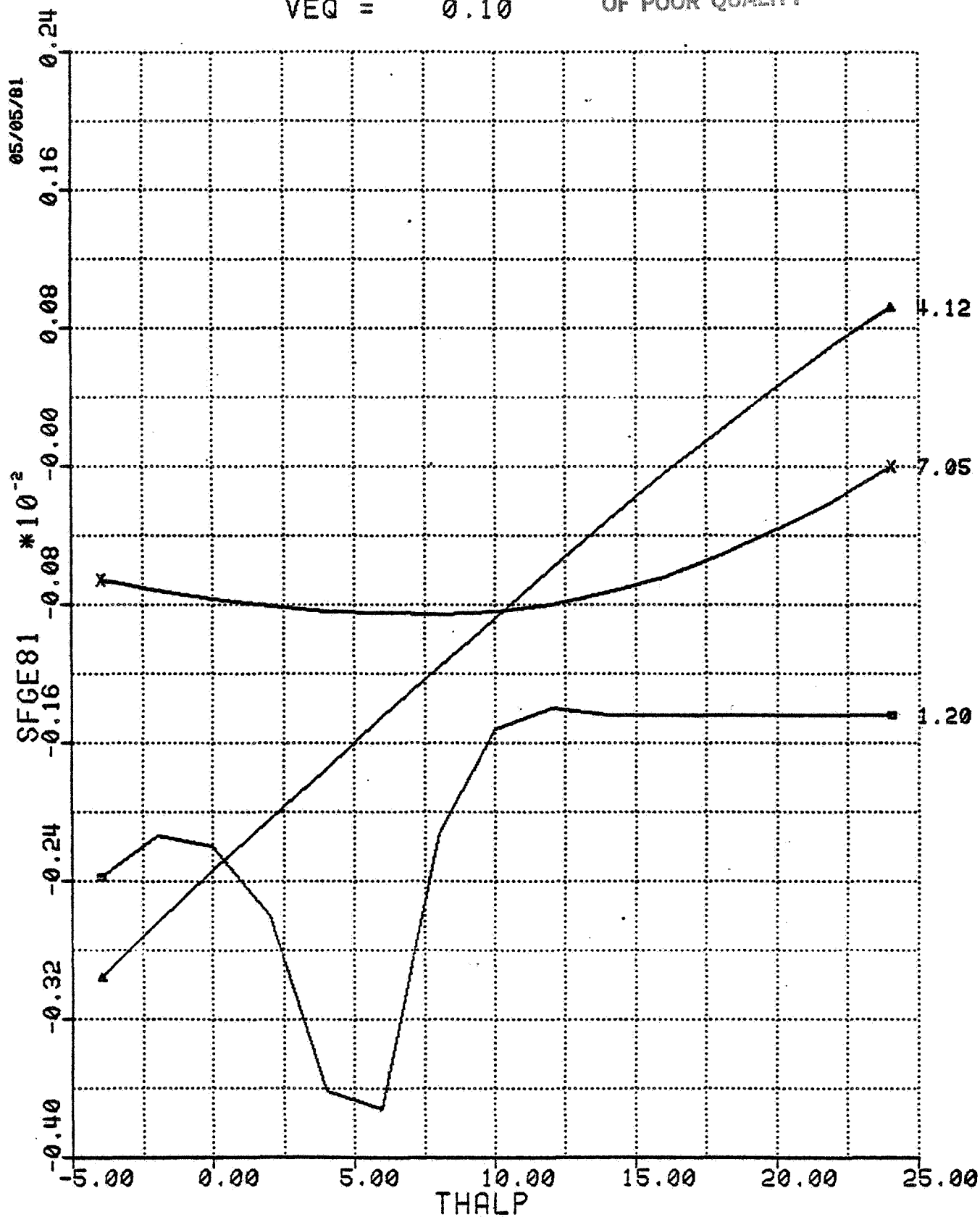
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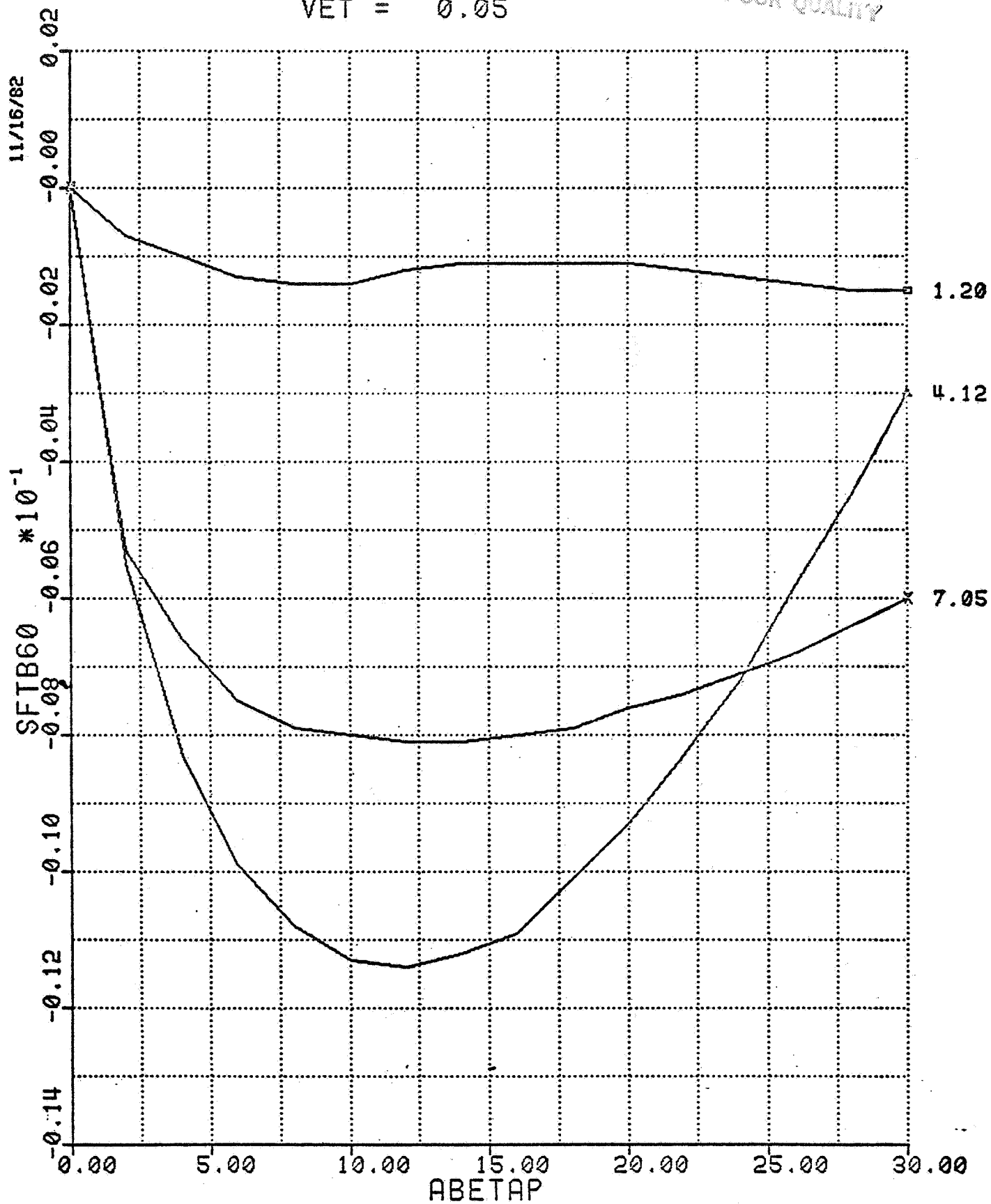
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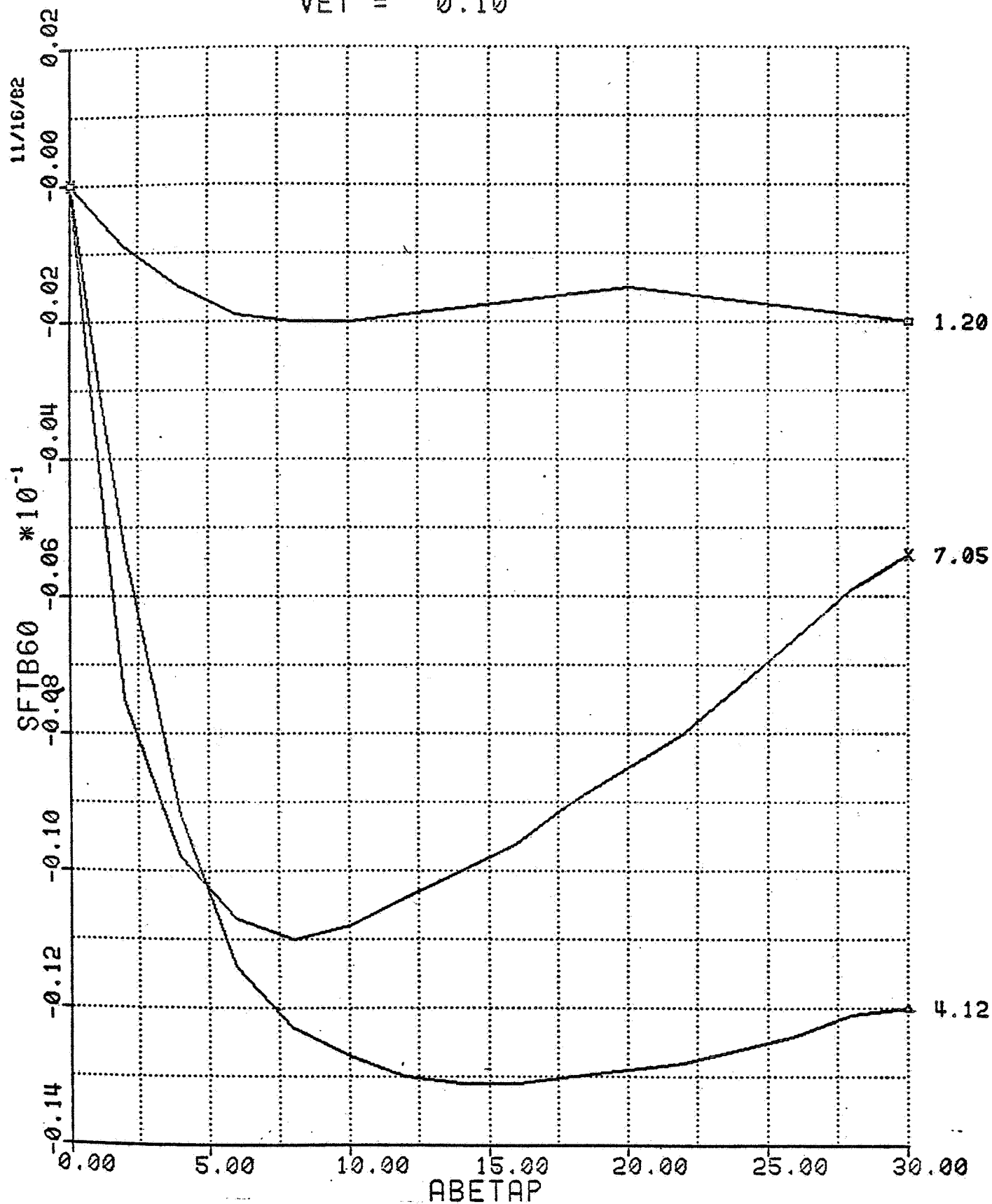
SFTB60 VS ABETAP
FOR VARYING HP
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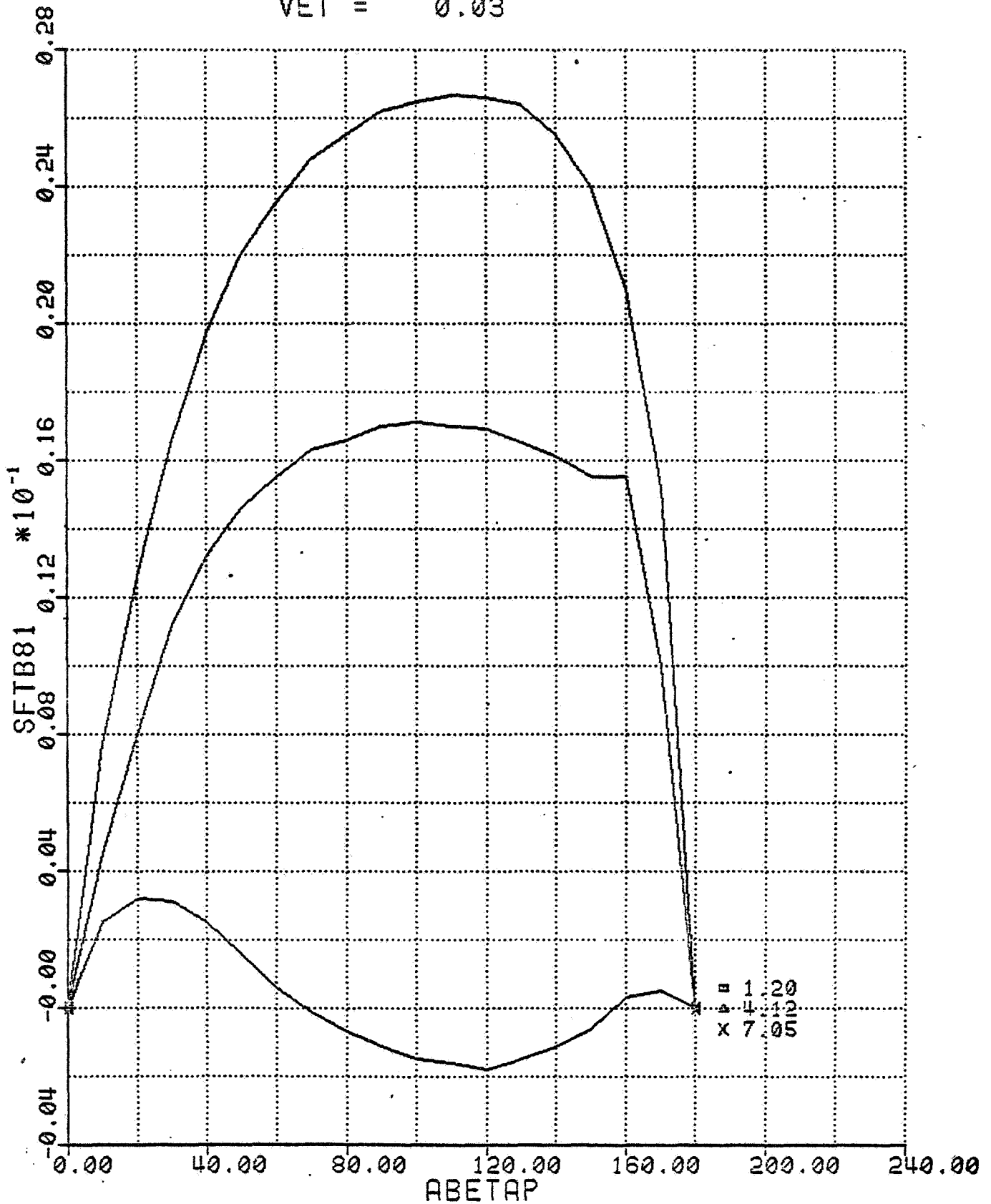
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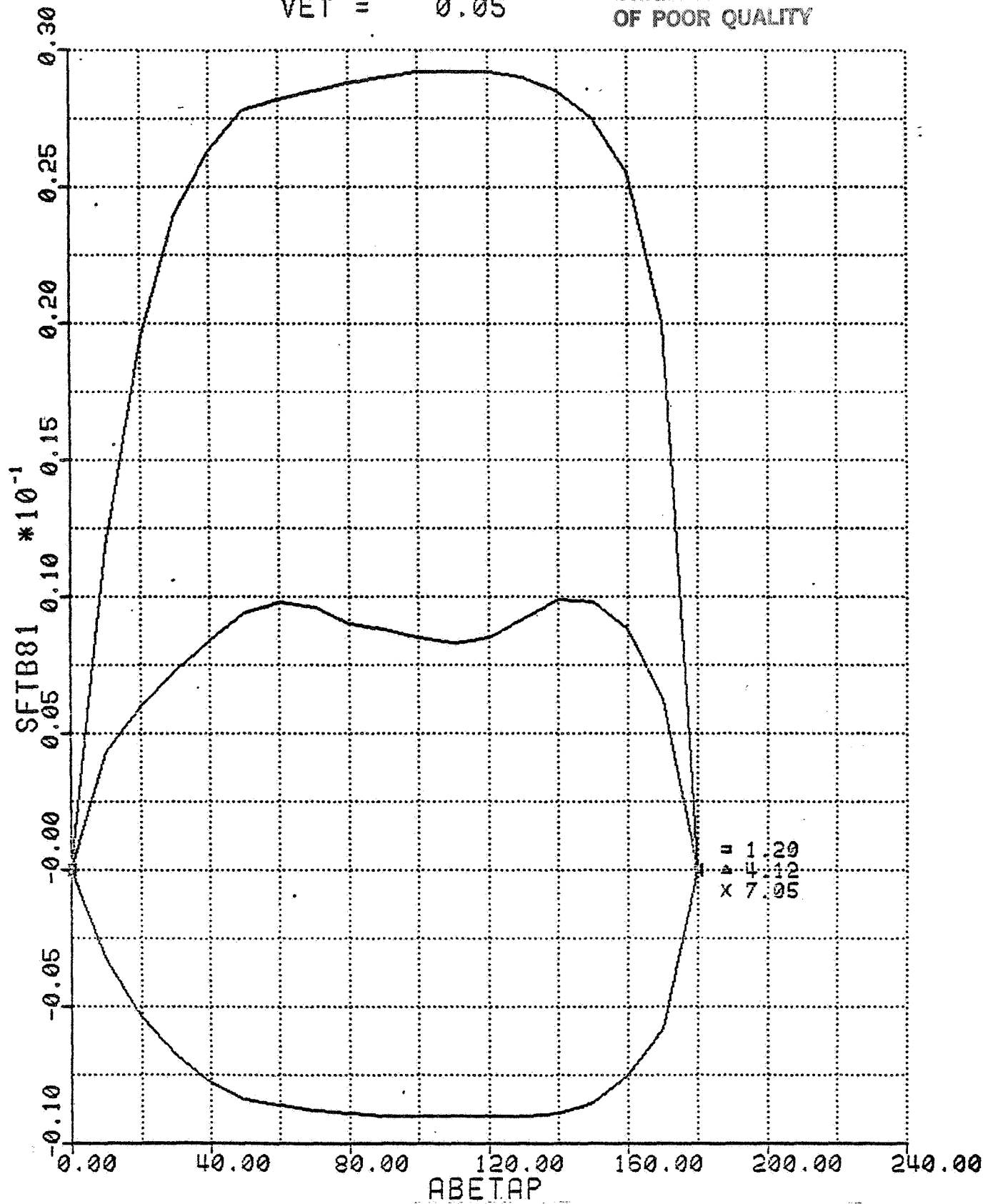
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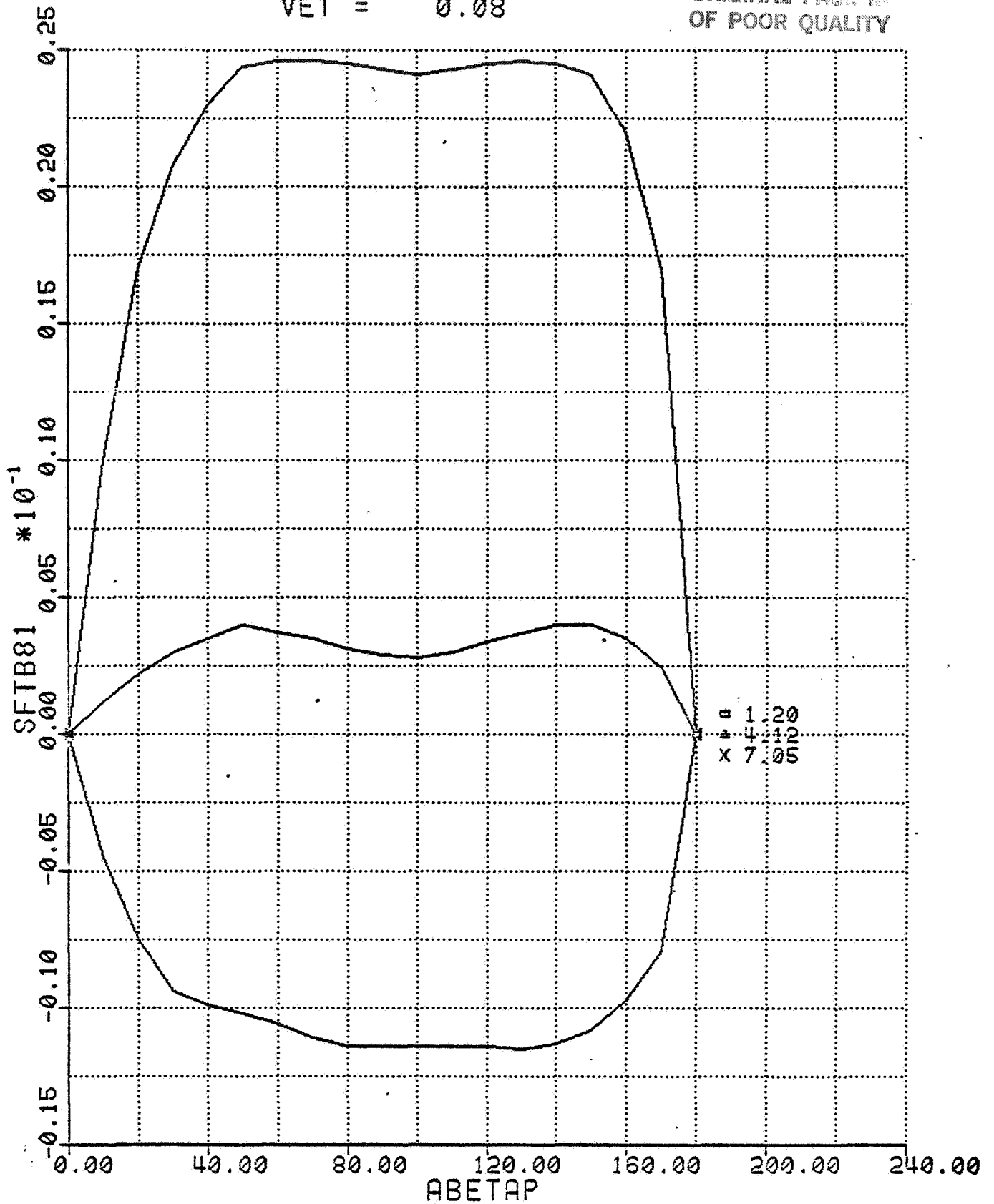
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FOR VARYING HP
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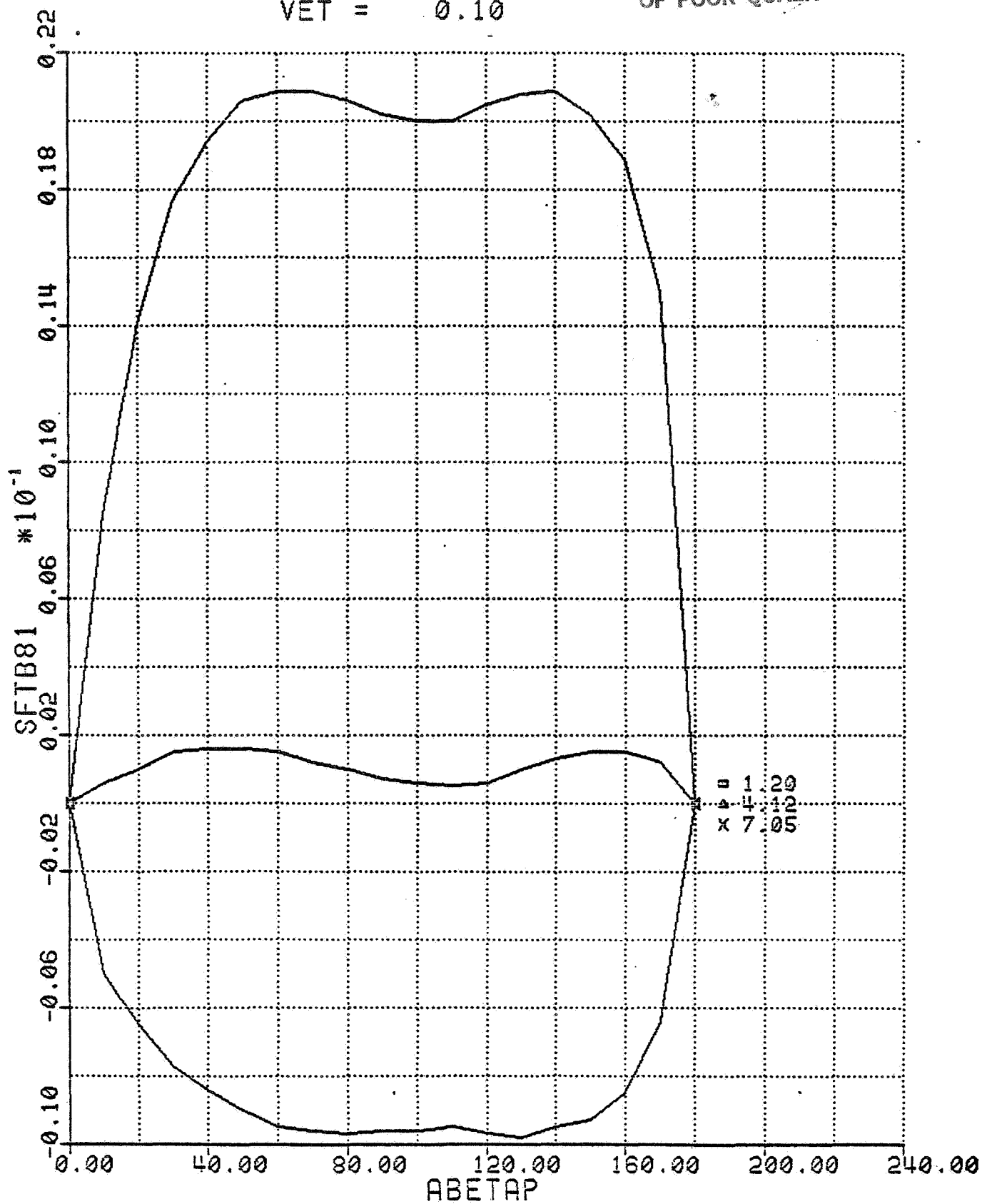
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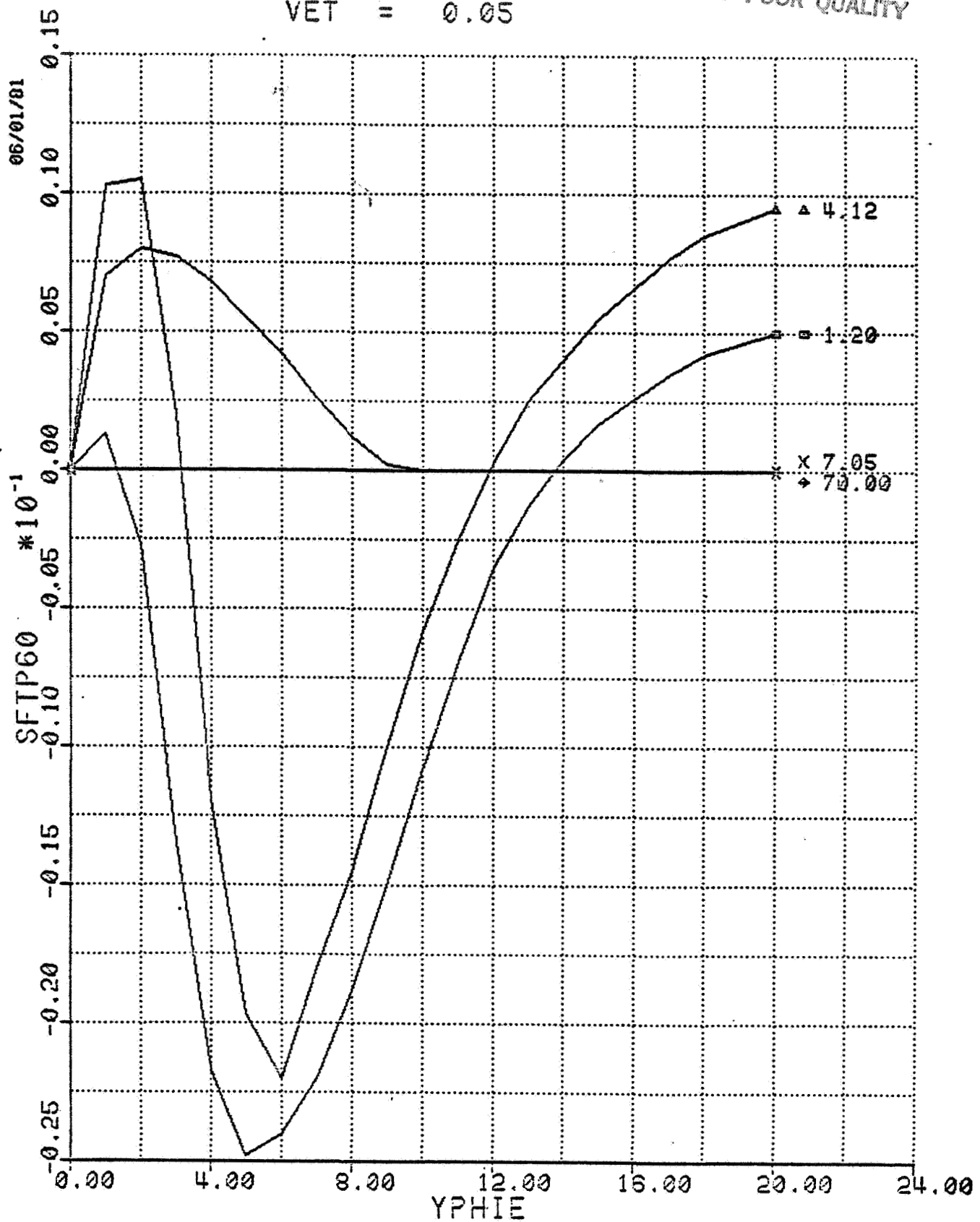
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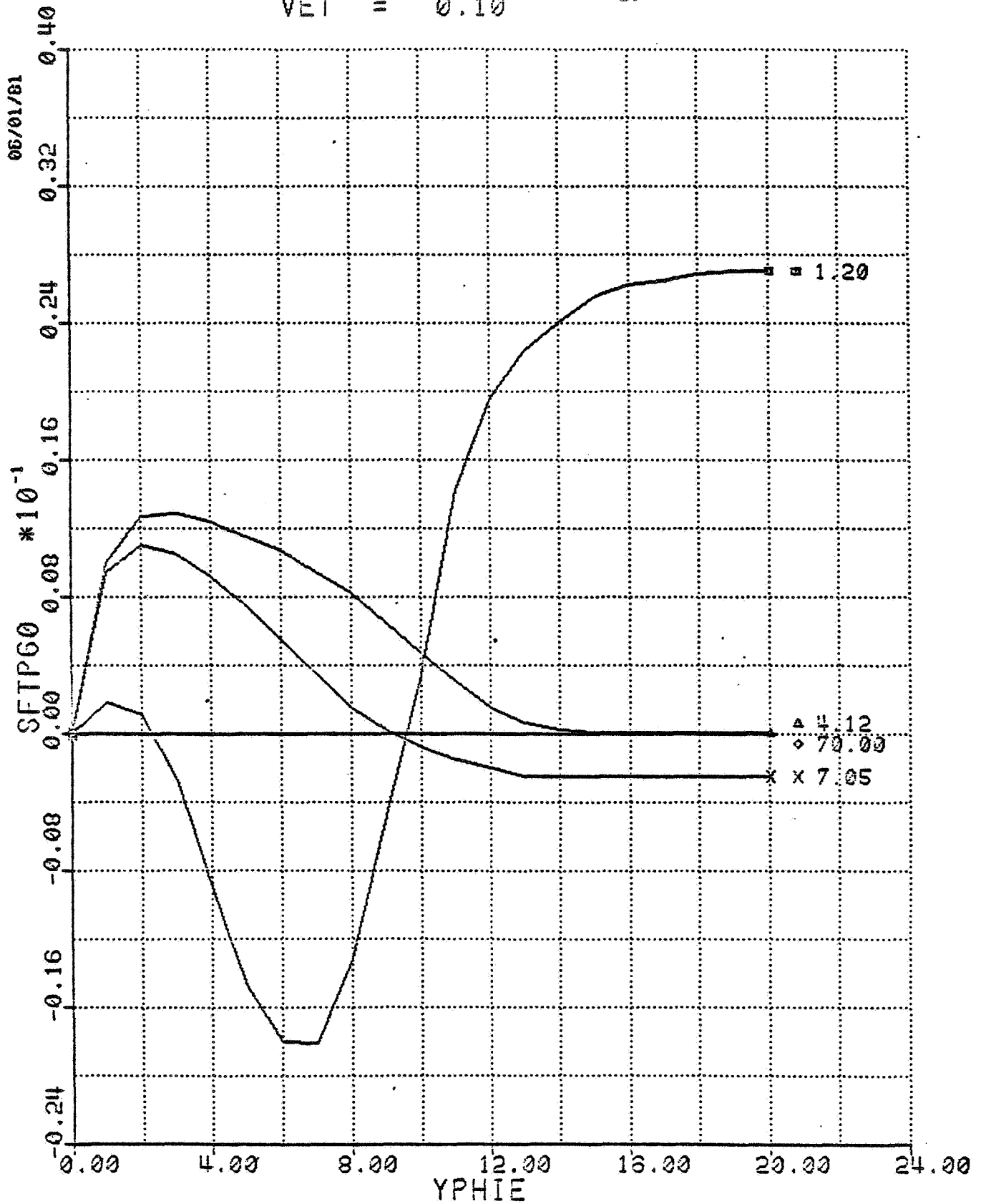
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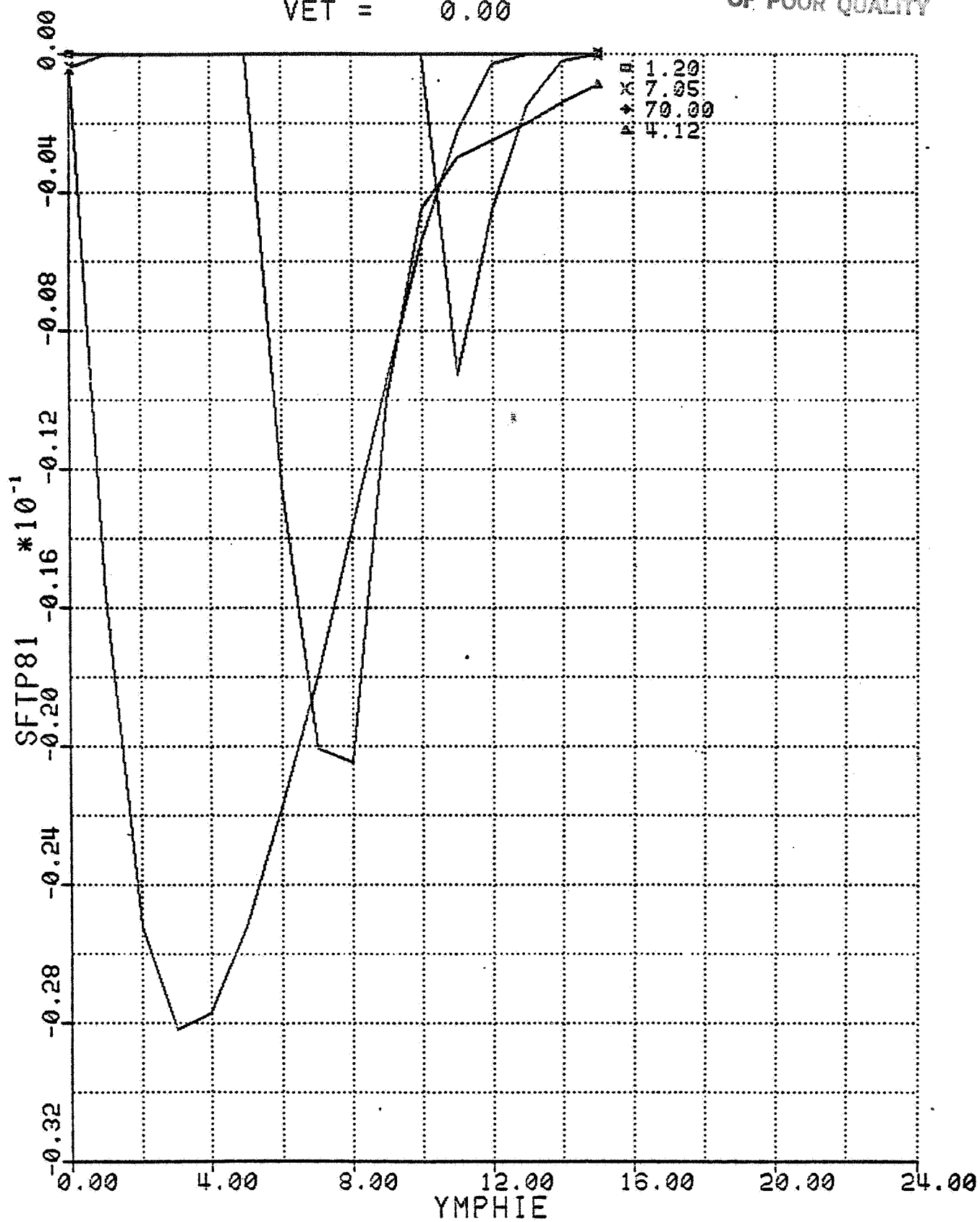
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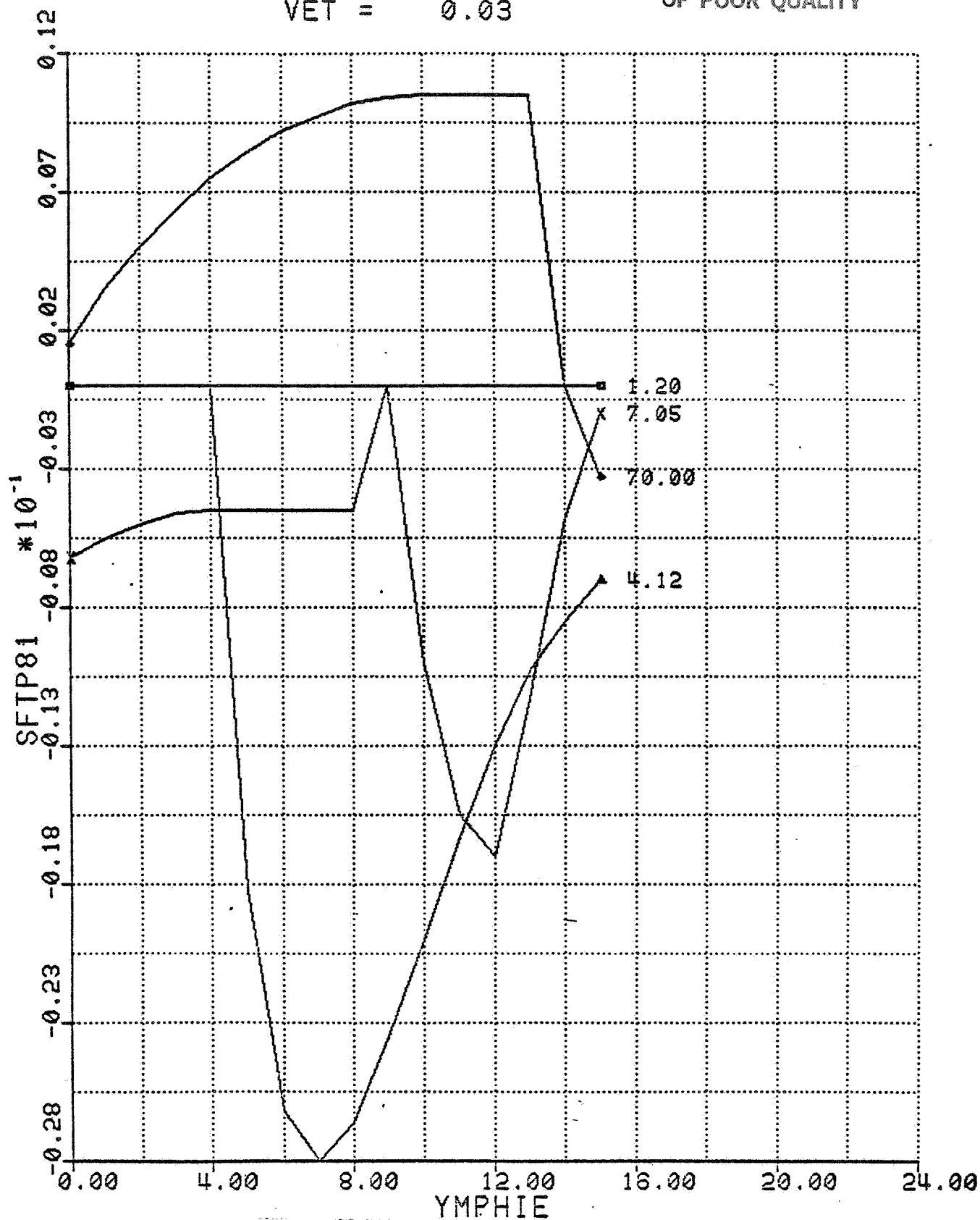
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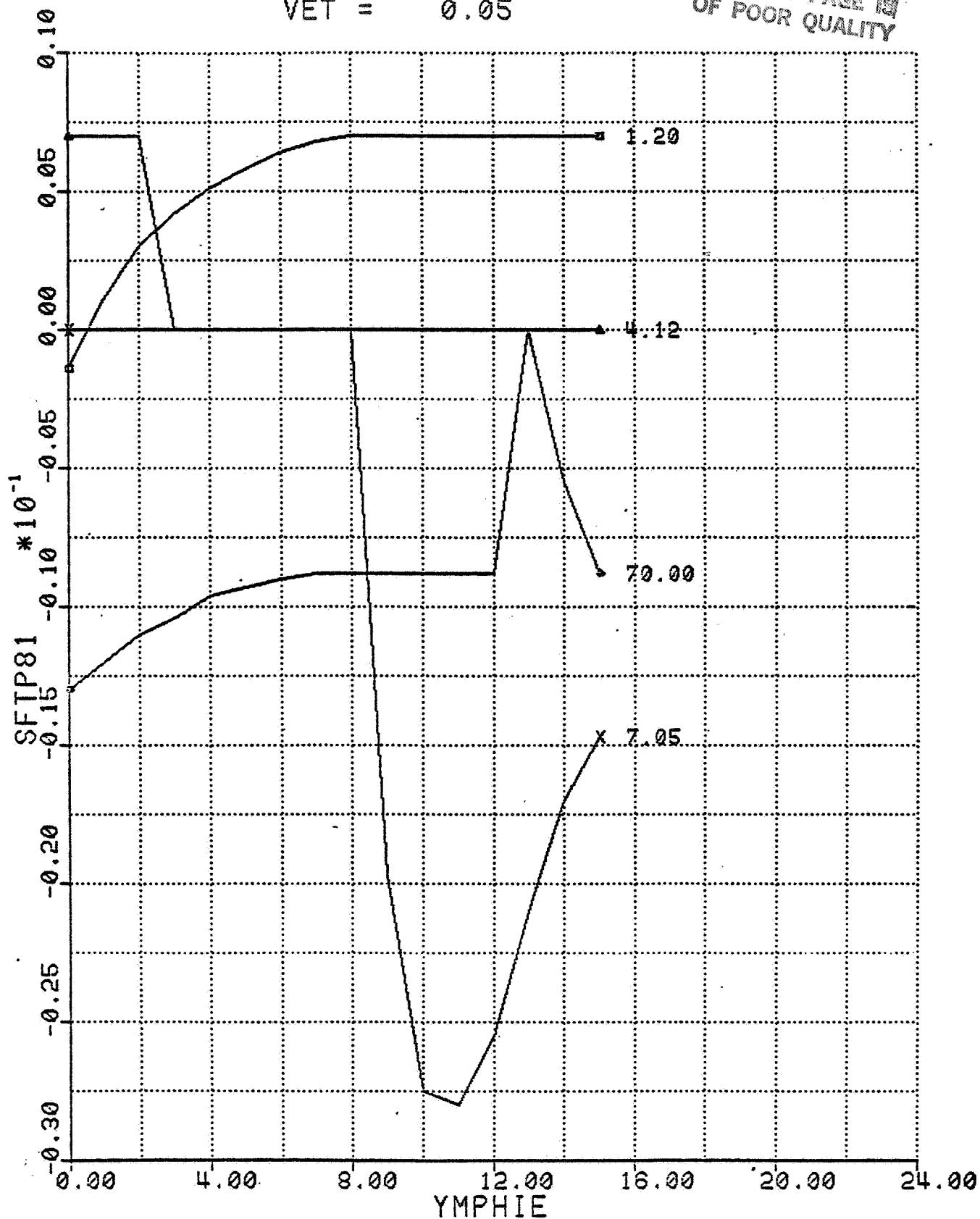
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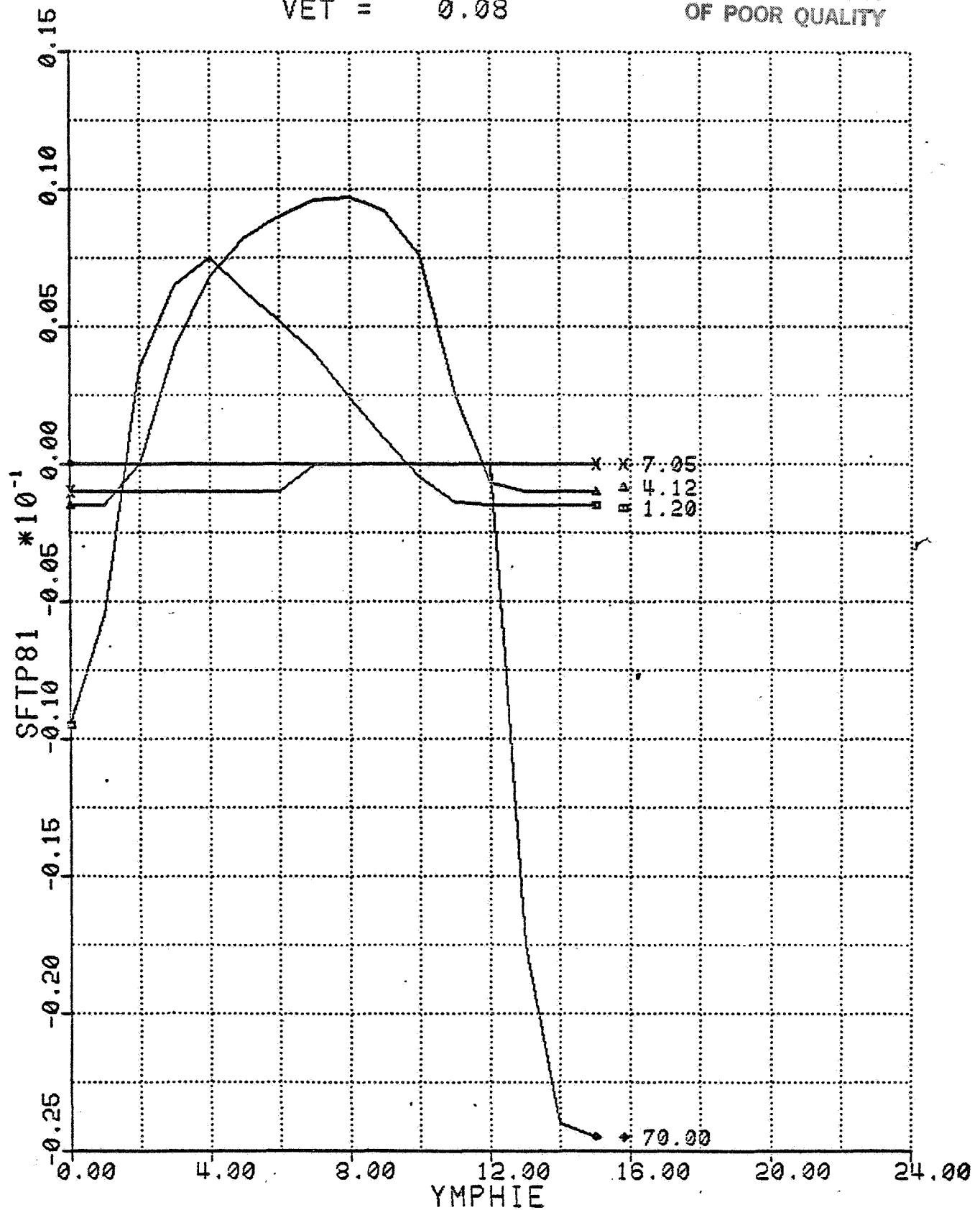
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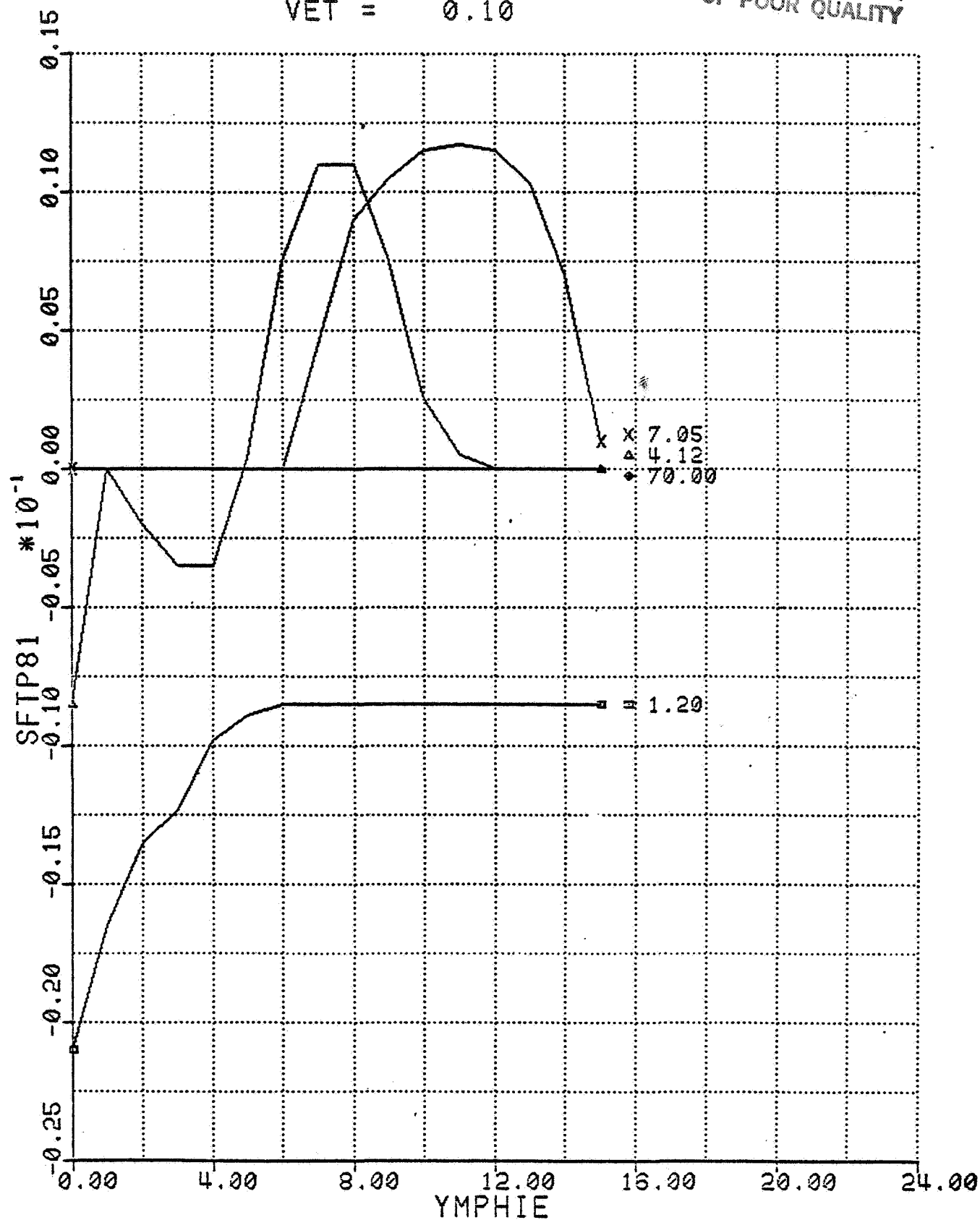
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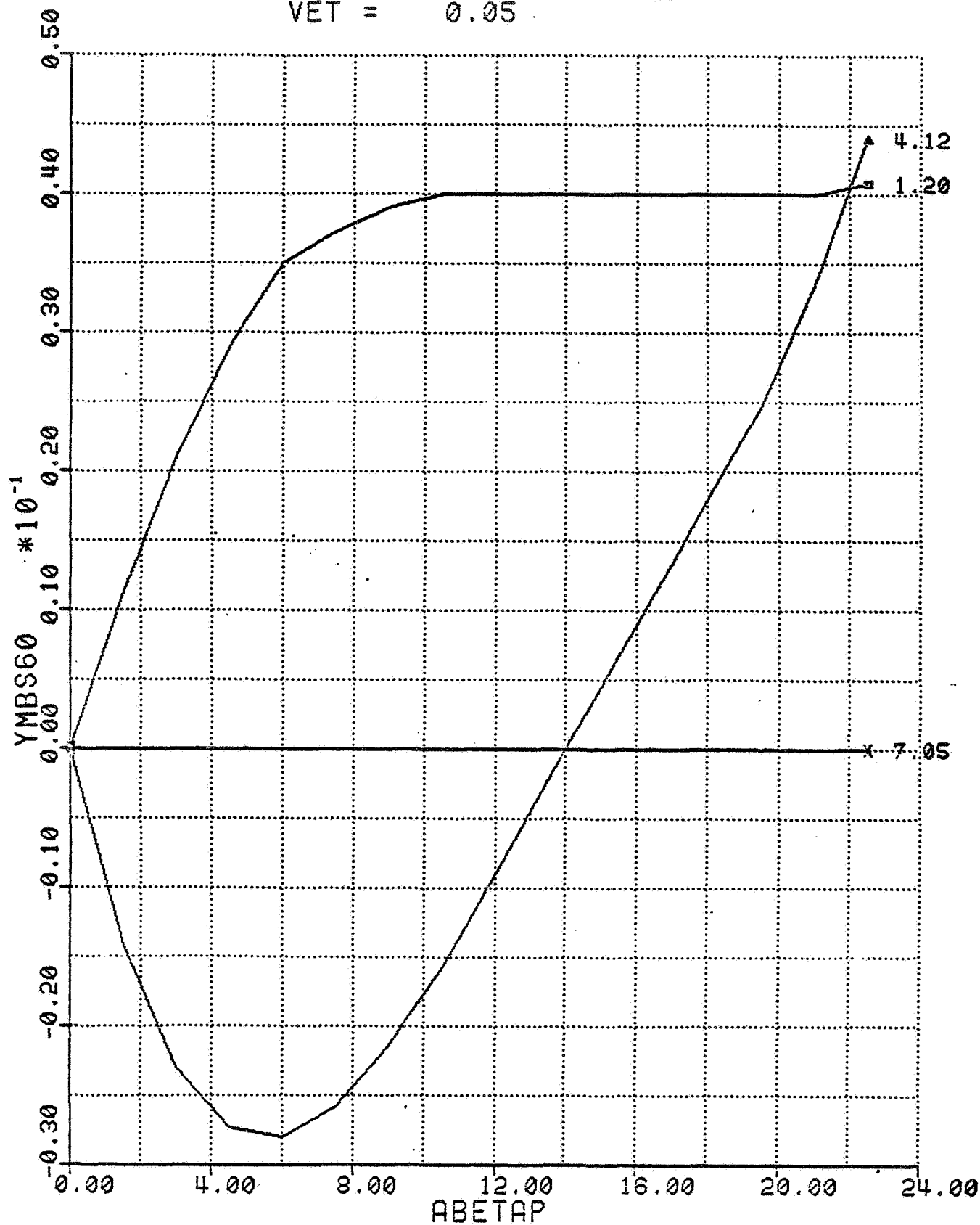
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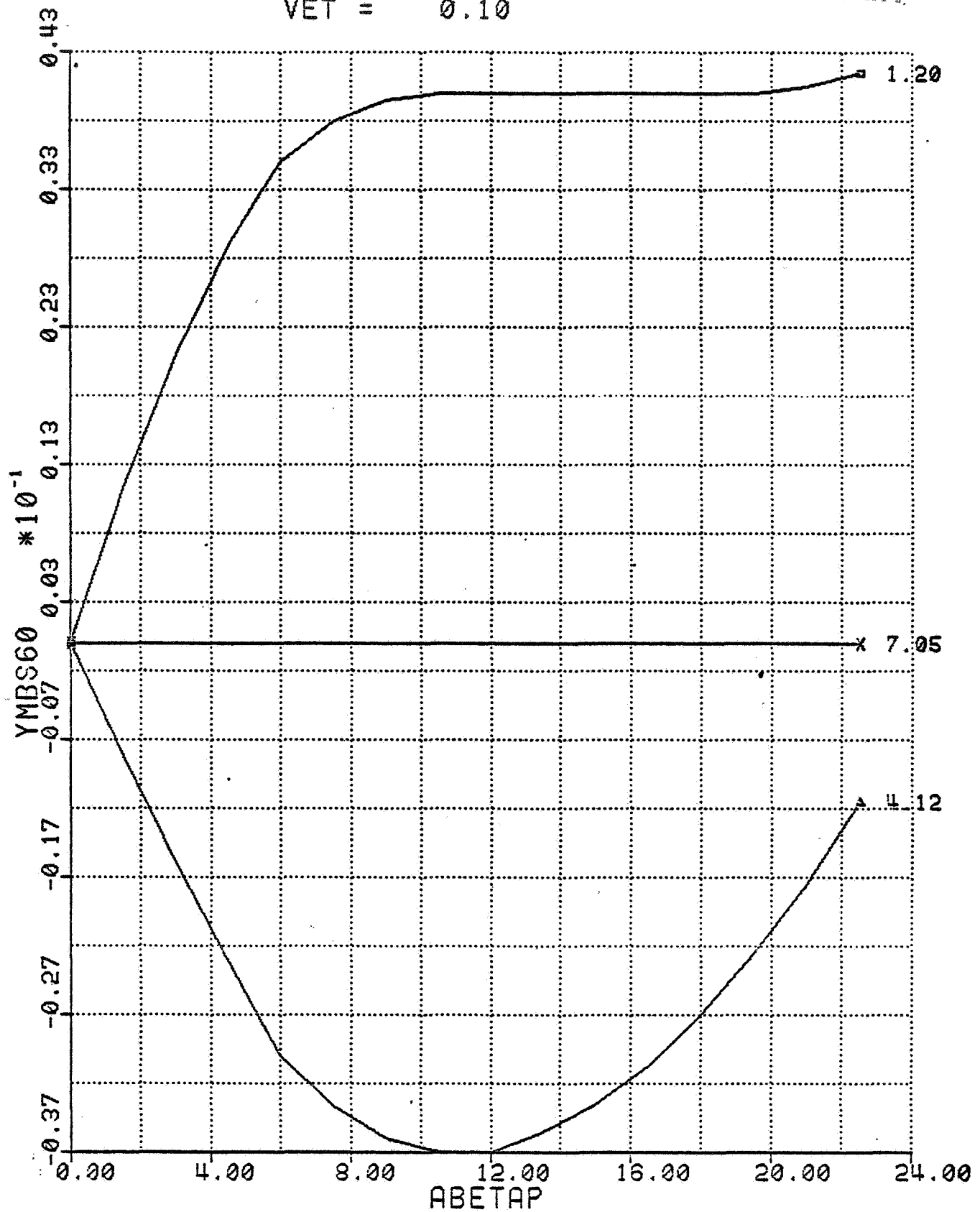
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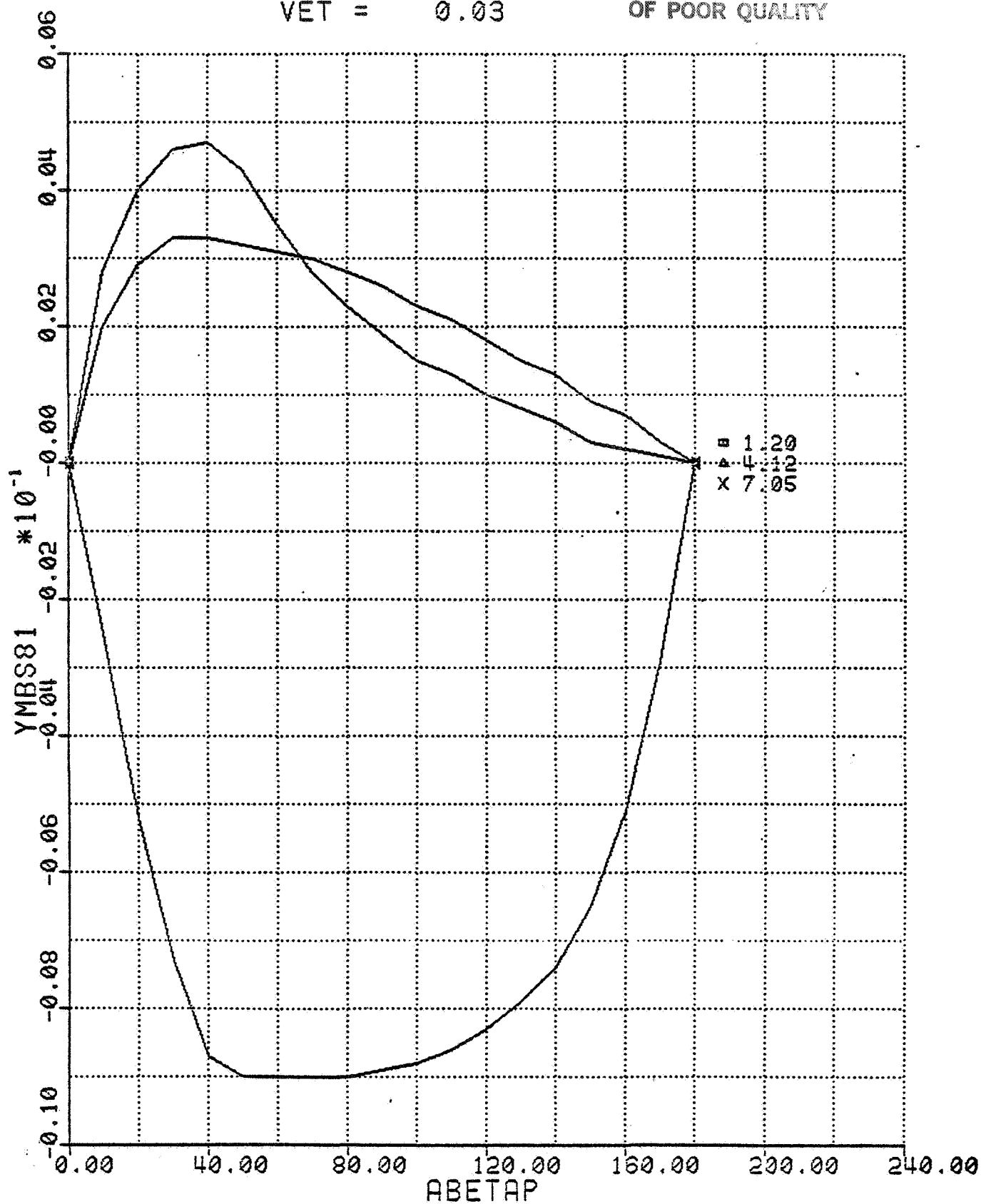
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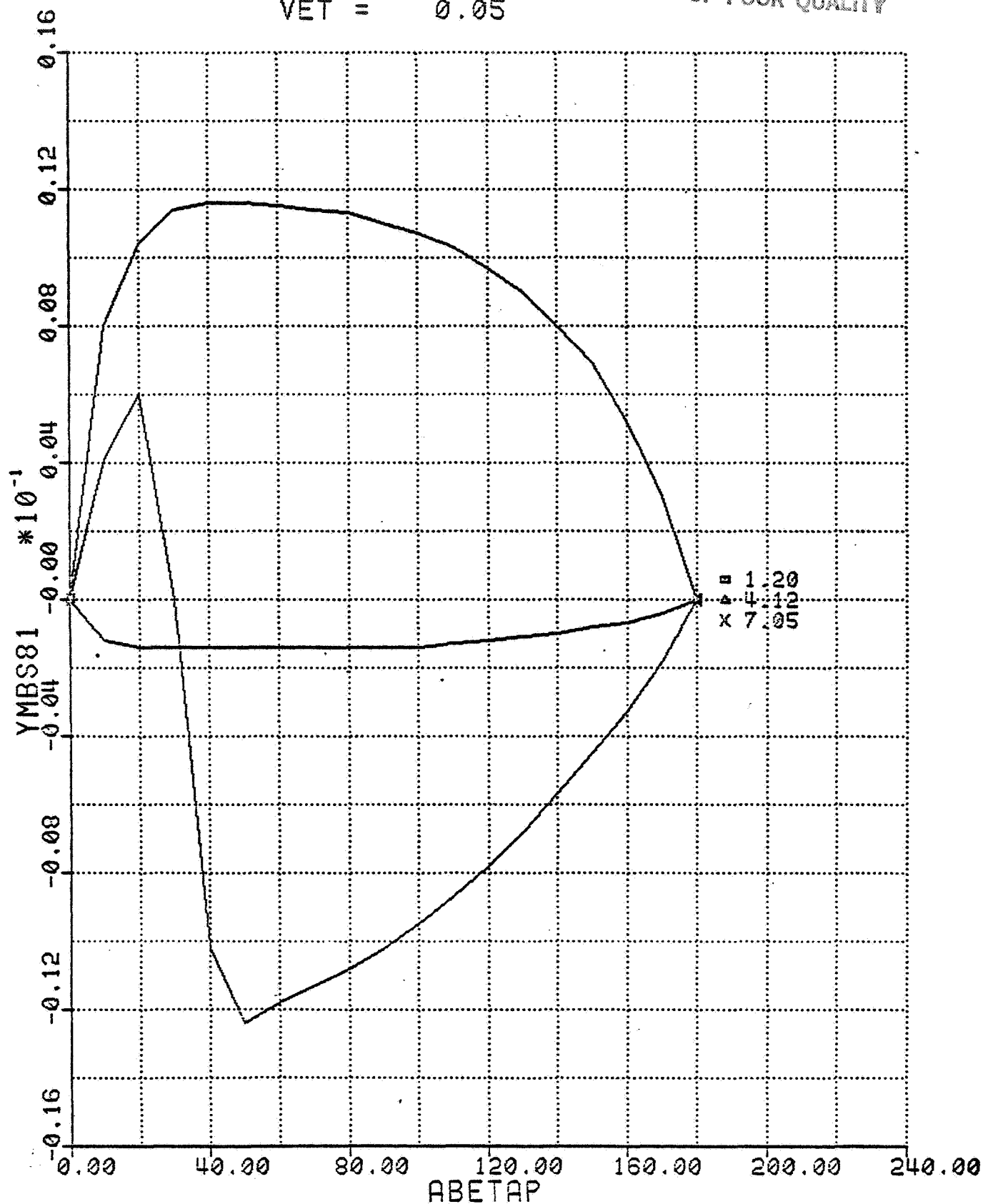
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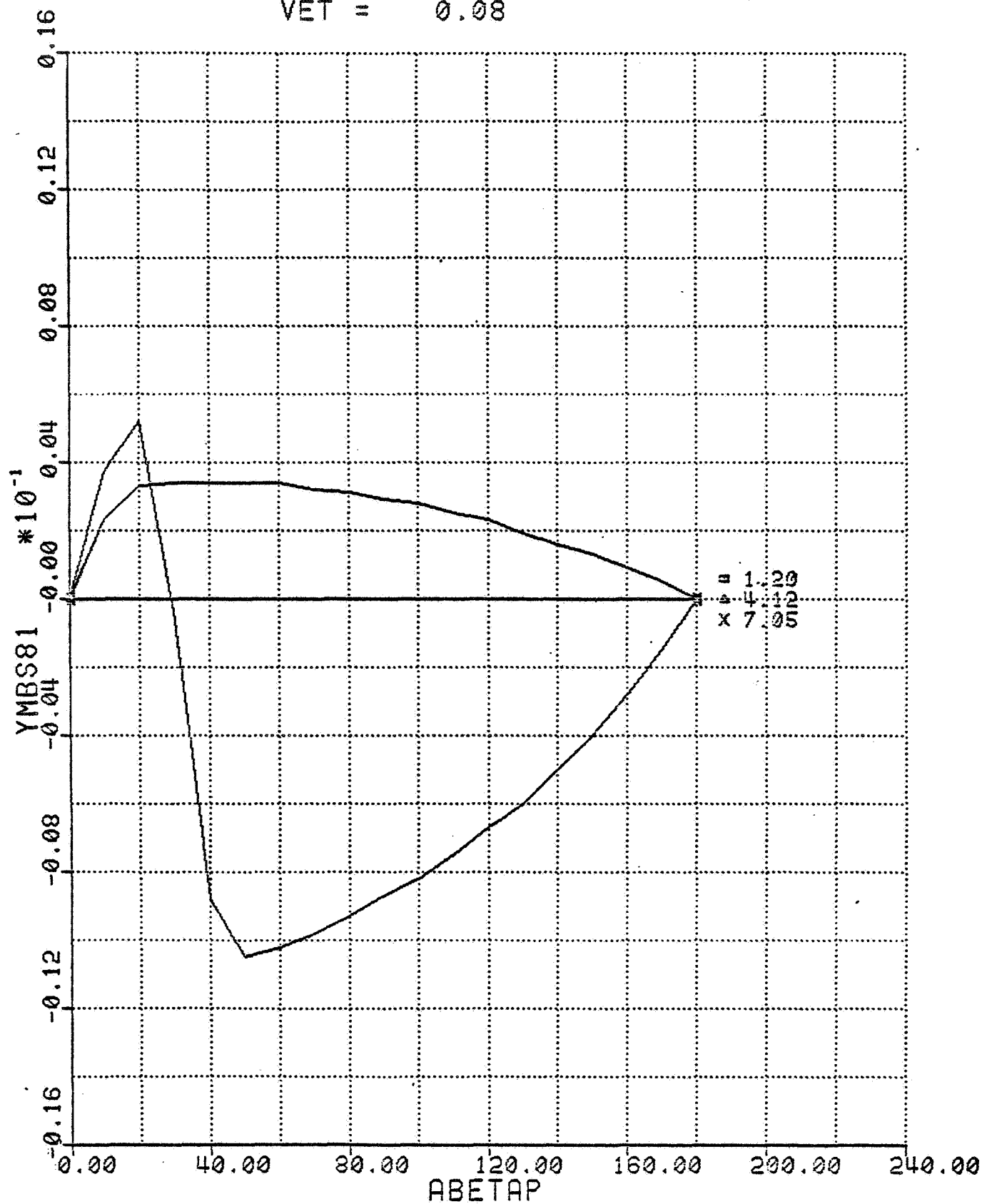
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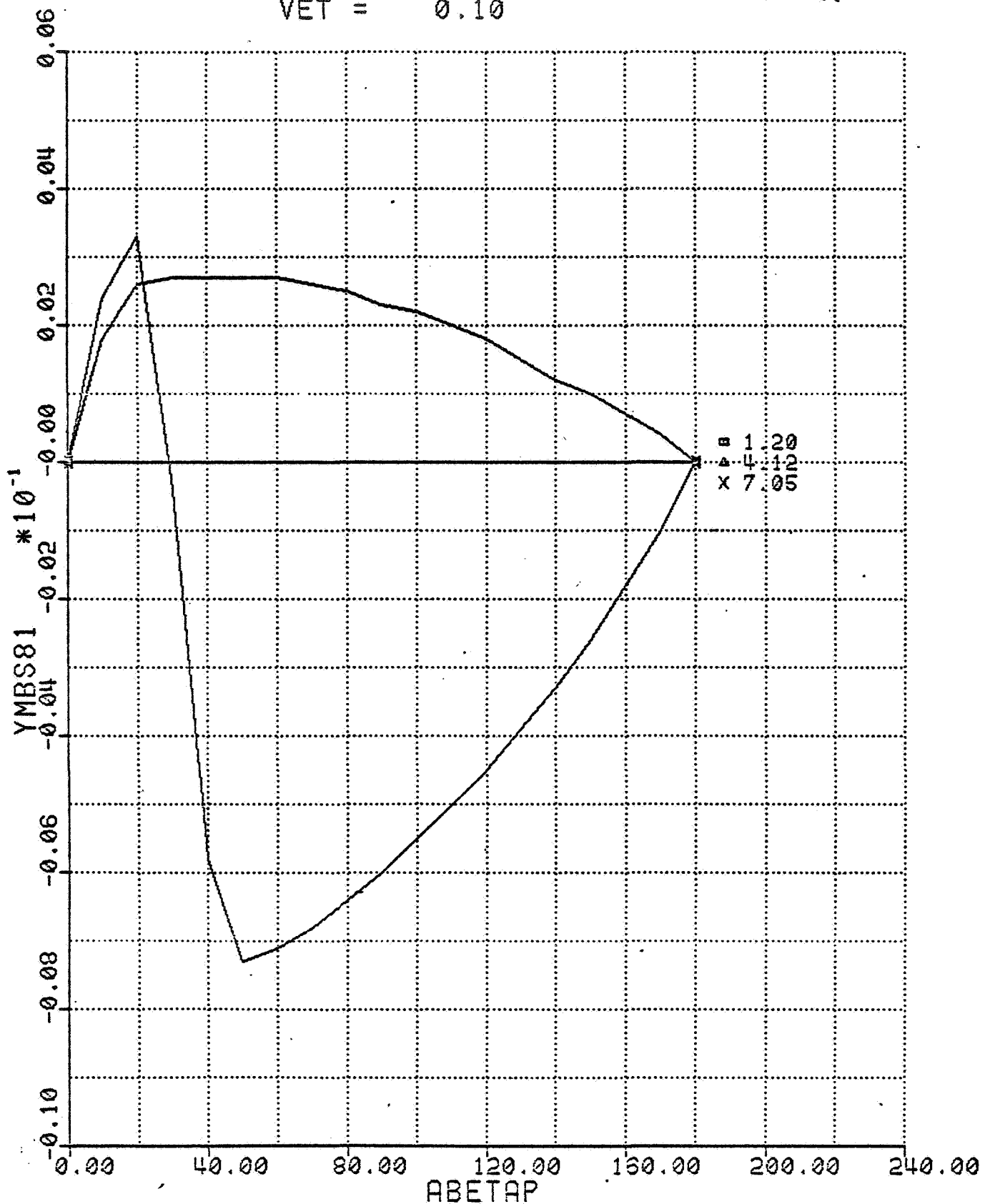
YMBS81 VS ABETAP
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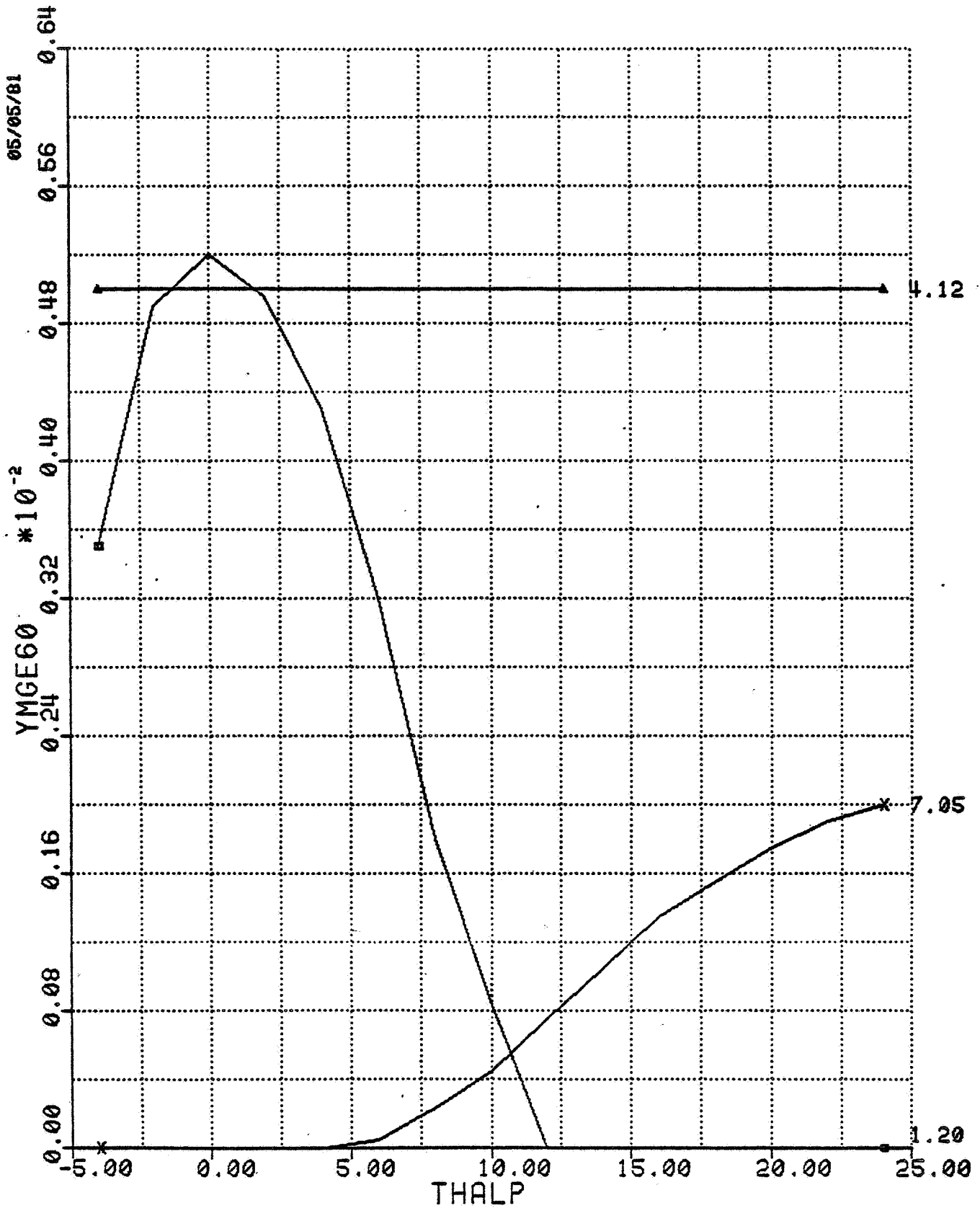


YMBS81 VS ABETAP
FOR VARYING HP
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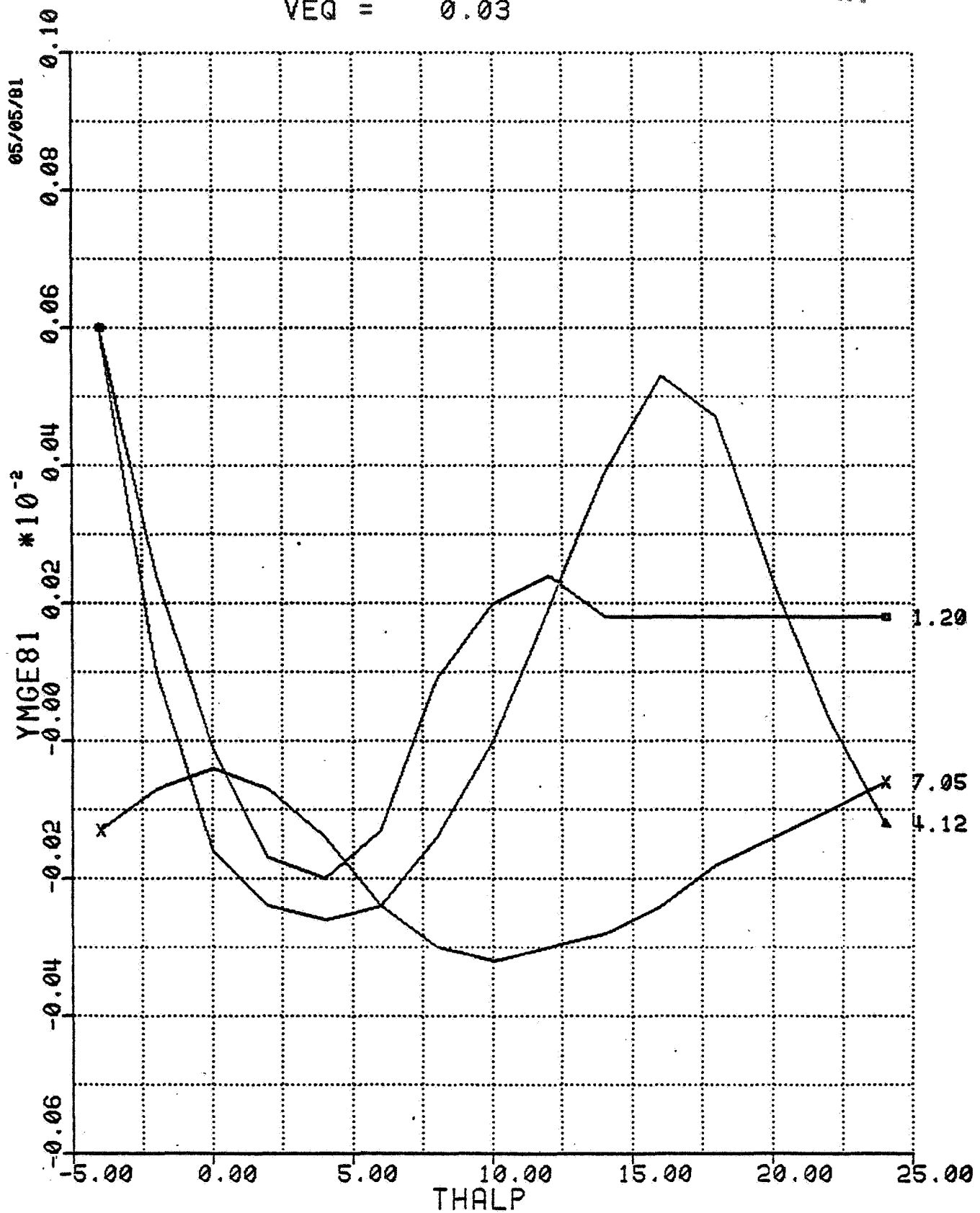


YMGE60 VS THALP
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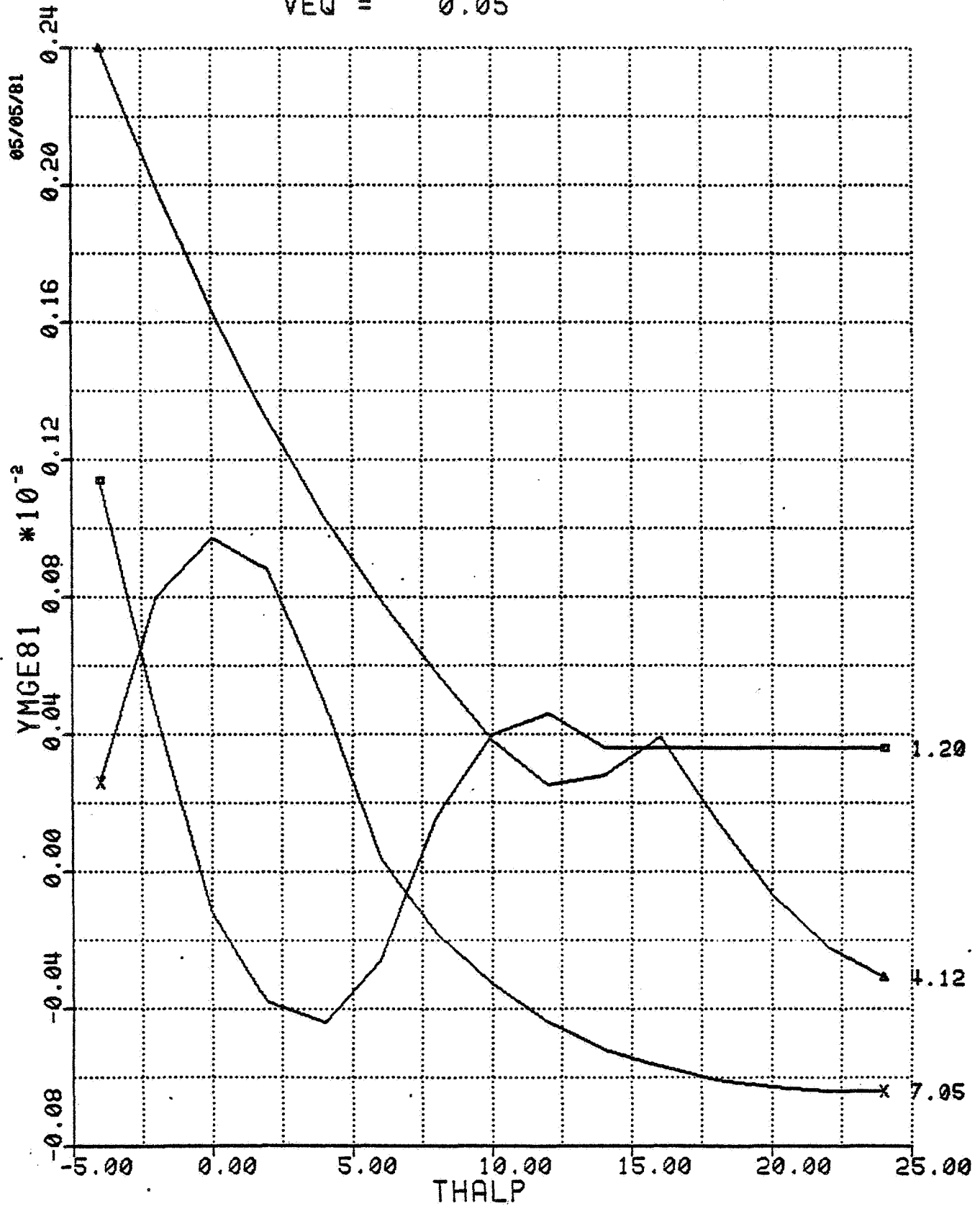
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FOR VARYING HP
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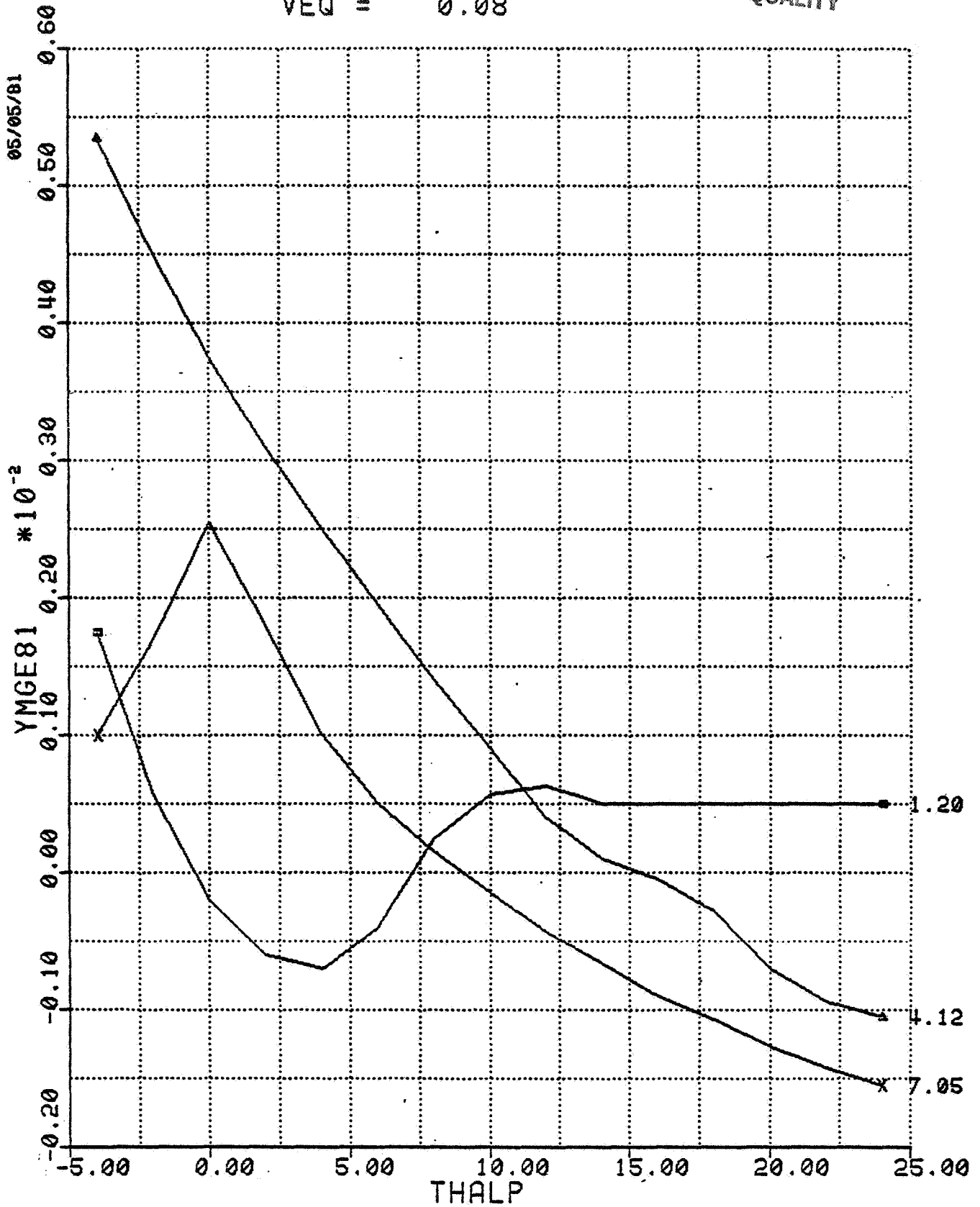
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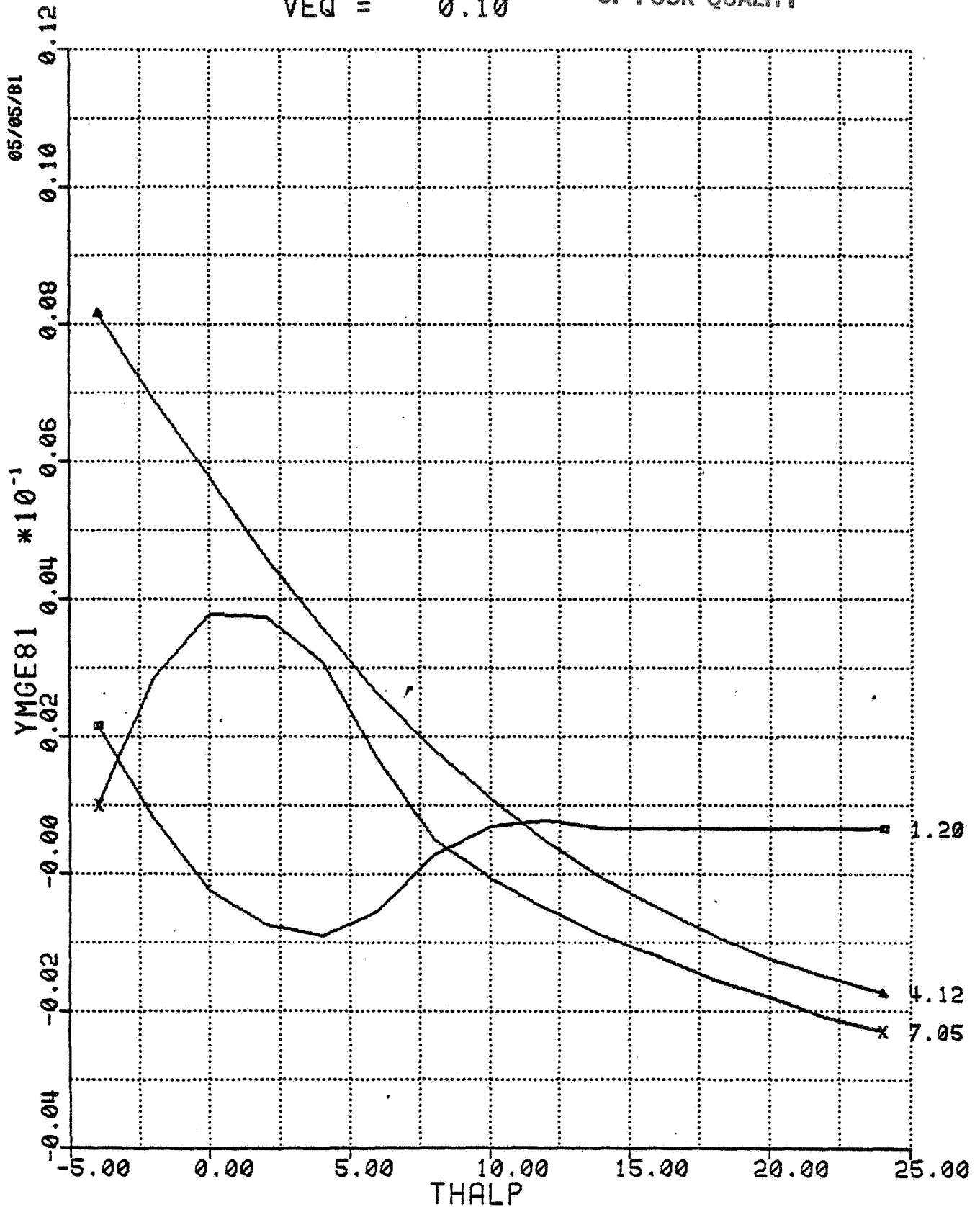
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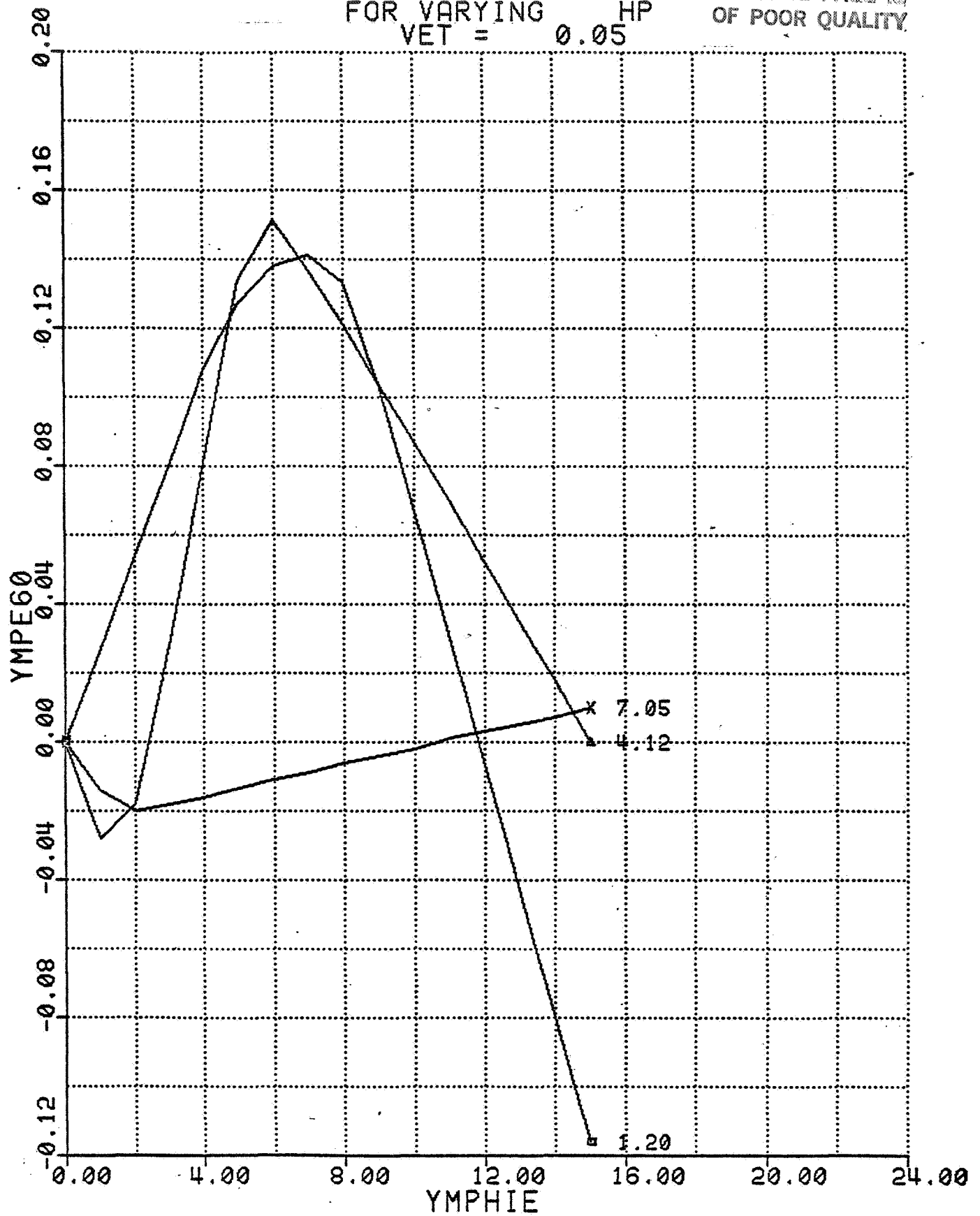
YMGE81 VS THALP
FOR VARYING HP
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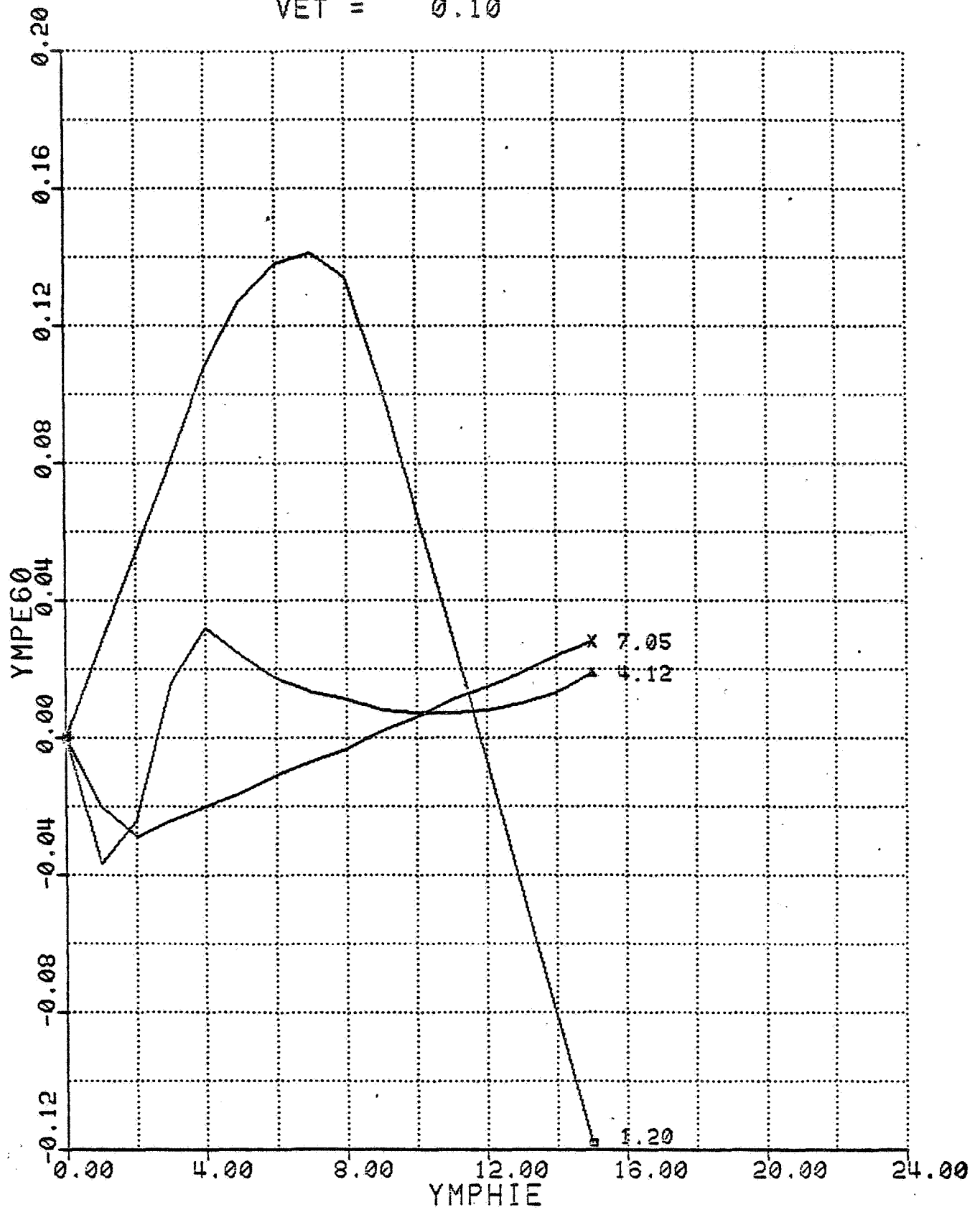


YMPE60 VS YMPHIE
FOR VARYING HP
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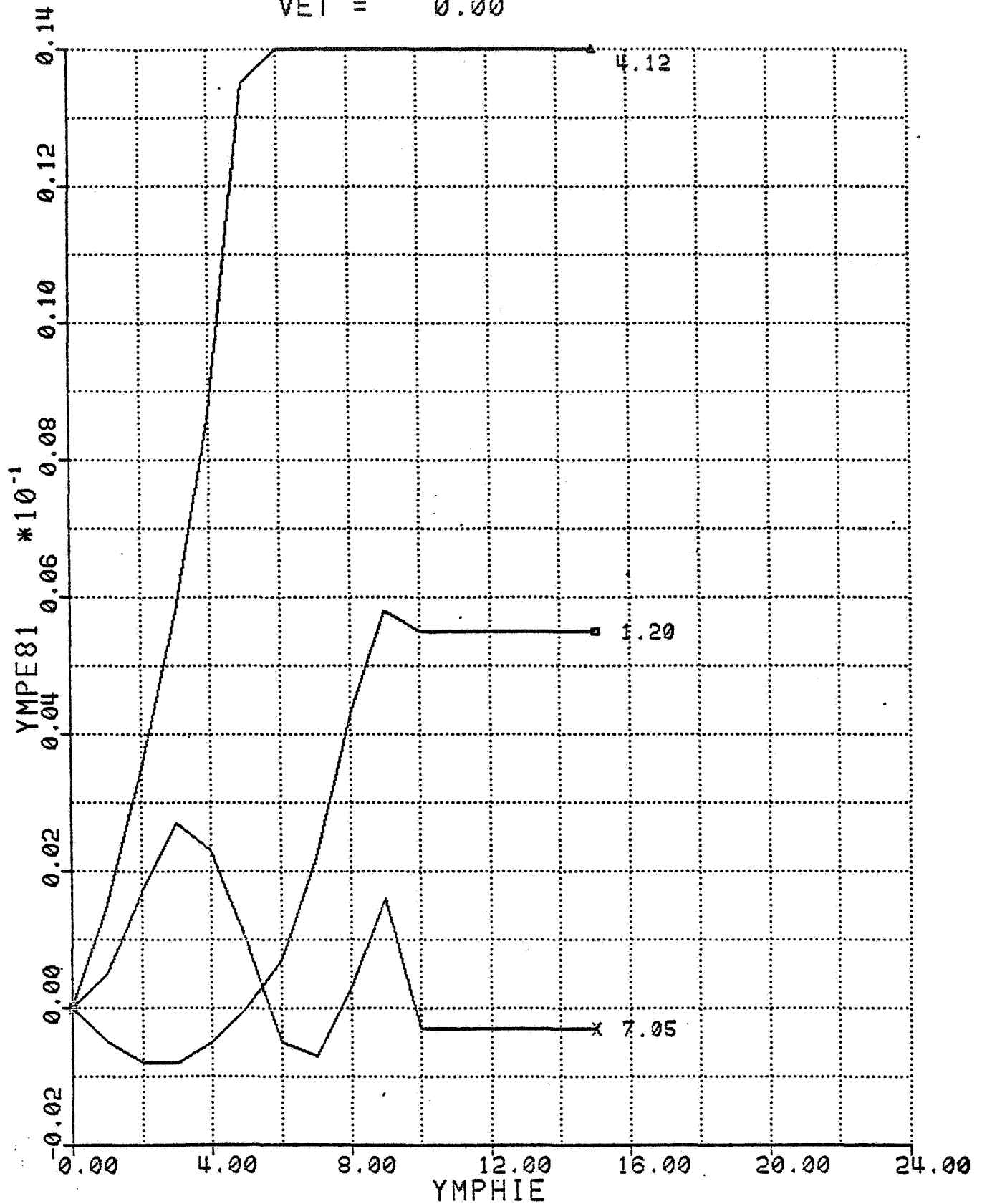
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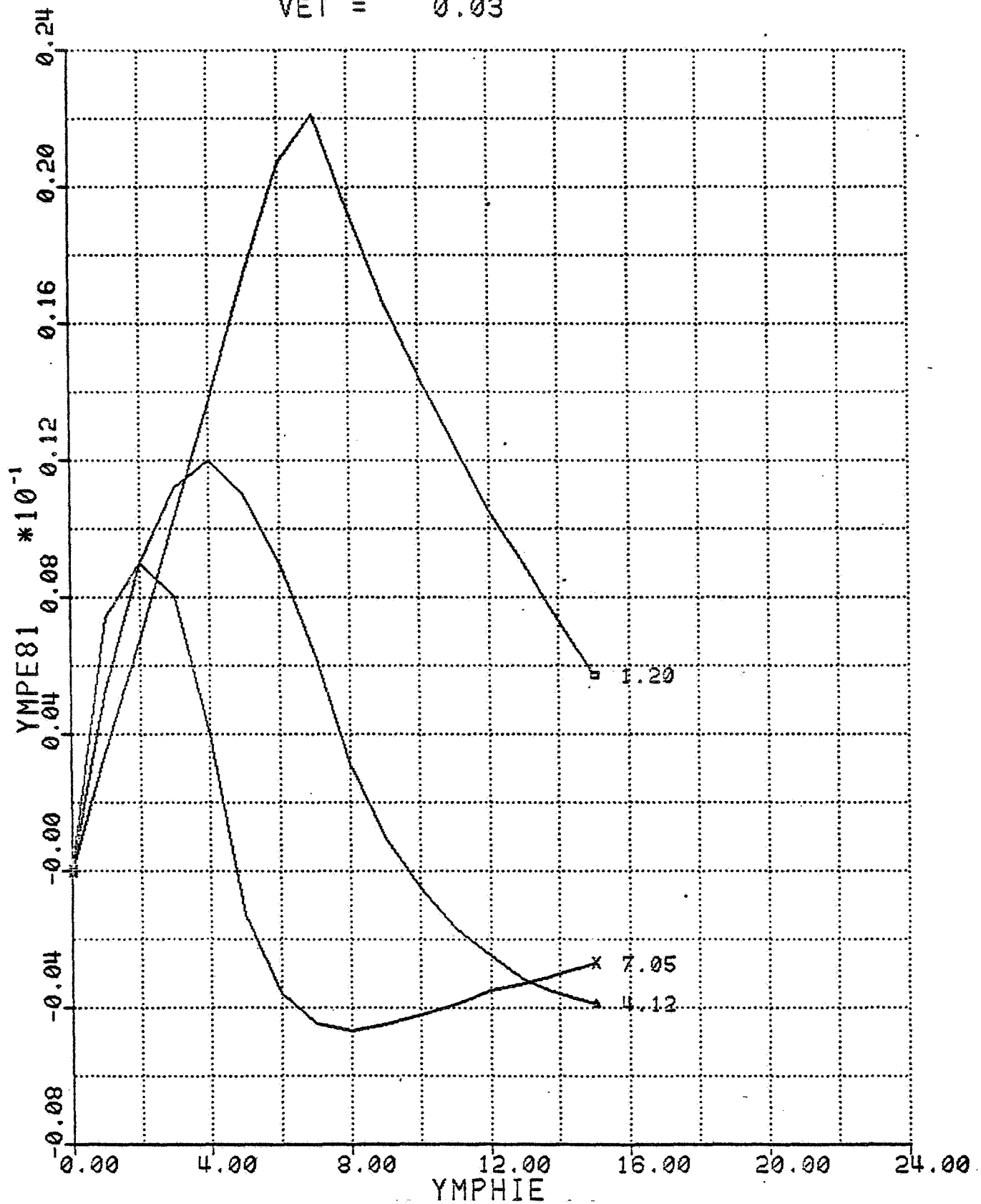
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FOR VARYING HP
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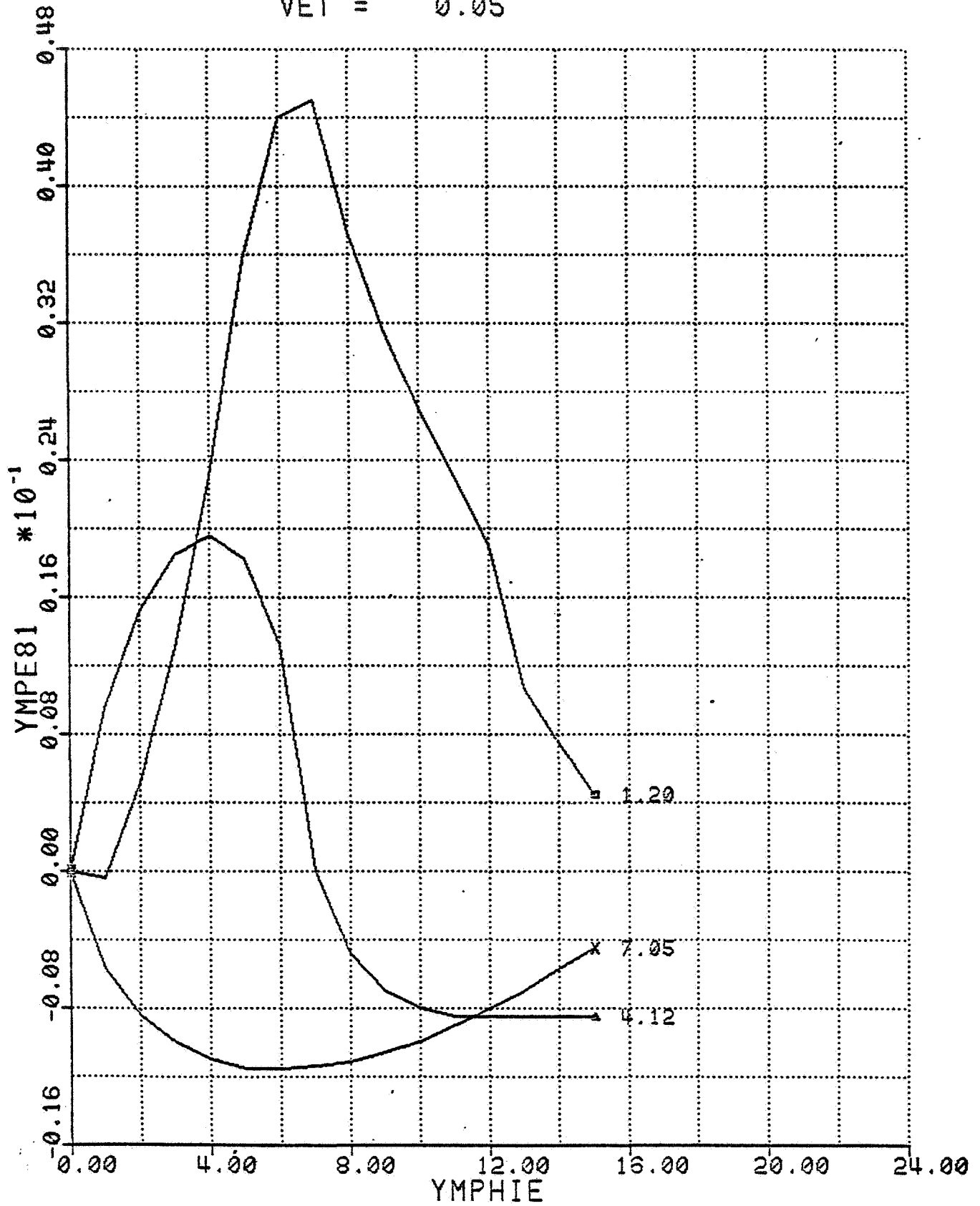
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FOR VARYING HP
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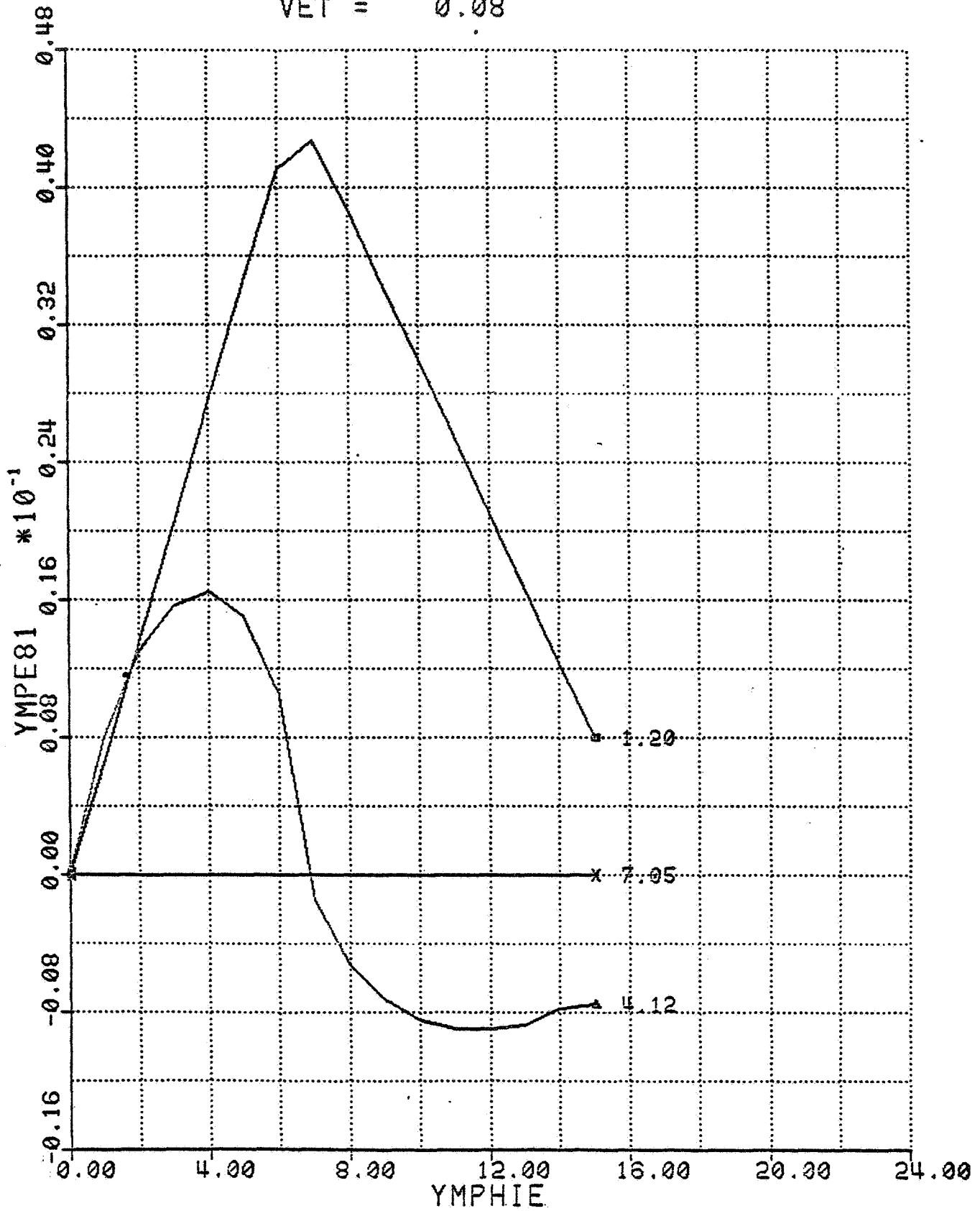
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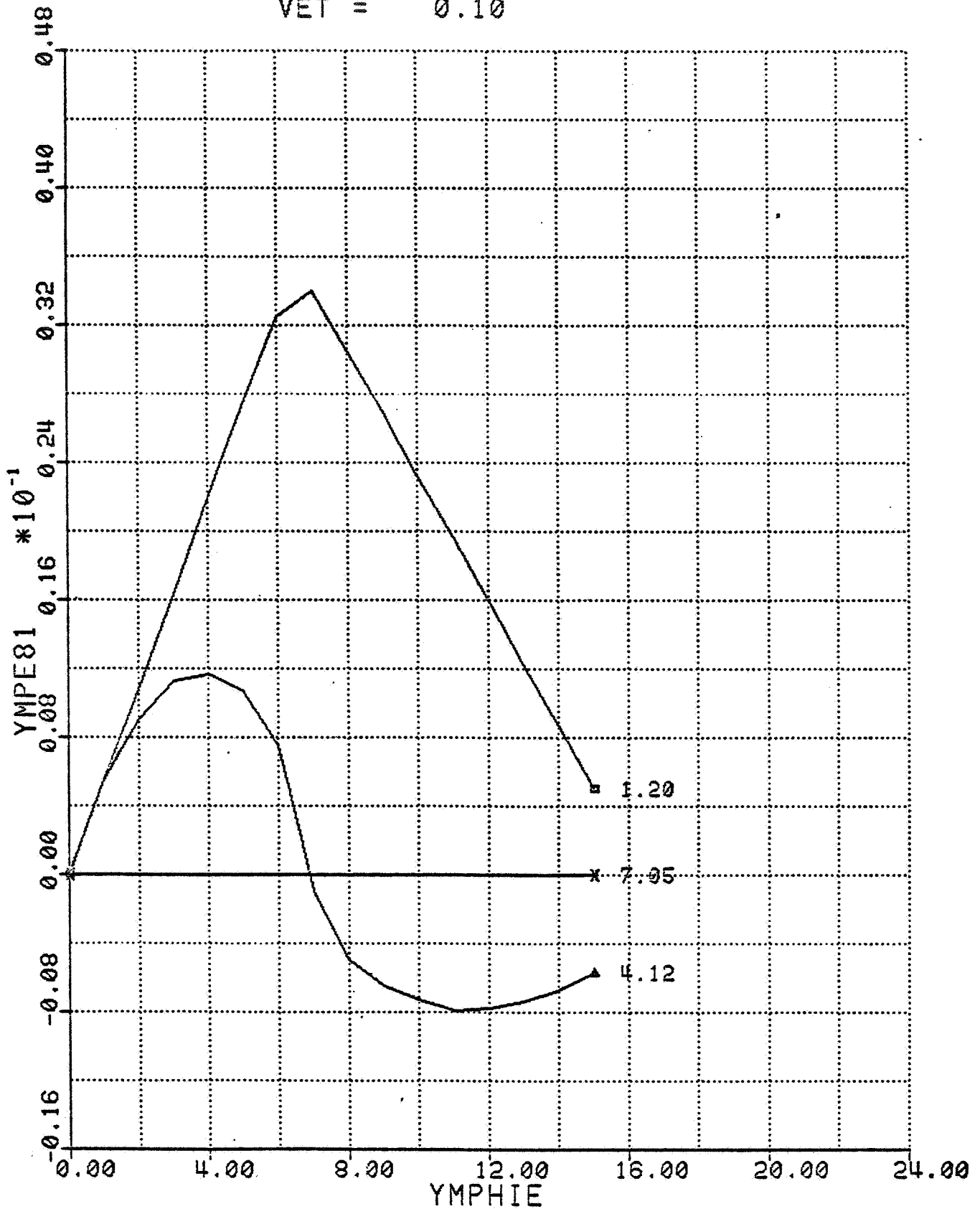
YMPE81 VS YMPHIE
FOR VARYING HP
VET = 0.05



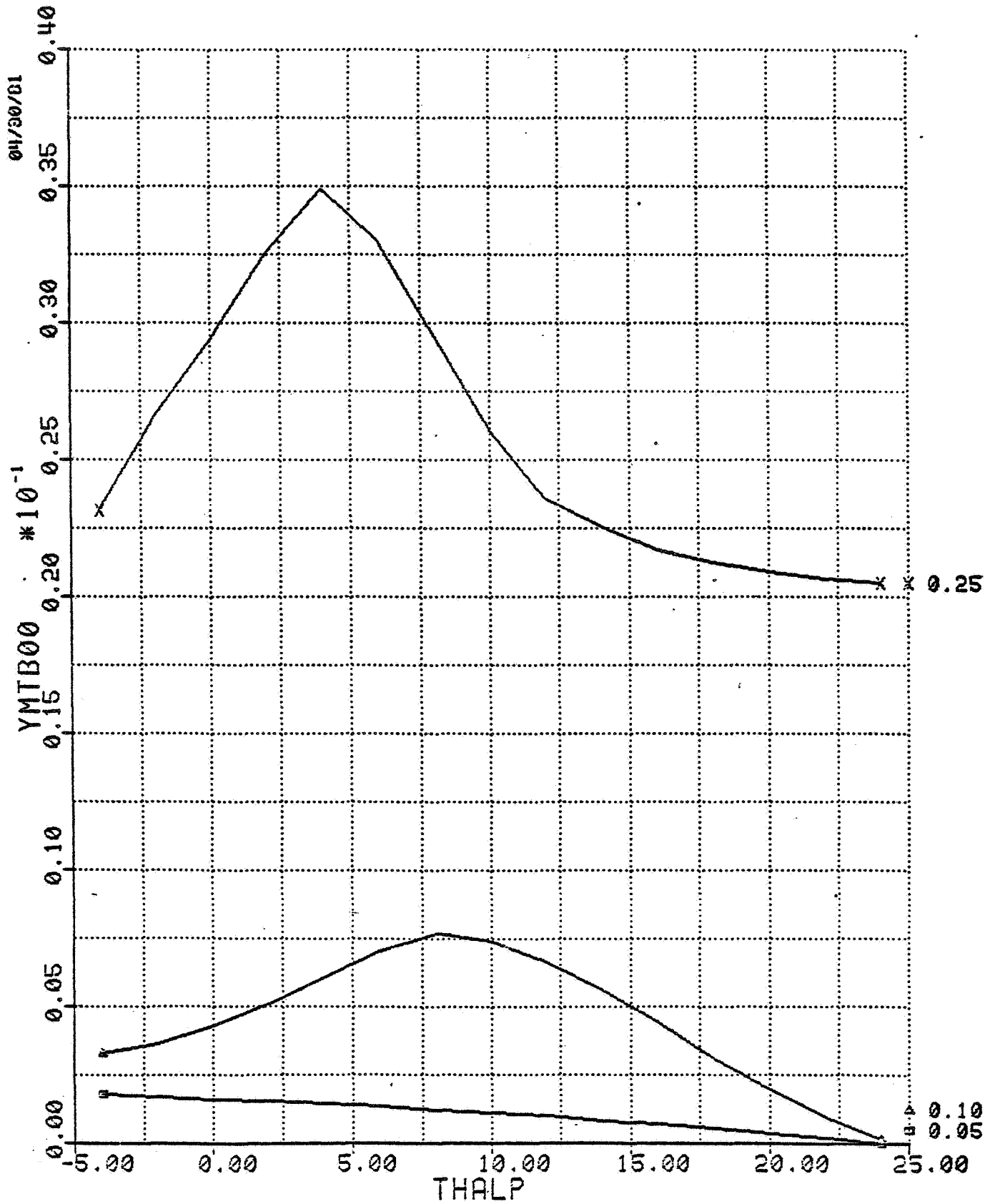
YMPE81 VS YMPHIE
FOR VARYING HP
VET = 0.08



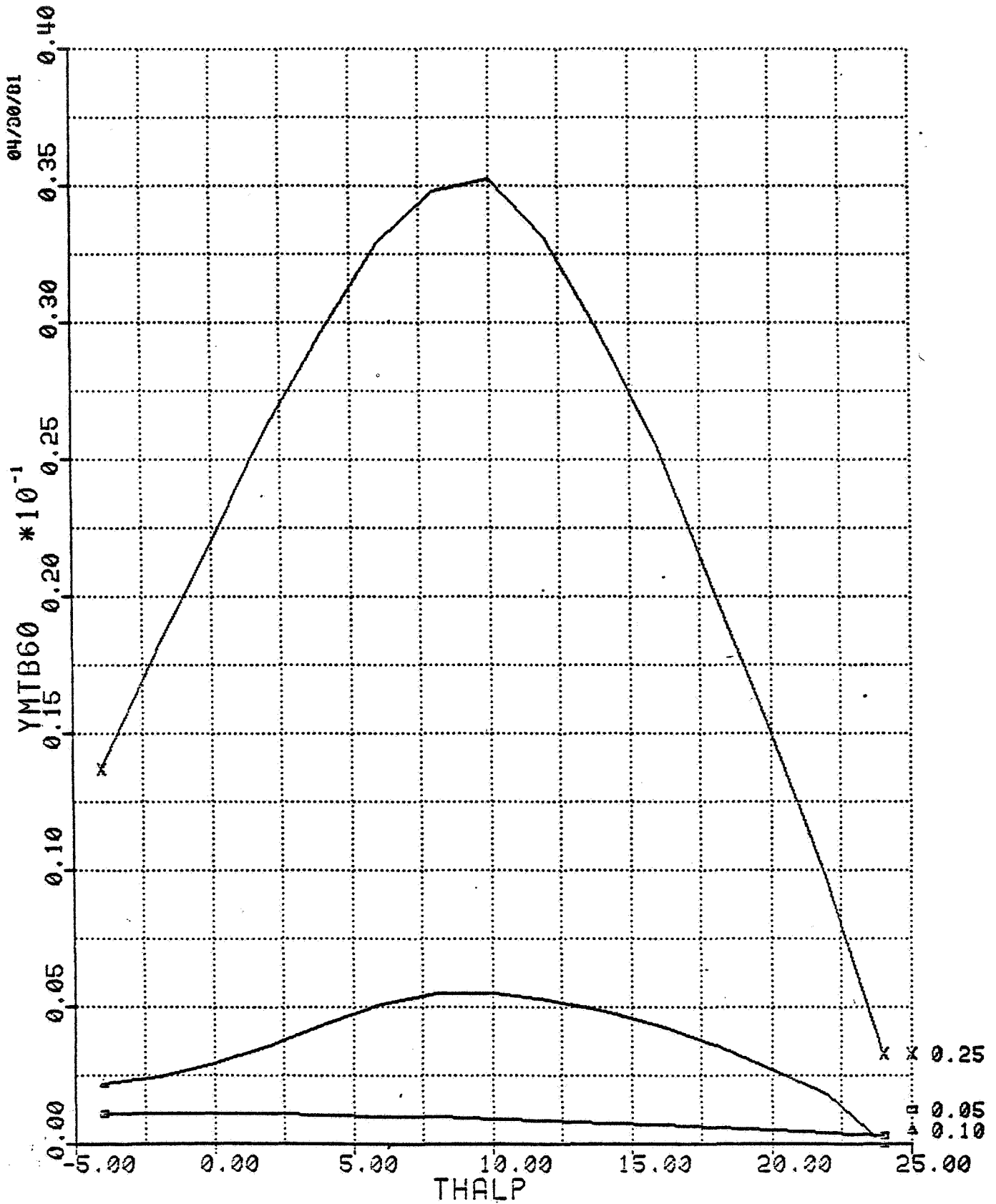
YMPE81 VS YMPHIE
FOR VARYING HP
VET = 0.10



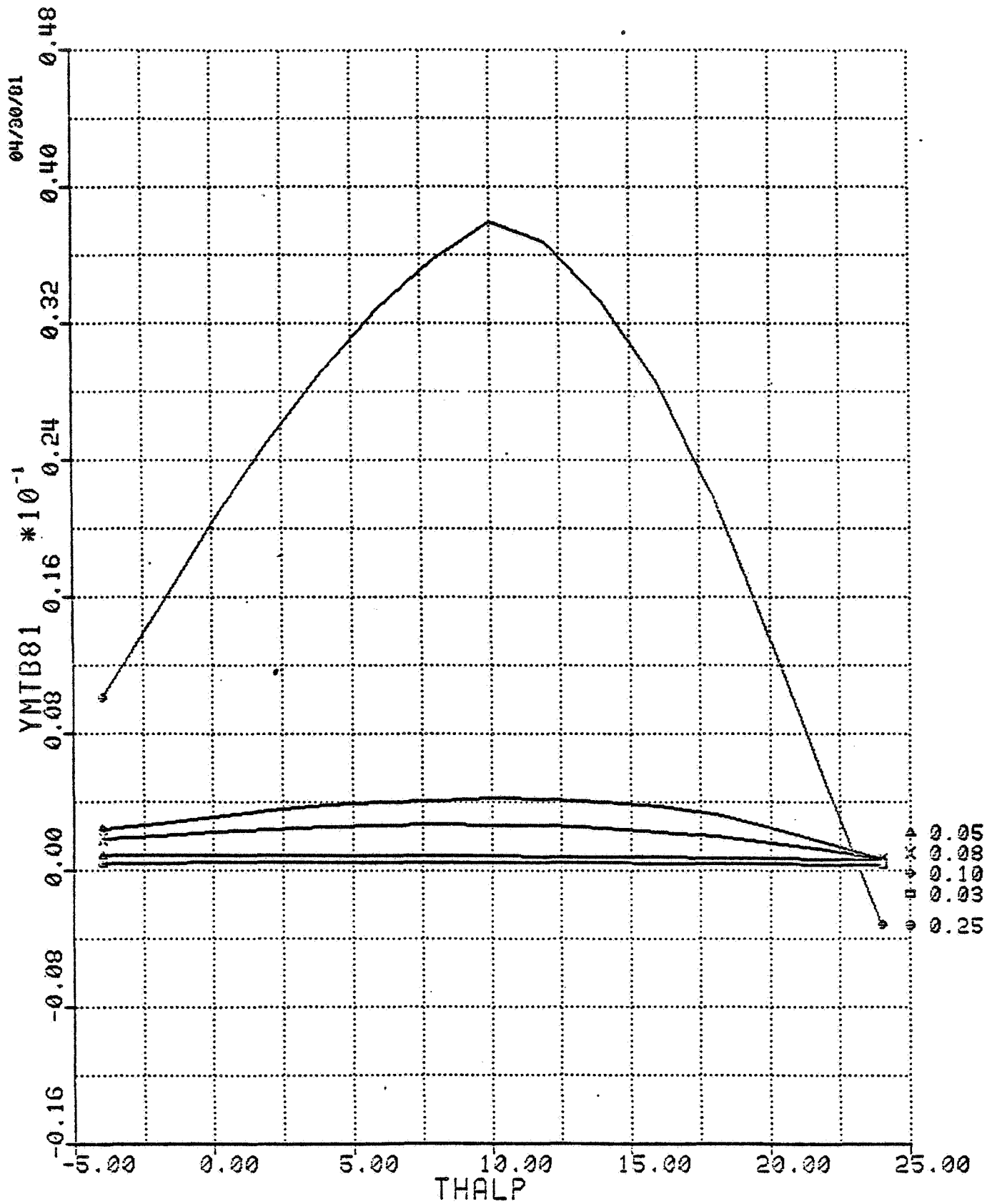
YMTB00 VS THALP
FOR VARYING VEQ



YMTB60 VS THALP
FOR VARYING VEQ



YMTB81 VS THALP
FOR VARYING VEQ



INDEX TO HIGH SPEED AERODYNAMIC PLOTS

DEPENDENT VARIABLE	DEFINITION	DATA TABLE NAME	PAGE
CDBAS1	Baseline drag coefficient as a function of alpha for high baseline lift coefficient	HCD1T	C-225
CDBAS2	Baseline drag coefficient as a function of Mach number and lift coefficient	HCD2T	C-226
CDDR	Drag coefficient due to rudder as a function of alpha and Mach number	HCDDRT	C-227
CLBAS1	Baseline lift coefficient as a function of alpha for high alpha	HCL1T	C-228
CLBAS2	Baseline lift coefficient as a function of alpha and Mach number	HCL2T	C-229
CMALPDT	Pitching moment coefficient due to alpha dot as a function of Mach number	HCMADT	C-230
CMBAS1	Baseline pitching moment coefficient as a function of alpha for high alpha	HCMB1T	C-231
CMBAS2	Baseline pitching moment coefficient as a function of Mach number and alpha	HCMB2T	C-232
CMQT	Pitching moment coefficient due to pitch rate as a function of Mach number	HCMQT	C-233
CNB	Yawing moment coefficient due to sideslip angle as a function of Mach number and alpha	HCNBHT	C-234
CNDAL	Increment of yawing moment coefficient due to aileron as a function of Mach number, alpha, and aileron deflection	HCNDAT	C-235
CNDR	Yawing moment coefficient due to rudder deflection as a function of Mach number and alpha	HCNDRT	C-243
CNP	Yawing moment coefficient due to roll rate as a function of Mach number and alpha	HCNPT	C-244

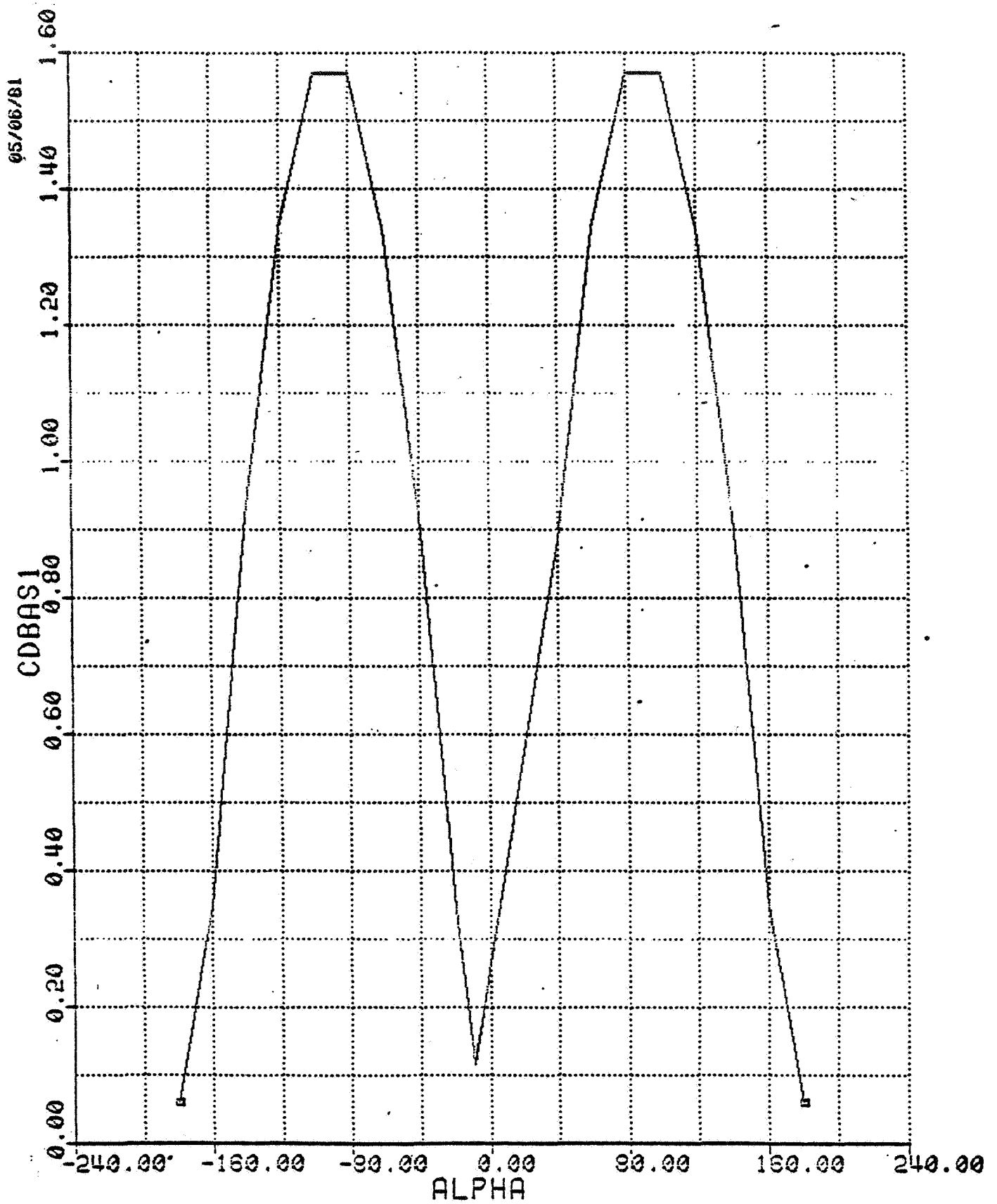
INDEX TO HIGH SPEED AERODYNAMIC PLOTS (Cont'd)

DEPENDENT VARIABLE	DEFINITION	DATA TABLE NAME	PAGE
CNR	Yawing moment coefficient due to yaw rate as a function of Mach number and alpha	HCNRT	C-245
DCDAL	Increment of drag coefficient due to aileron as a function of aileron deflection, Mach number, and alpha	HCDAILT	C-246
DCDFL	Increment of drag coefficient due to flap as a function of alpha, flap deflection, and Mach number	HCDFT	C-250
DCDSTAB	Increment of drag coefficient due to stabilator as a function of alpha, stabilator position, and Mach number	HCDSTT	C-256
DCLAL	Increment of lift coefficient due to aileron as a function of aileron deflection and Mach number	HCLAILT	C-260
DCLFL	Increment of lift coefficient due to flap as a function of alpha, flap deflection, and Mach number	HCLFT	C-261
DCMFL	Increment of pitching moment coefficient due to flap as a function of alpha, flap deflection, and Mach number	HCMFT	C-269
DCMST	Increment of pitching moment coefficient due to stabilator as a function of stabilator position, alpha, and Mach number	HCMSTT	C-277
DCNPOW1	Increment of normal force coefficient due to power effects as a function of THETAJ, VEQ, and alpha	CNPOWT	C-285
HCLDAL	Increment of rolling moment coefficient due to aileron as a function of Mach number, alpha, and aileron deflection	HCLLDAT	C-293

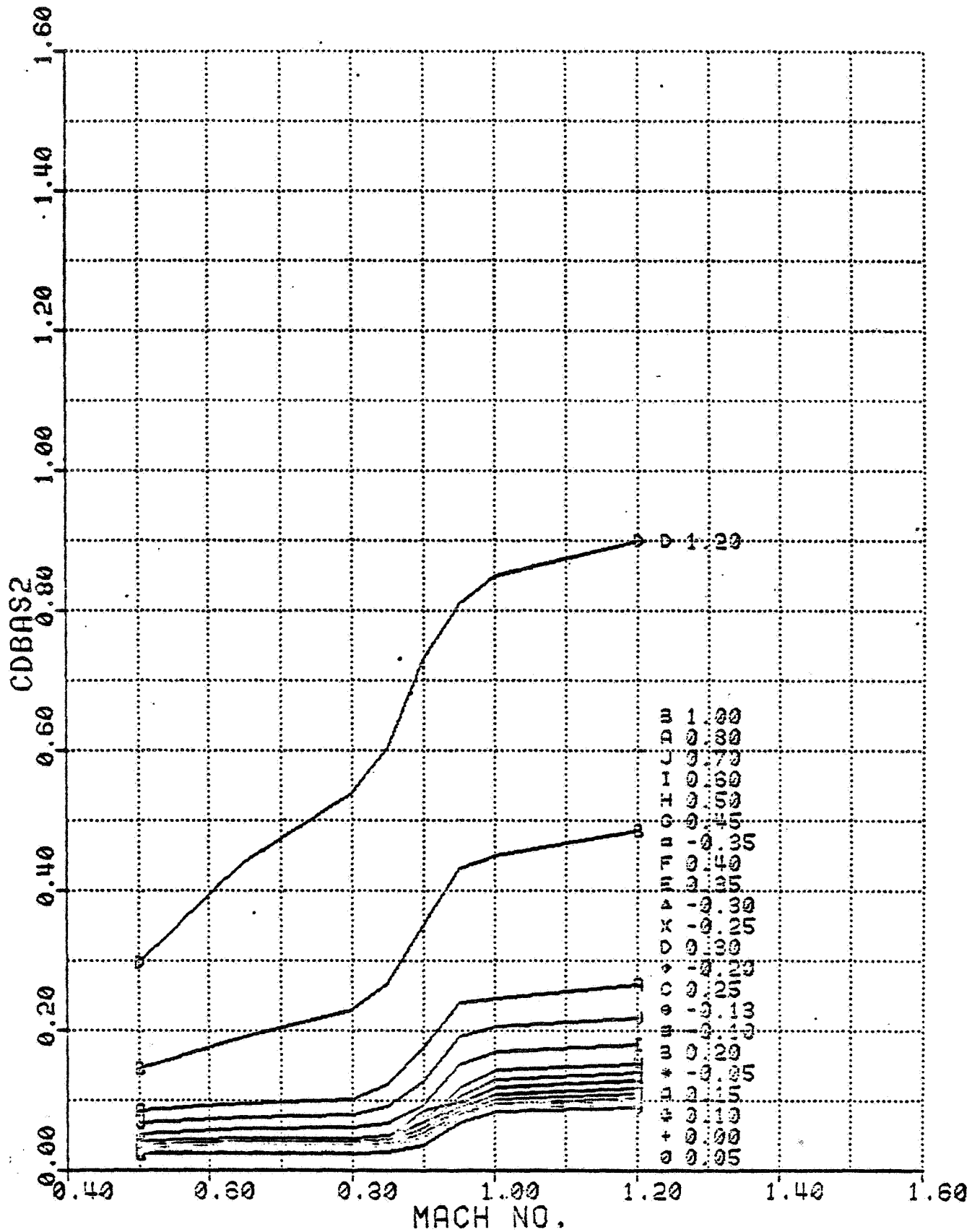
INDEX TO HIGH SPEED AERODYNAMIC PLOTS (Cont'd)

DEPENDENT VARIABLE	DEFINITION	DATA TABLE NAME	PAGE
HCLLB	Rolling moment coefficient due to sideslip angle as a function of Mach number and alpha	HCLBT	C-301
HCLLBF	Rolling moment coefficient due to flap as a function of Mach number and alpha	HCLBFT	C-302
HCLLDR	Rolling moment coefficient due to rudder as a function of Mach number and alpha	HCLLDRT	C-303
HCLLP	Rolling moment coefficient due to roll rate as a function of Mach number and alpha	HCLLPT	C-304
HCLLR	Rolling moment coefficient due to yaw rate as a function of Mach number and alpha	HCLLRT	C-305
HCMDAL	Increment of pitching moment coefficient due to aileron as a function of aileron deflection and alpha	HCMDAT	C-306
HCMP1	Increment of pitching moment coefficient due to power effects as a function of alpha, VEQ, and THETAJ	HCMPOWT	C-307
HCYB	Side force coefficient due to sideslip angle and flap as a function of Mach number, alpha, and flap deflection.	HCYBT	C-319
HCYDAL	Increment of side force coefficient due to aileron as a function of aileron deflection and alpha	HCYDAT	C-320
HCYDR	Side force coefficient due to rudder as a function of Mach number and alpha	HCYDRT	C-321
HCYR	Side force coefficient due to yaw rate as a function of Mach number	HCYRT	C-322

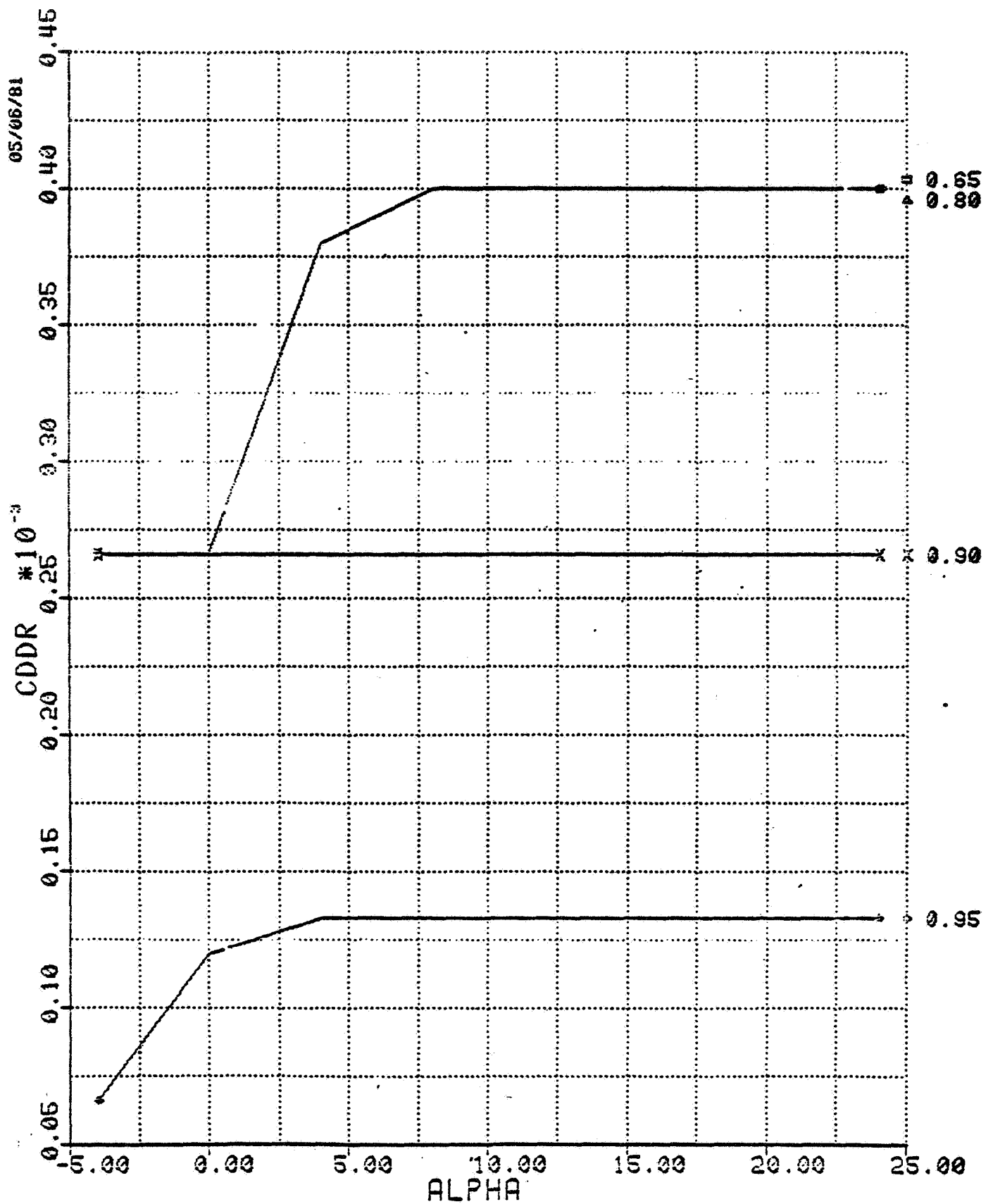
CDBAS1 VS ALPHA



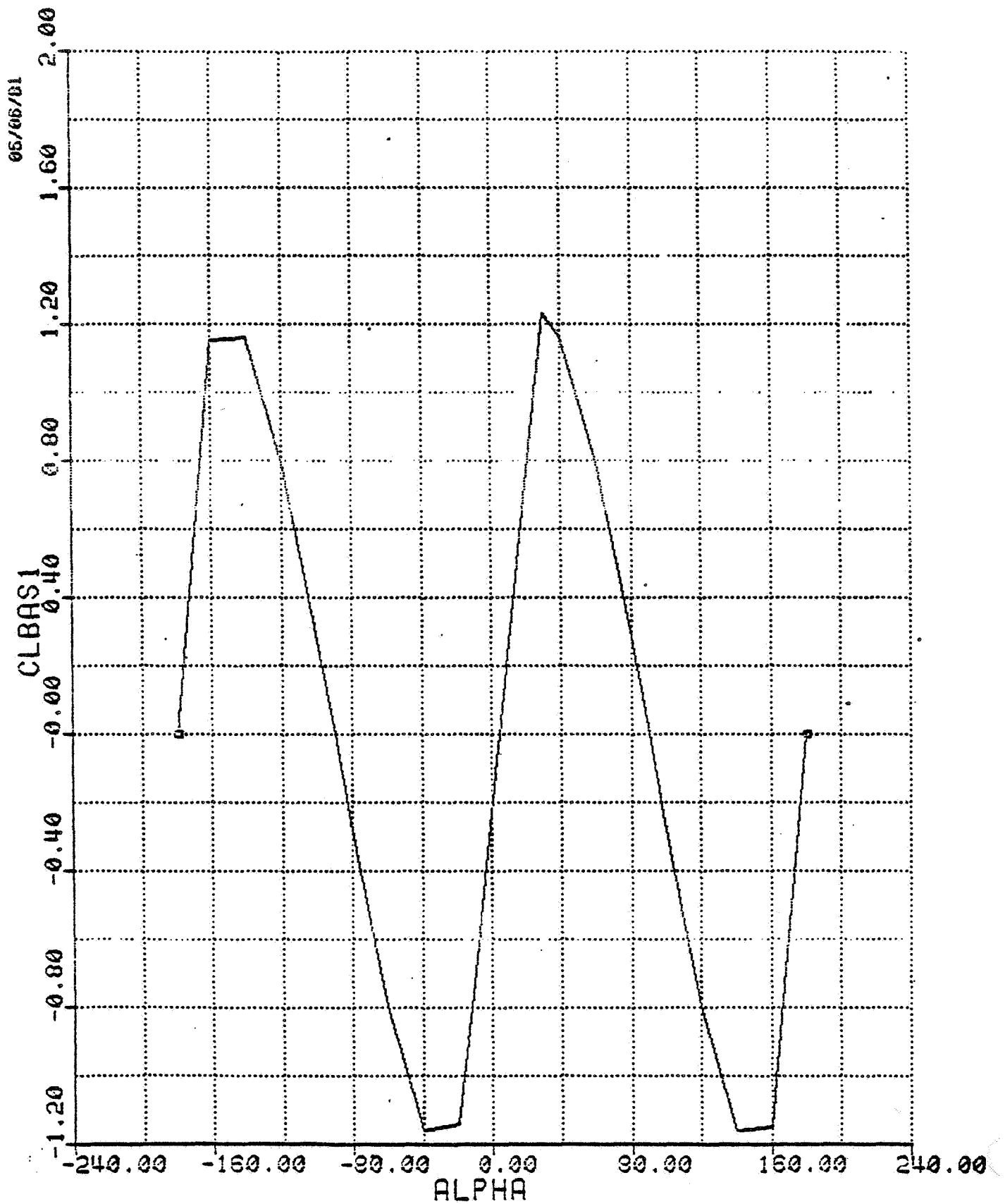
CDBAS2 VS MACH NO.
FOR VARYING CLBASE



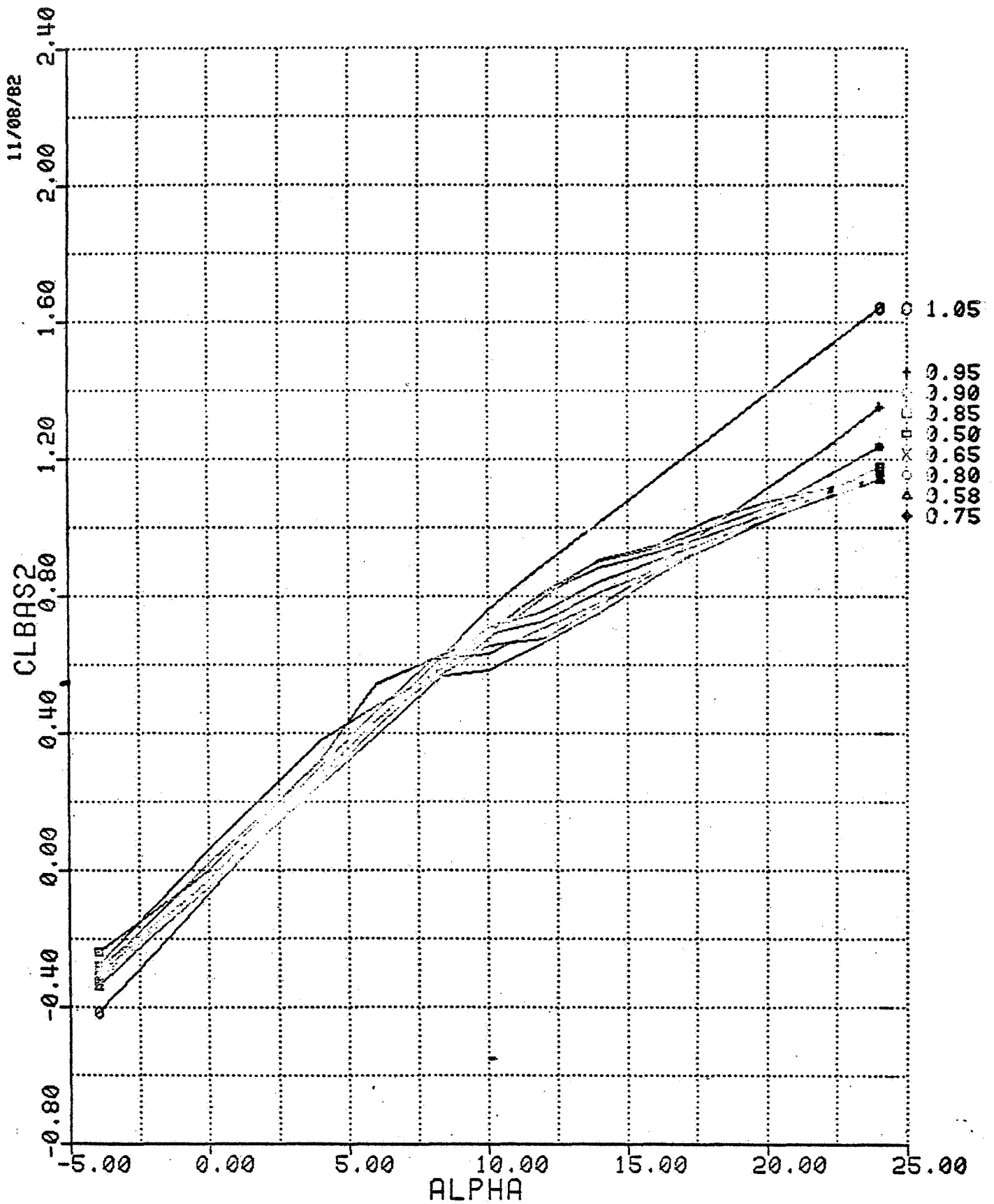
CDDR VS ALPHA
FOR VARYING MACH NO.



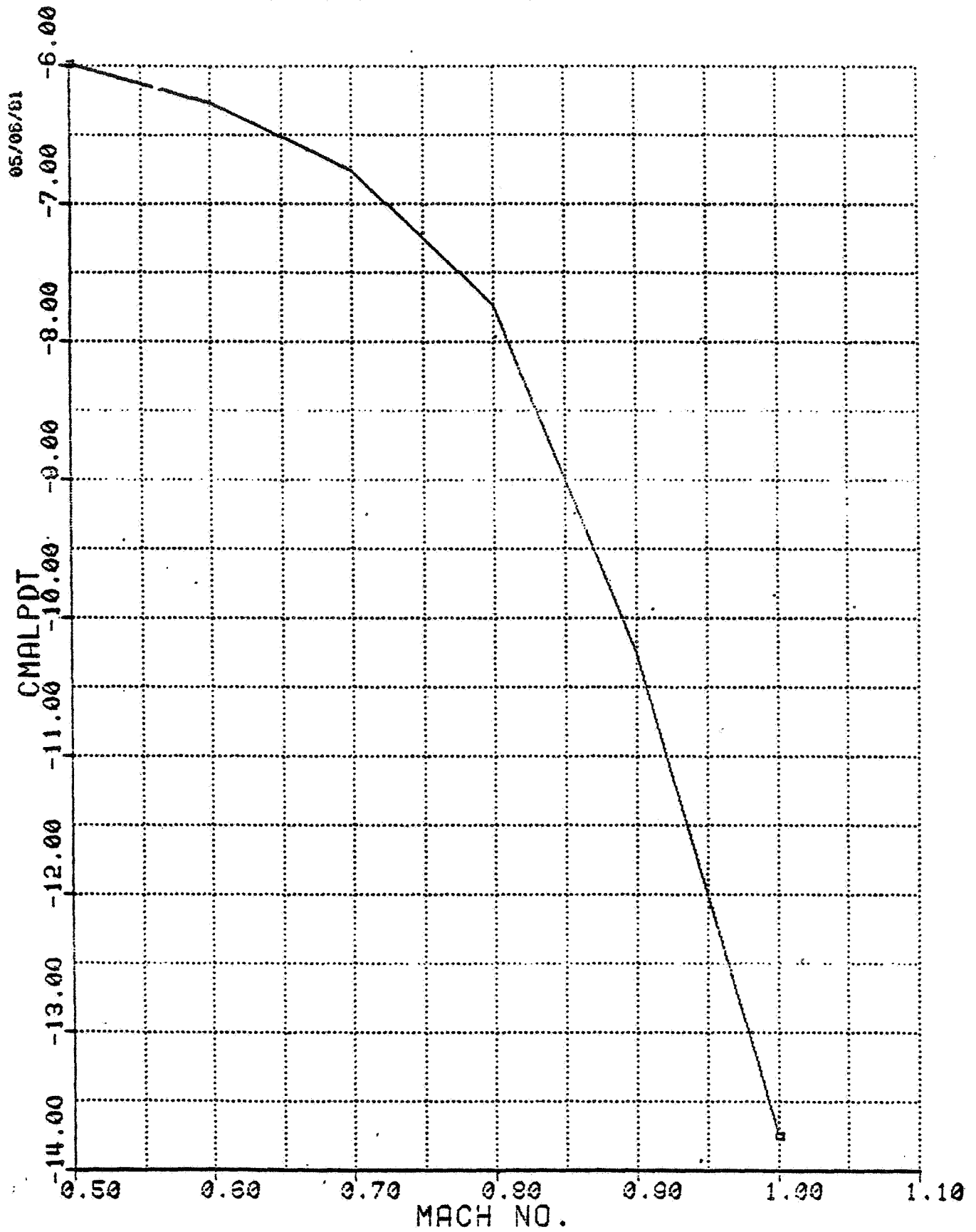
CLBAS1 VS ALPHA



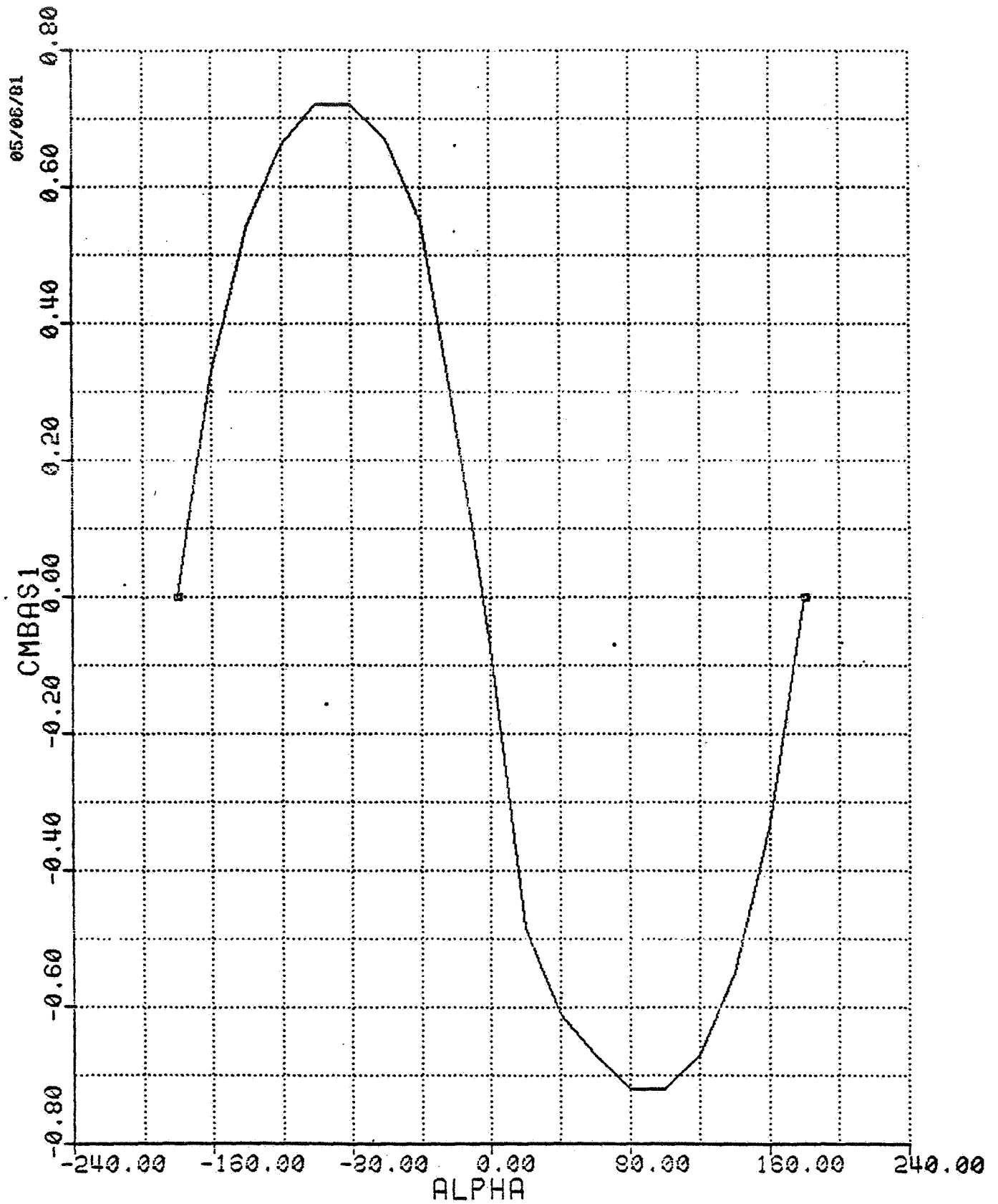
CLBAS2 VS ALPHA
FOR VARYING RMACH



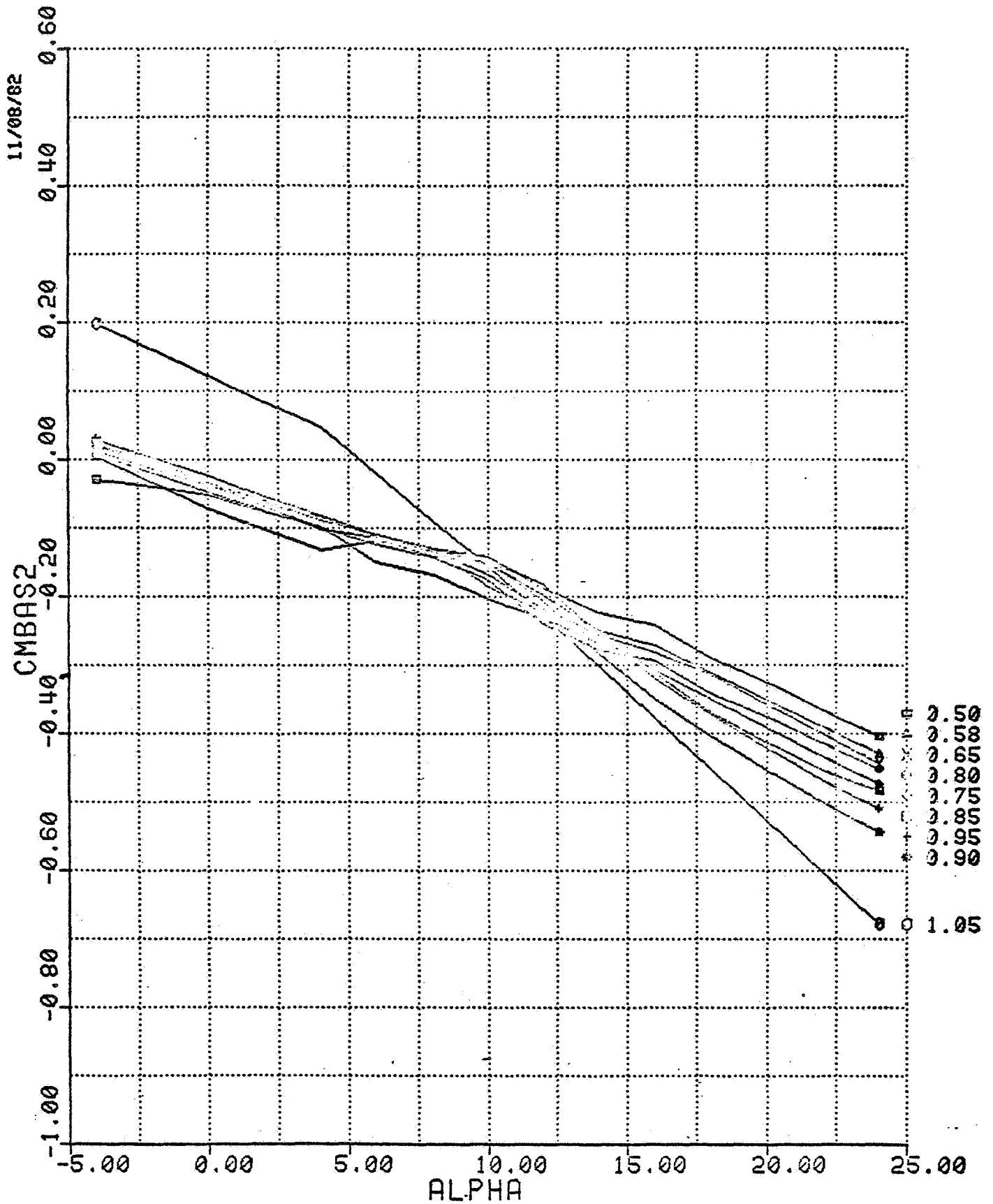
CMALPDT VS MACH NO.



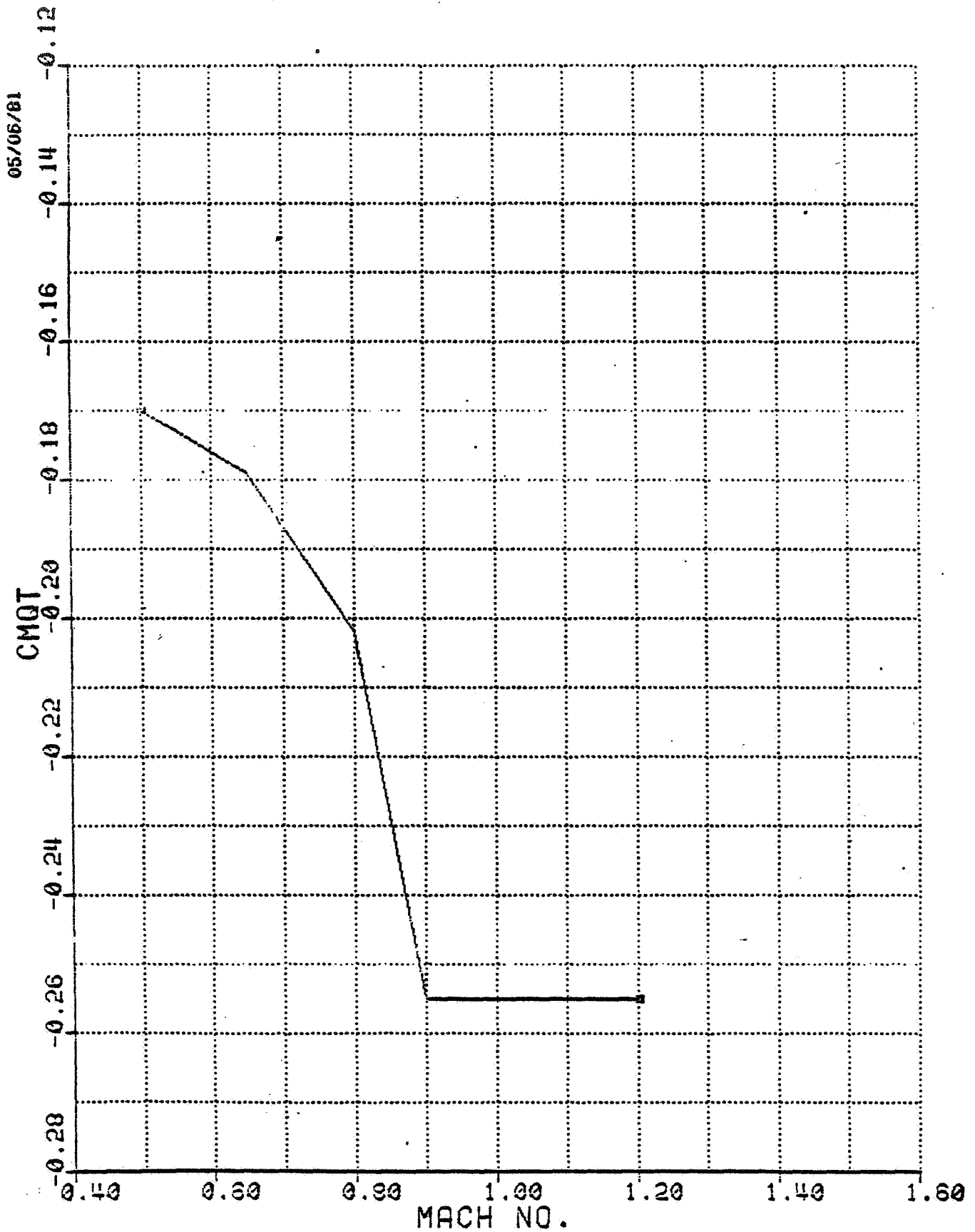
CMBAS1 VS ALPHA



CMBAS2 VS ALPHA
FOR VARYING RMACH

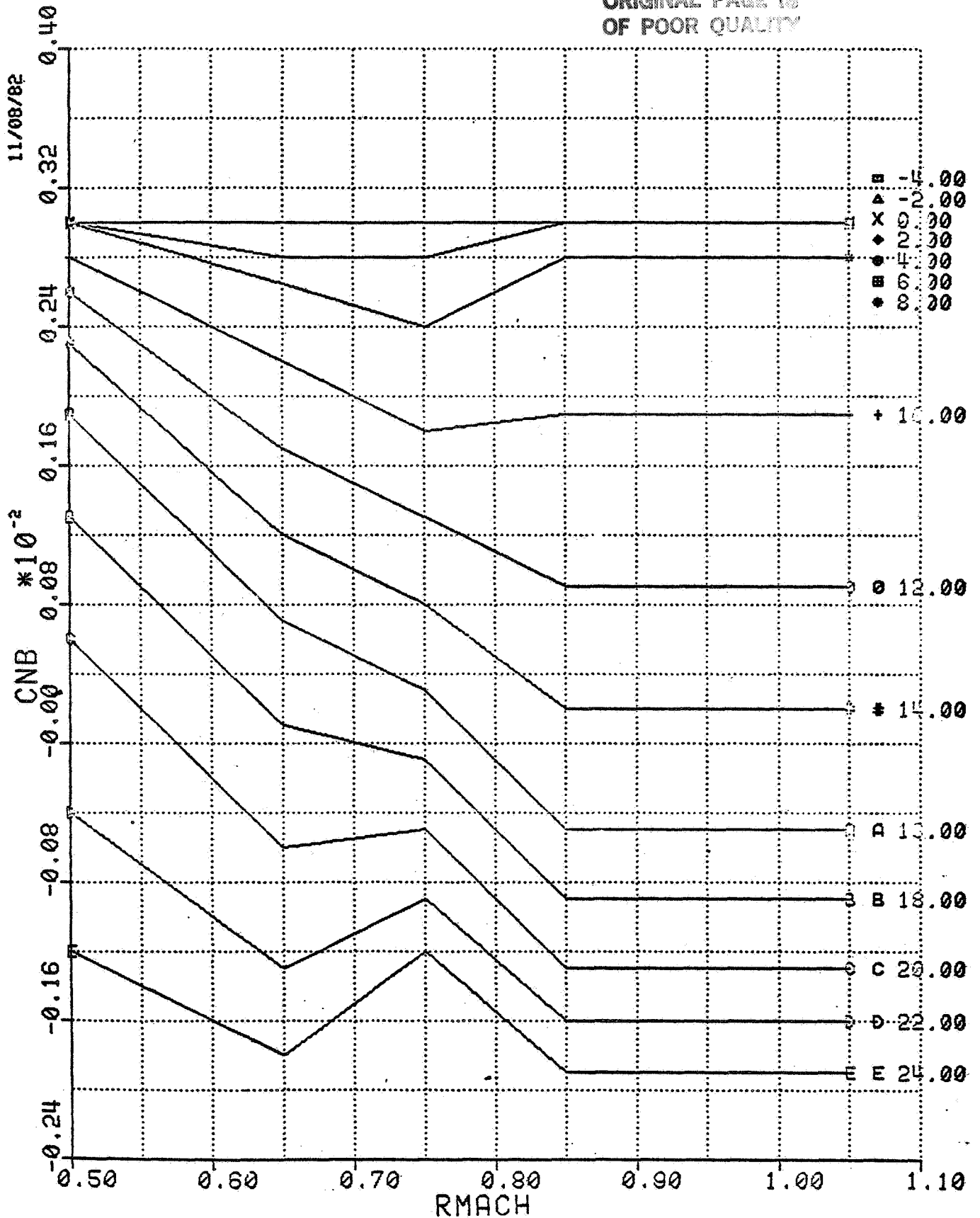


CMQT VS MACH NO.



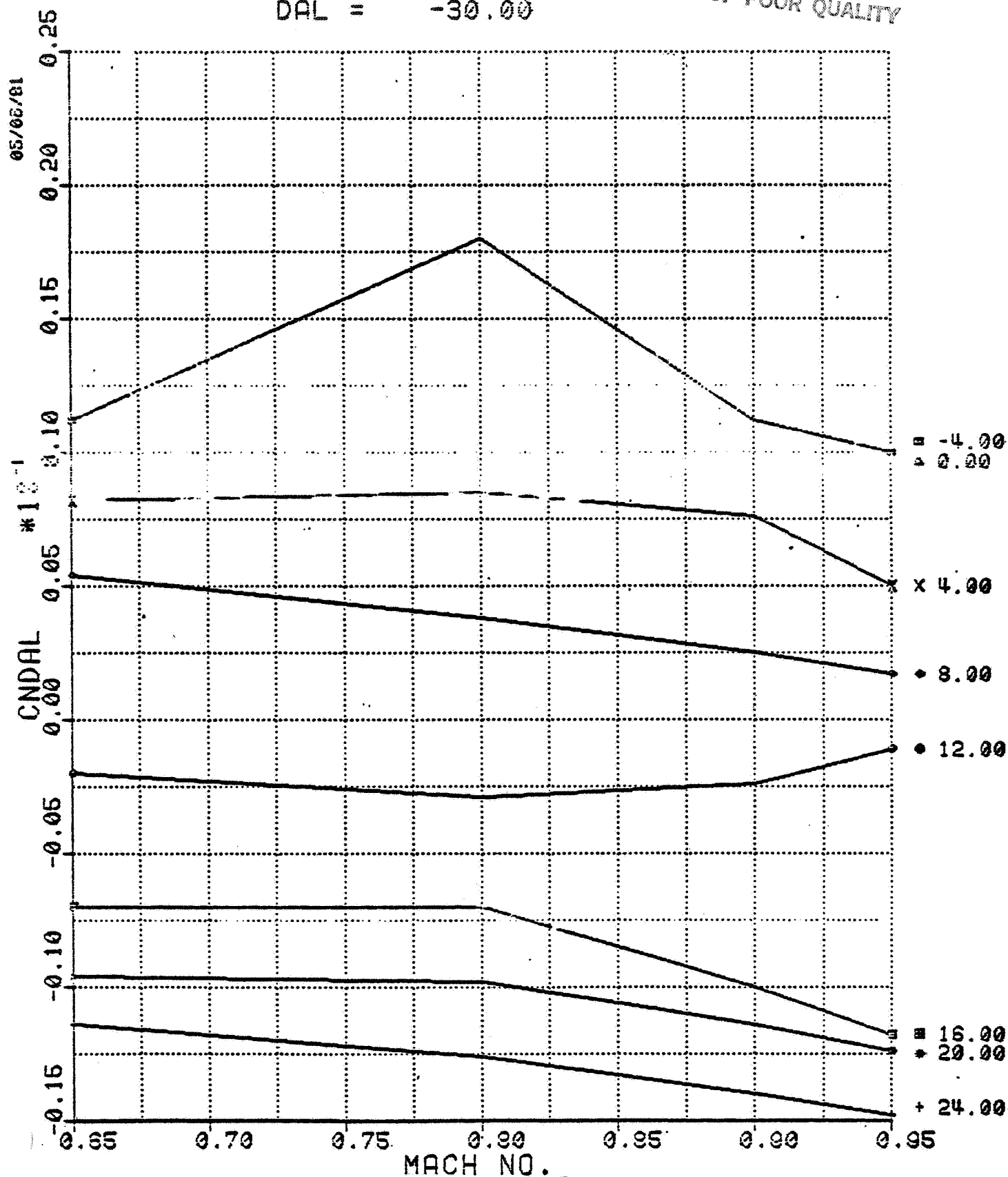
CNB VS RMACH FOR VARYING ALPHA

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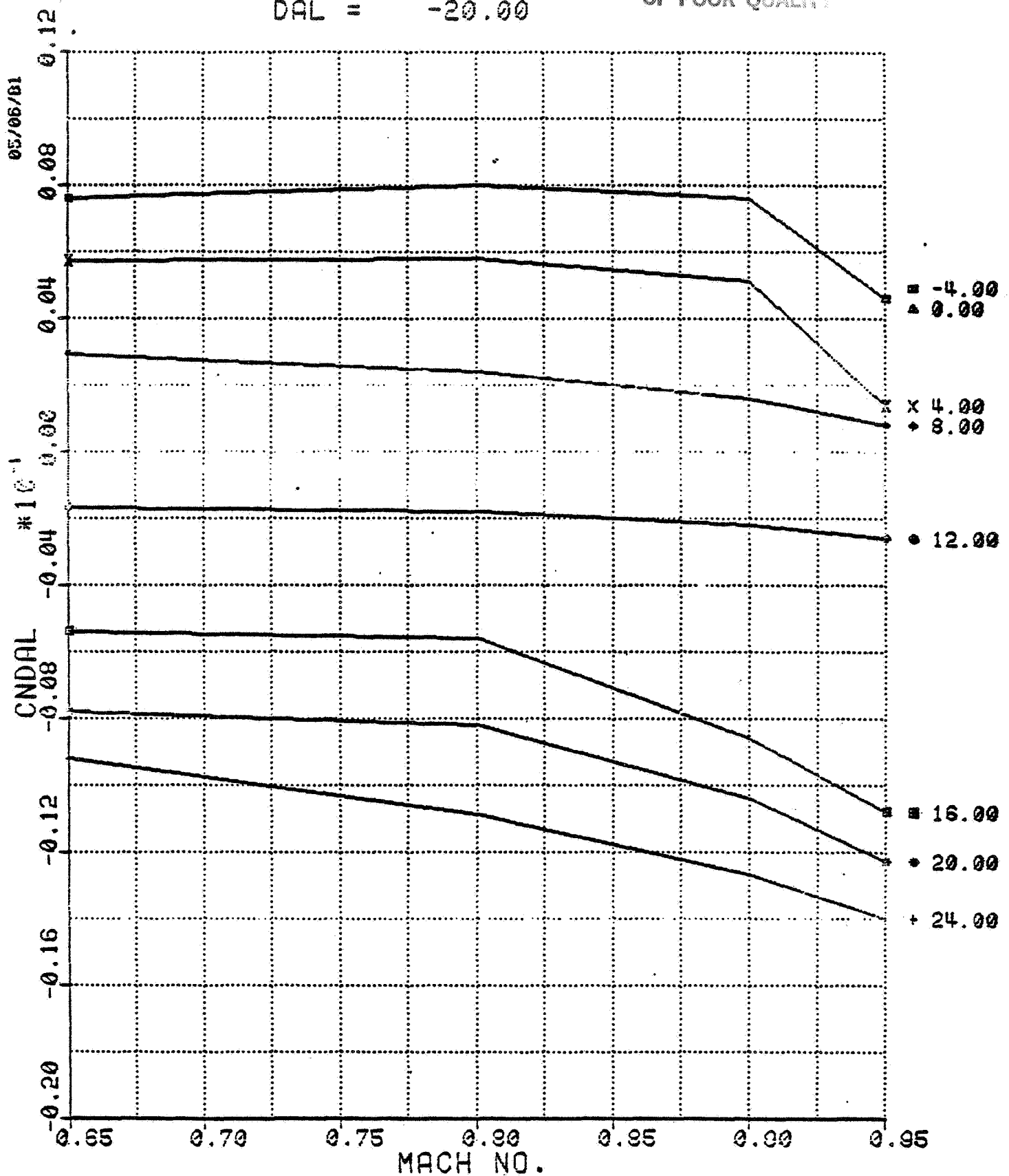
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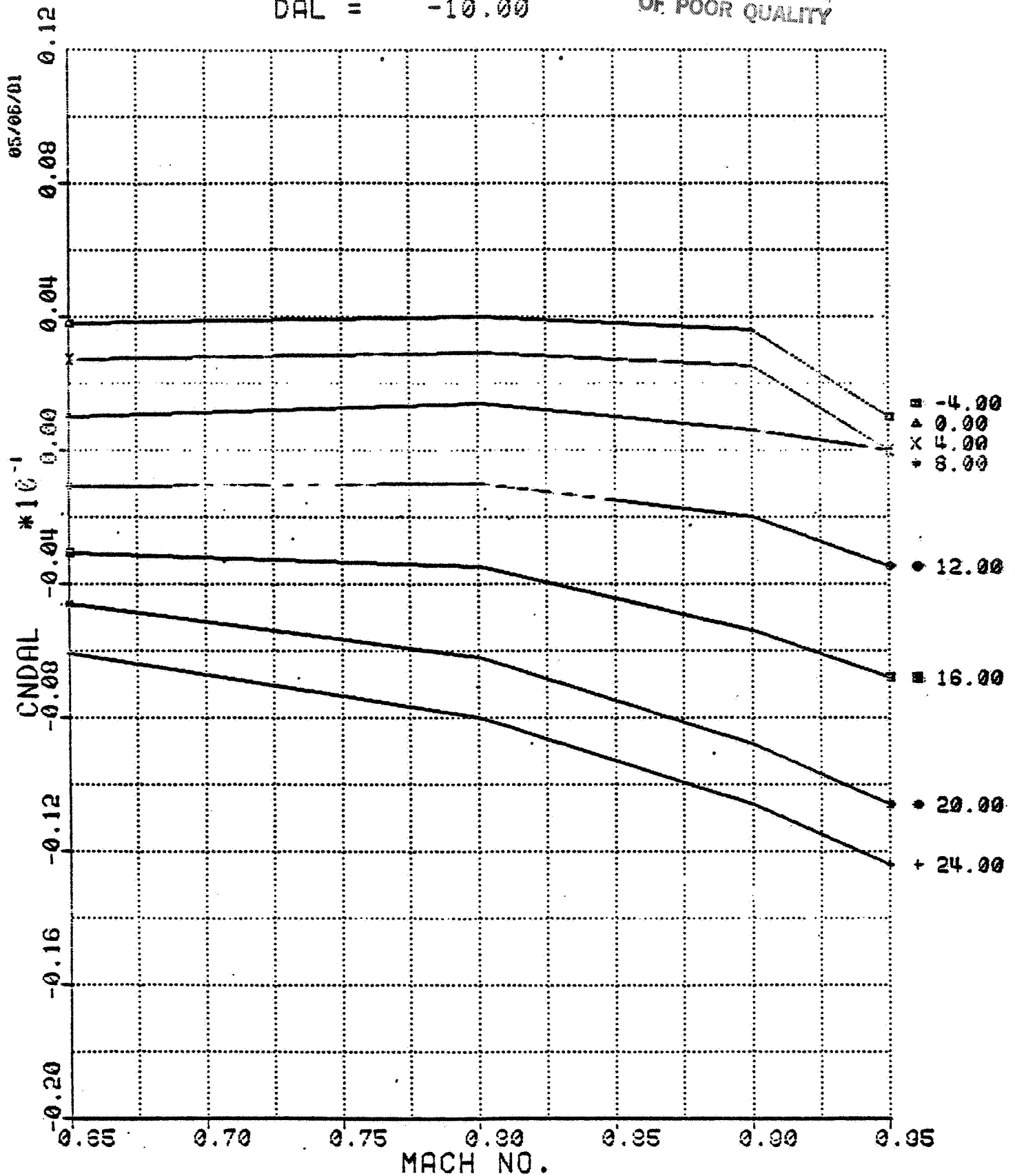
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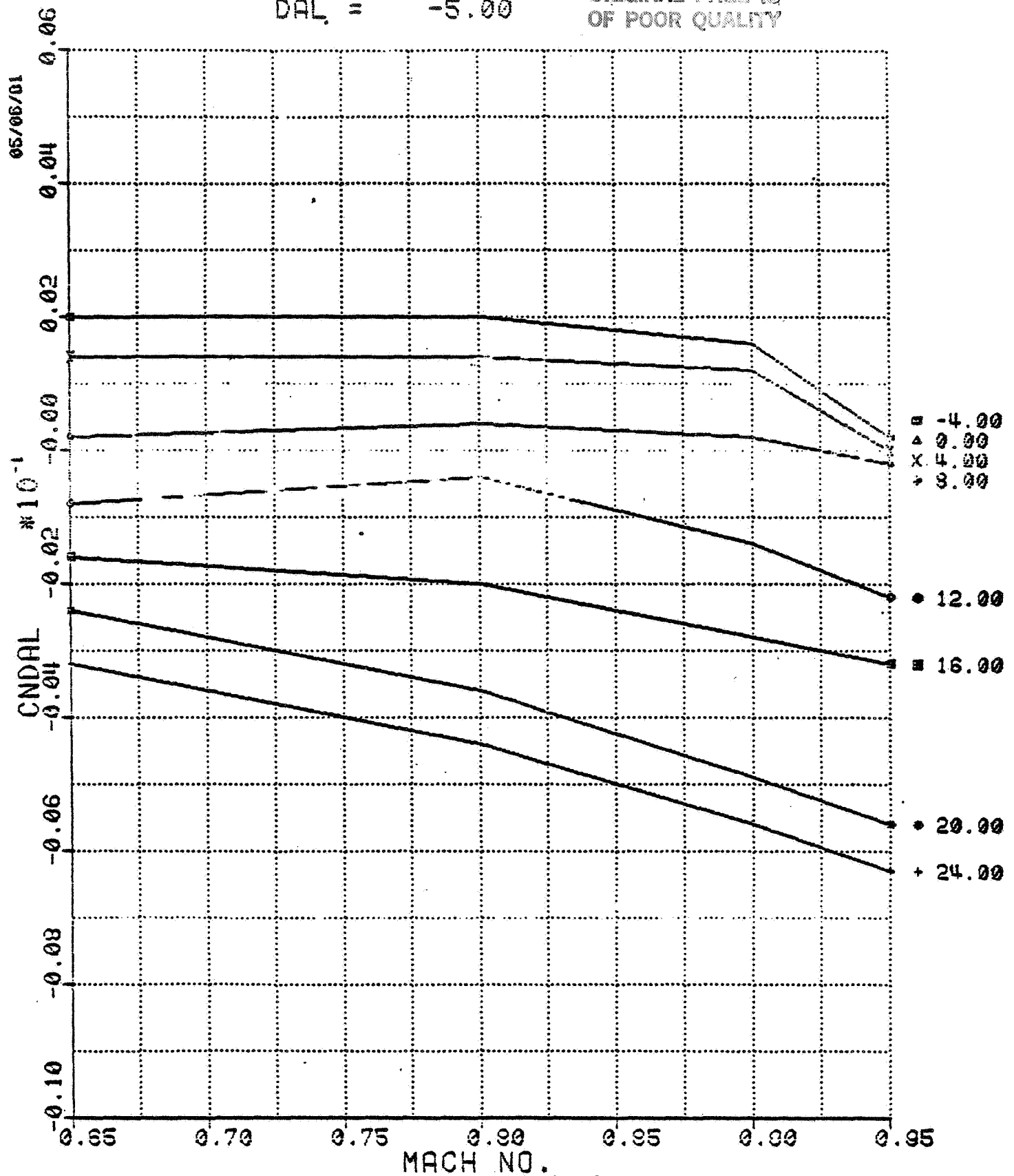
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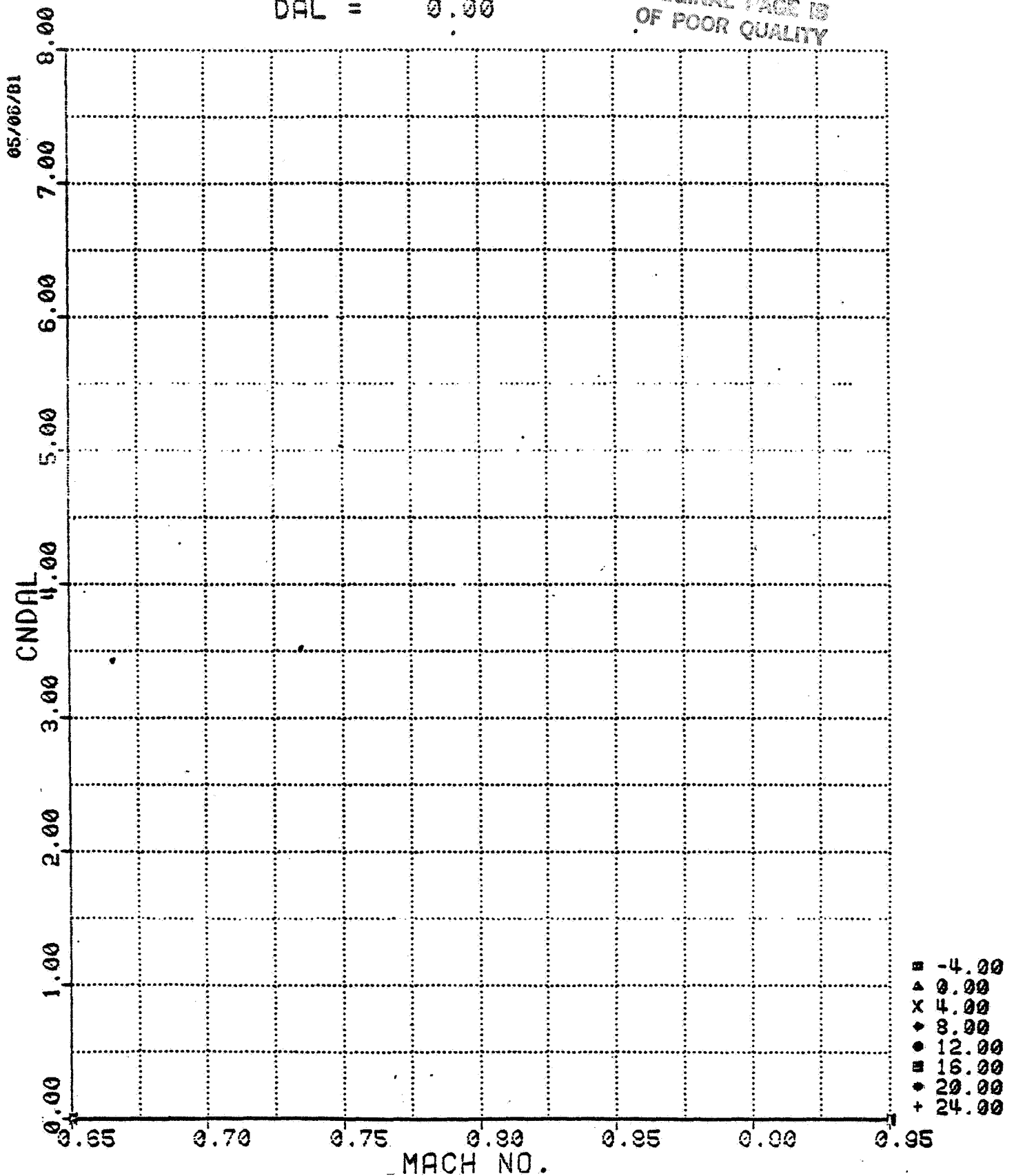
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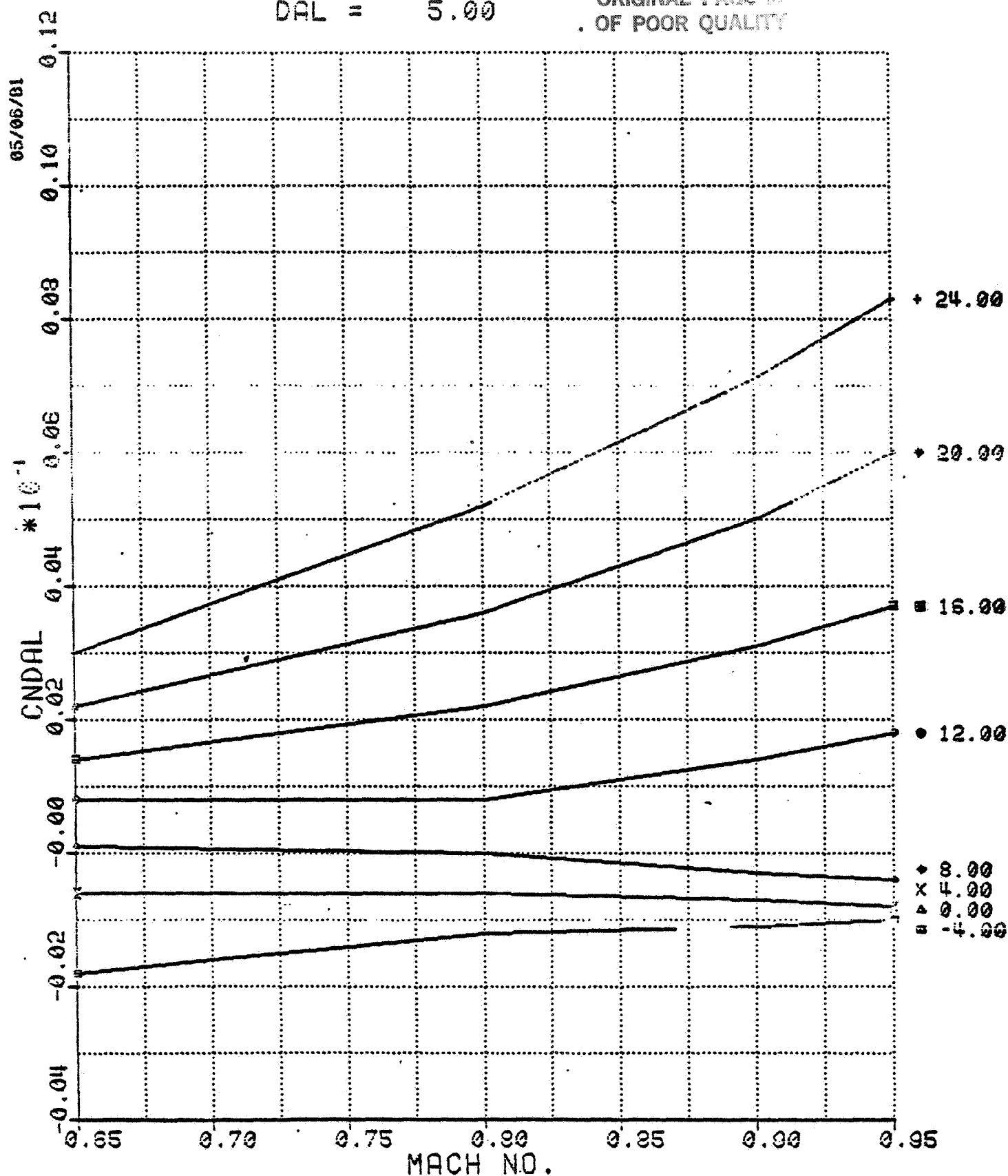
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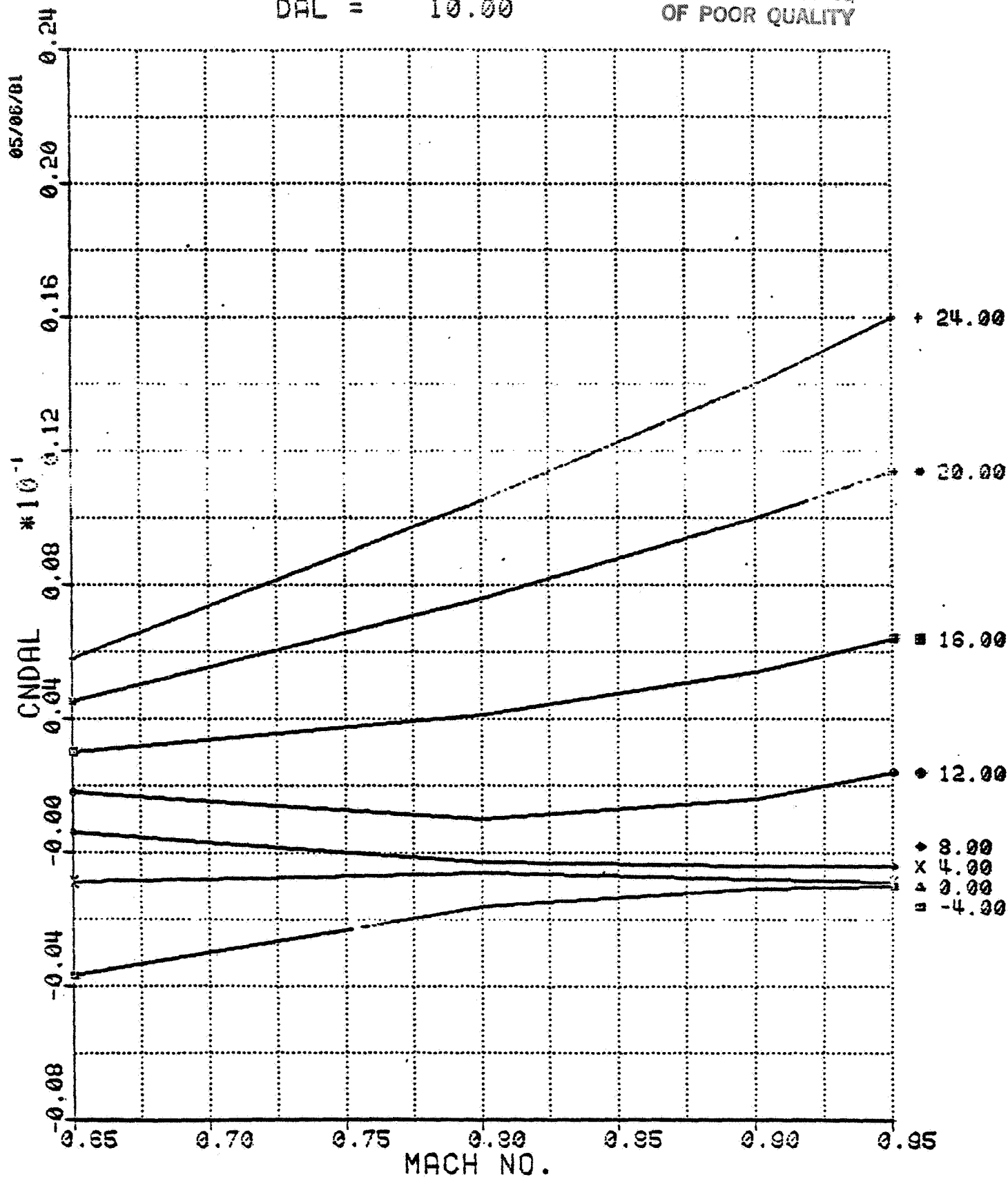
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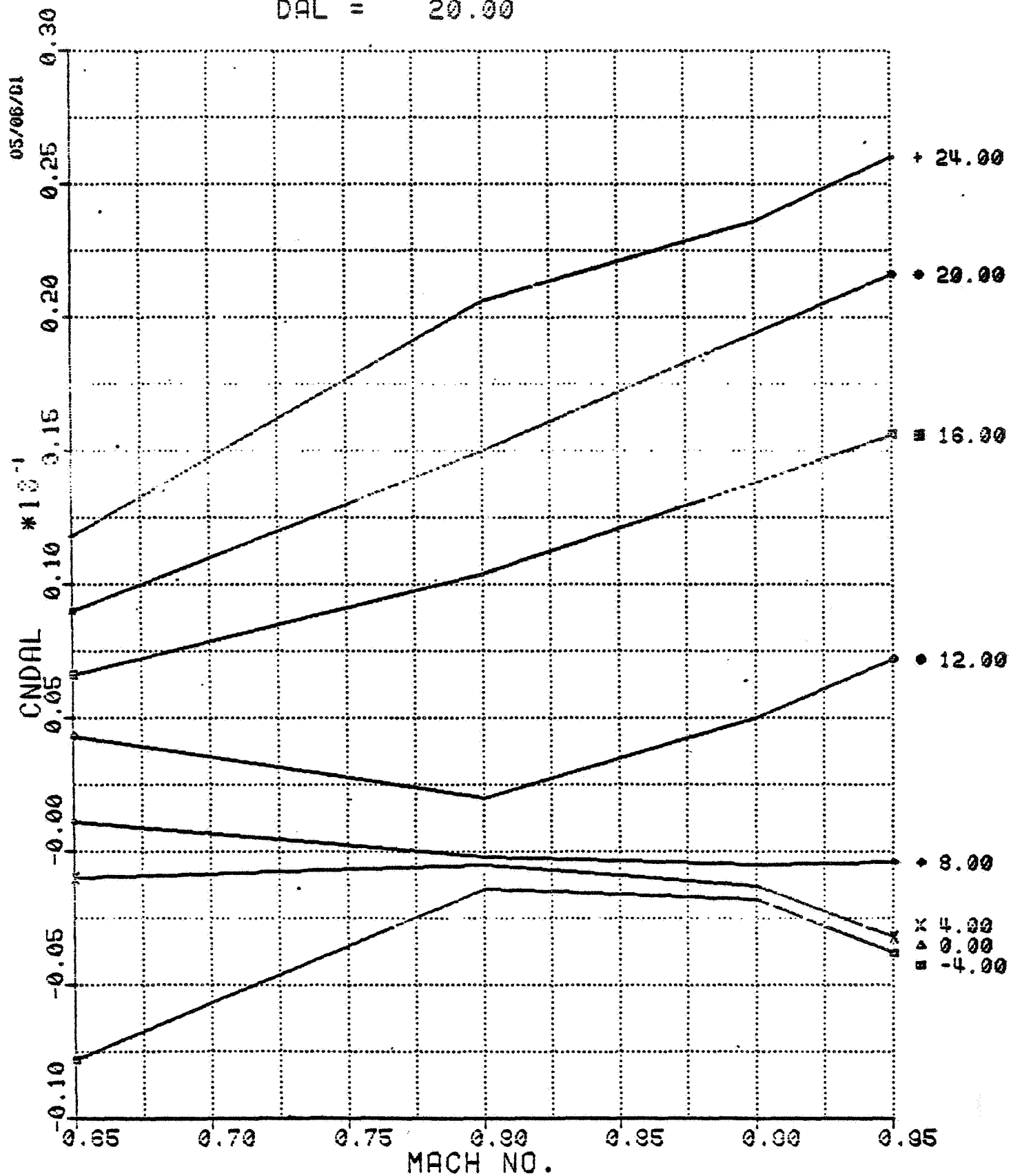


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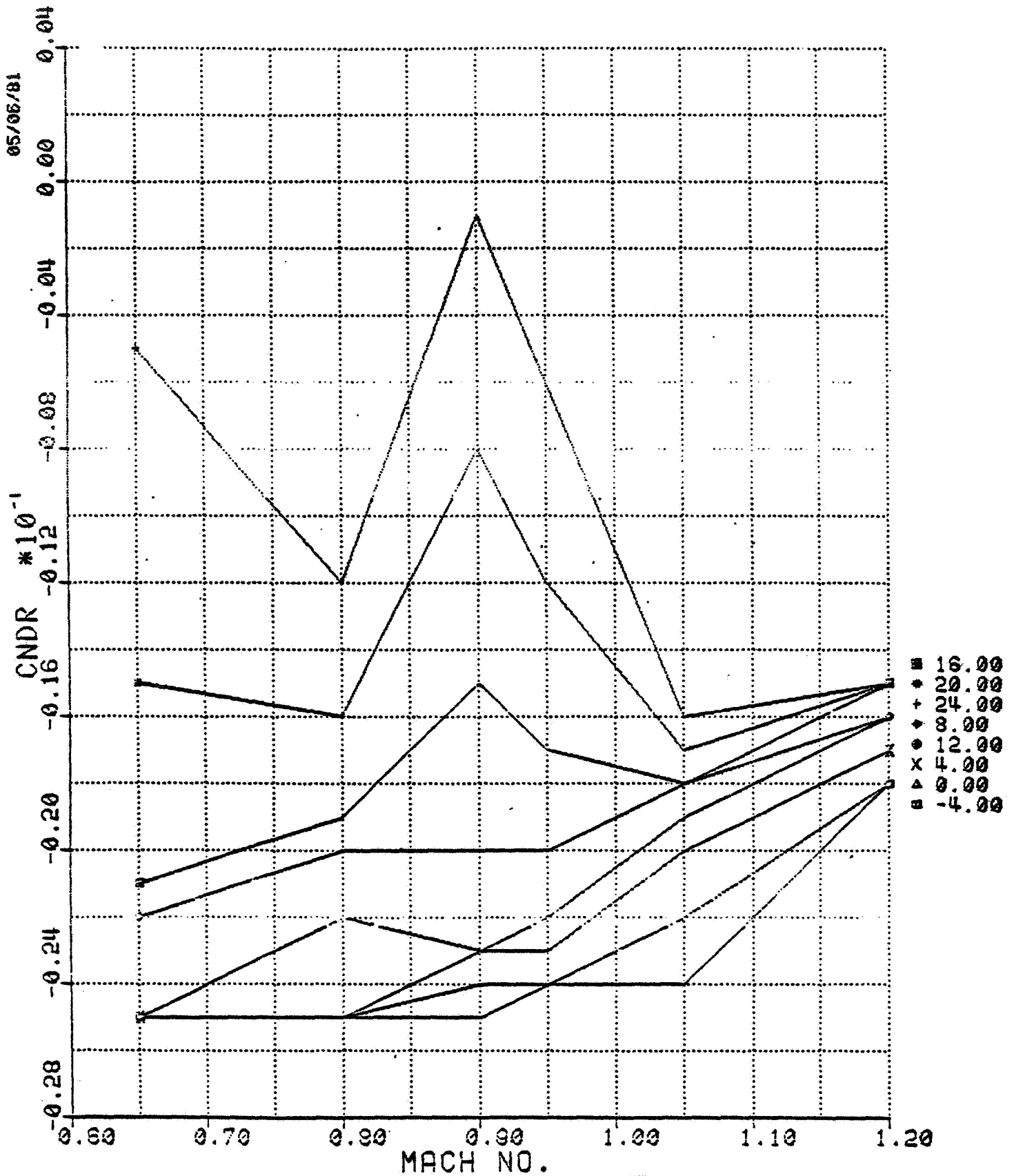
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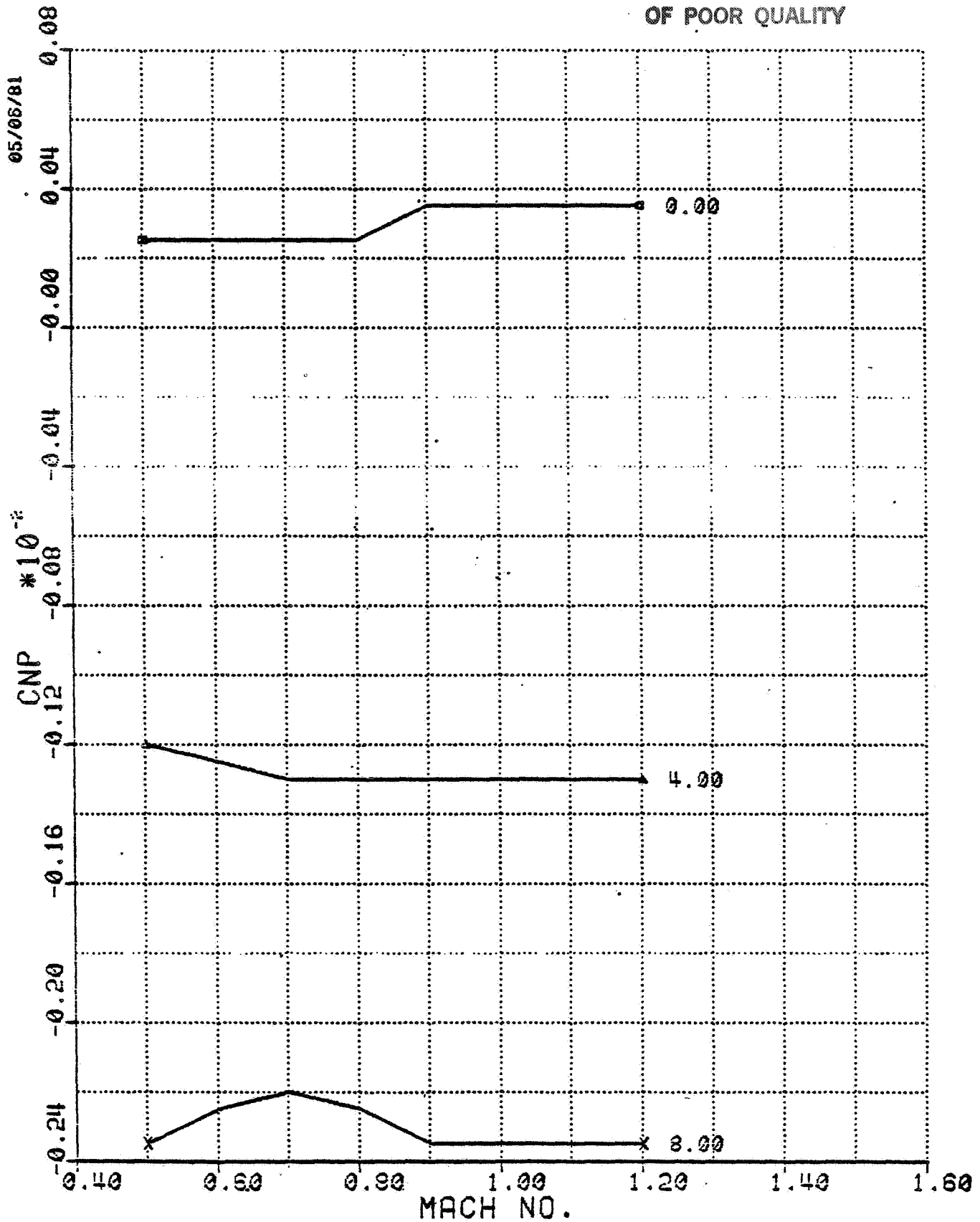


CNDR VS MACH NO.
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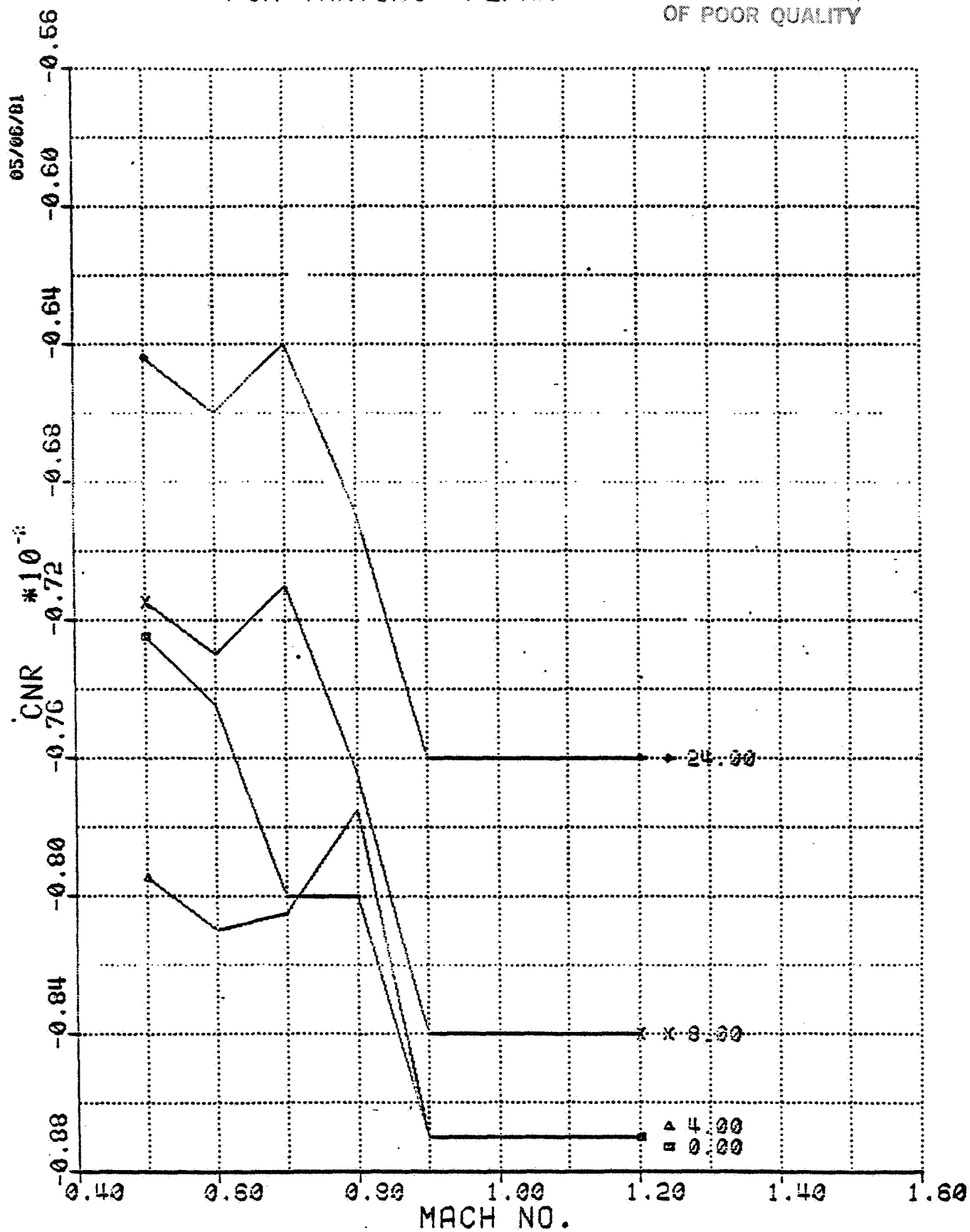
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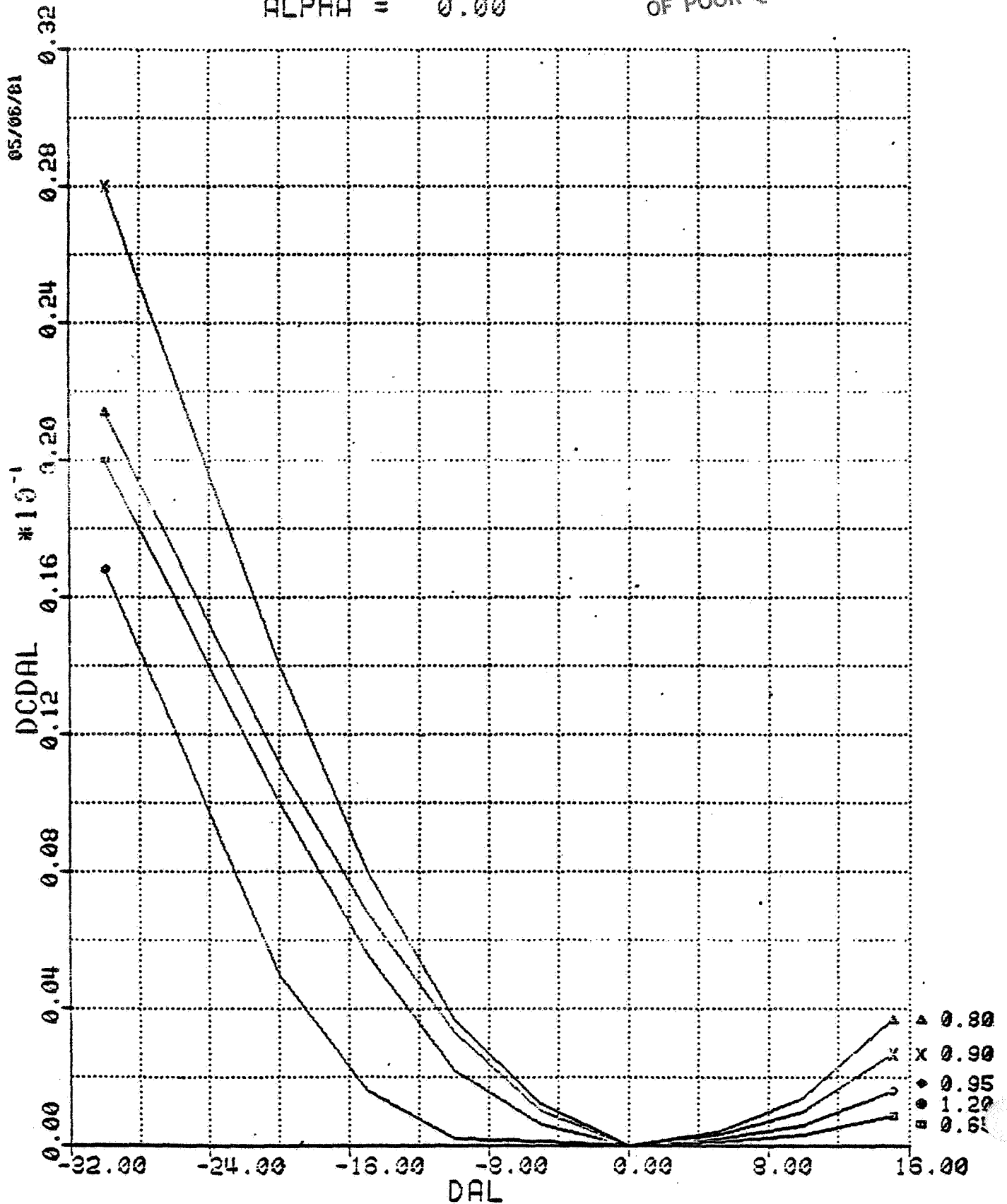
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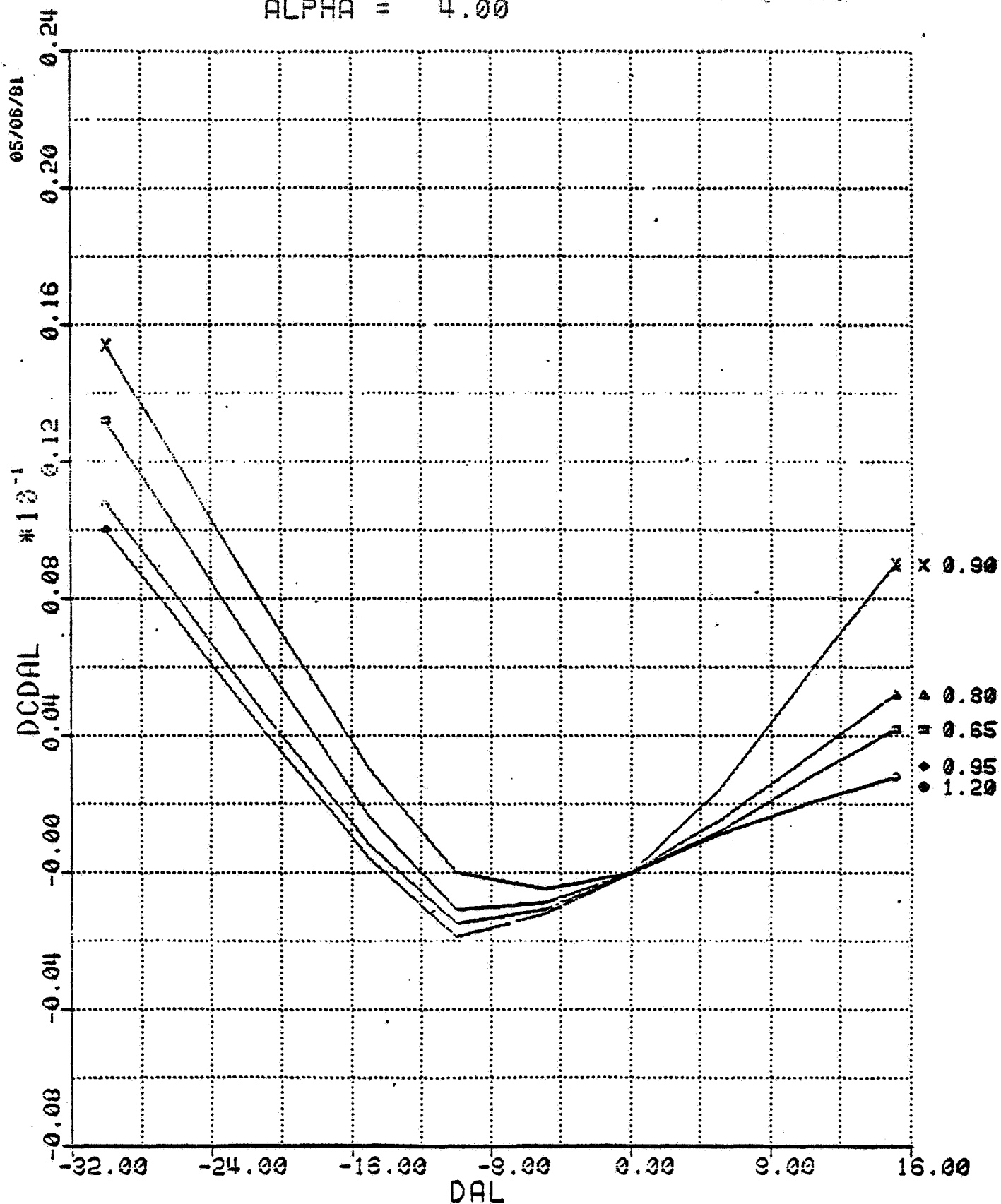
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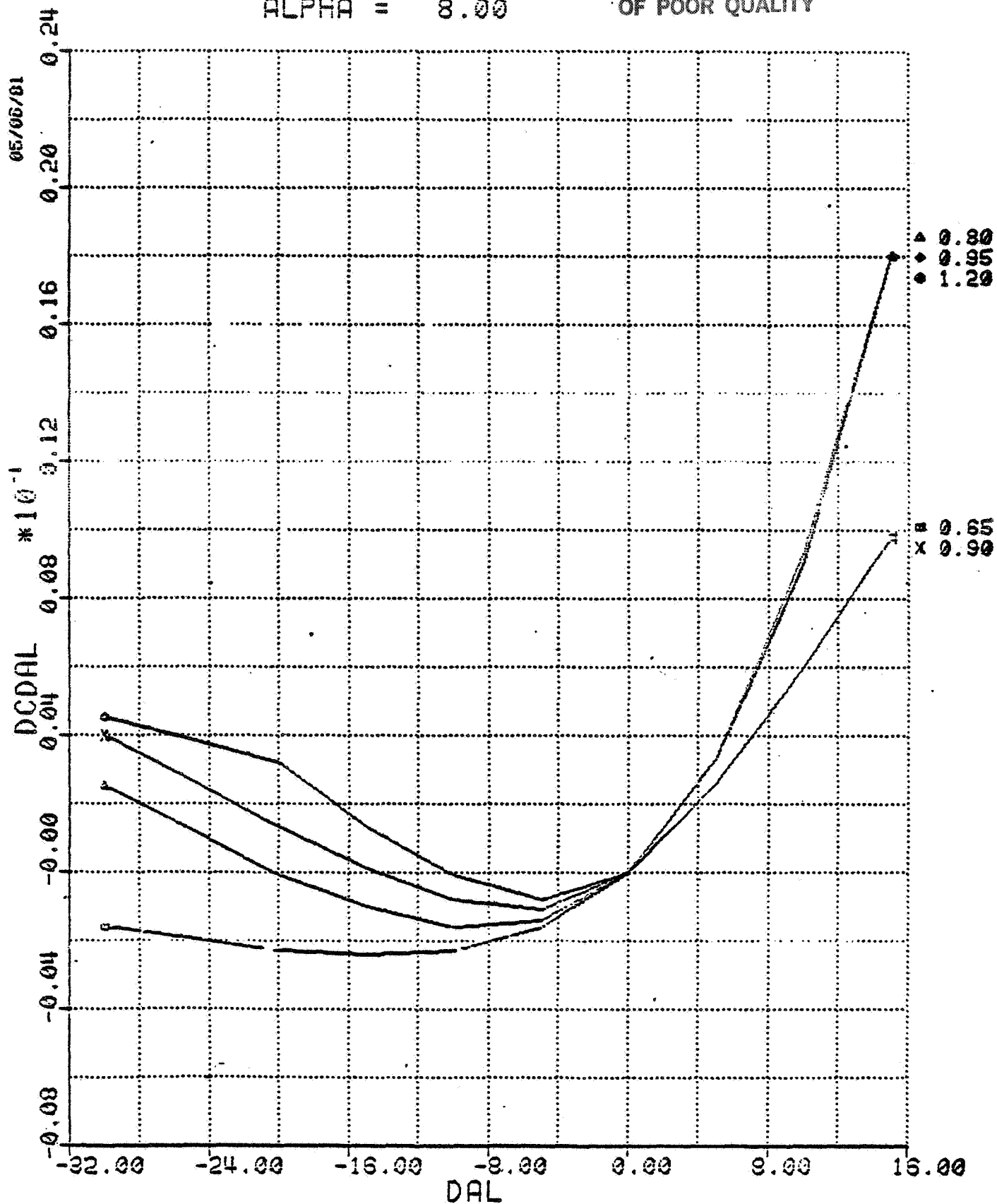
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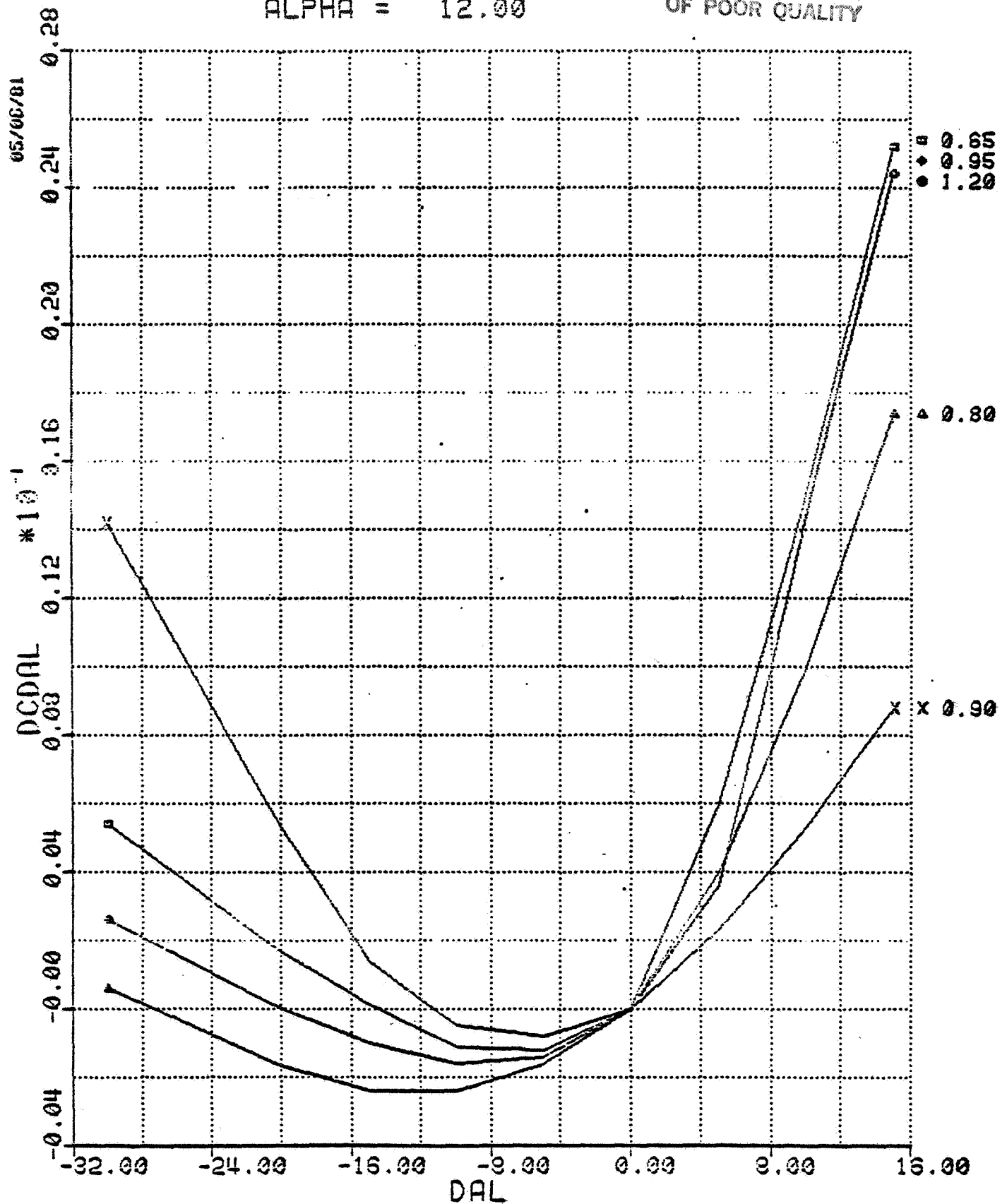
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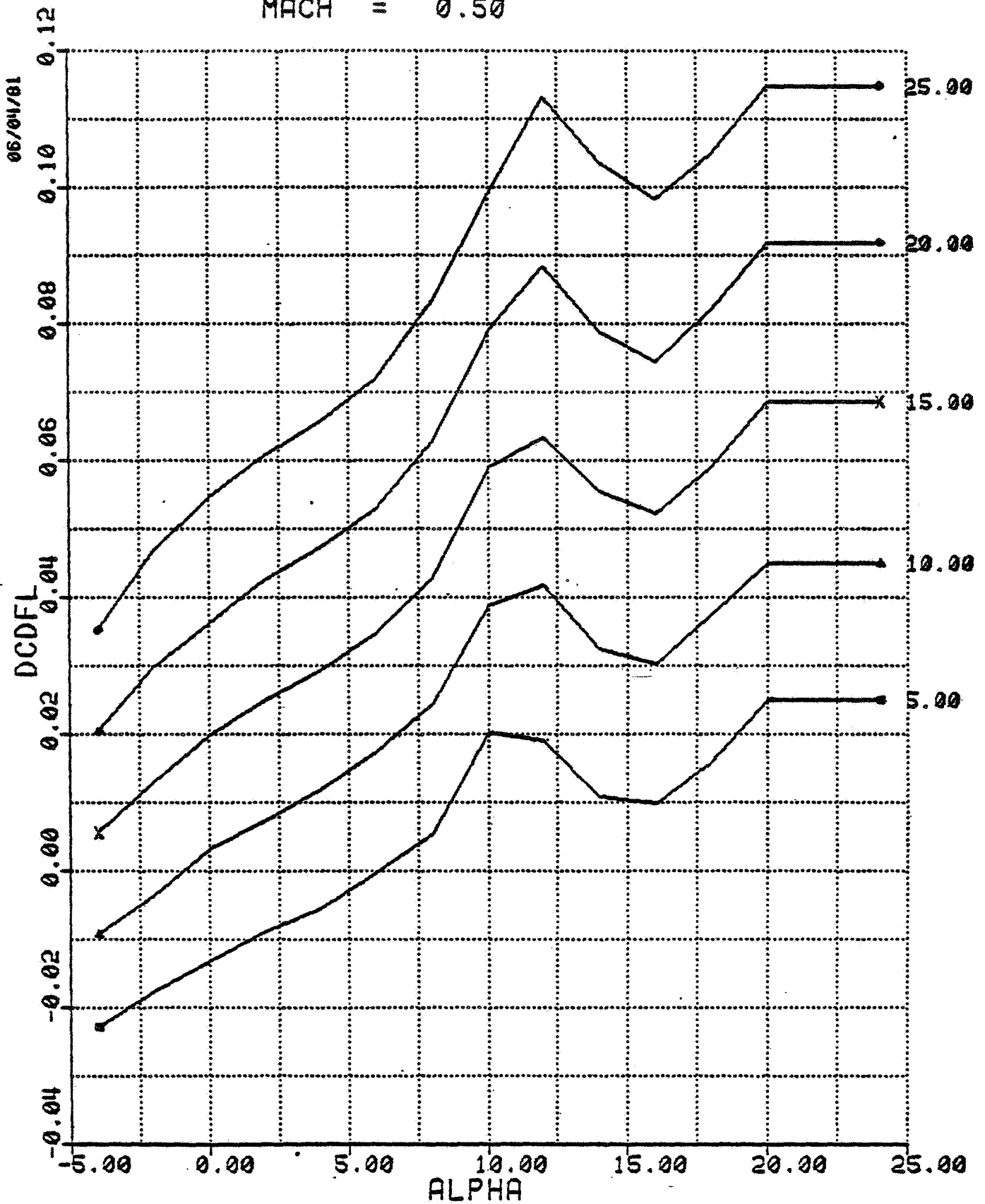
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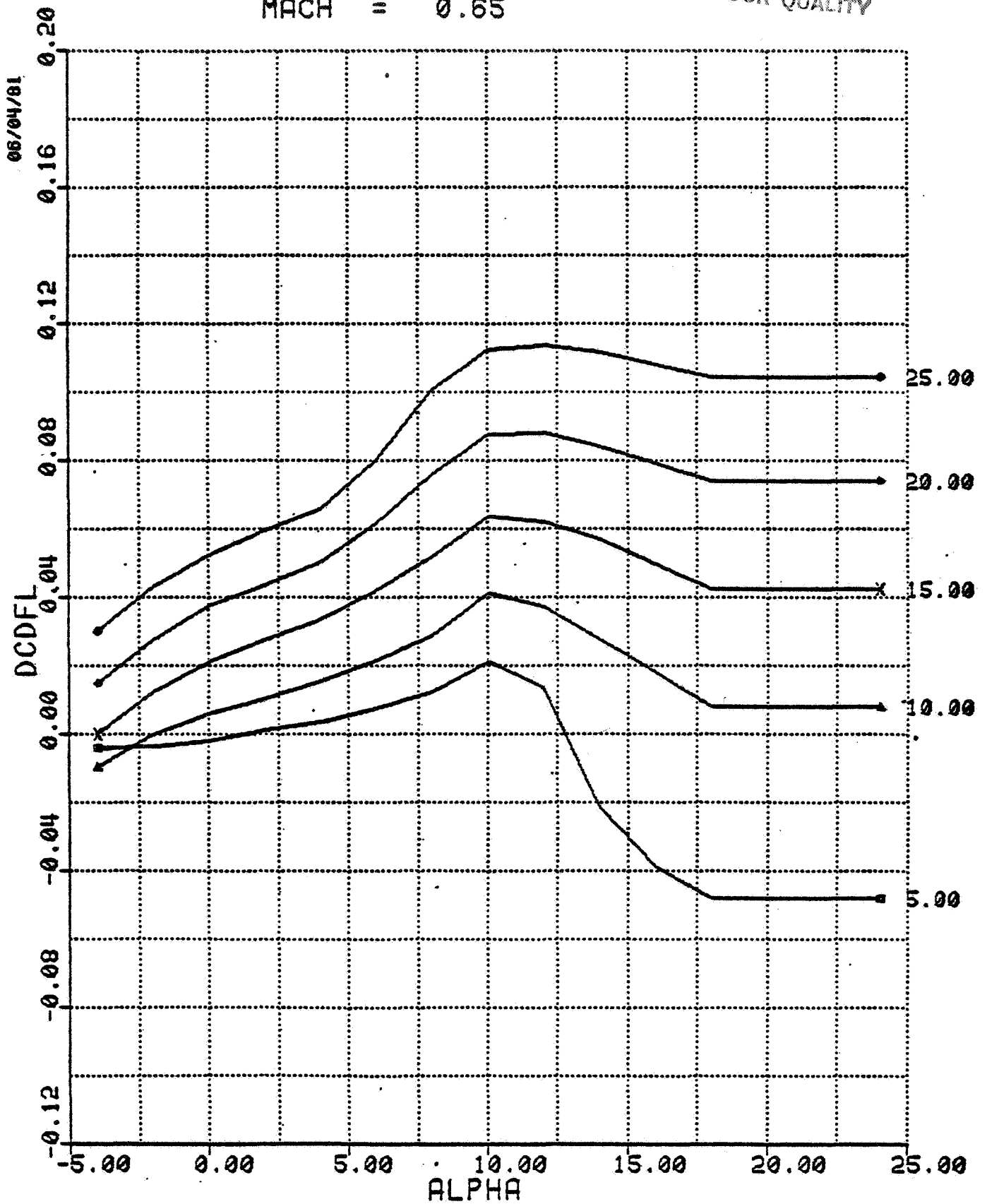
DCDFL VS ALPHA
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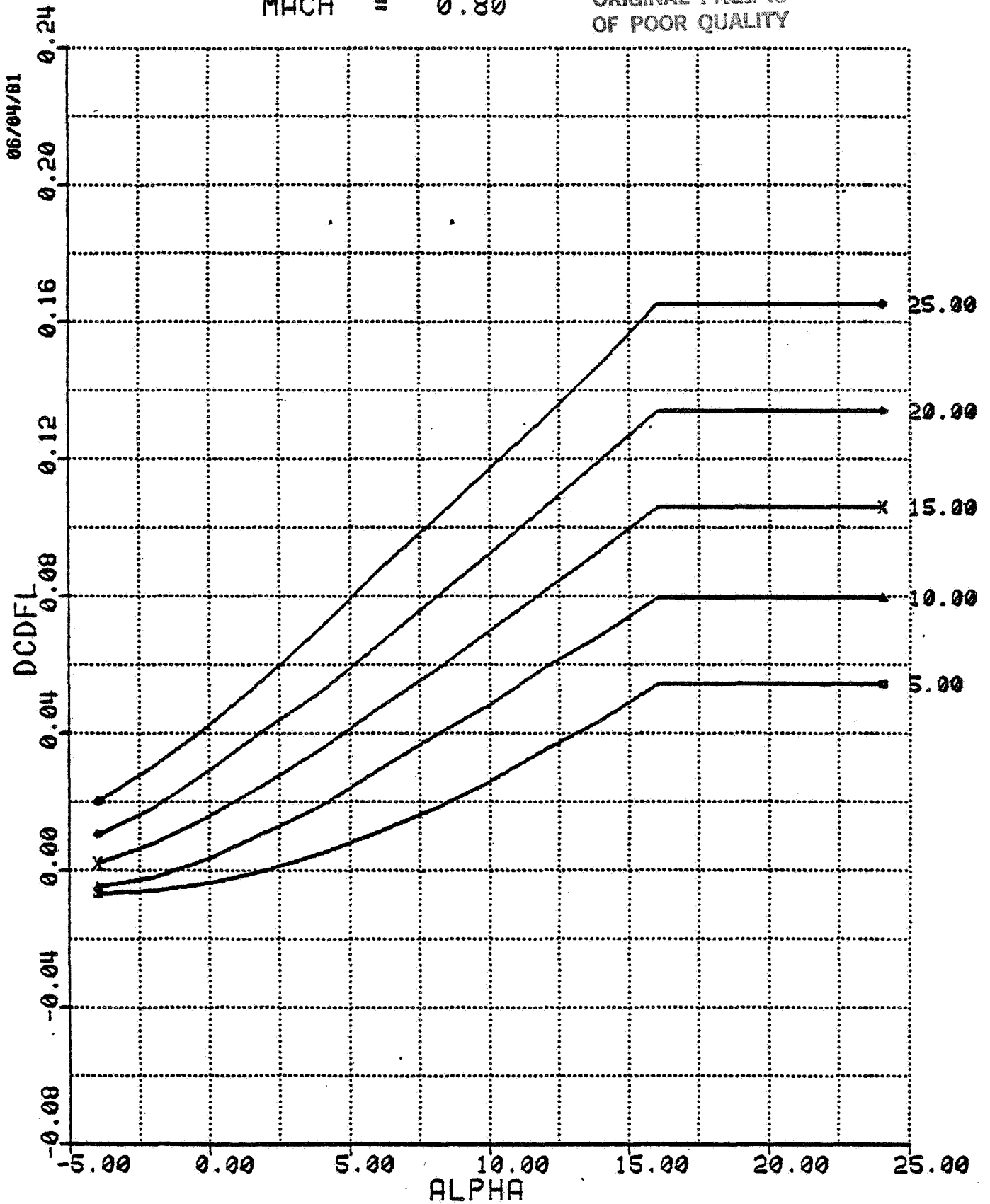
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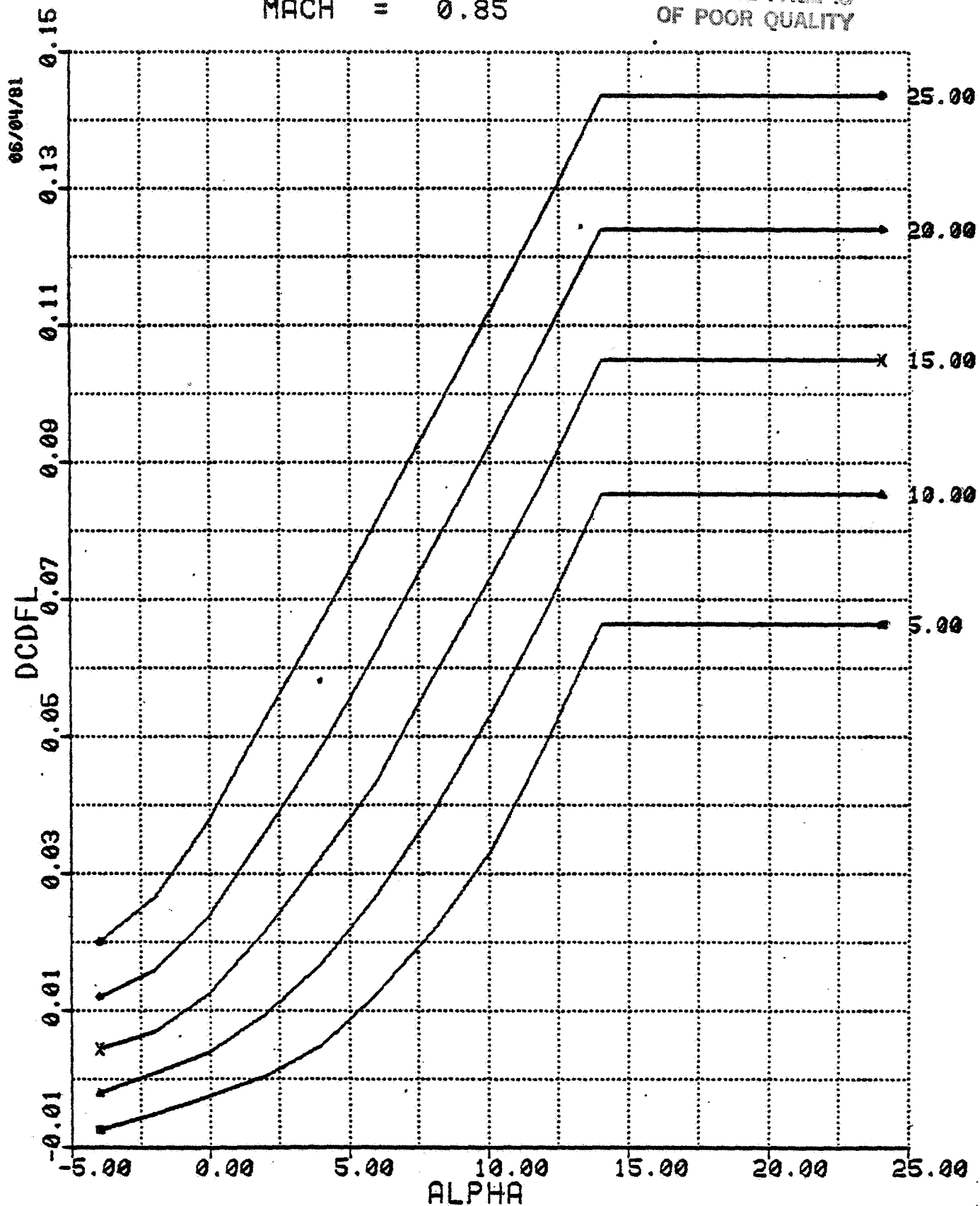
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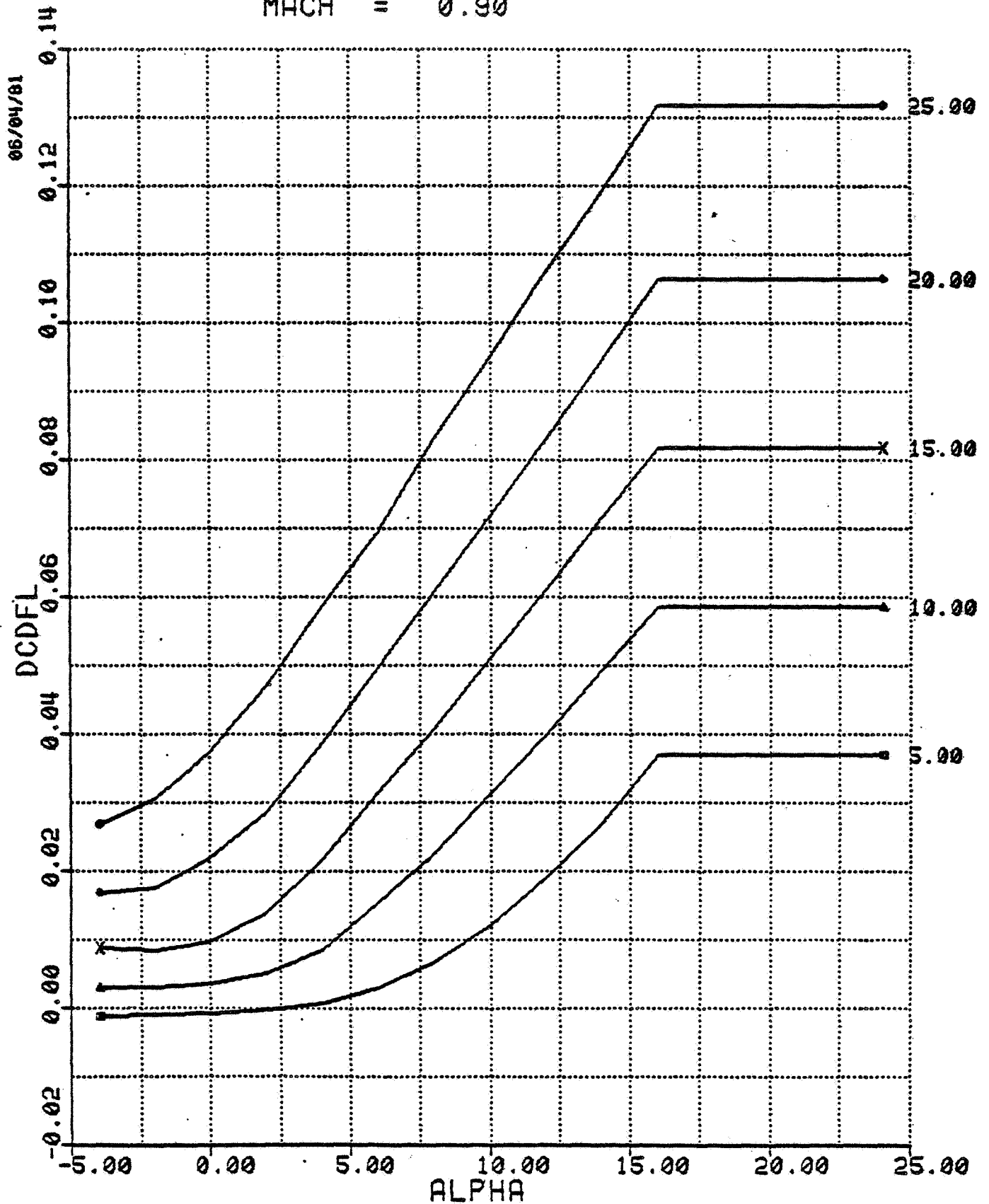
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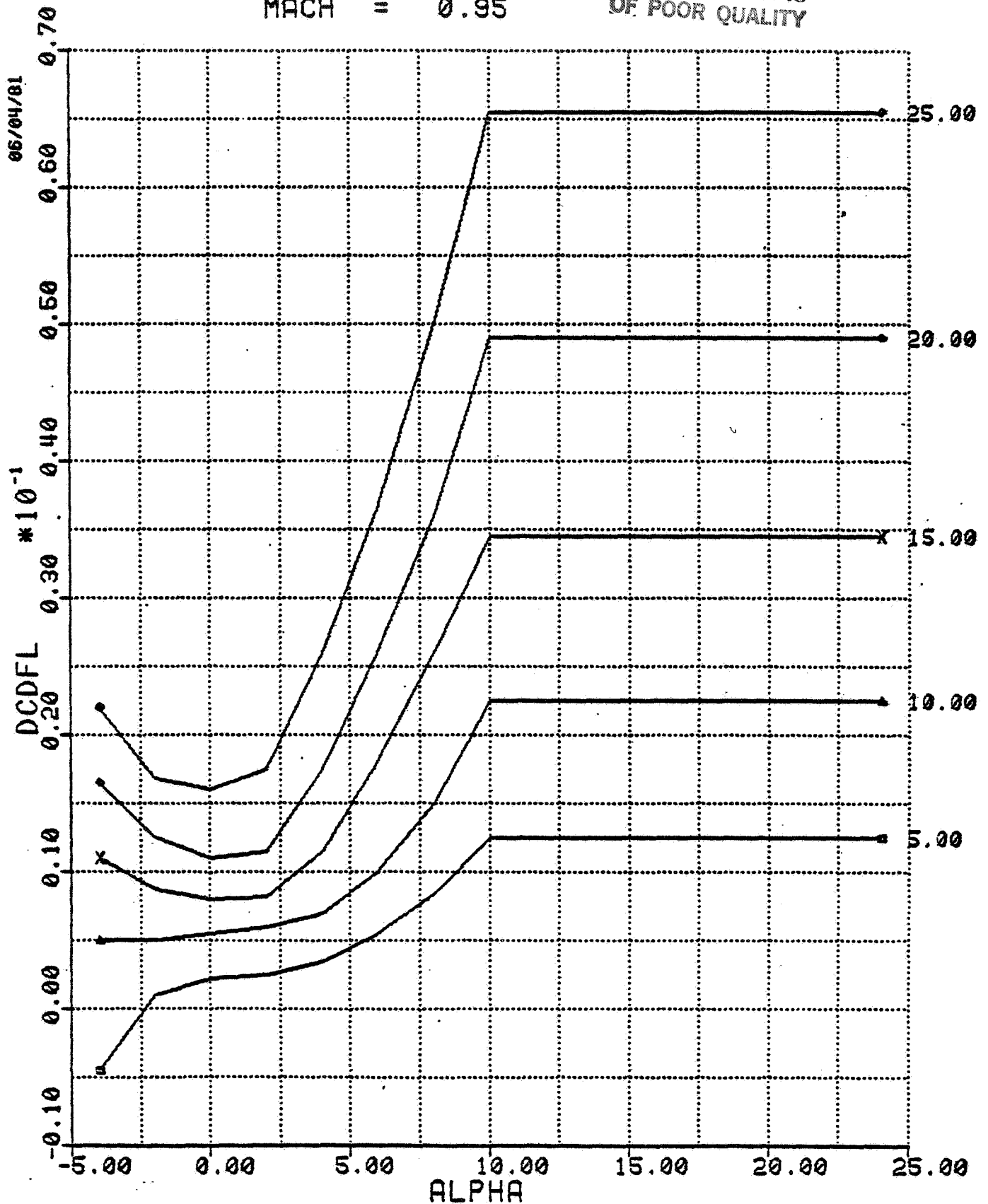
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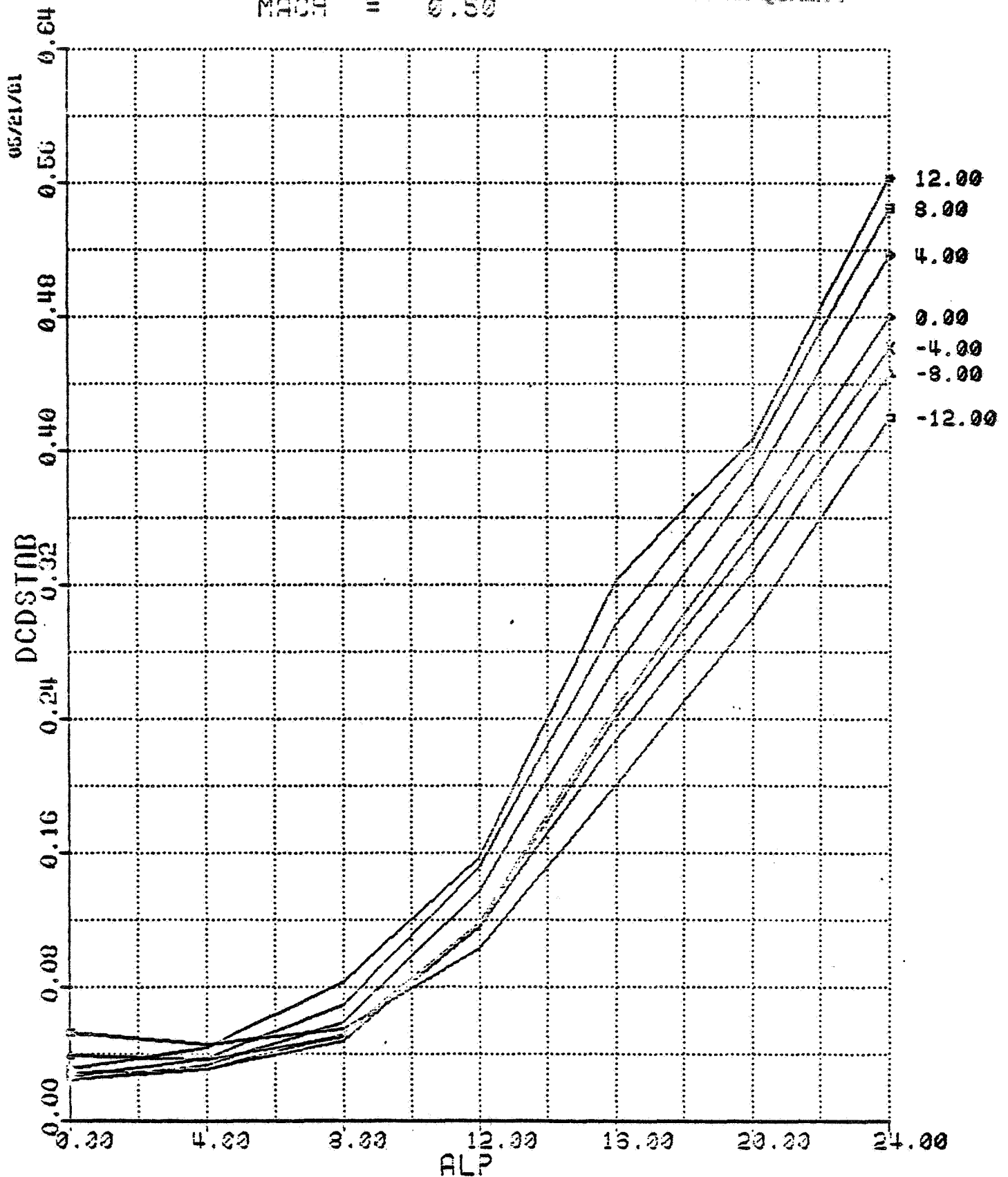
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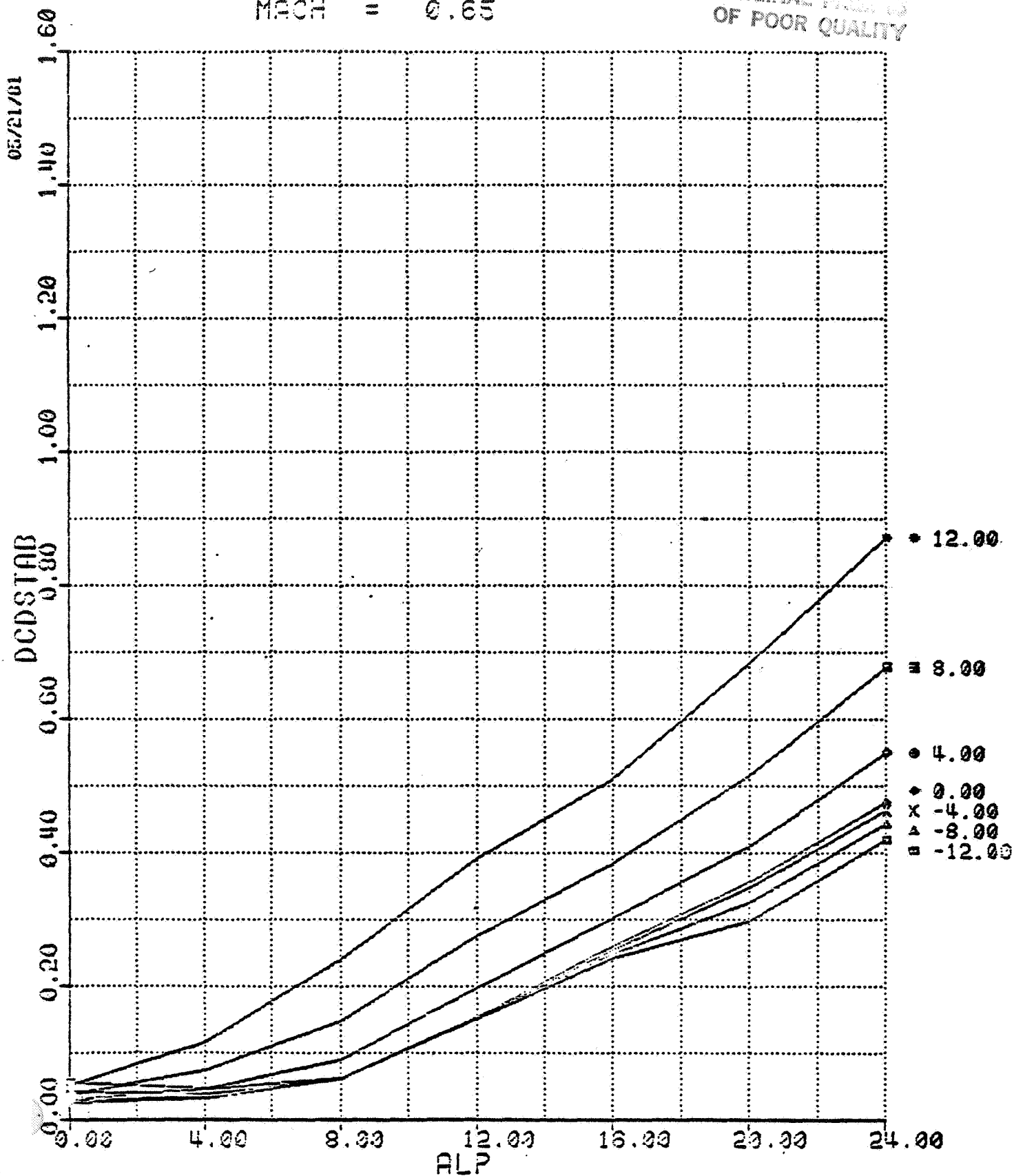
DCDSTAB VS ALP
FOR VARYING DHTD
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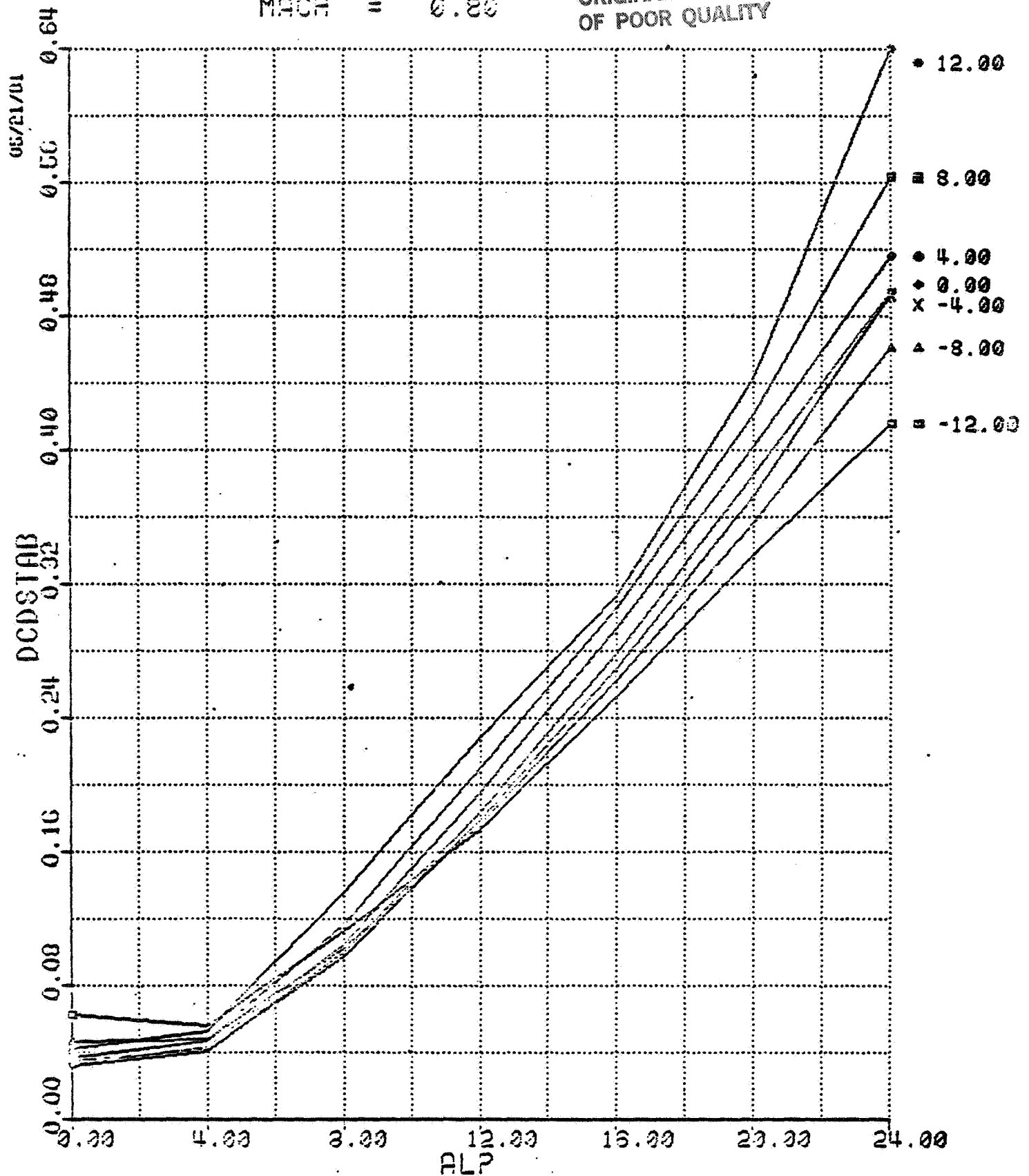
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FOR VARYING DHTD
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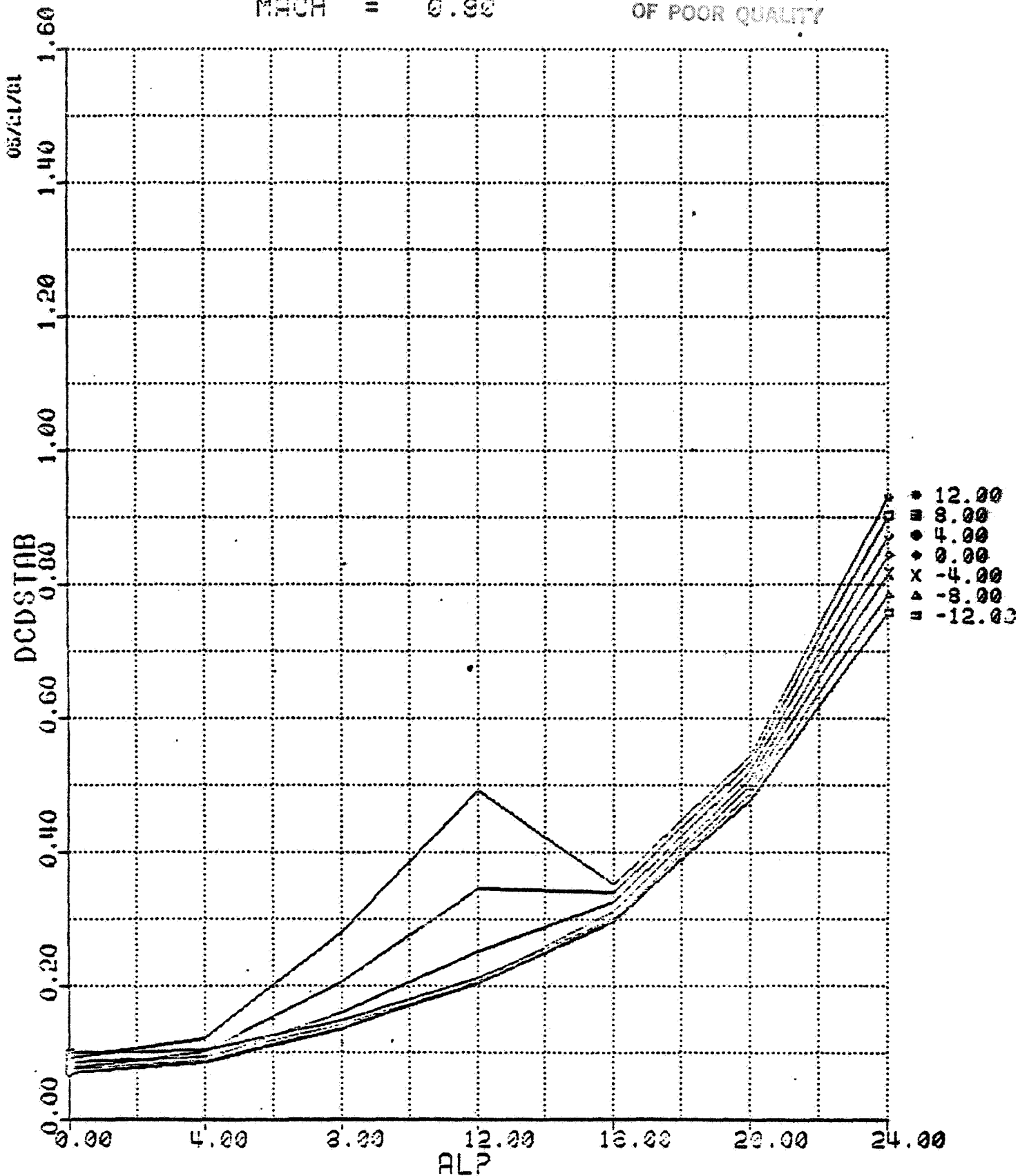
DCDSTAB .VS ALP
FOR VARYING DHTD
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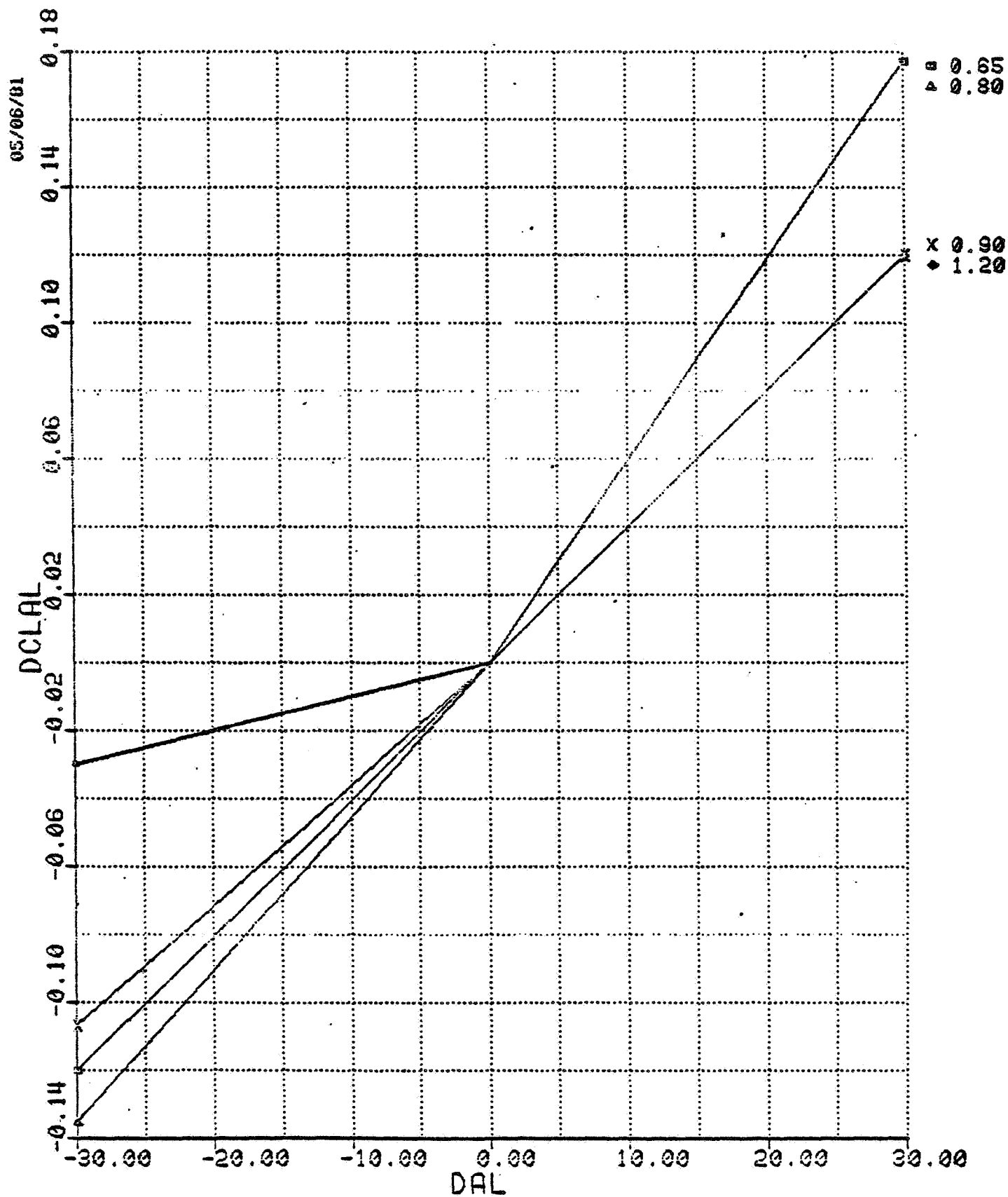


DCDSTAB VS ALP
FOR VARYING DHTD
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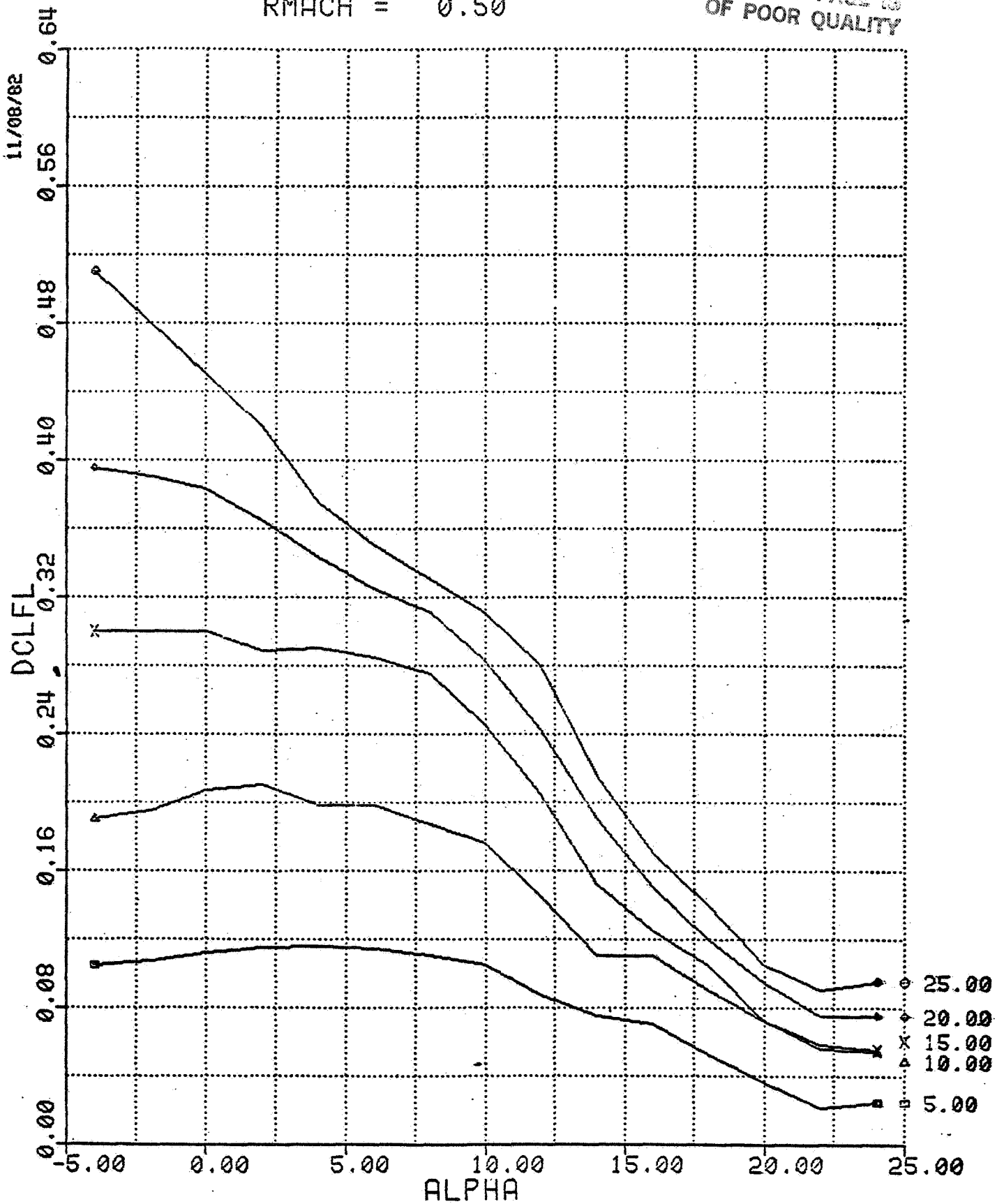


DCLAL VS DAL ORIGINAL PAGE IS
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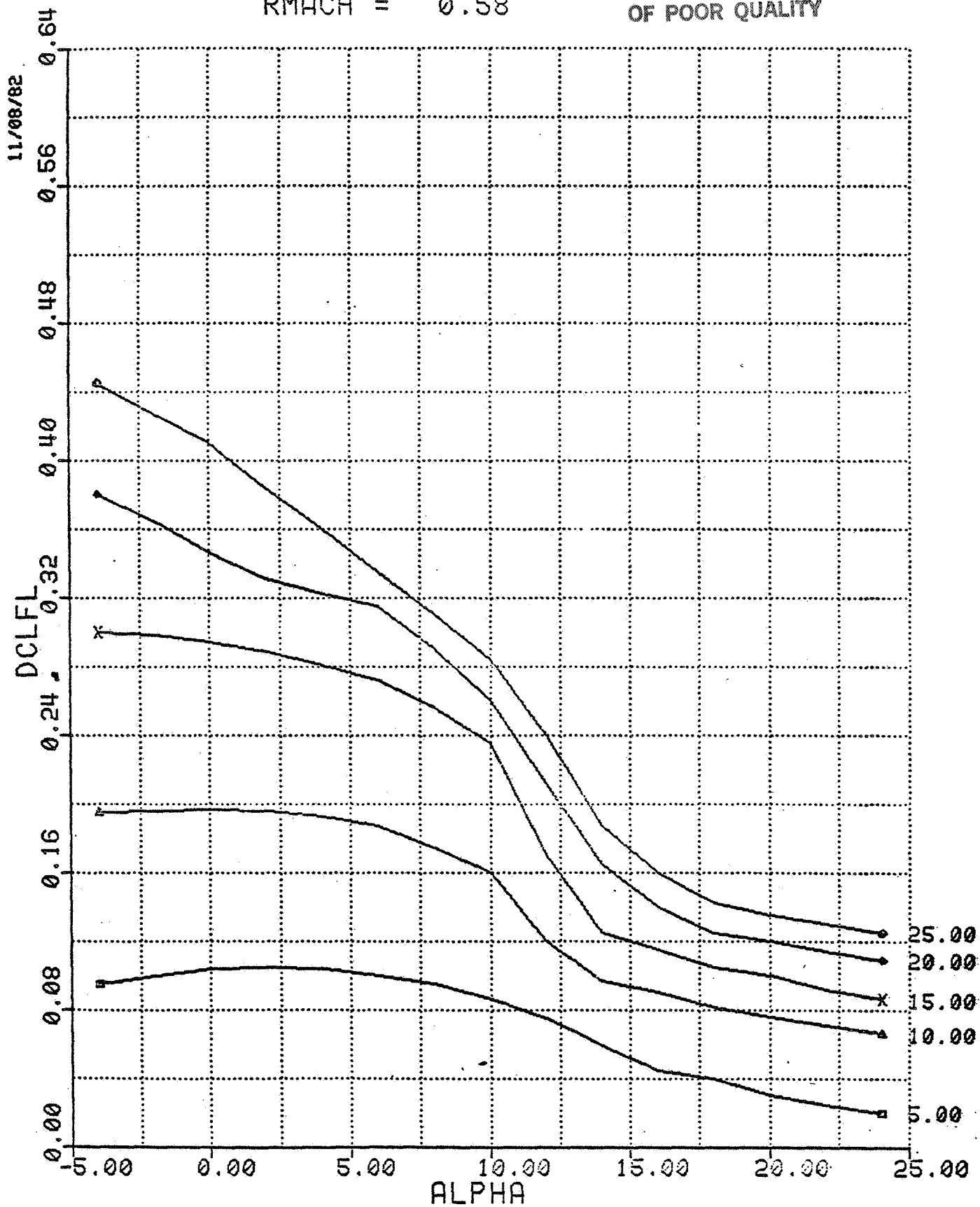
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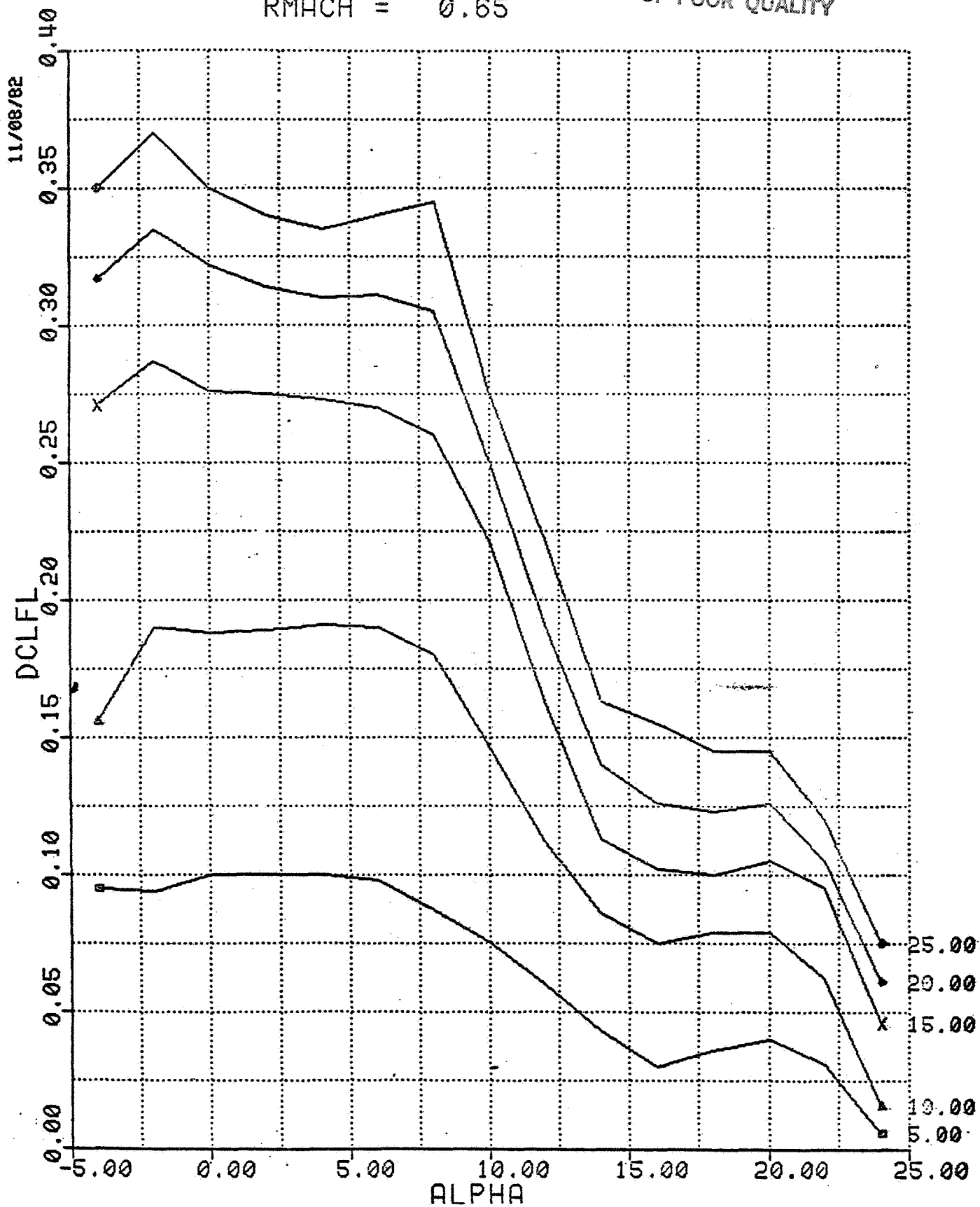
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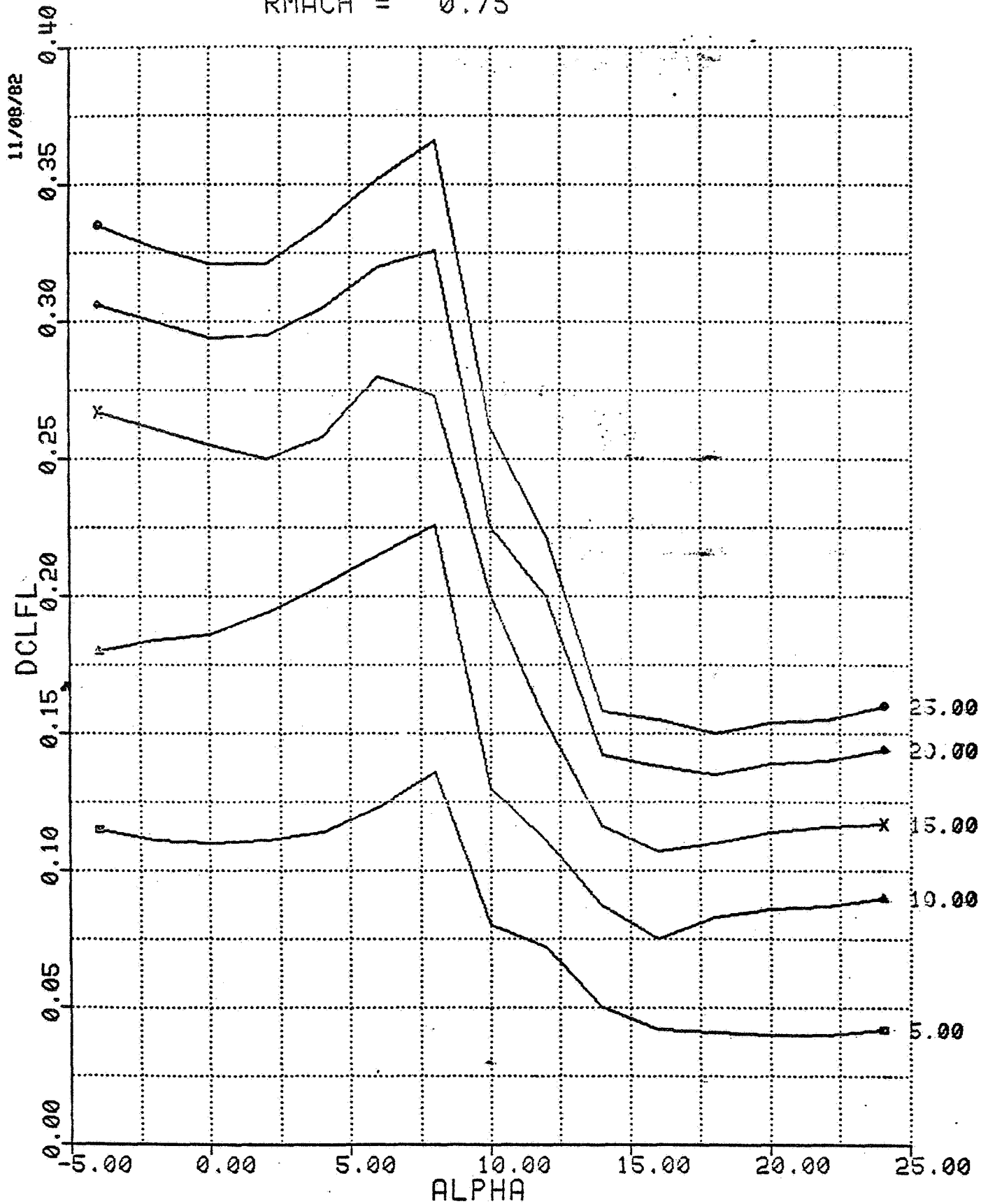


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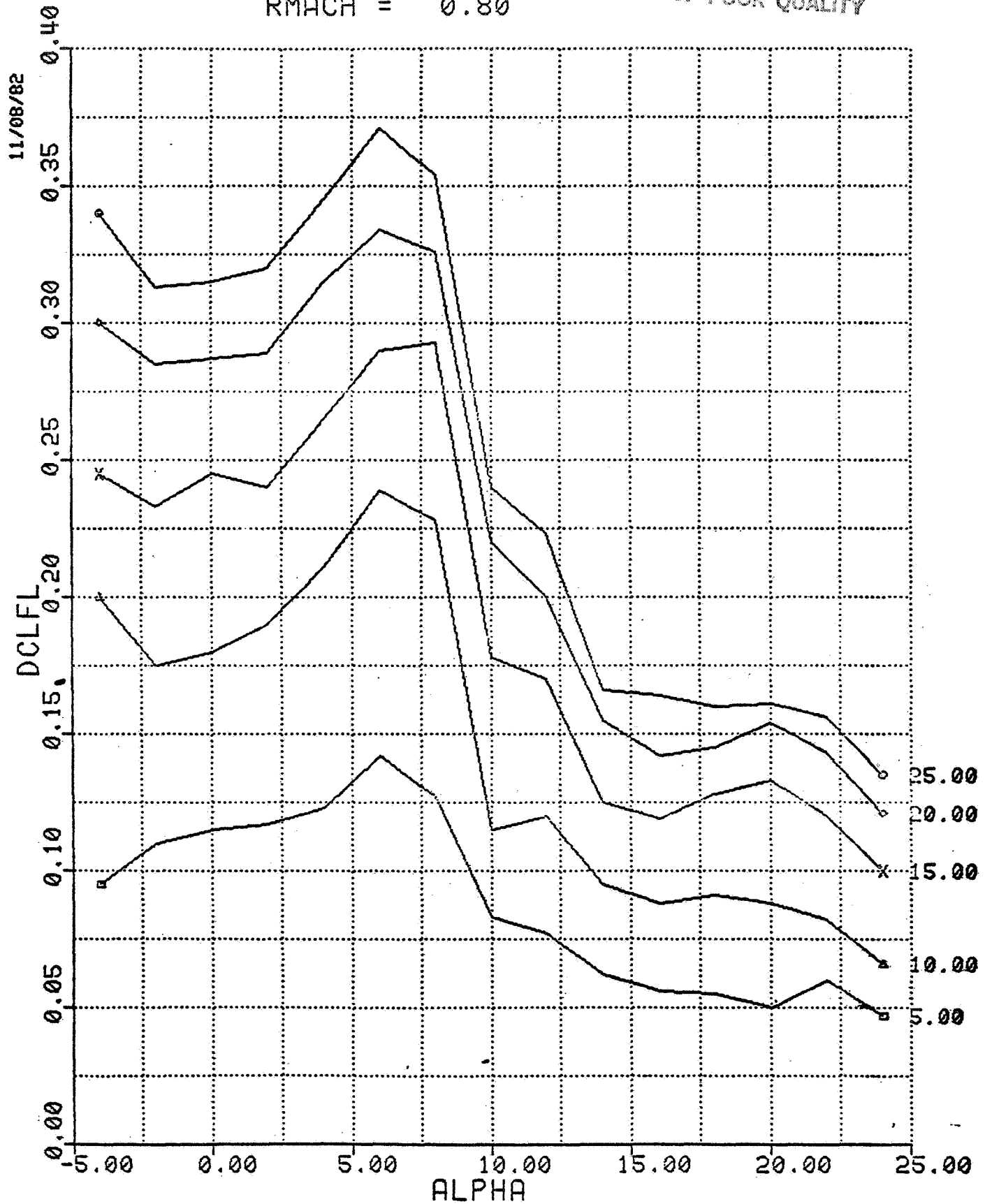


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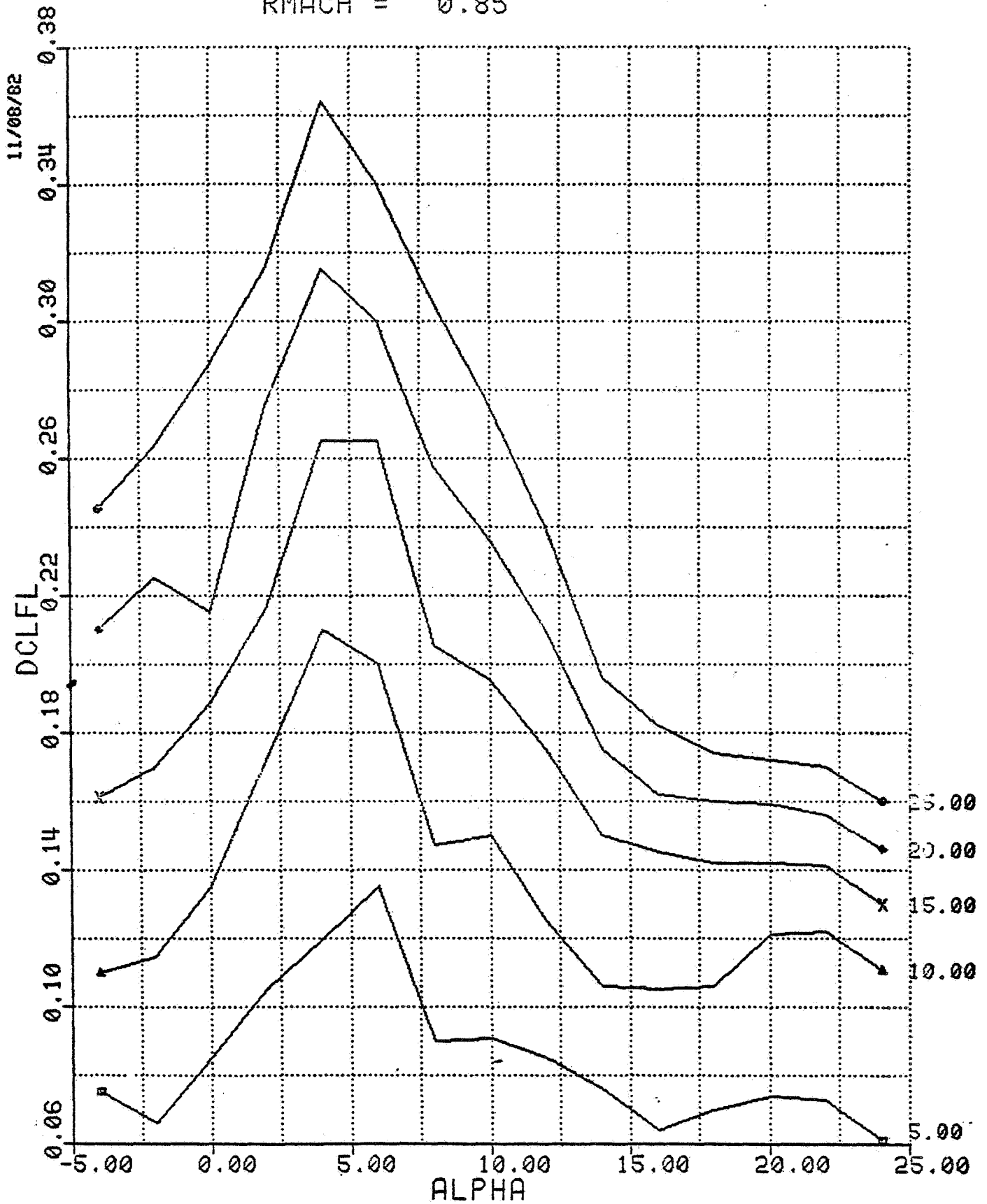
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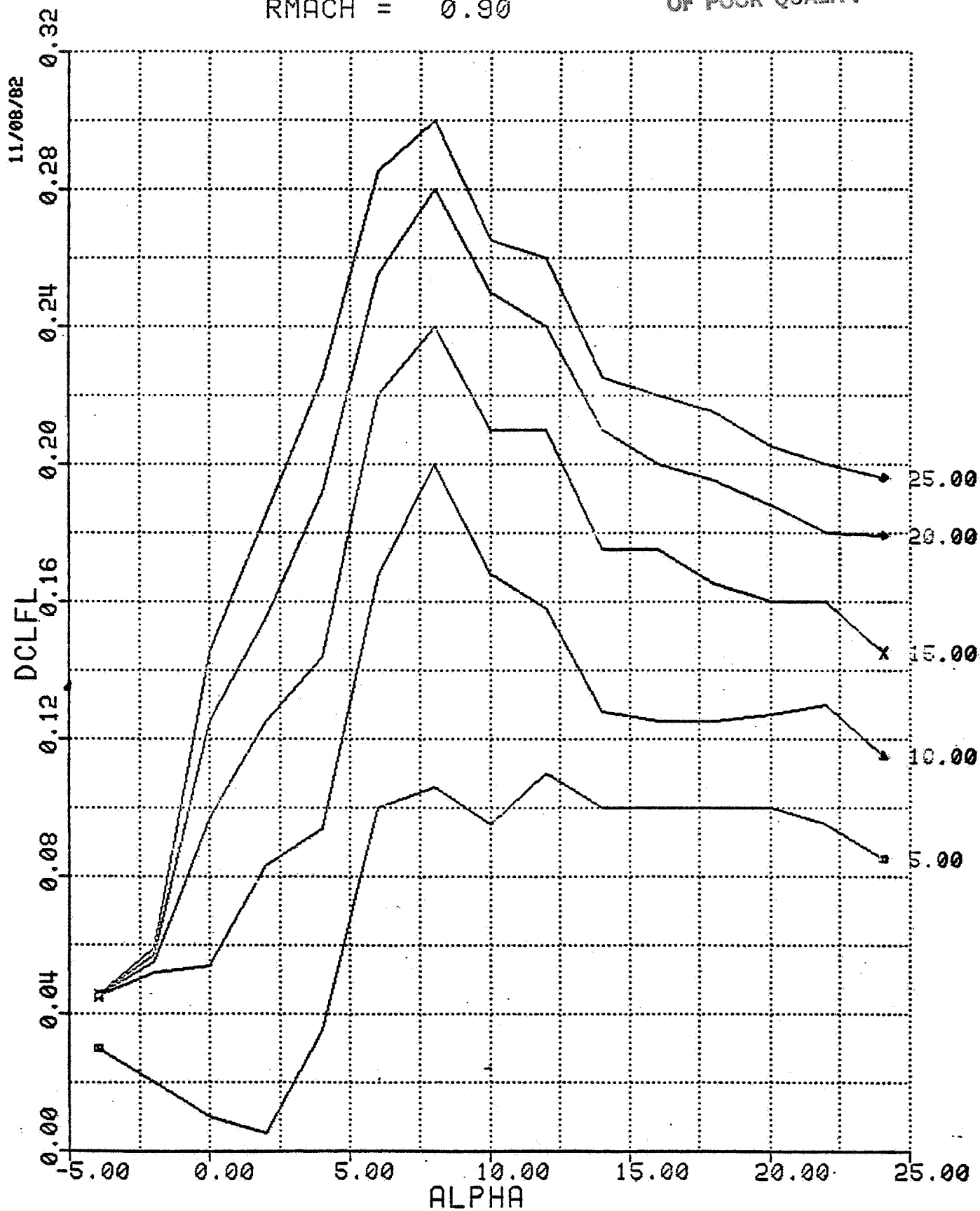
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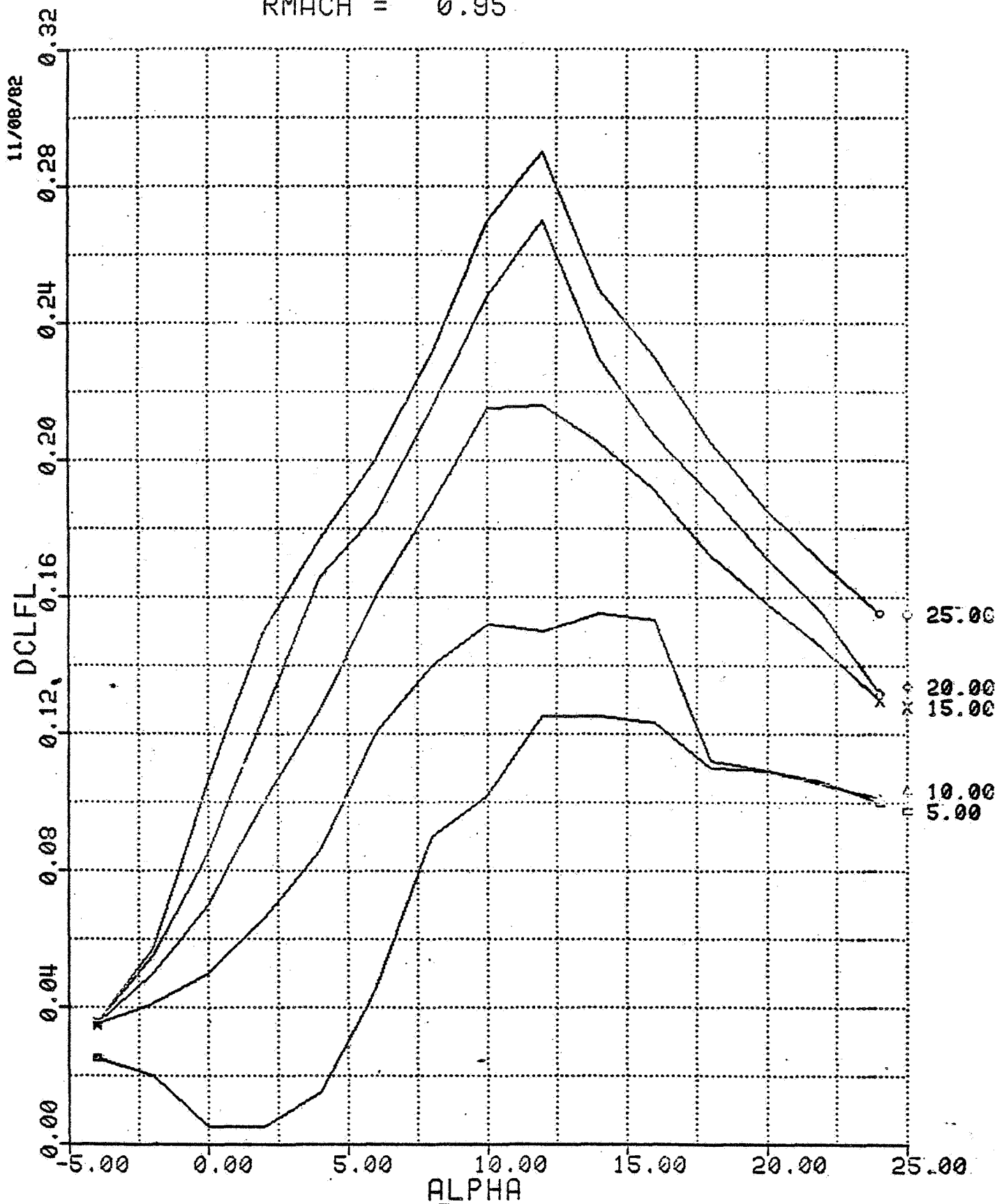


DCLFL VS ALPHA
FOR VARYING DFLAPL
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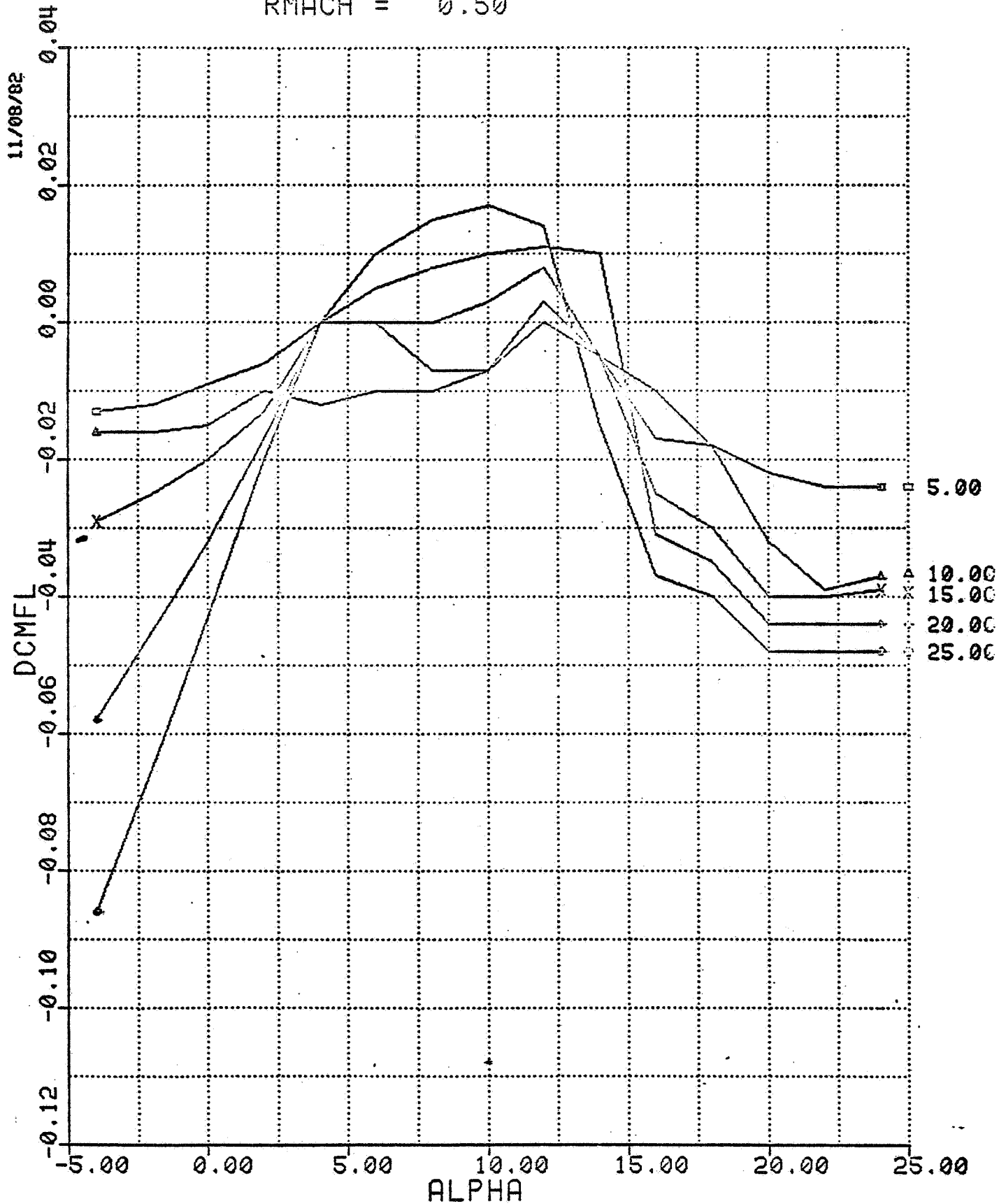
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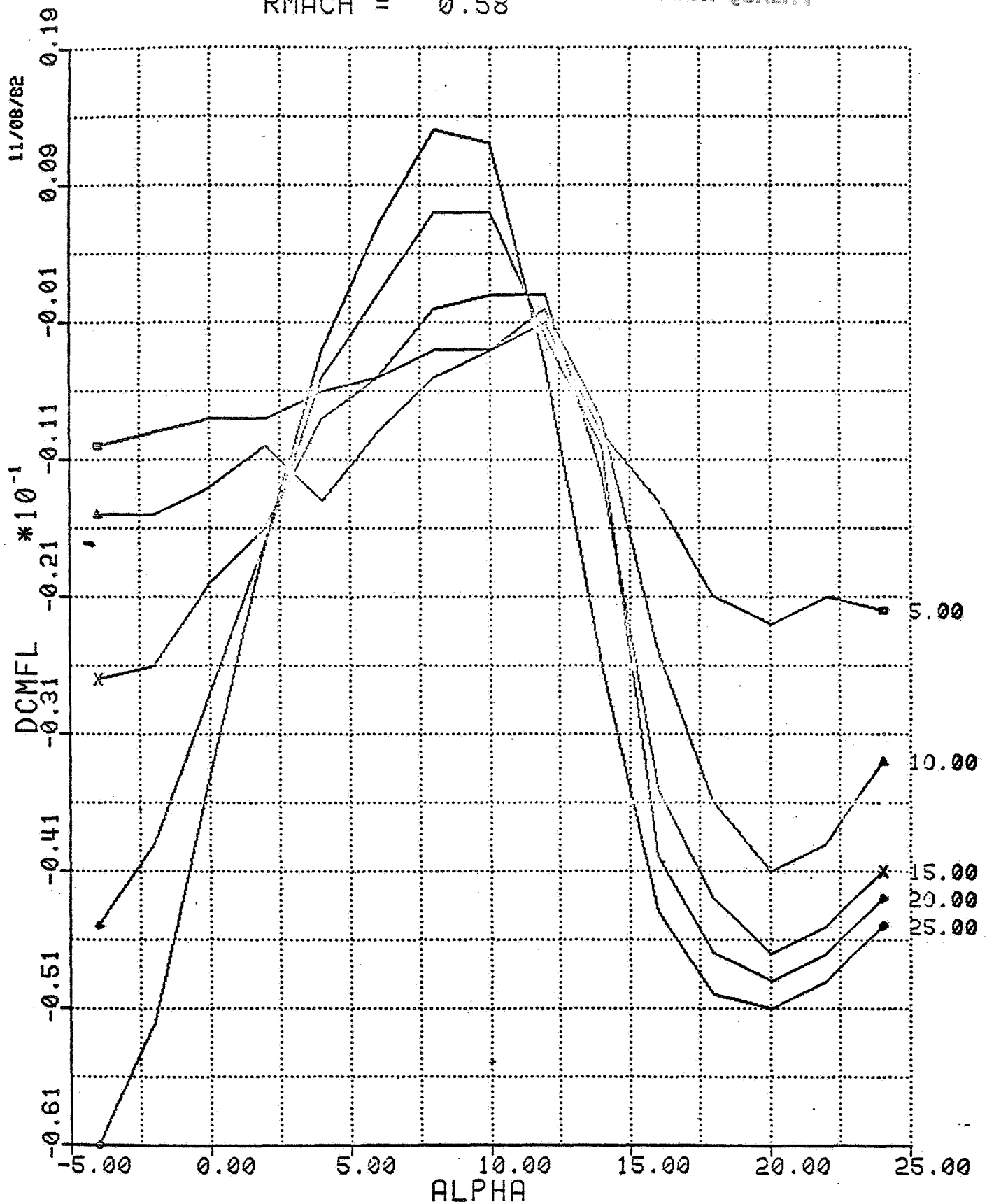
MDC A7910
Volume II

DCMFL VS ALPHA
FOR VARYING DFLAPL
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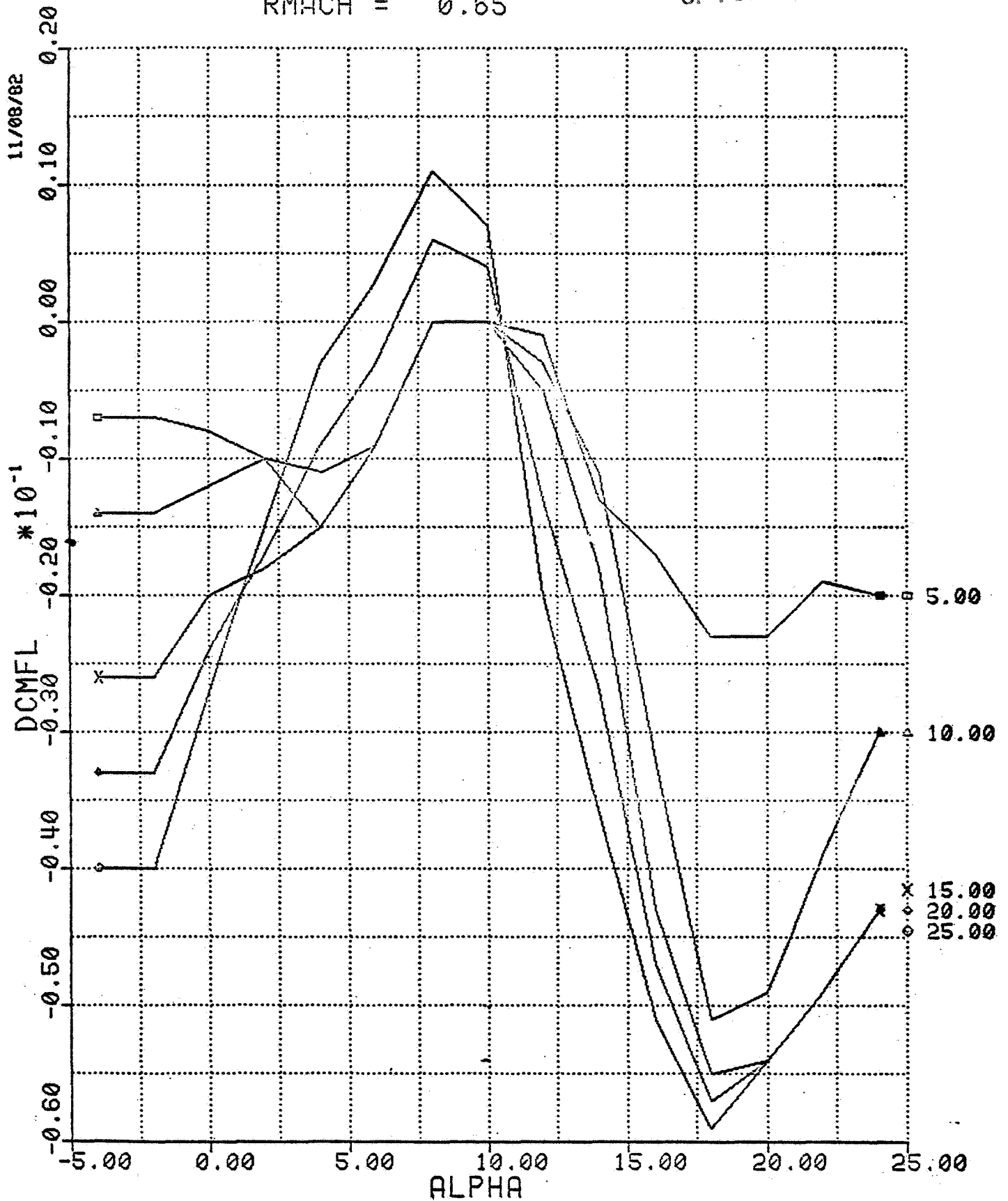
DCMFL VS ALPHA
FOR VARYING DFLAPL
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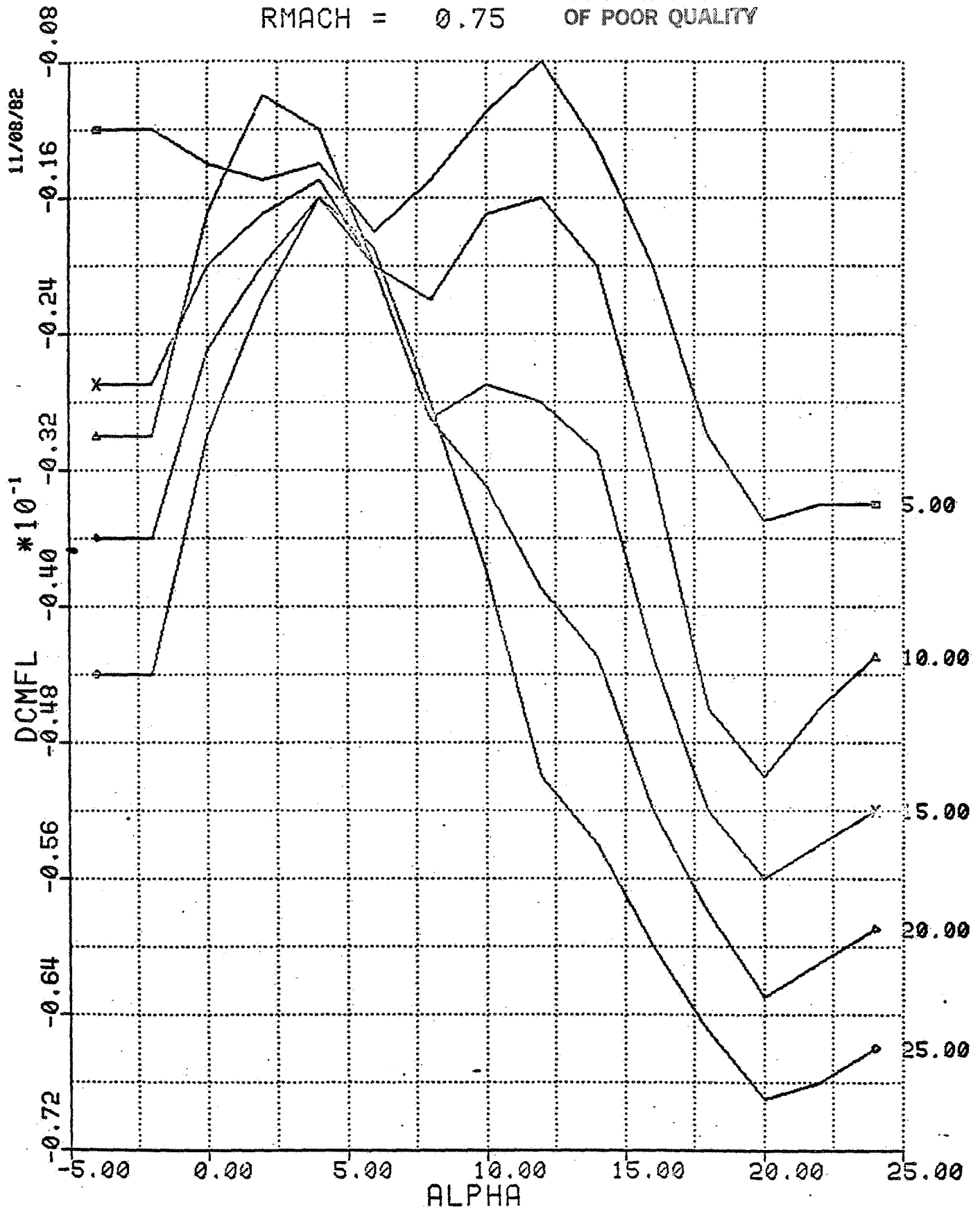


DCMFL VS ALPHA
FOR VARYING DFLAPL
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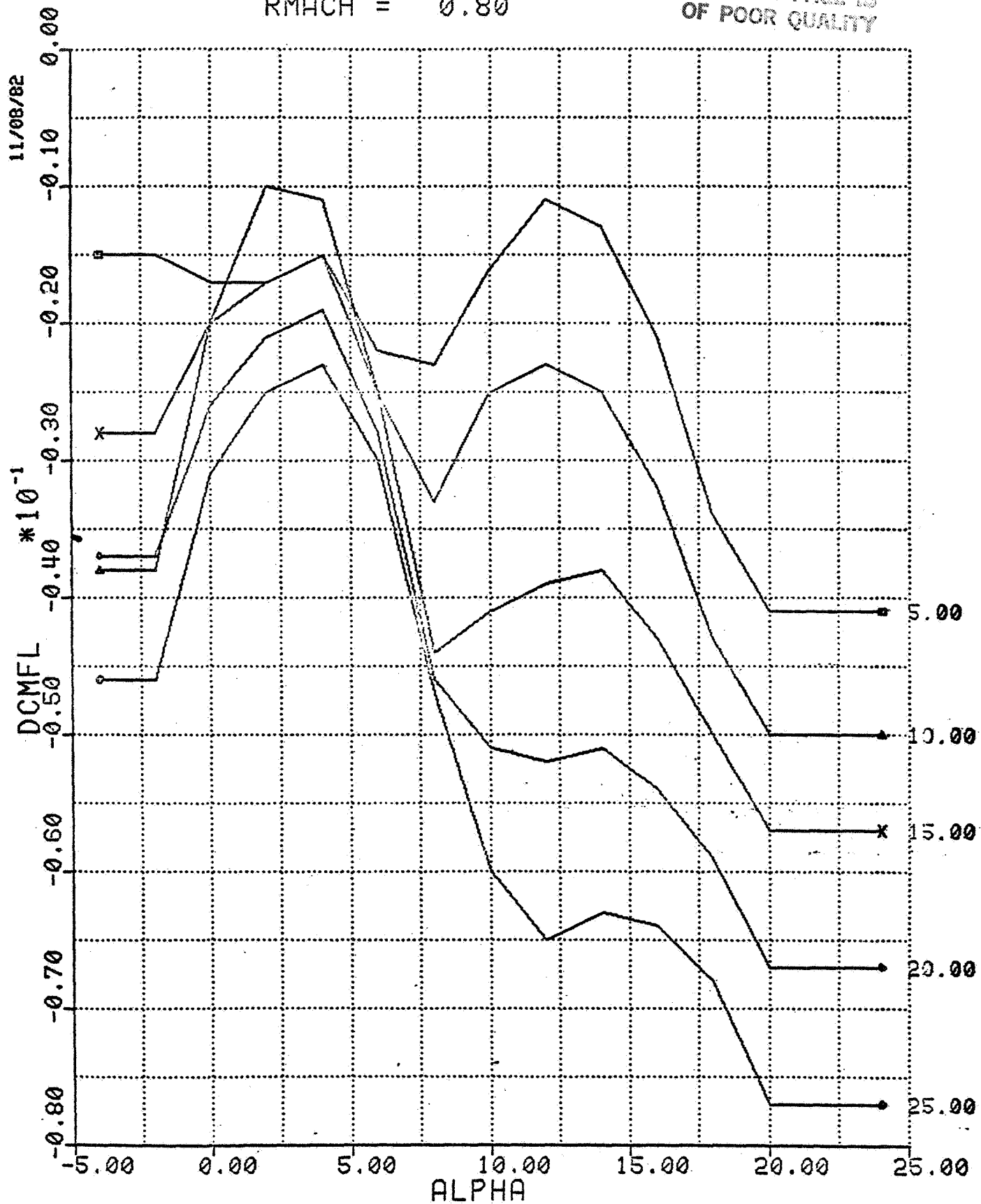


DCMFL VS ALPHA
FOR VARYING DFLAPL
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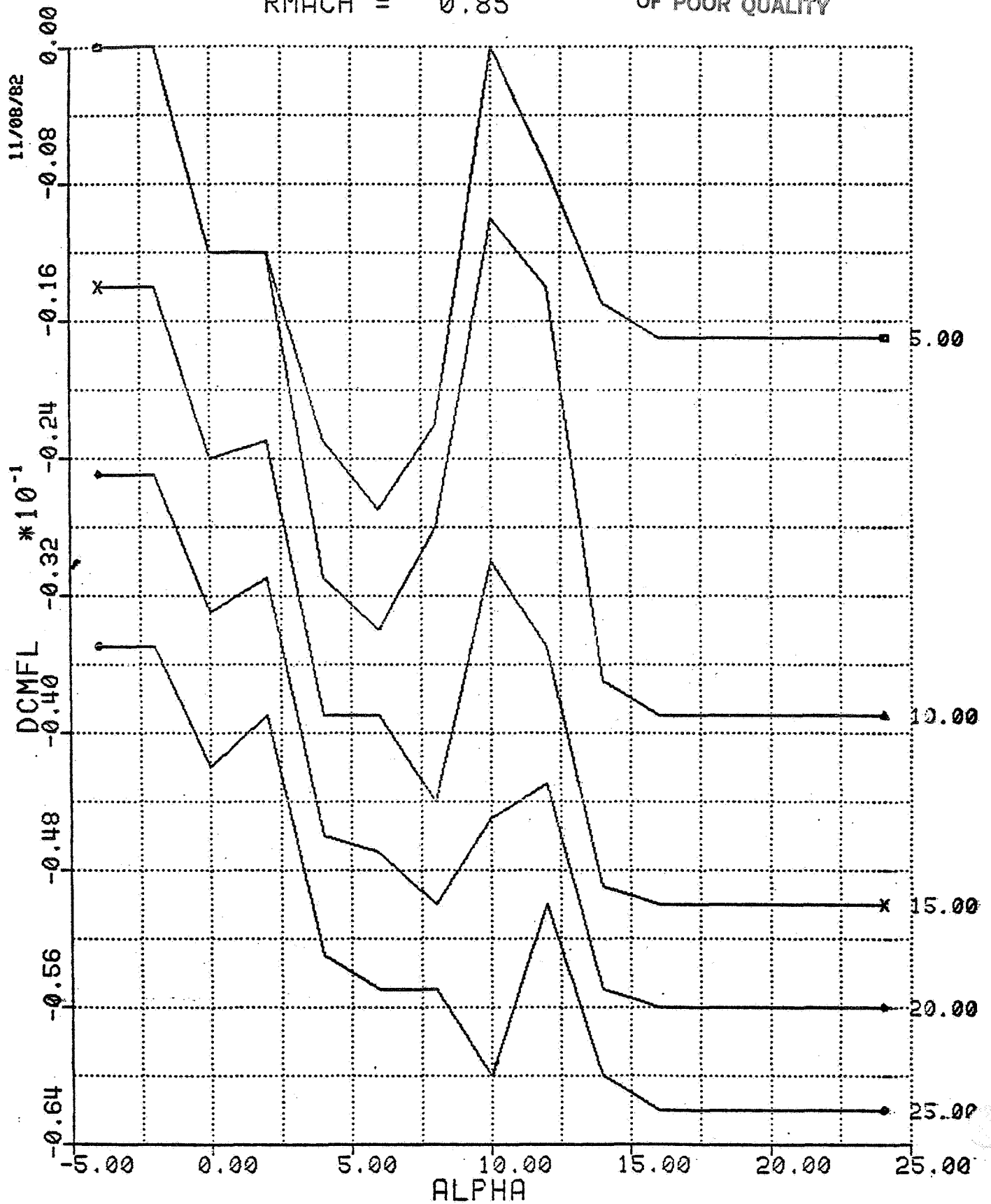
DCMFL VS ALPHA
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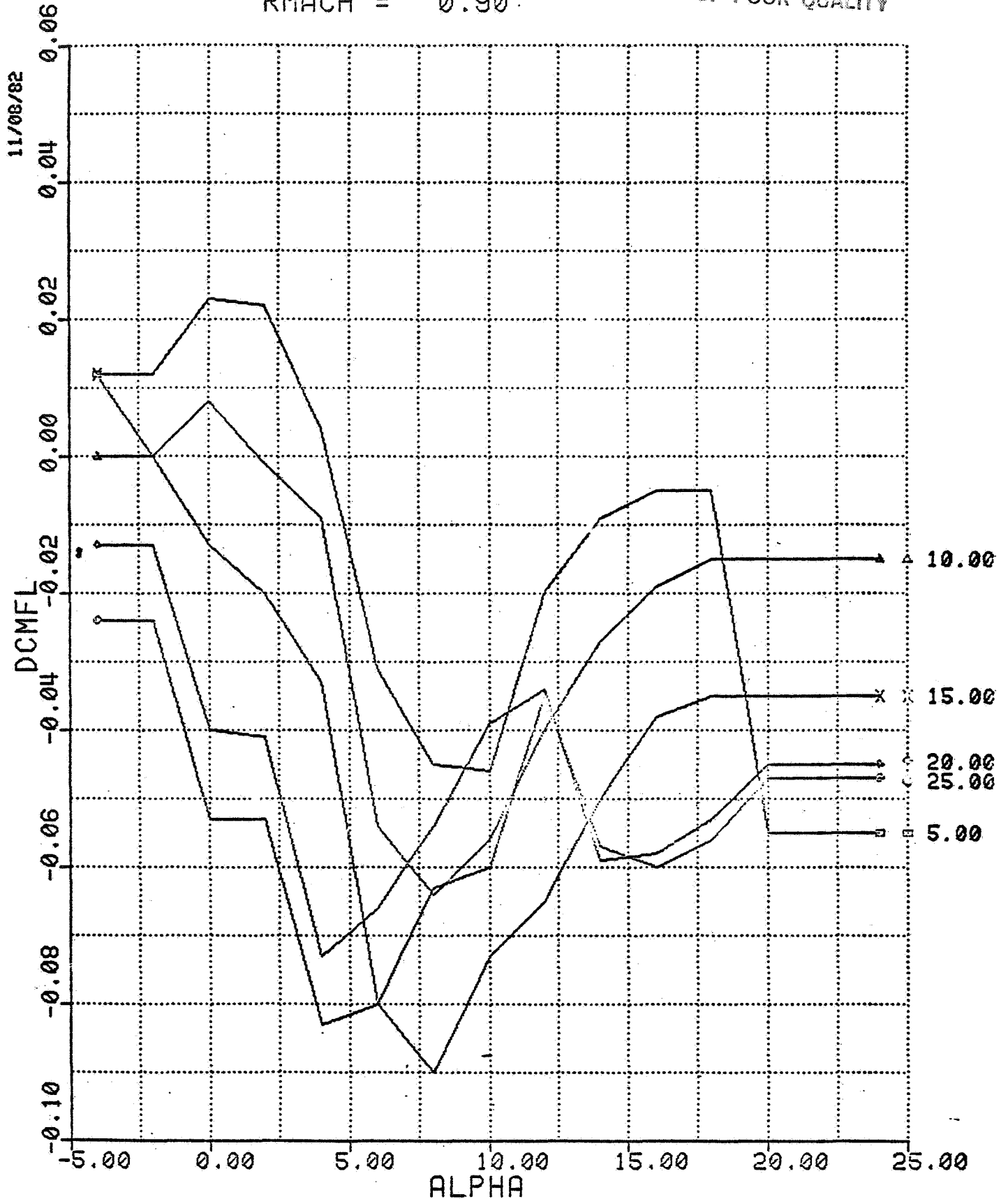
DCMFL VS ALPHA
FOR VARYING DFLAPL
RMACH = 0.85

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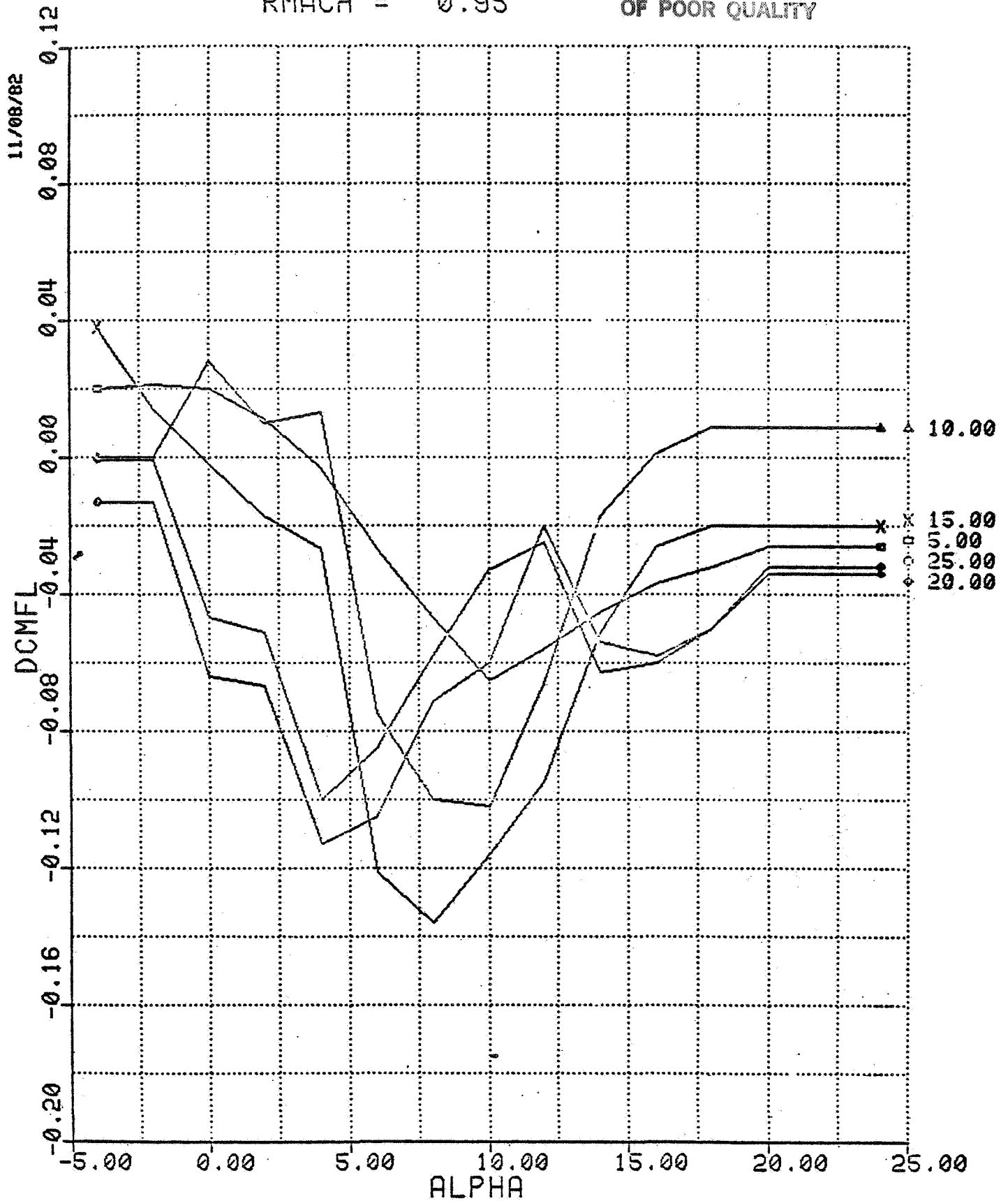
DCMFL VS ALPHA
FOR VARYING DFLAPL
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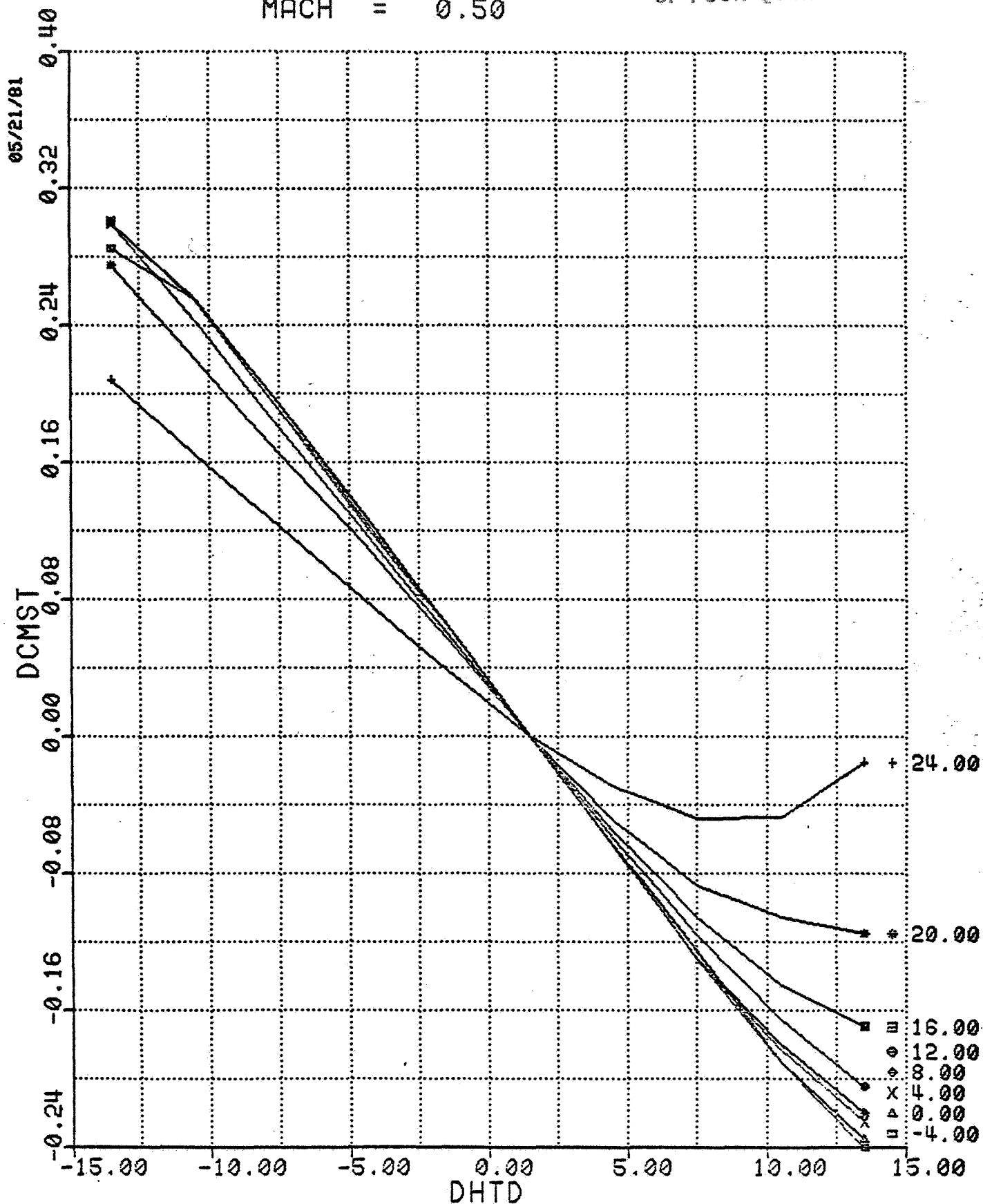
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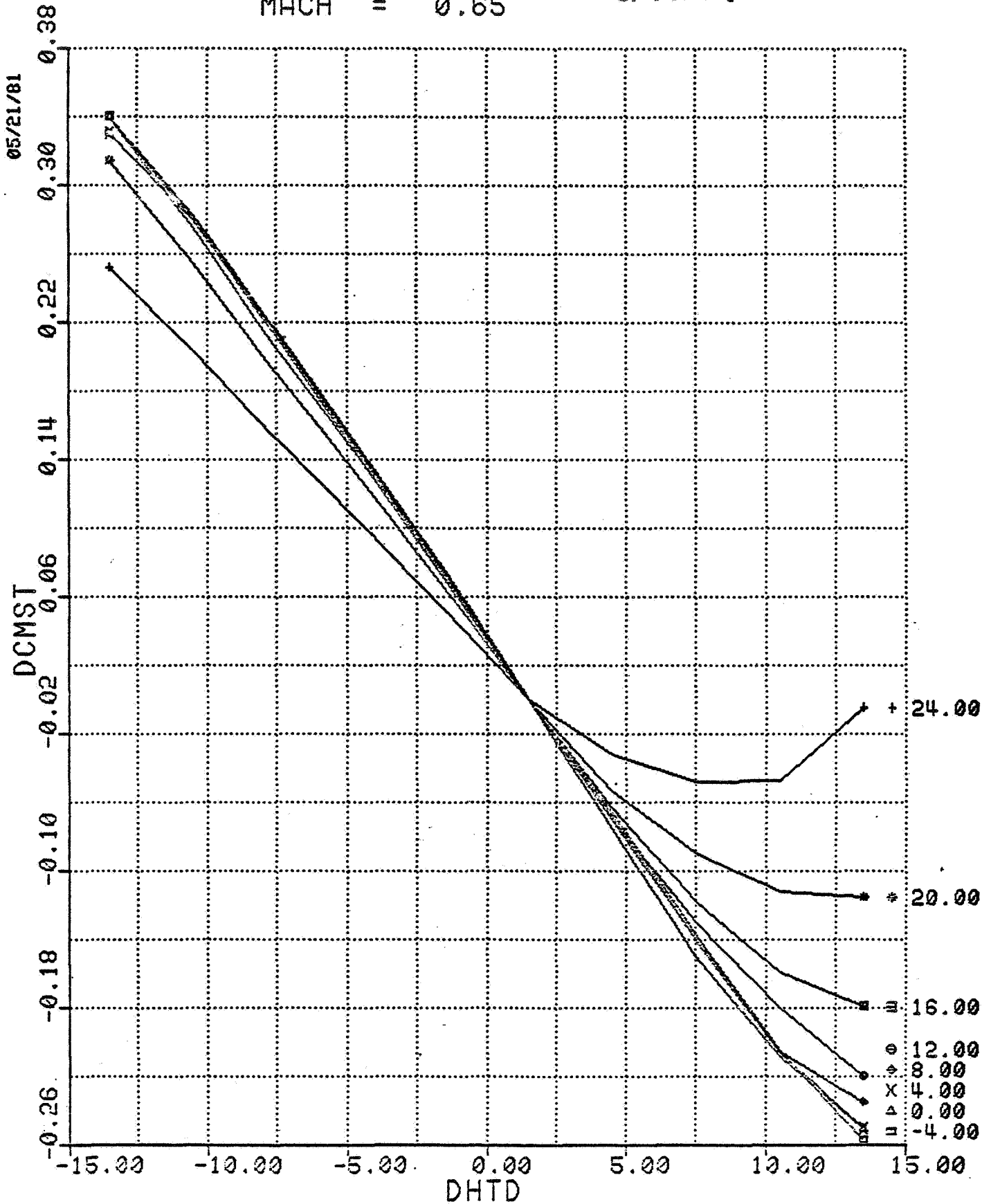
DCMST VS DHTD
FOR VARYING ALP
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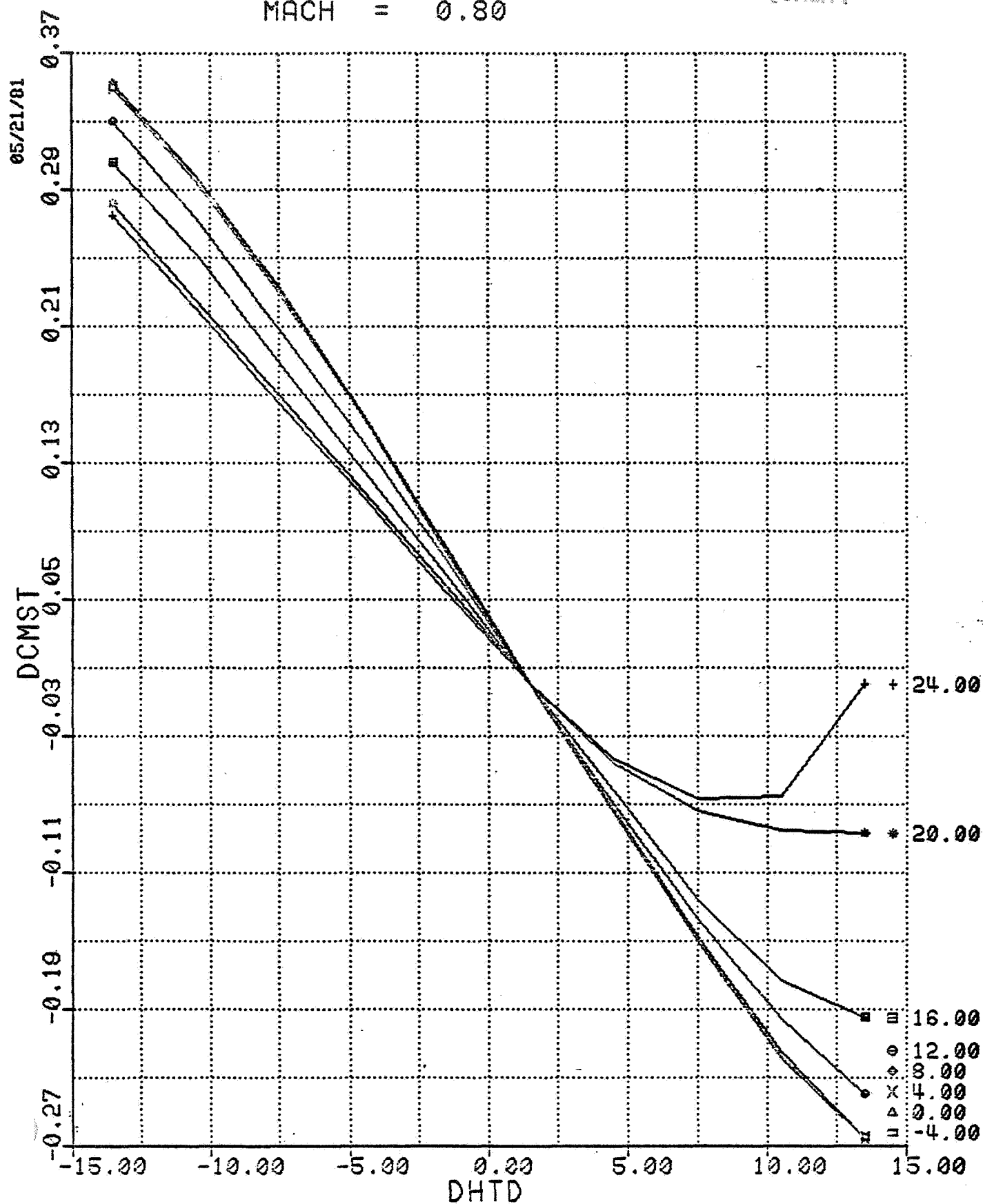
DCMST VS DHTD
FOR VARYING ALP
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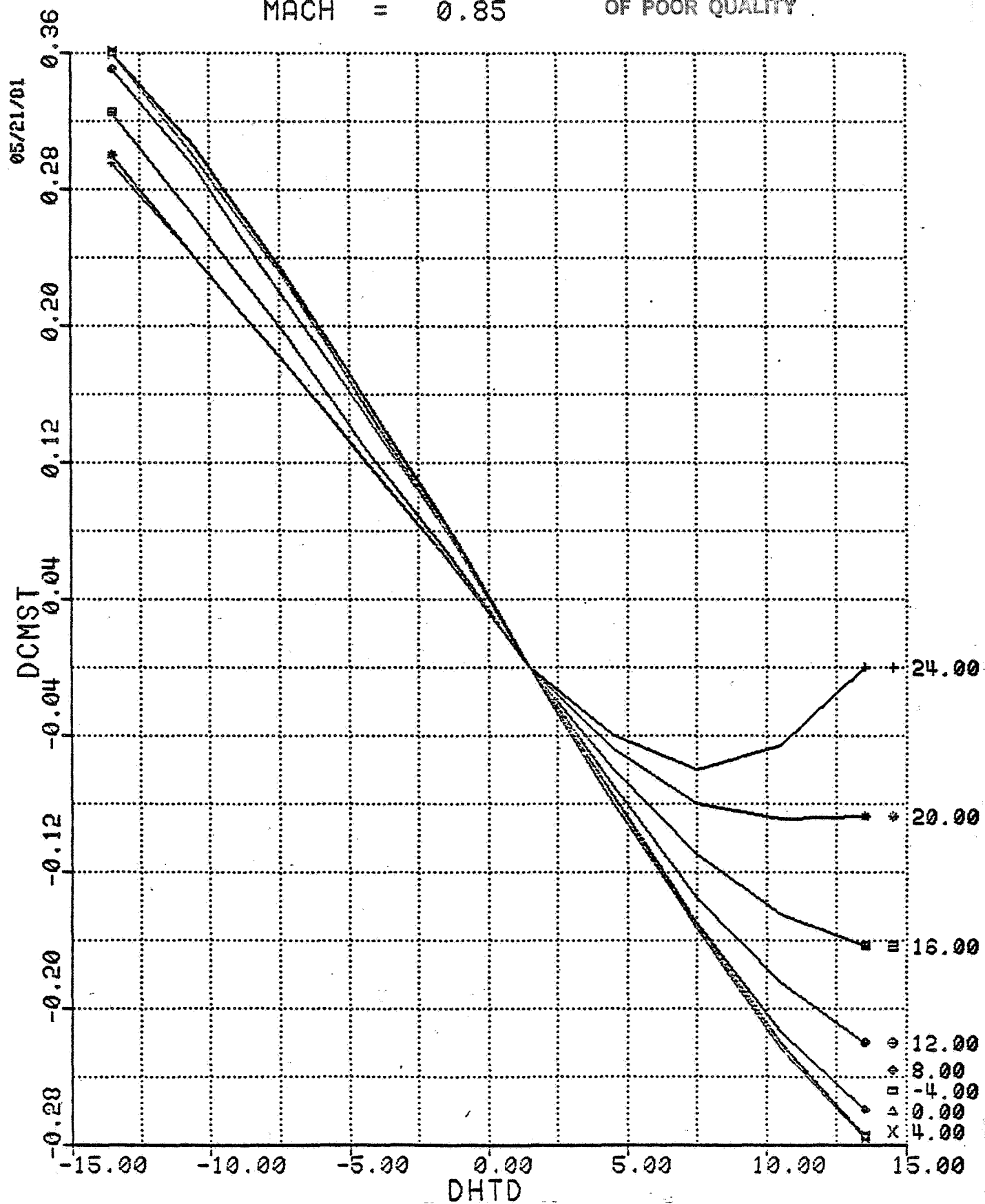
DCMST VS DHTD
FOR VARYING ALP
MACH = 0.80

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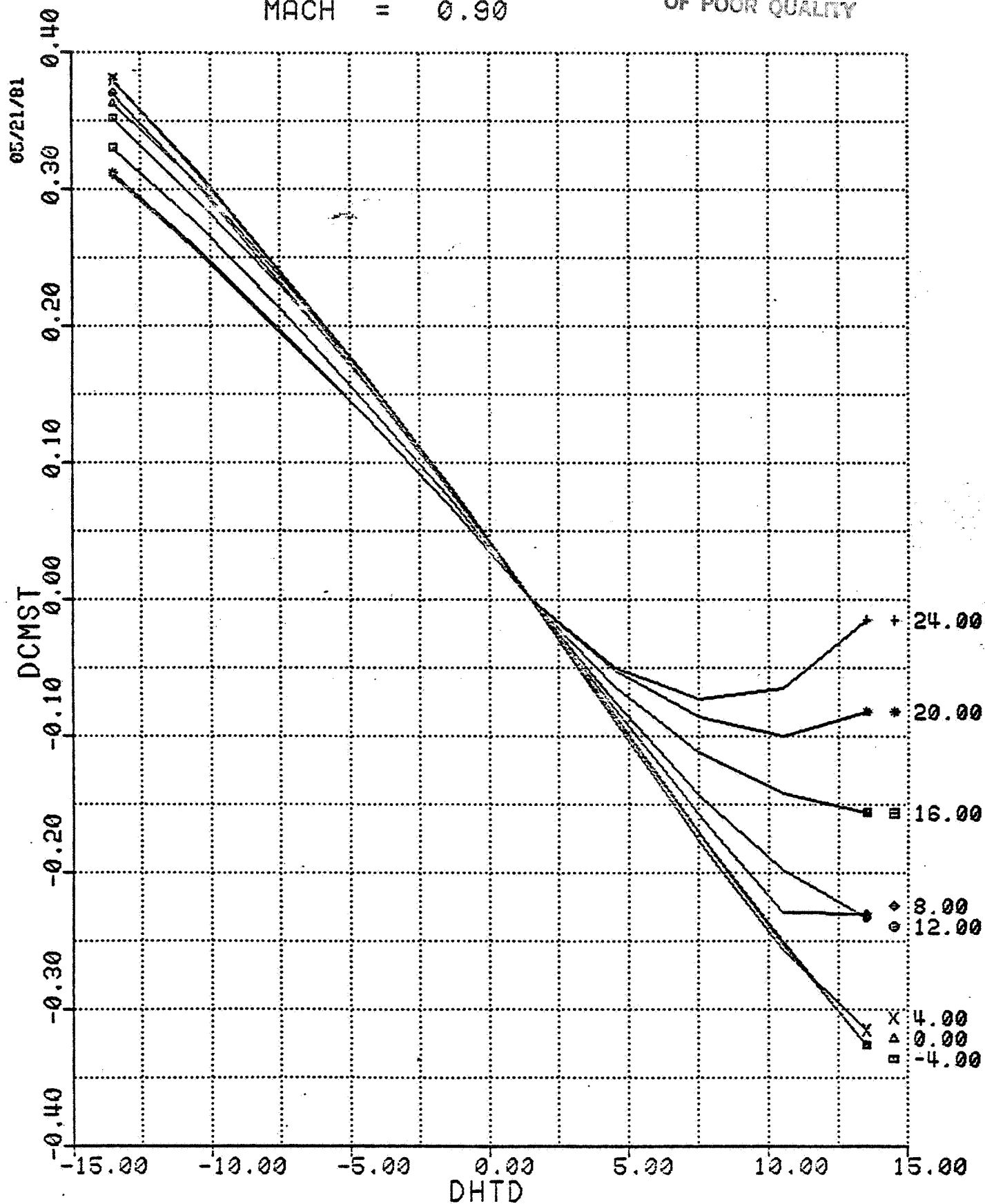
DCMST VS DHTD
FOR VARYING ALP
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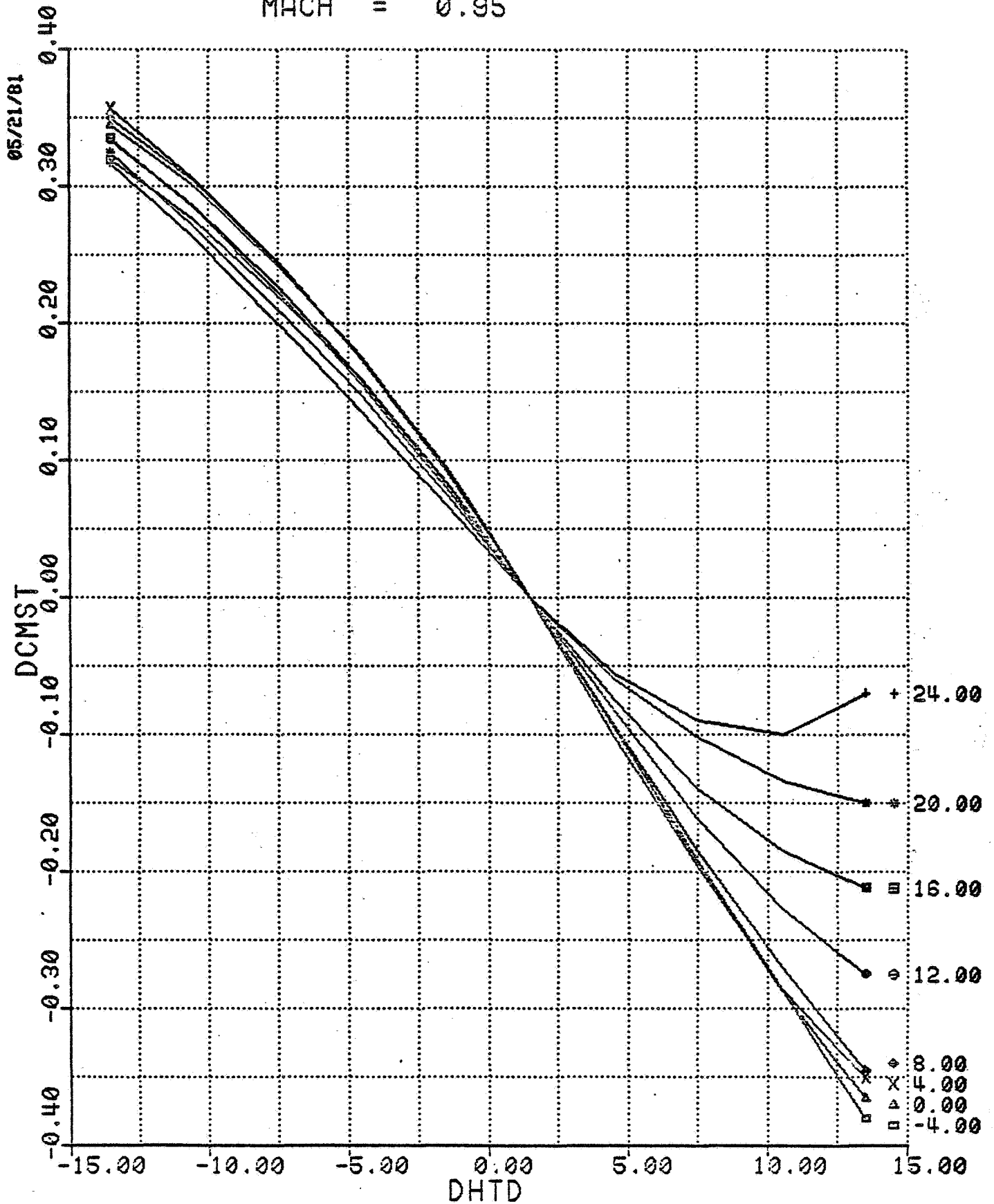
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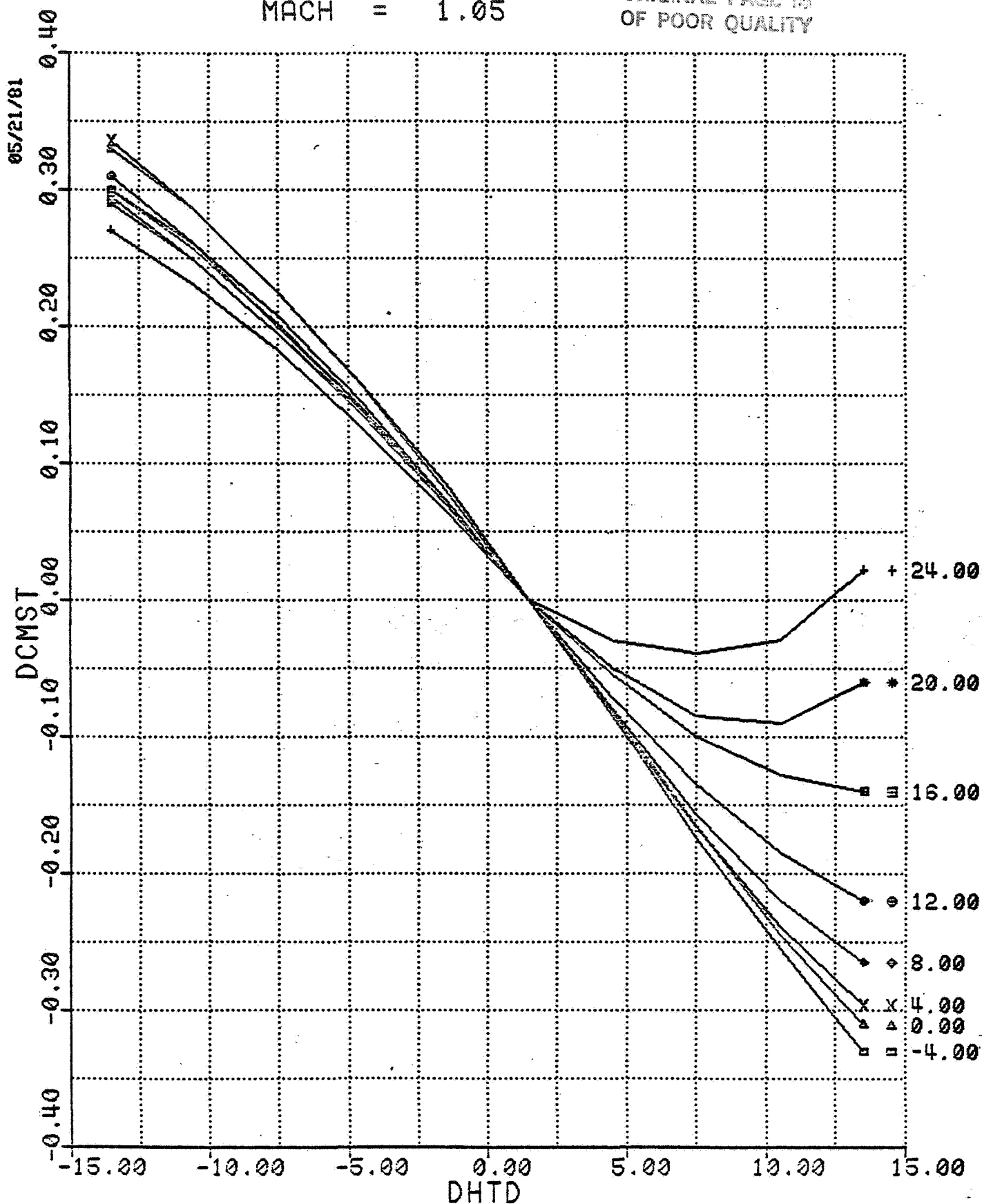
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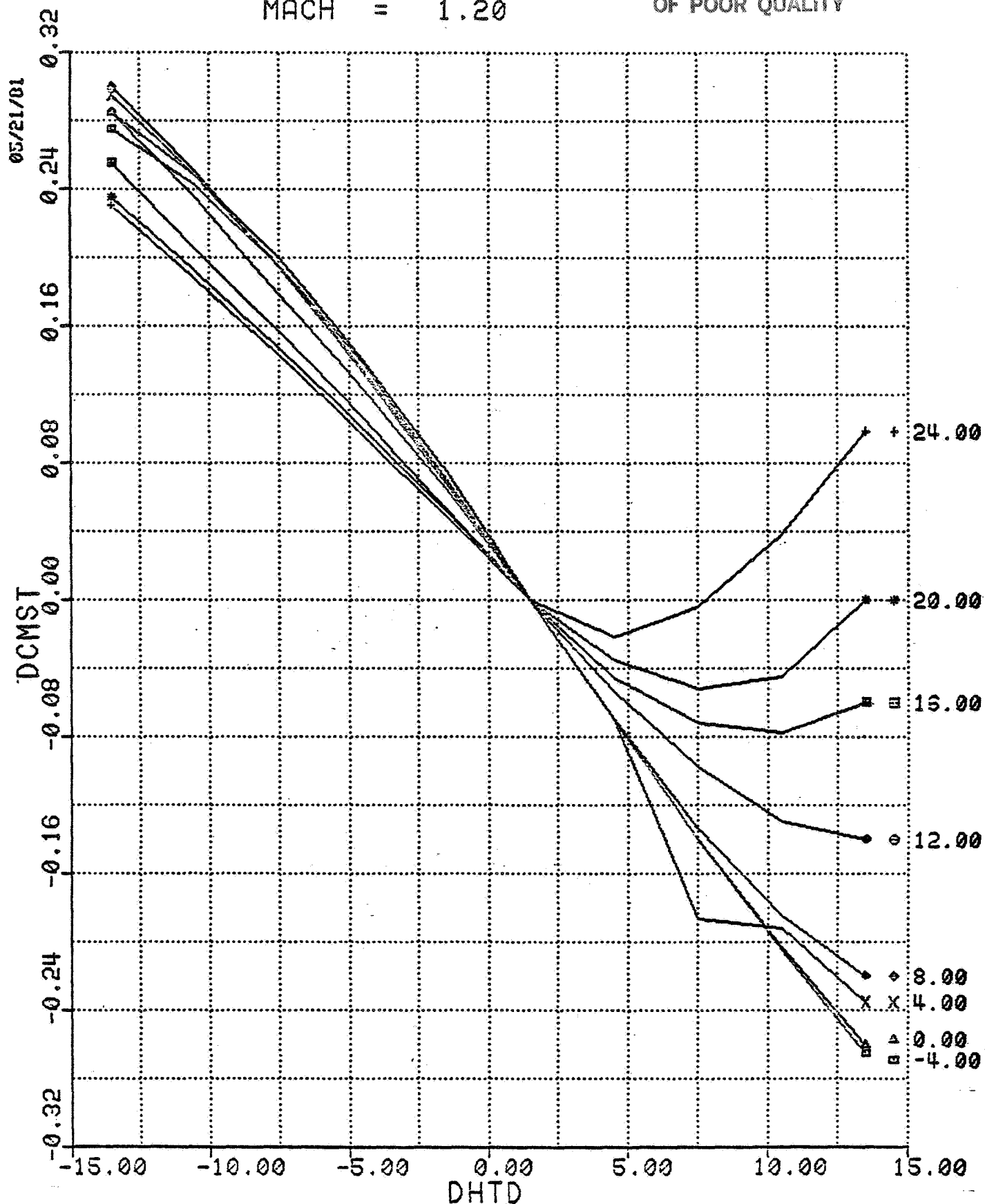
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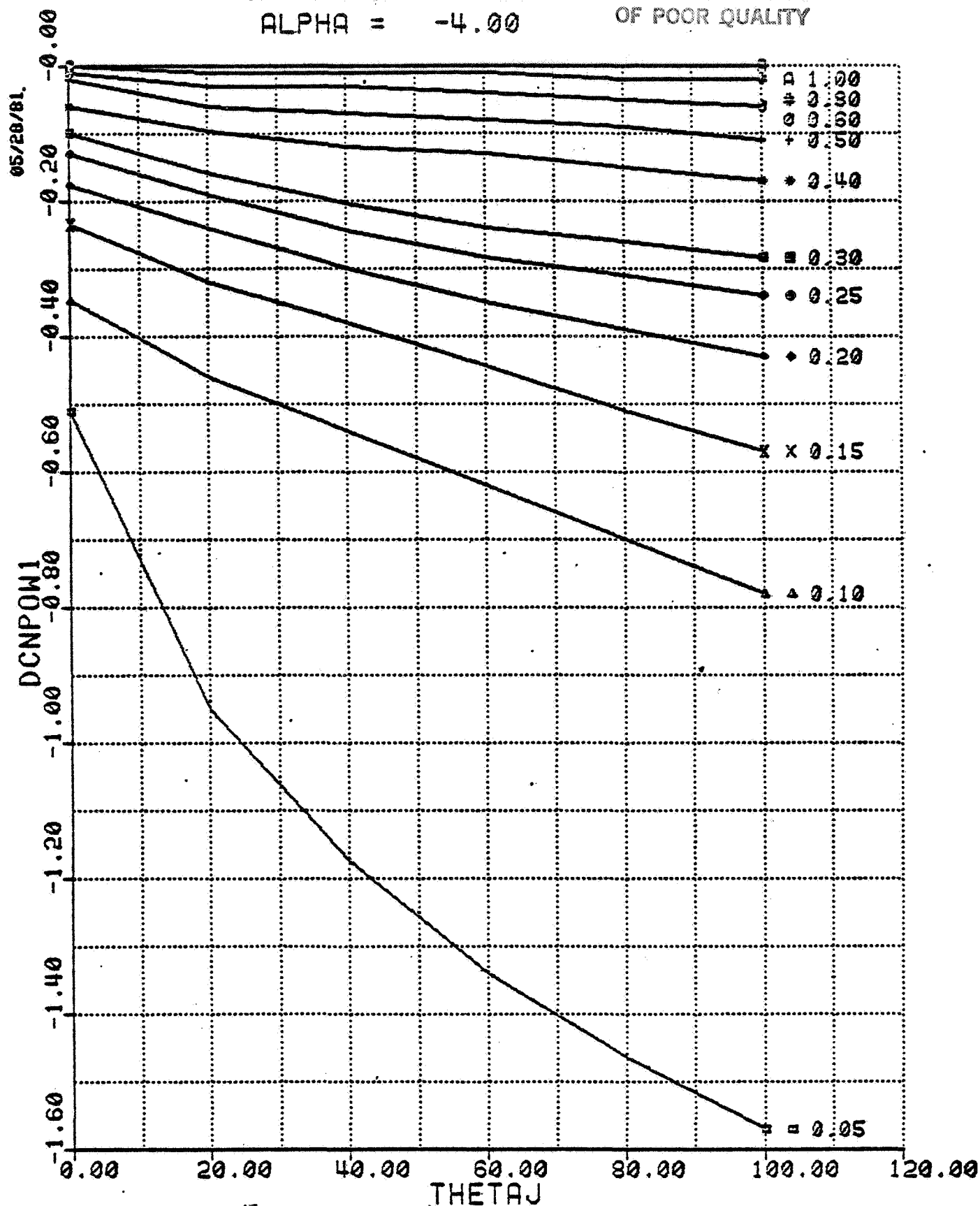
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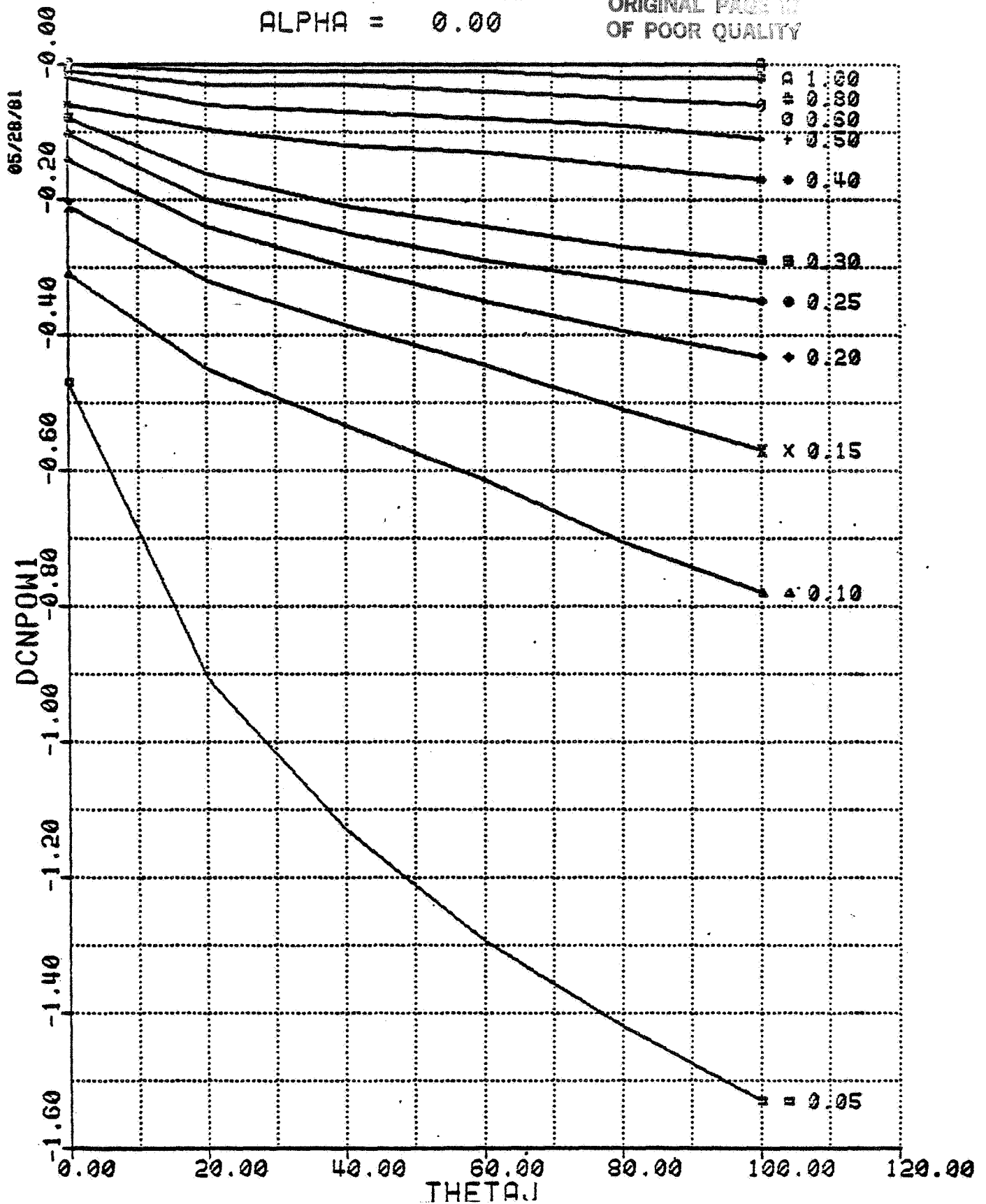
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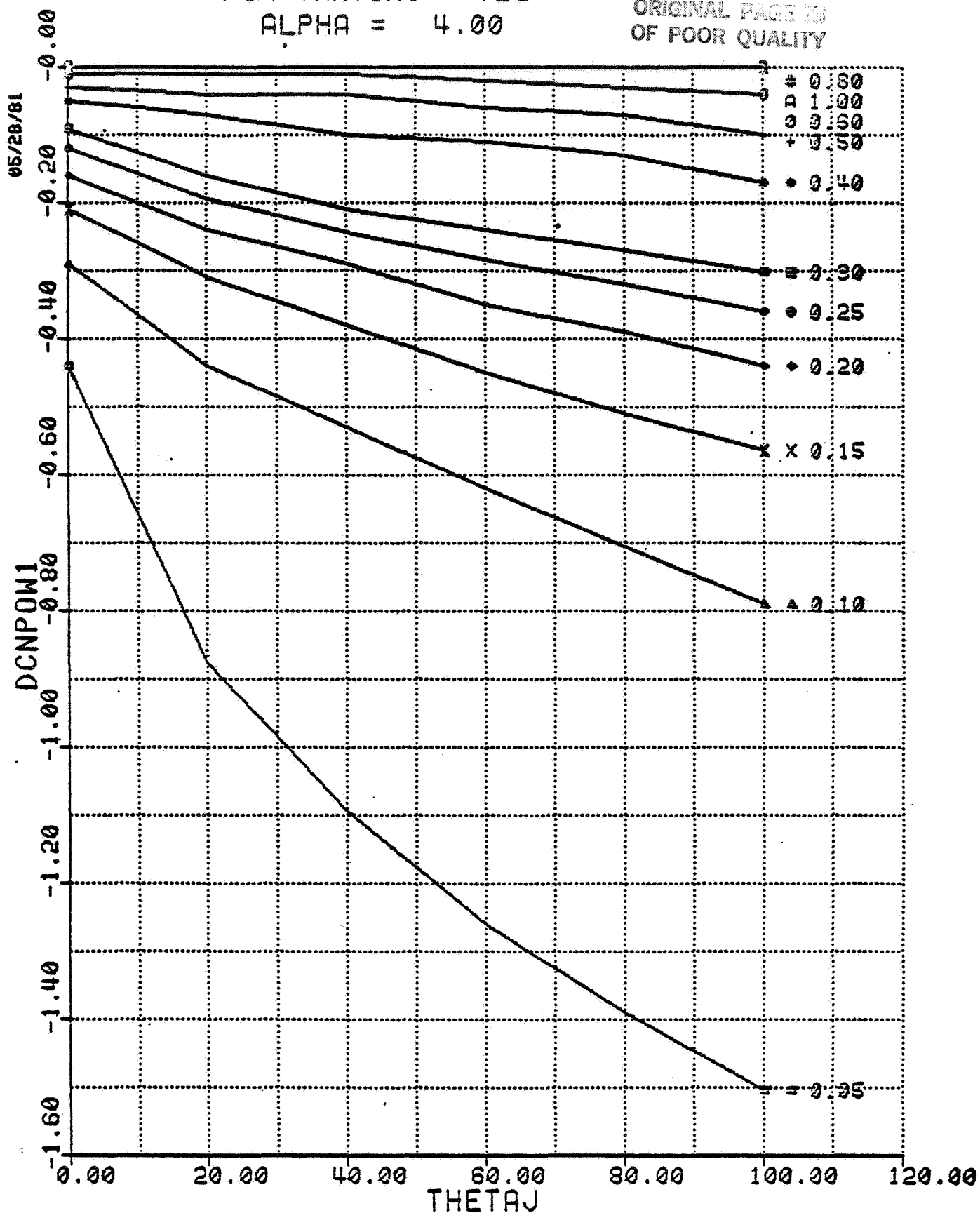
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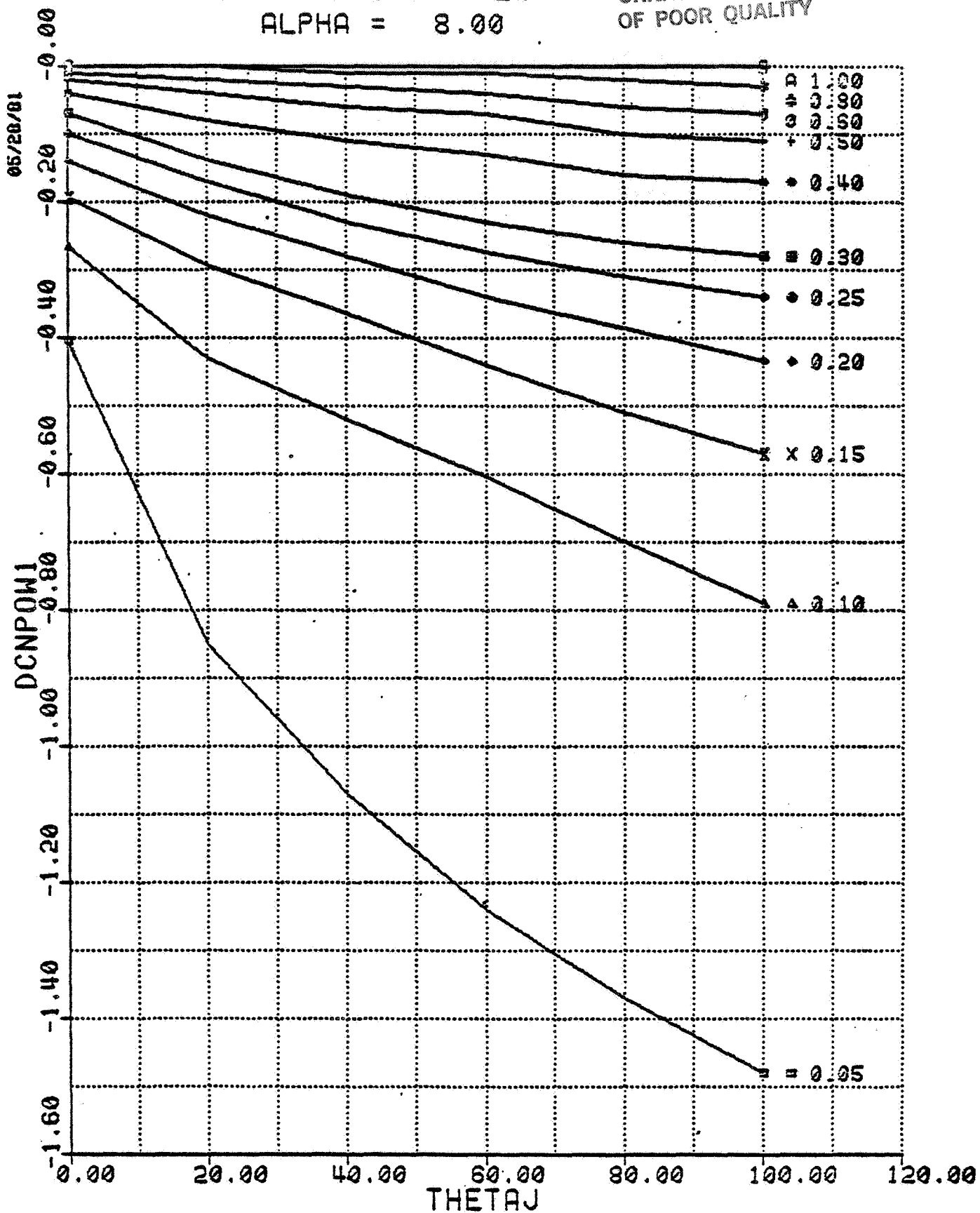
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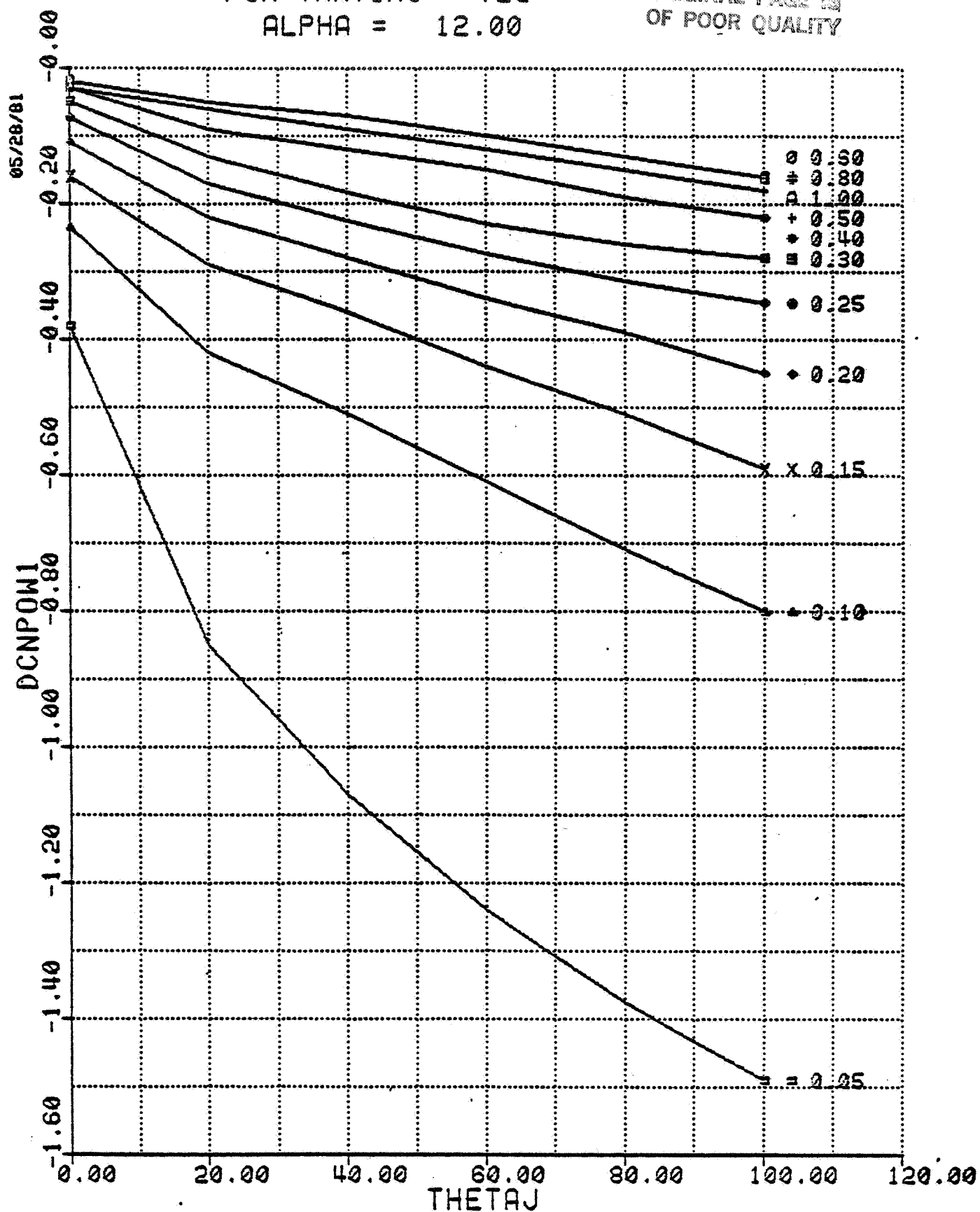
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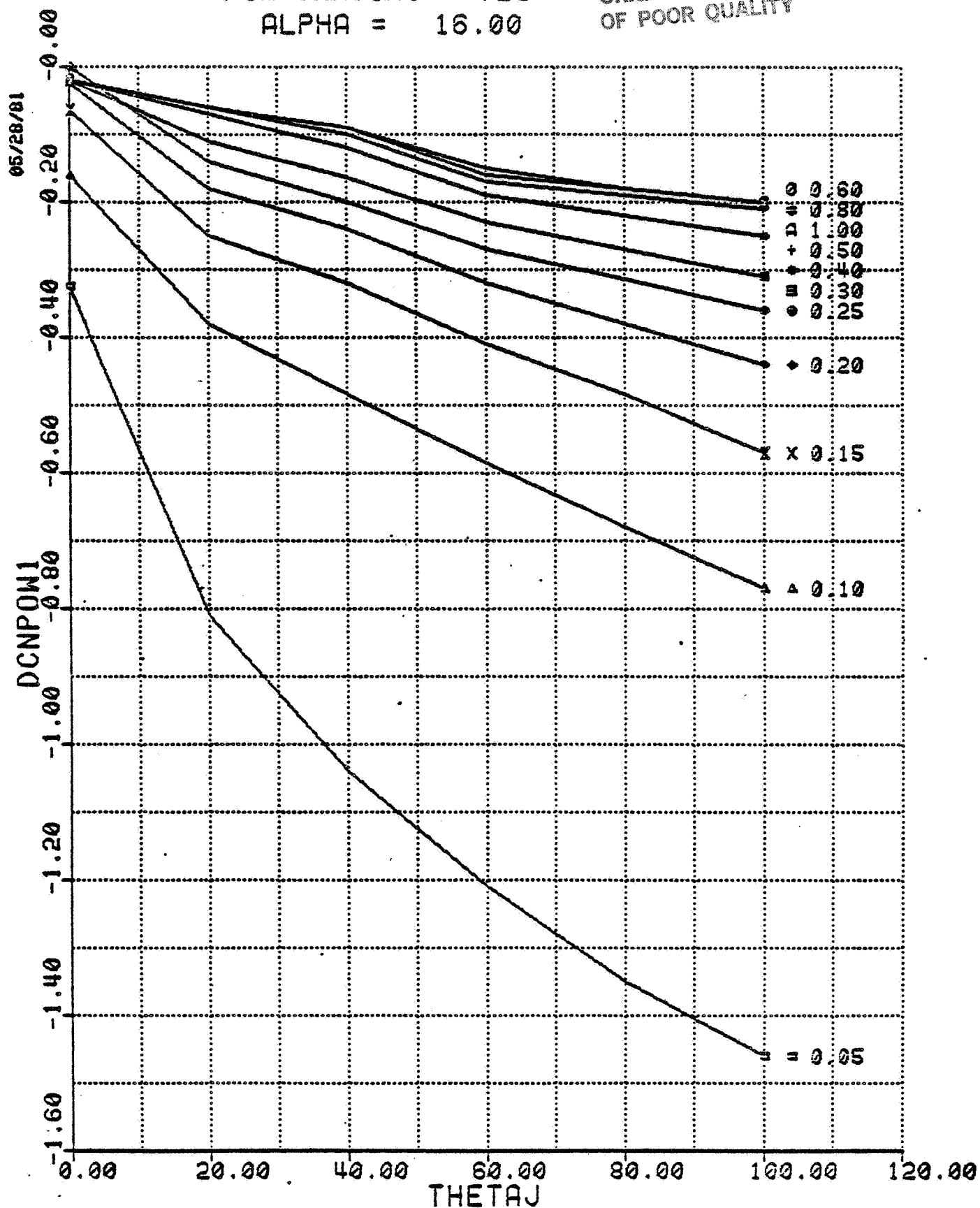
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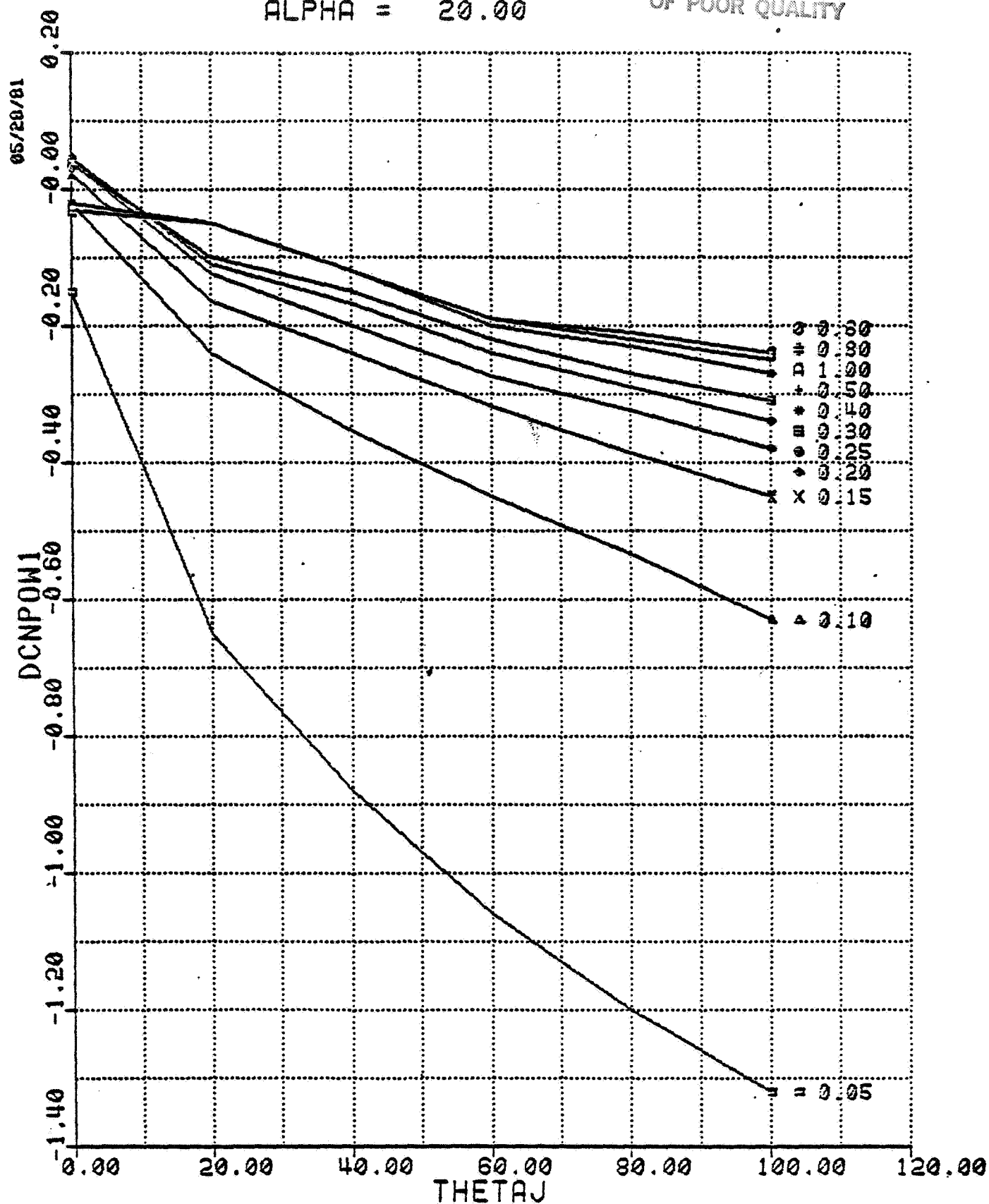
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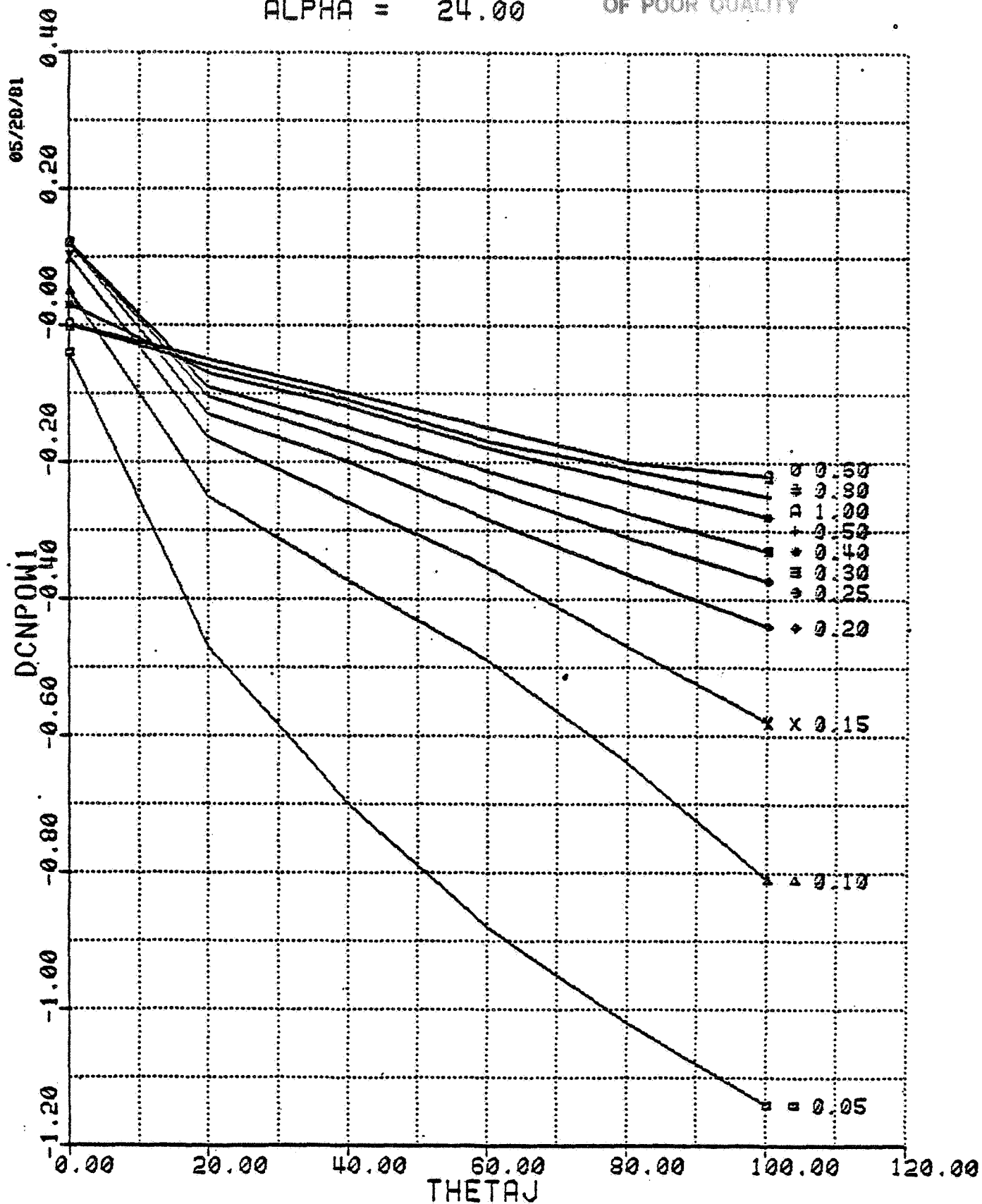
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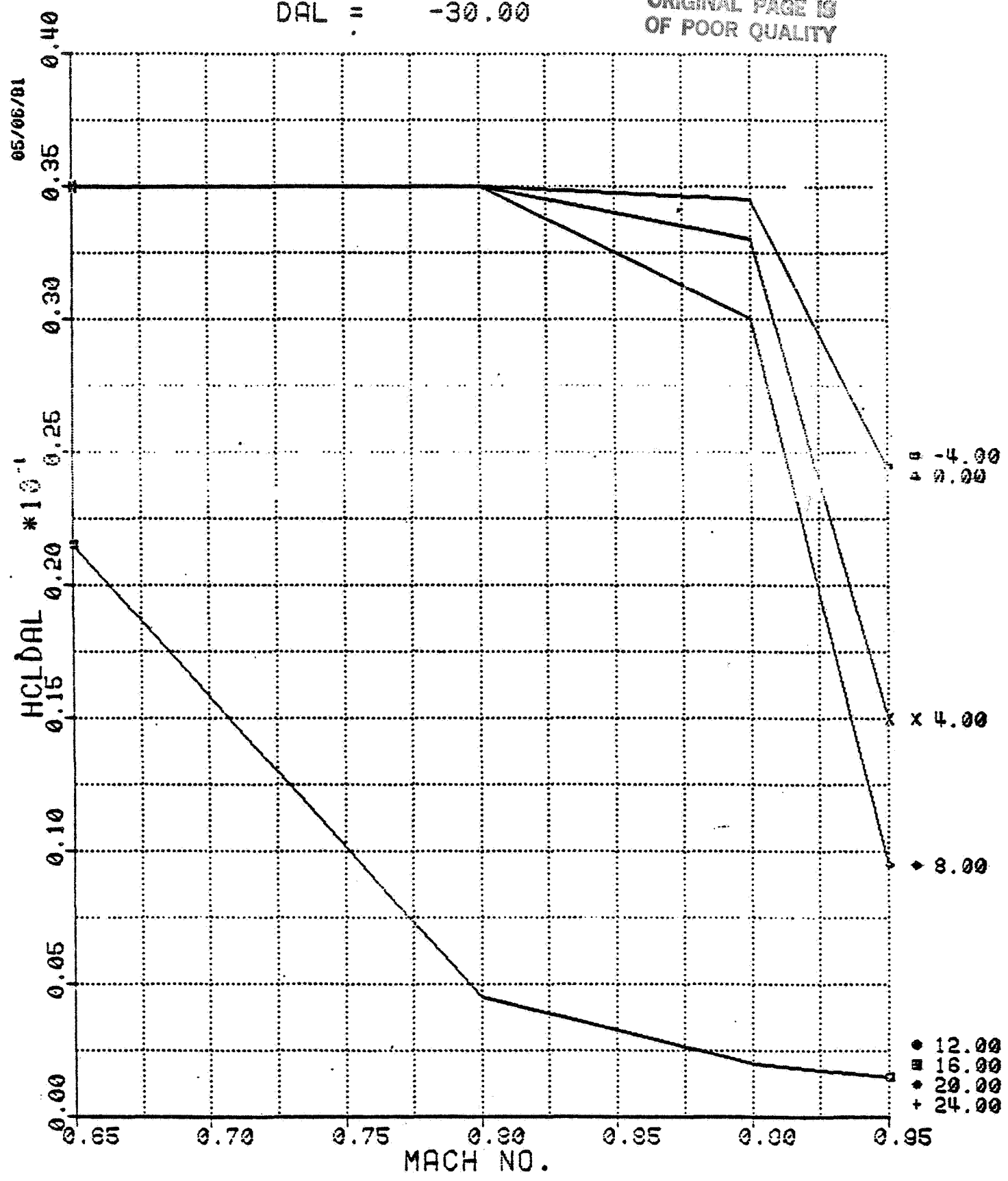
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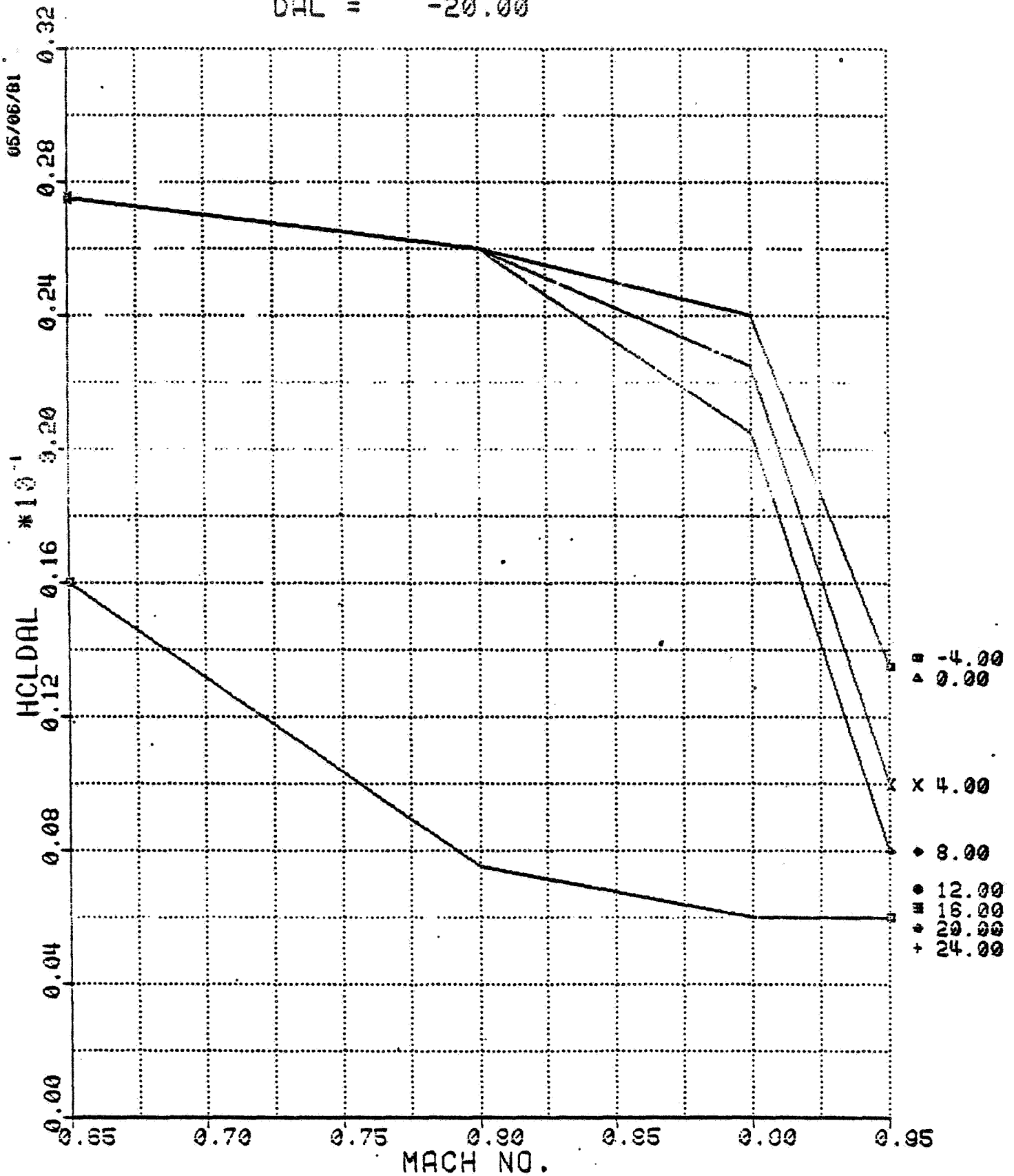
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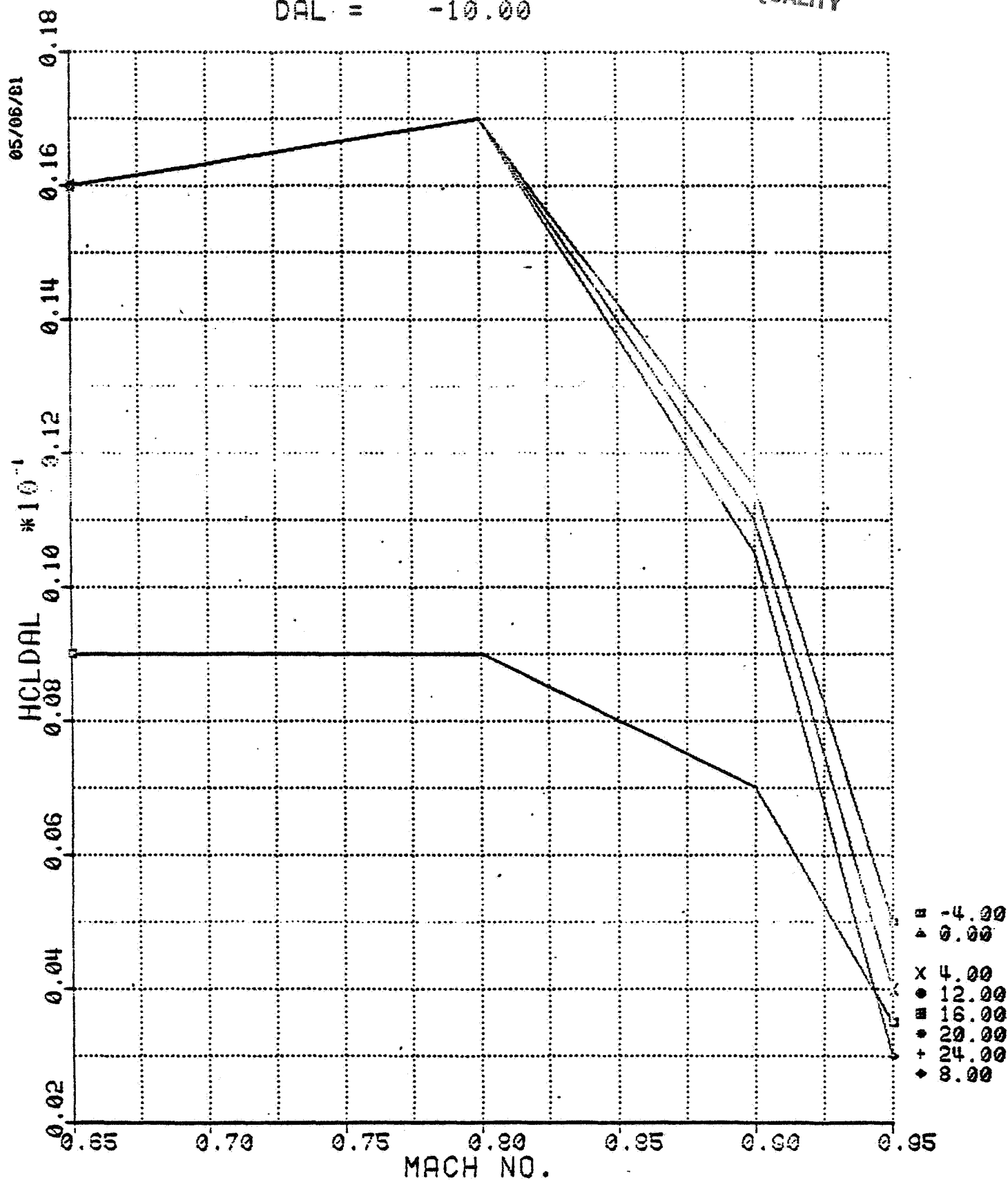
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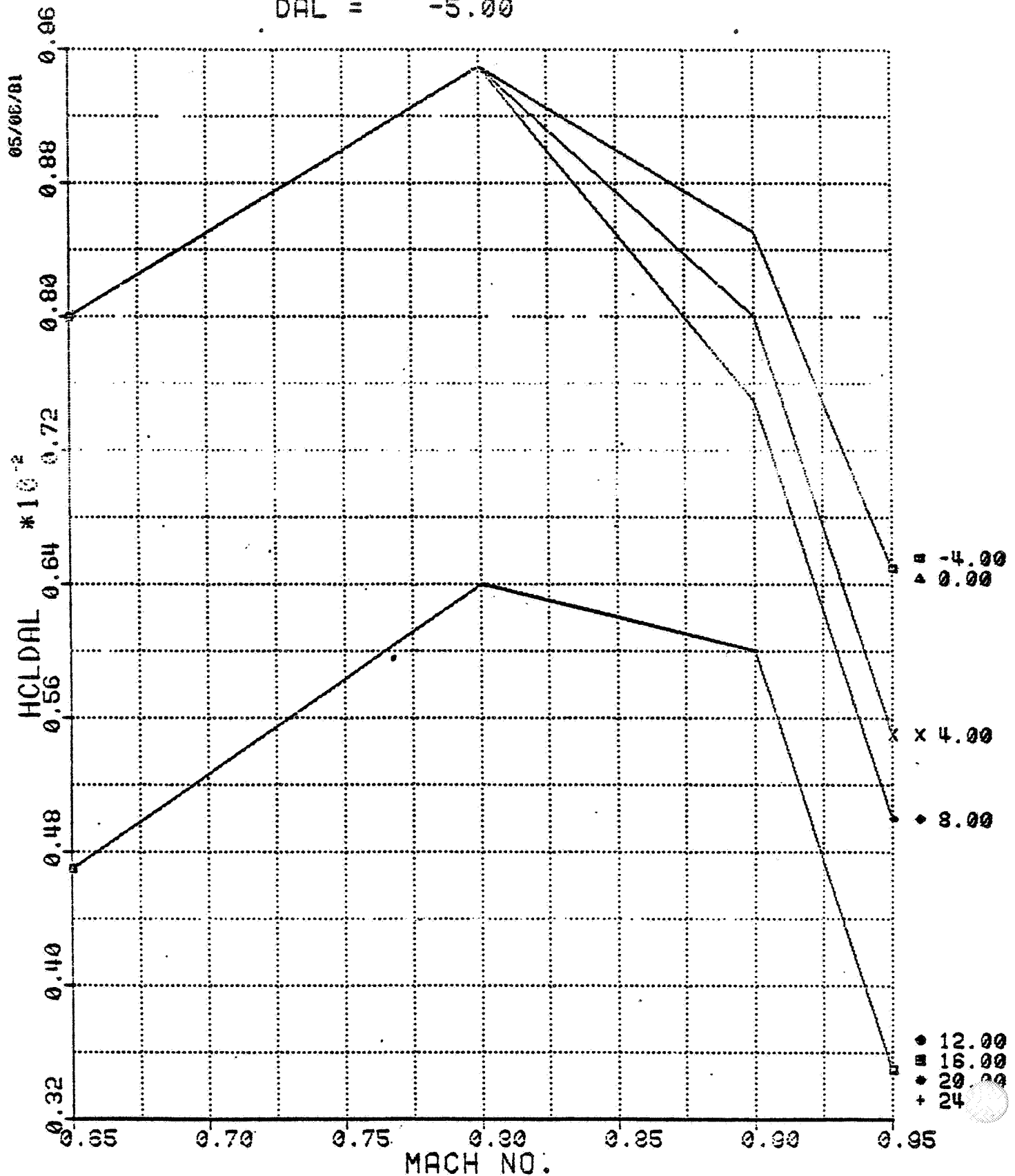


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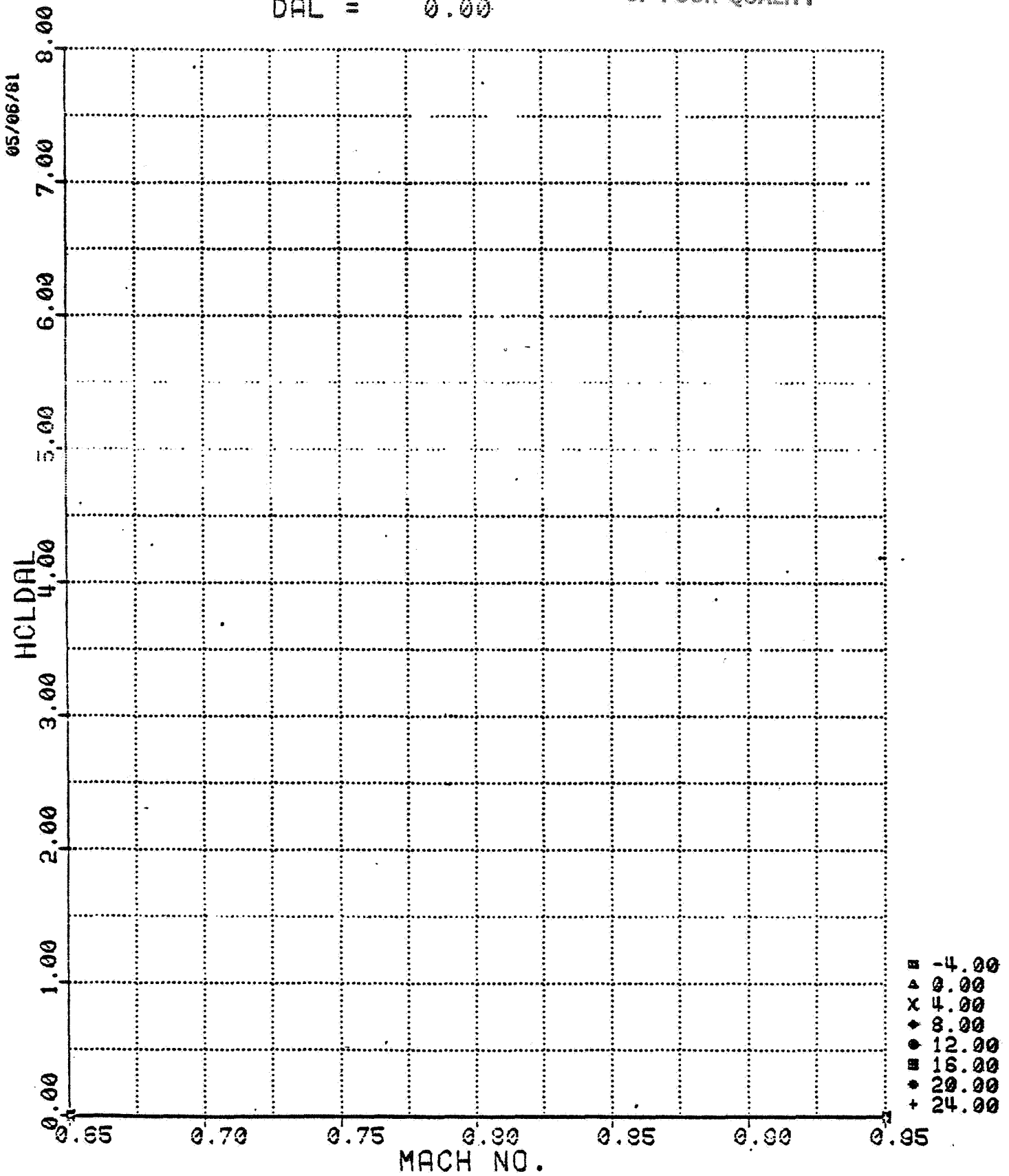


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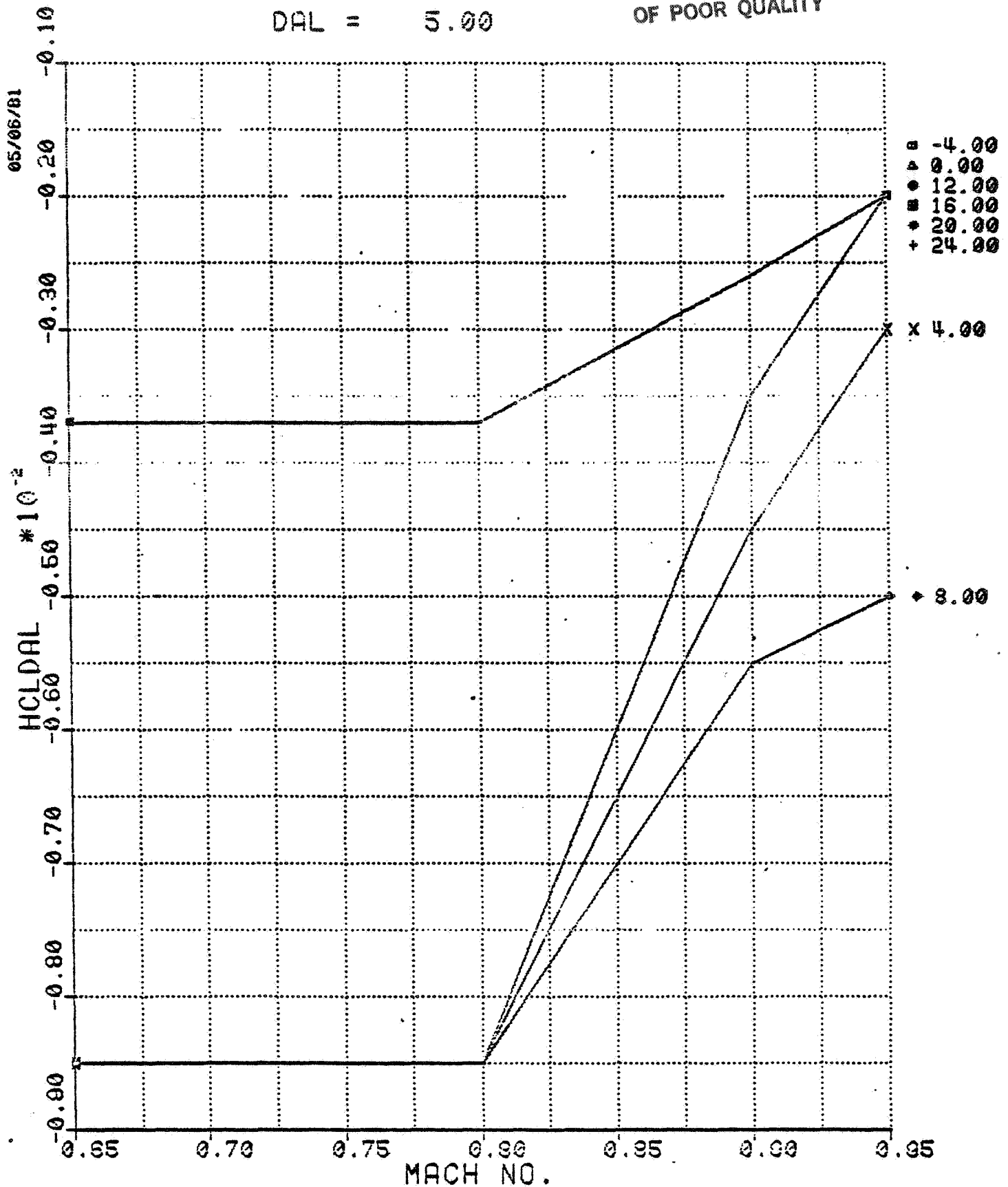
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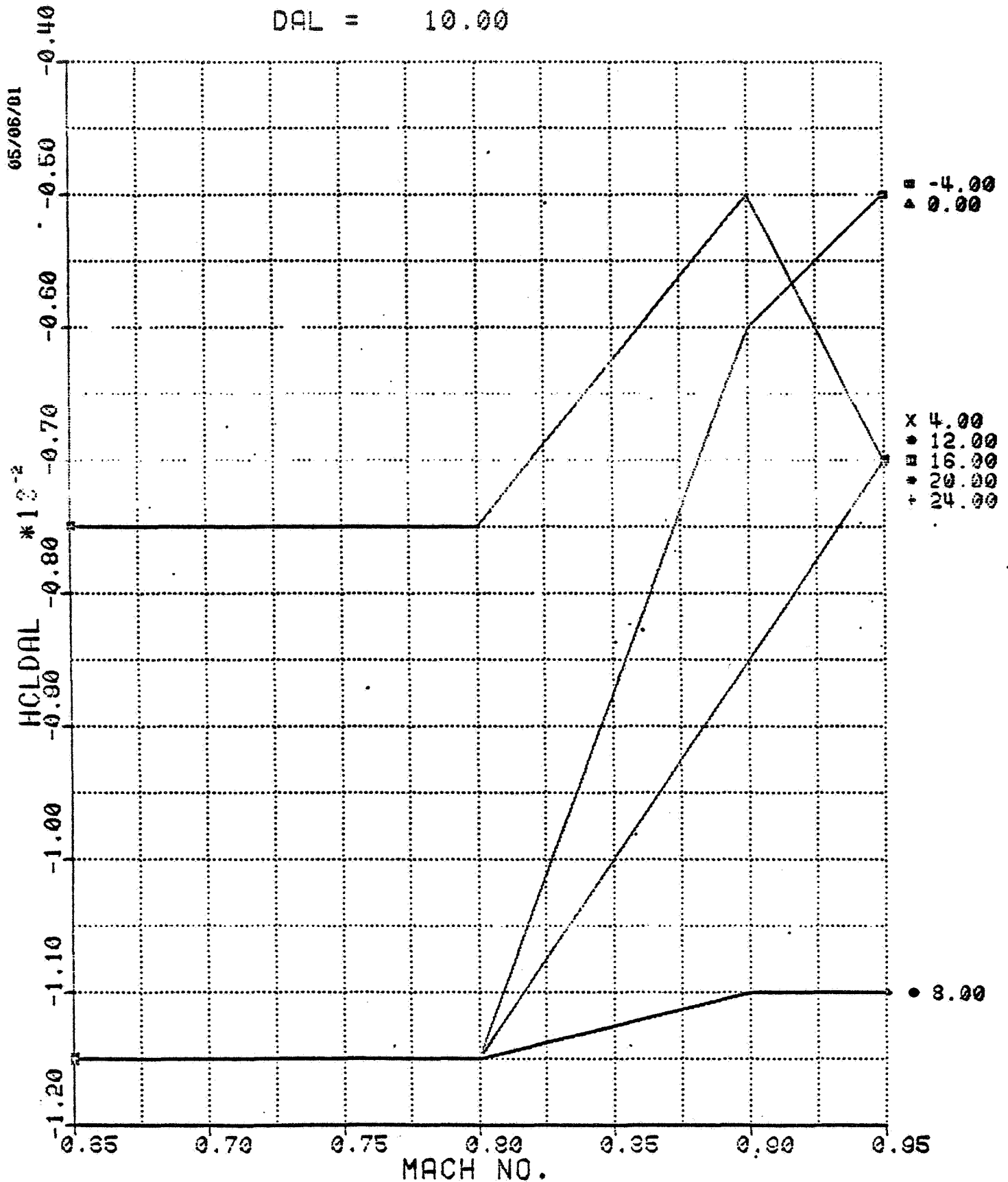


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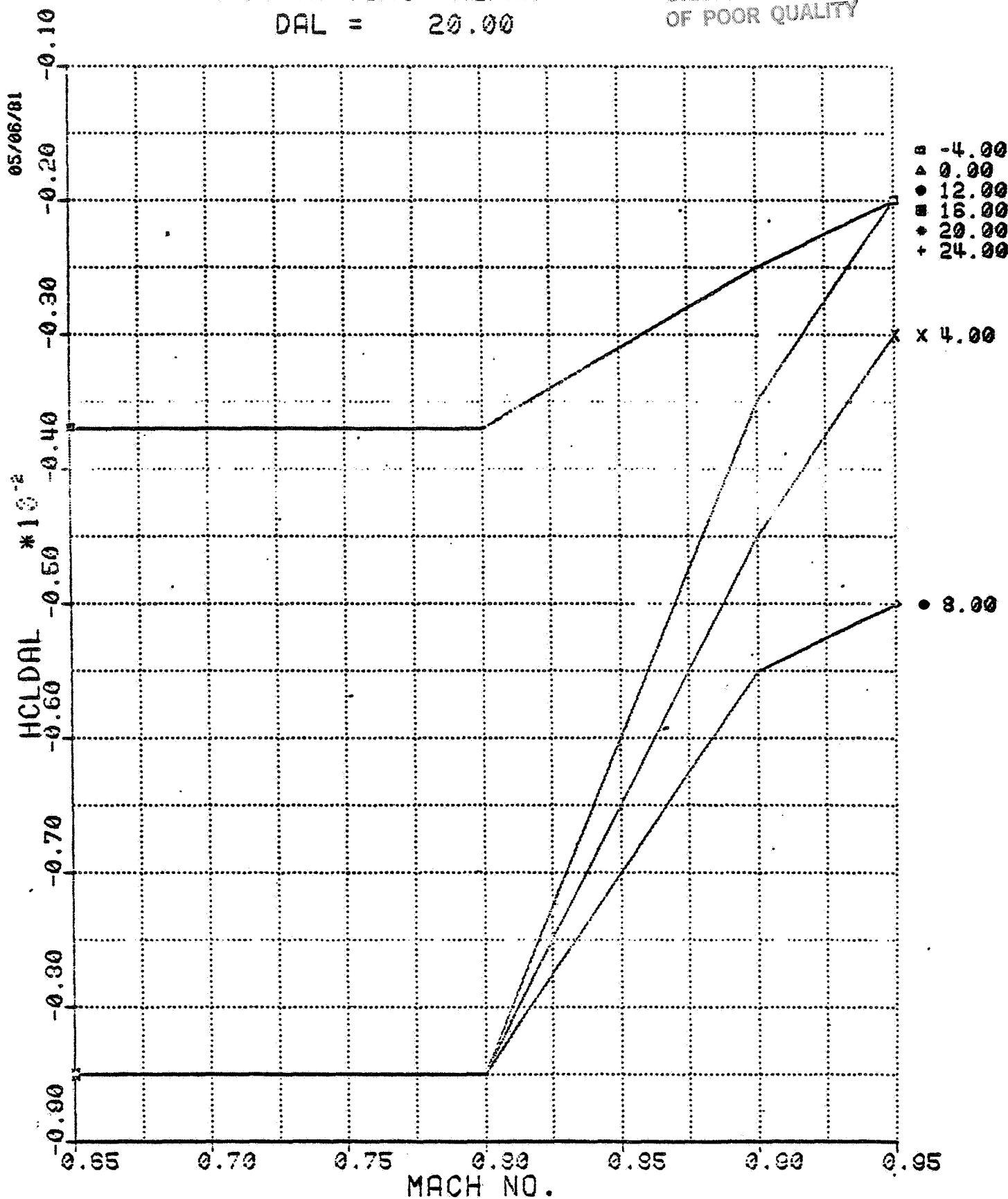


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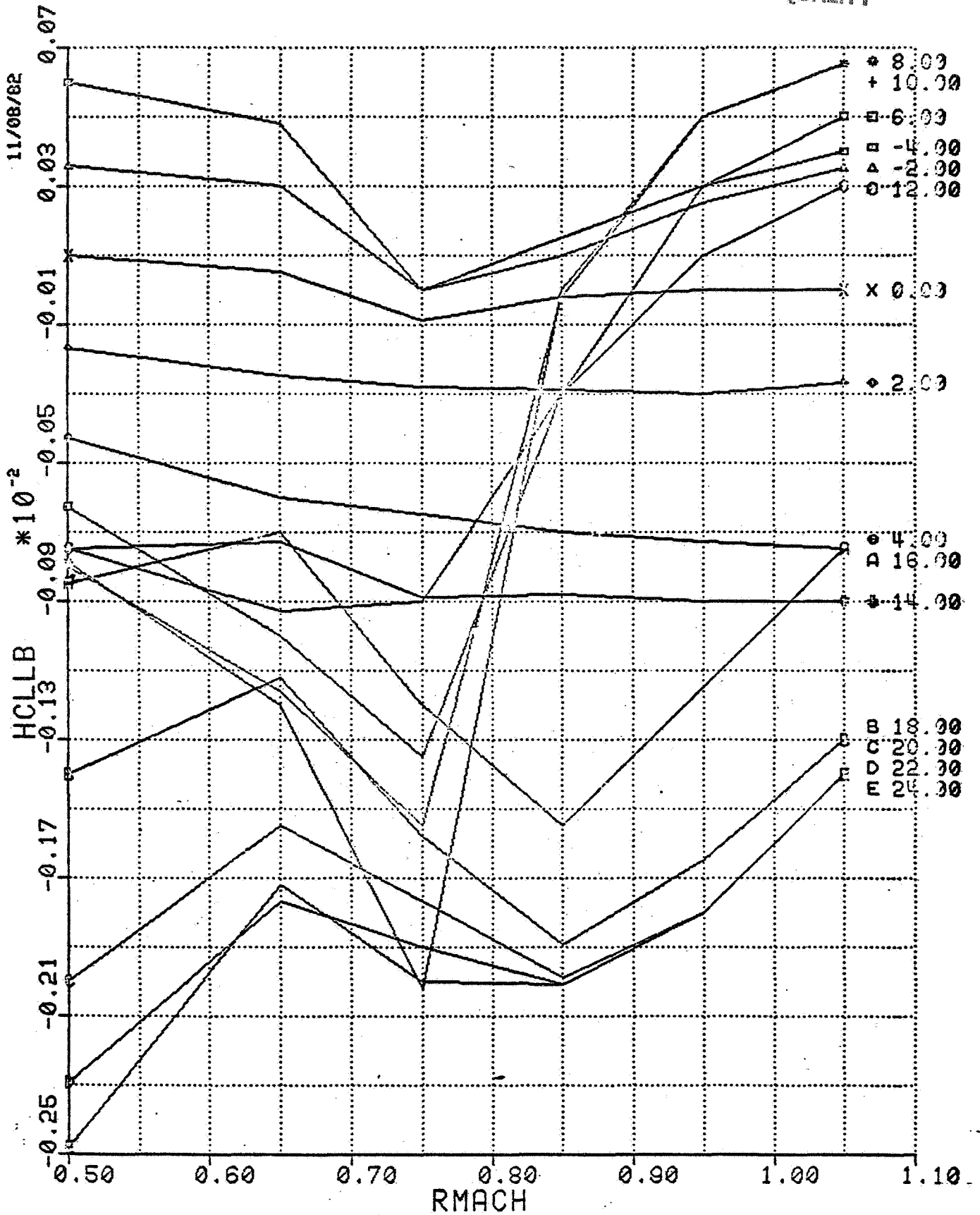
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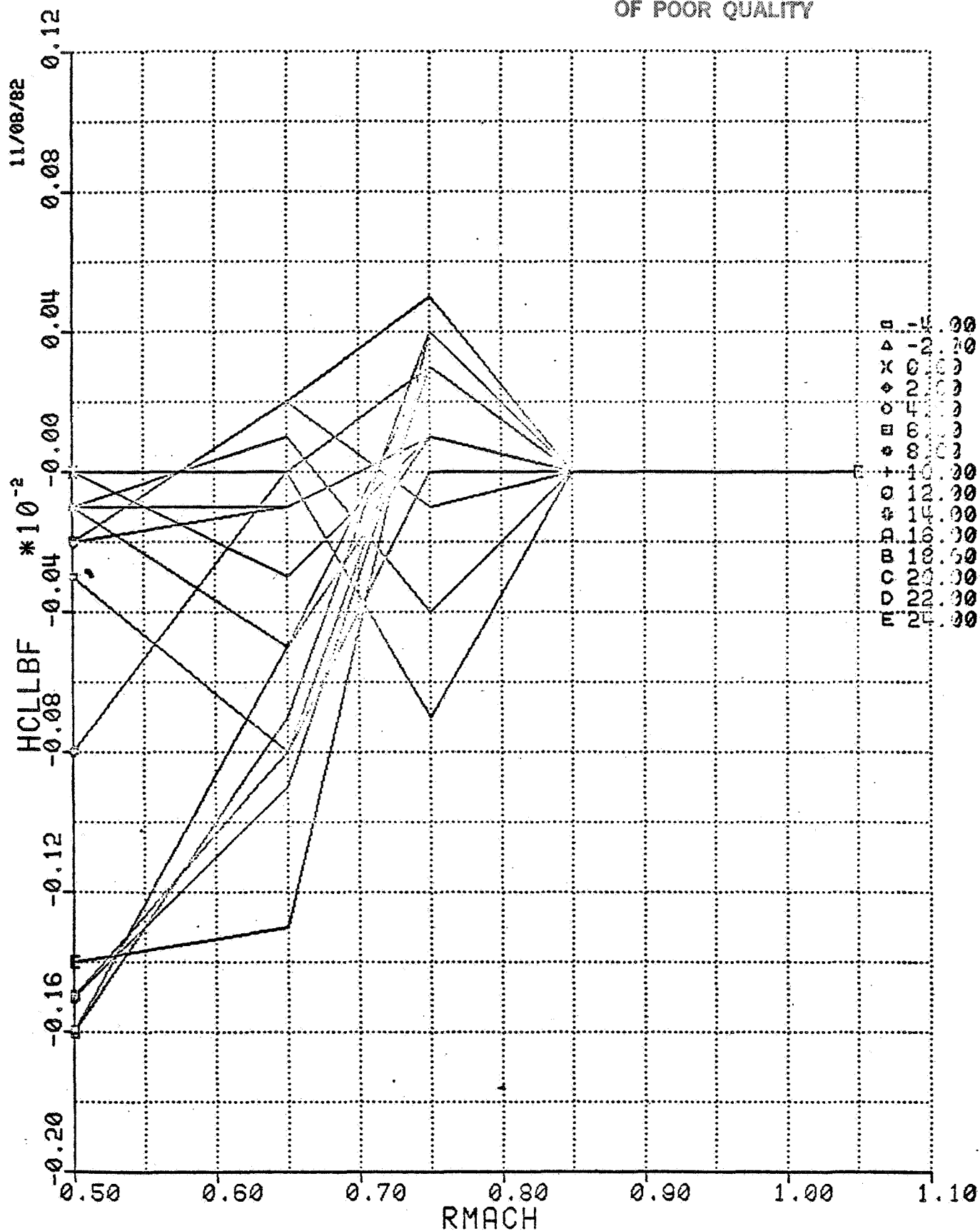
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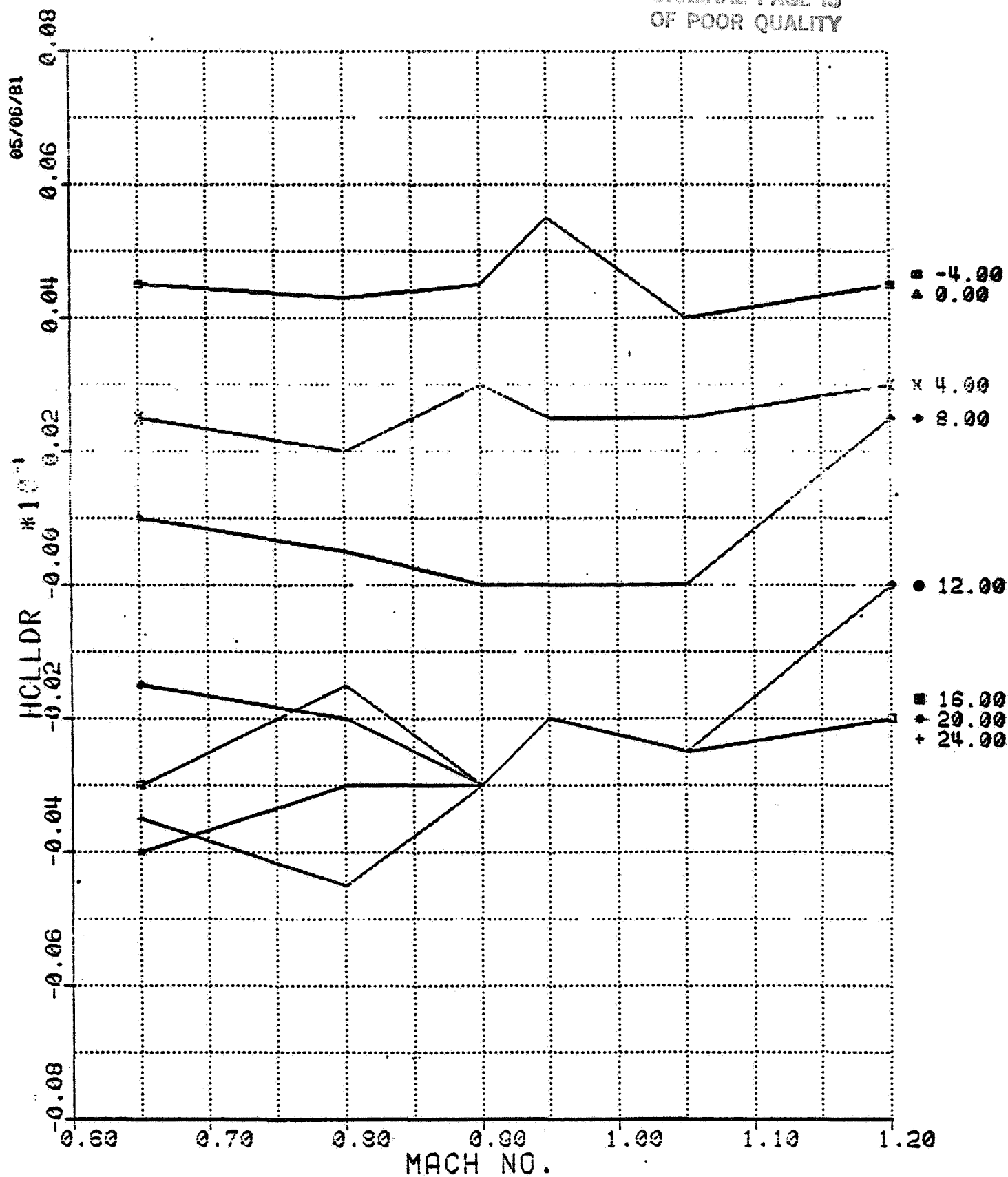
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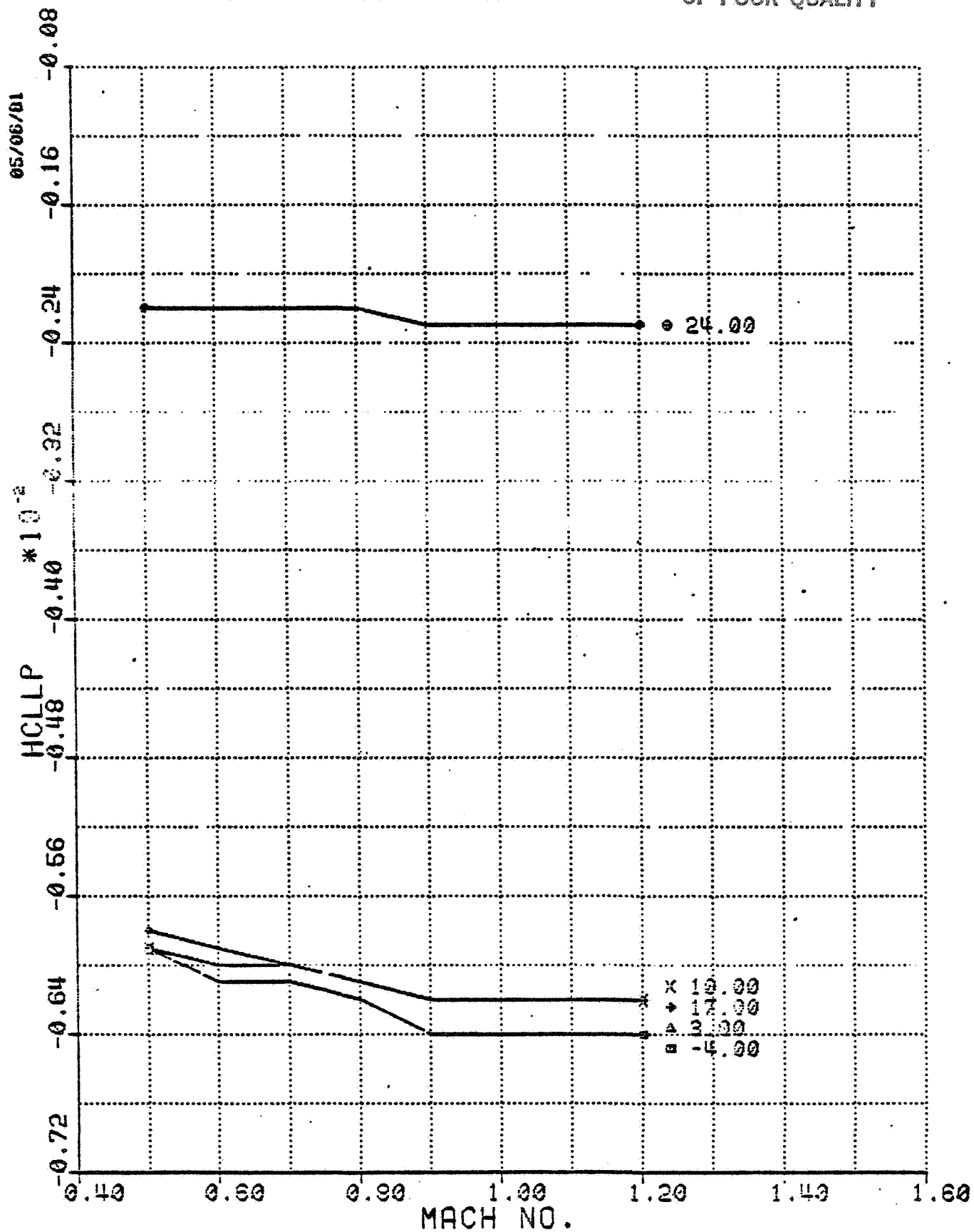
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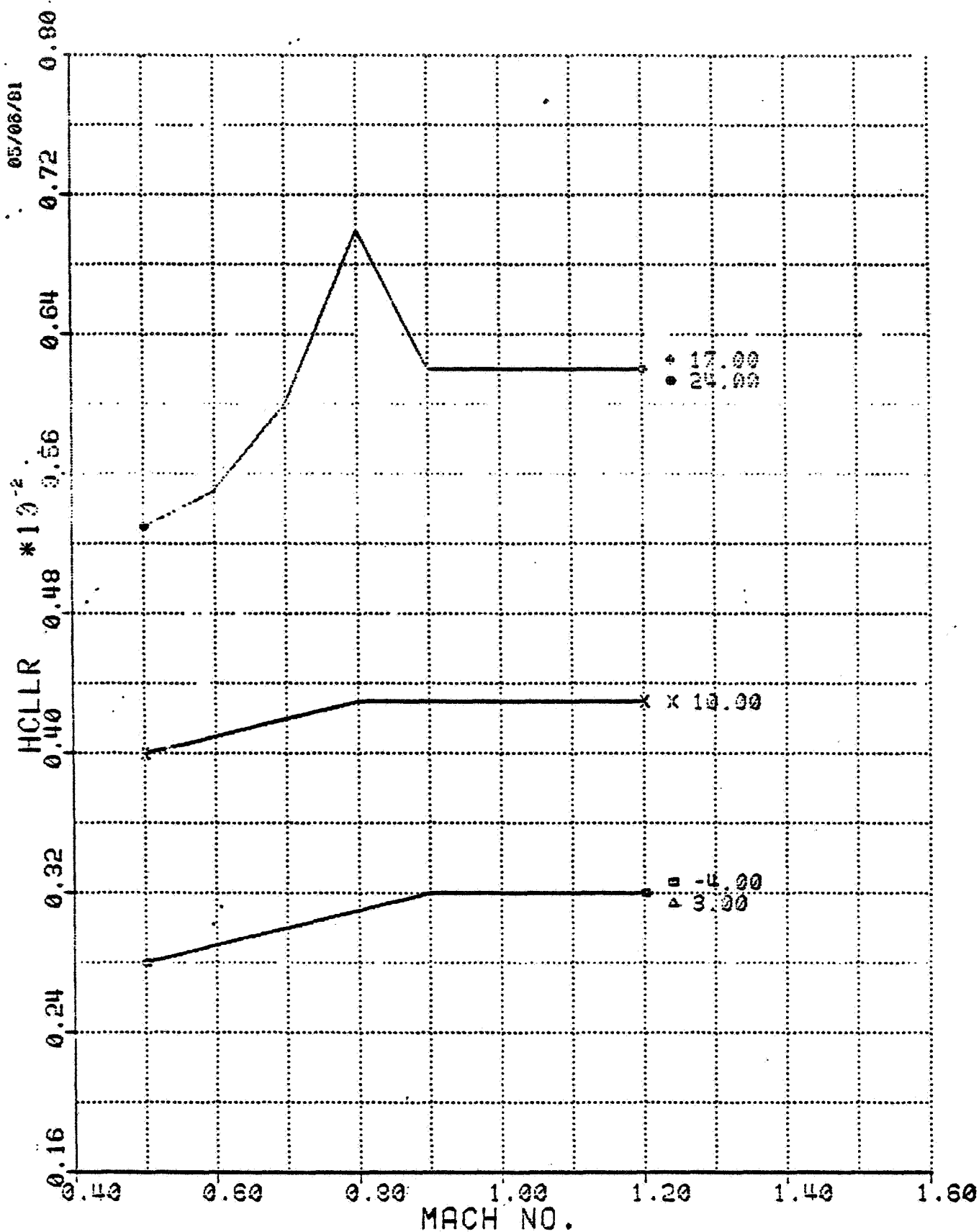
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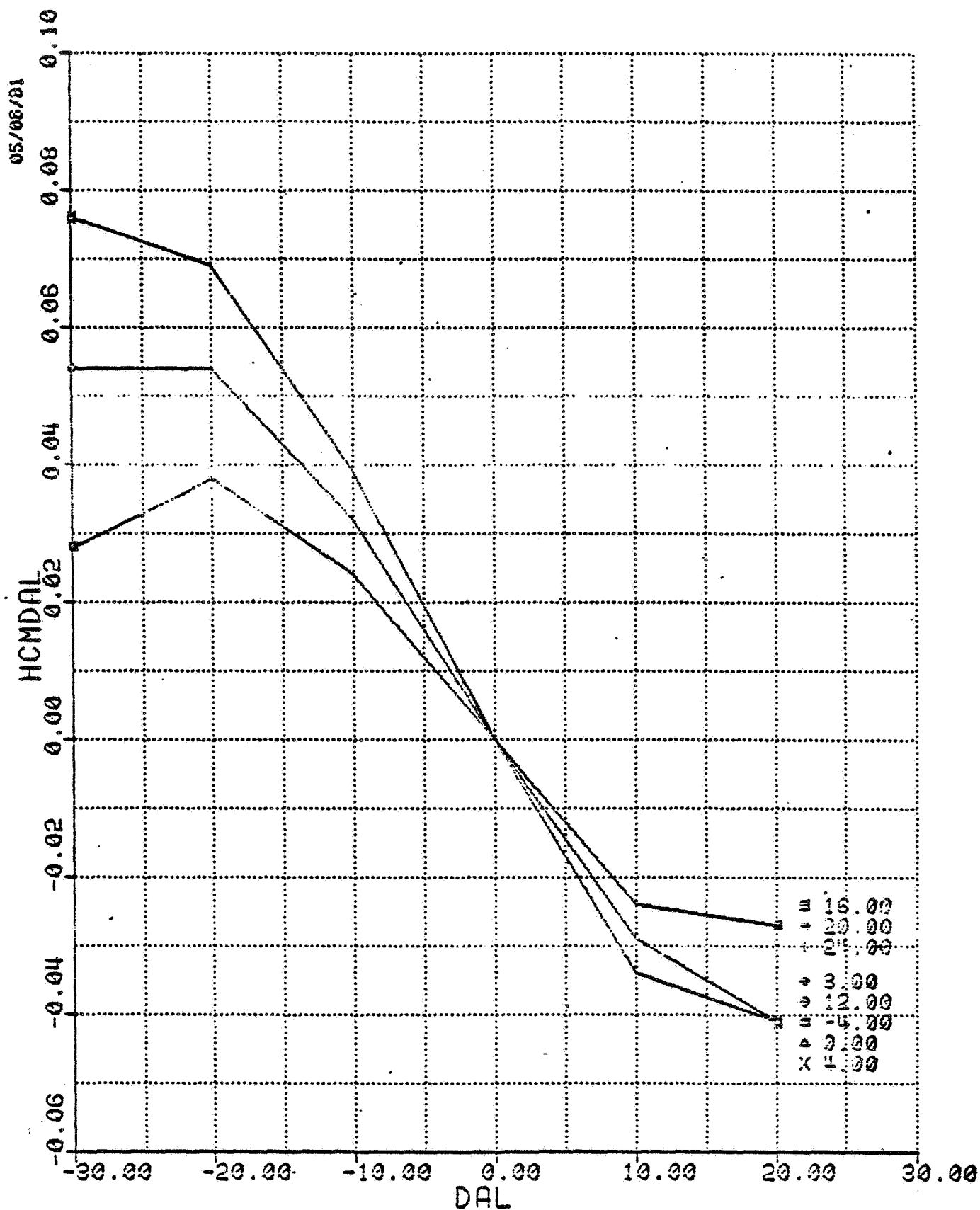
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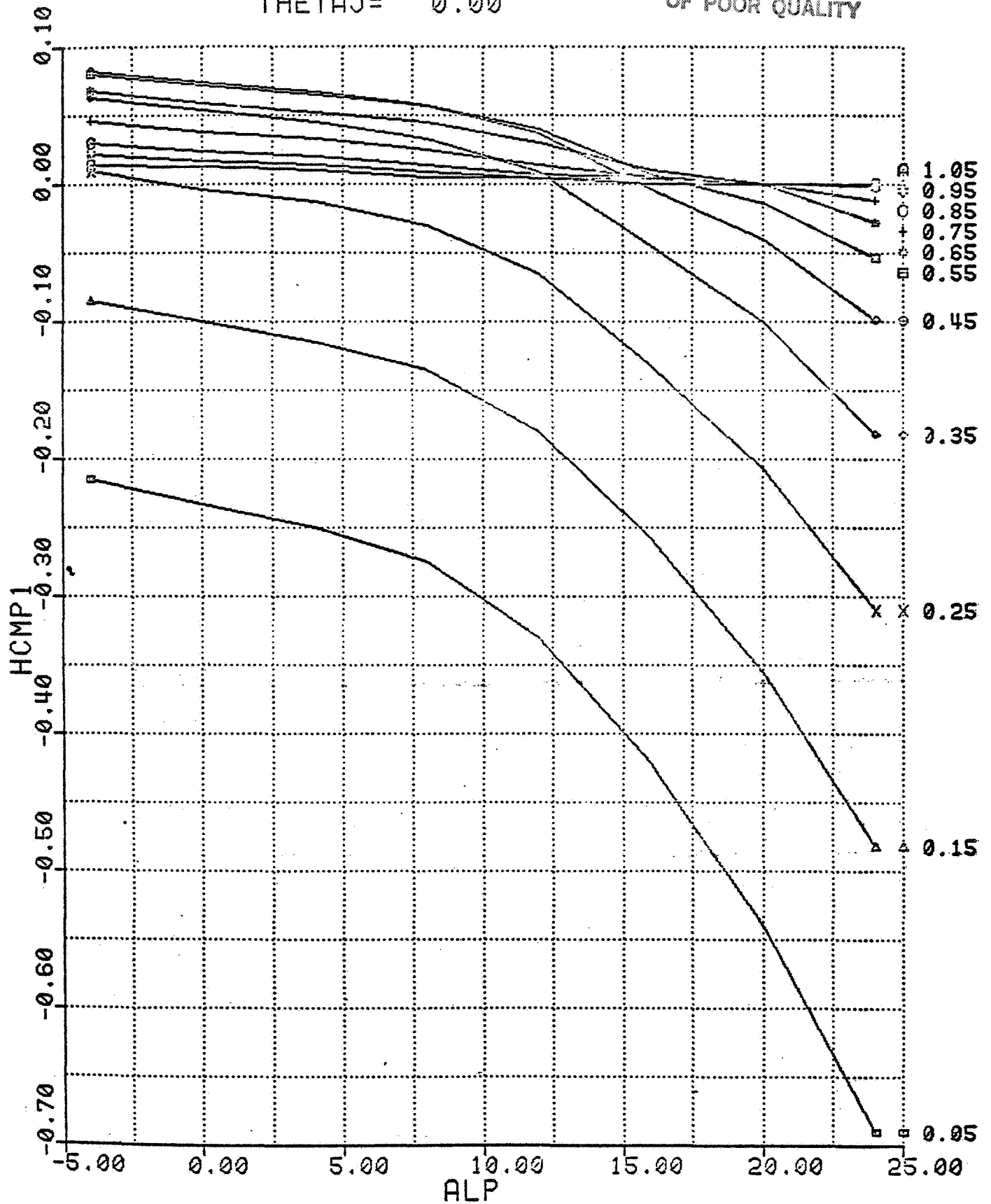
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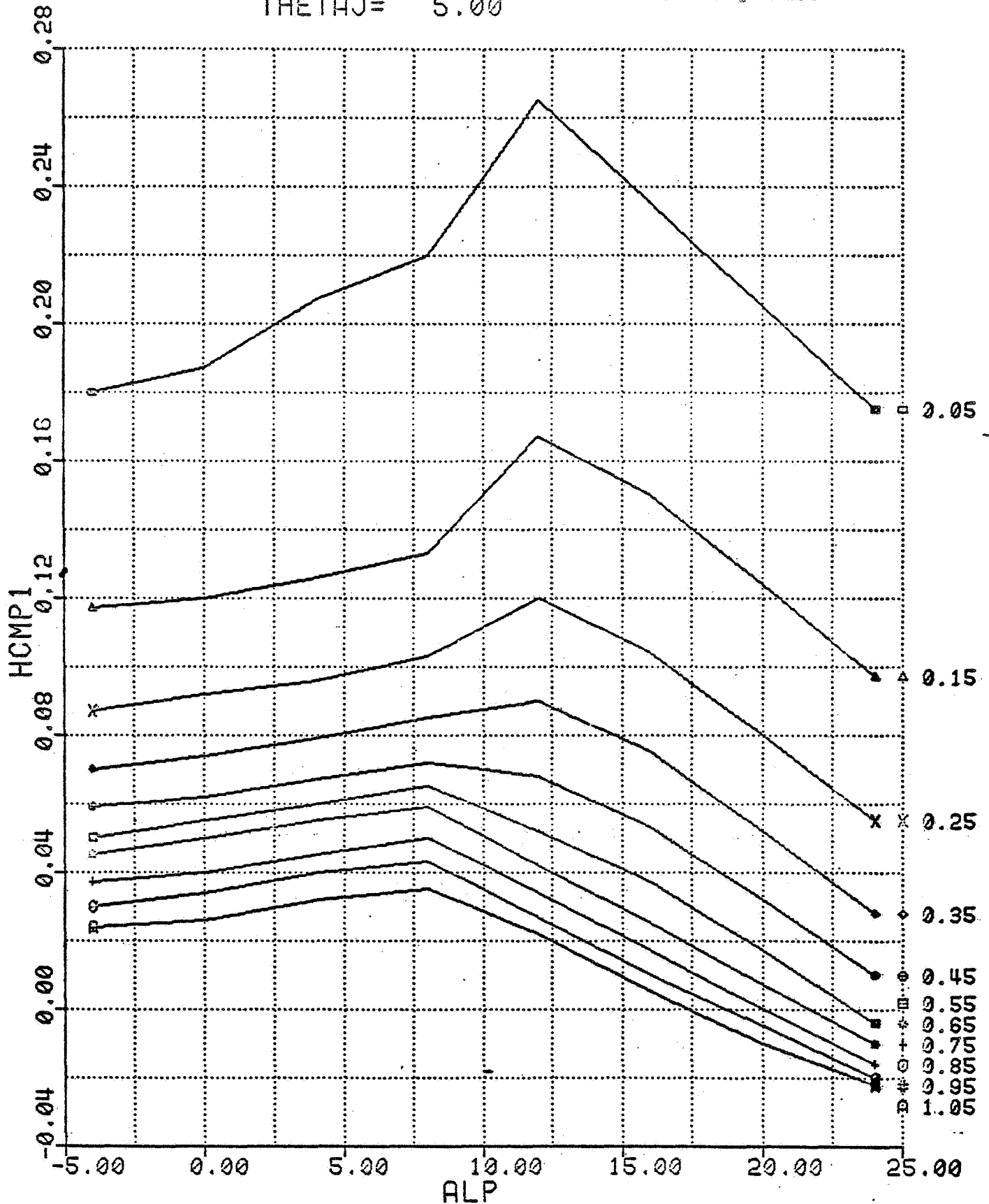
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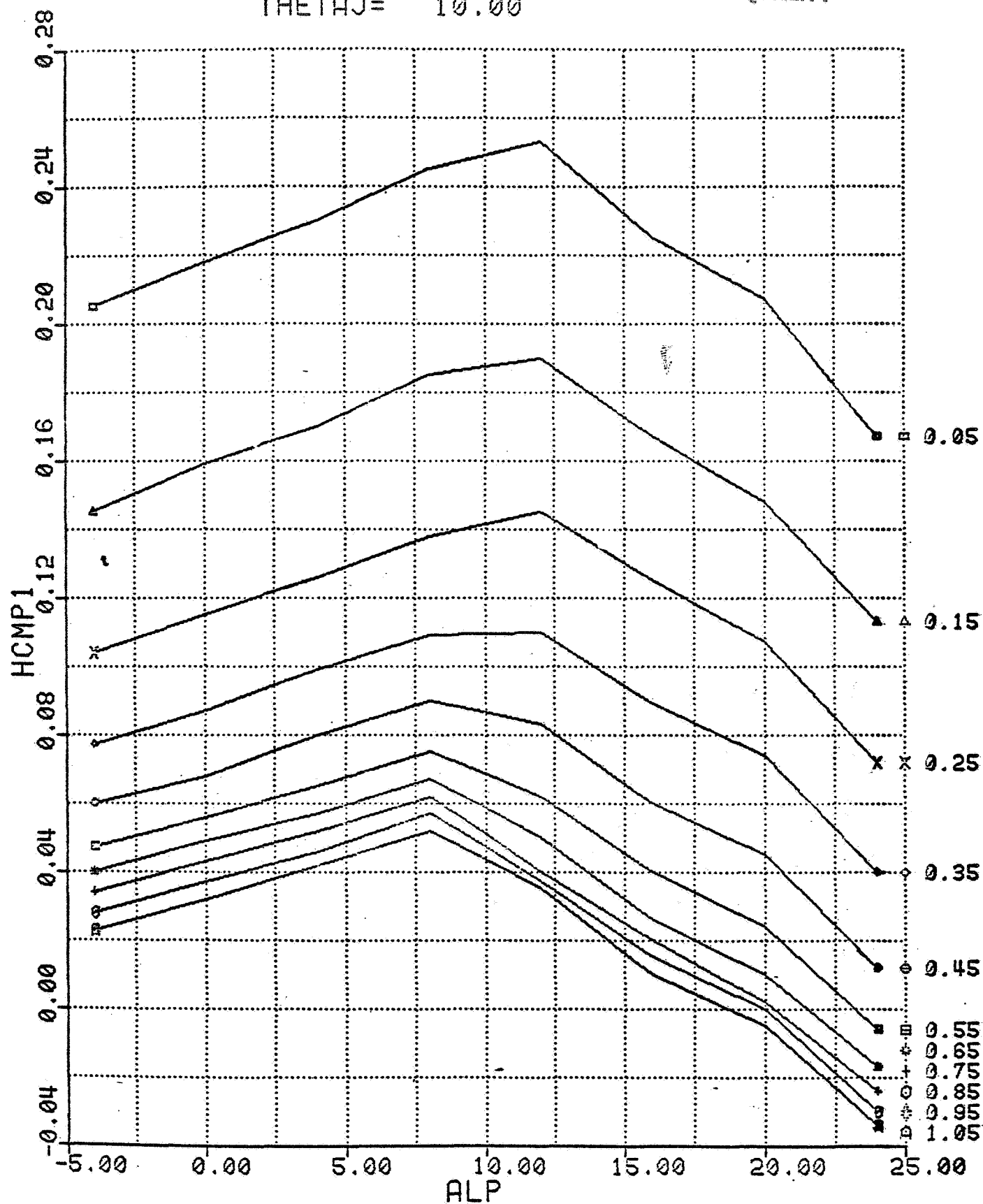
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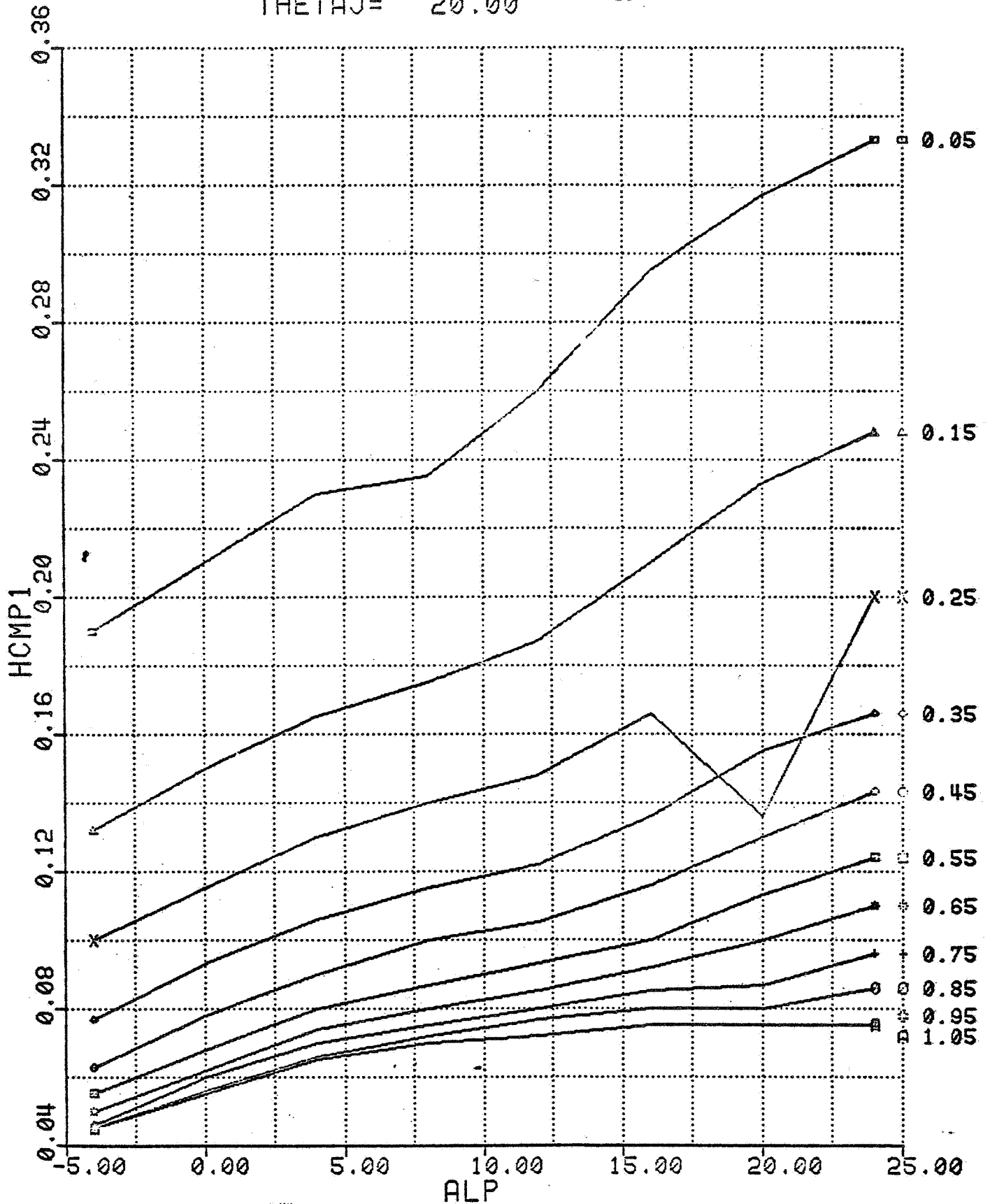
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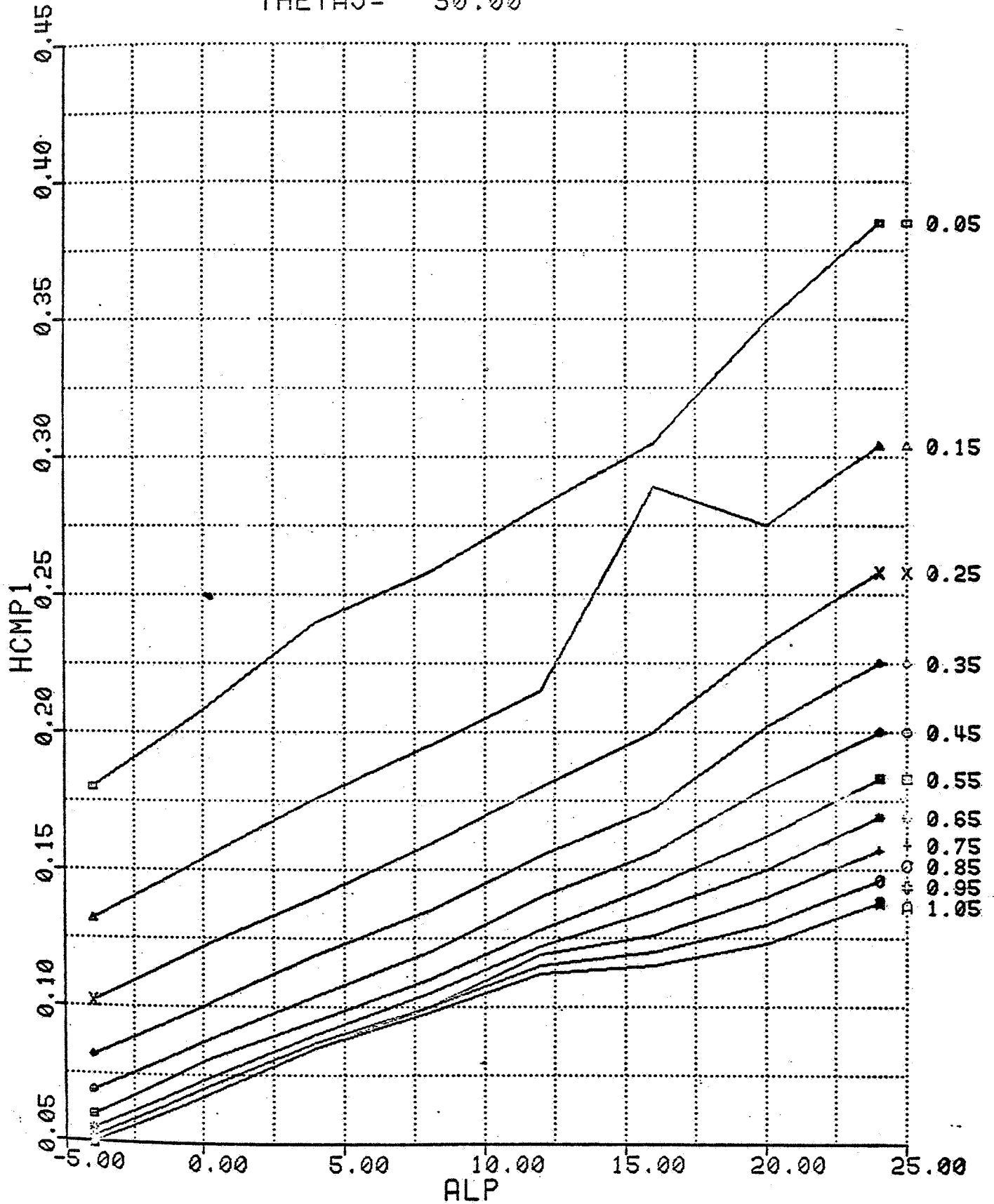
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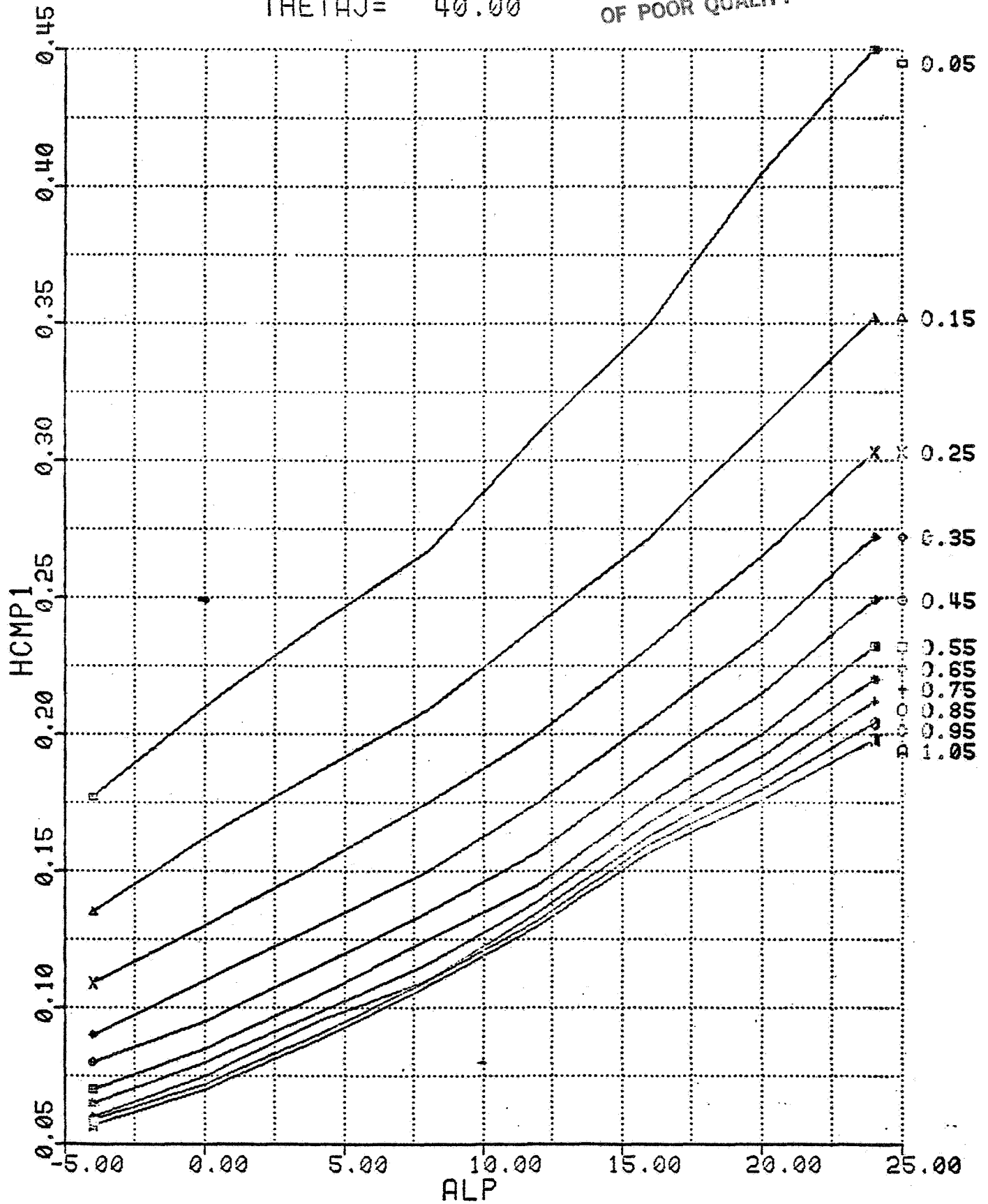
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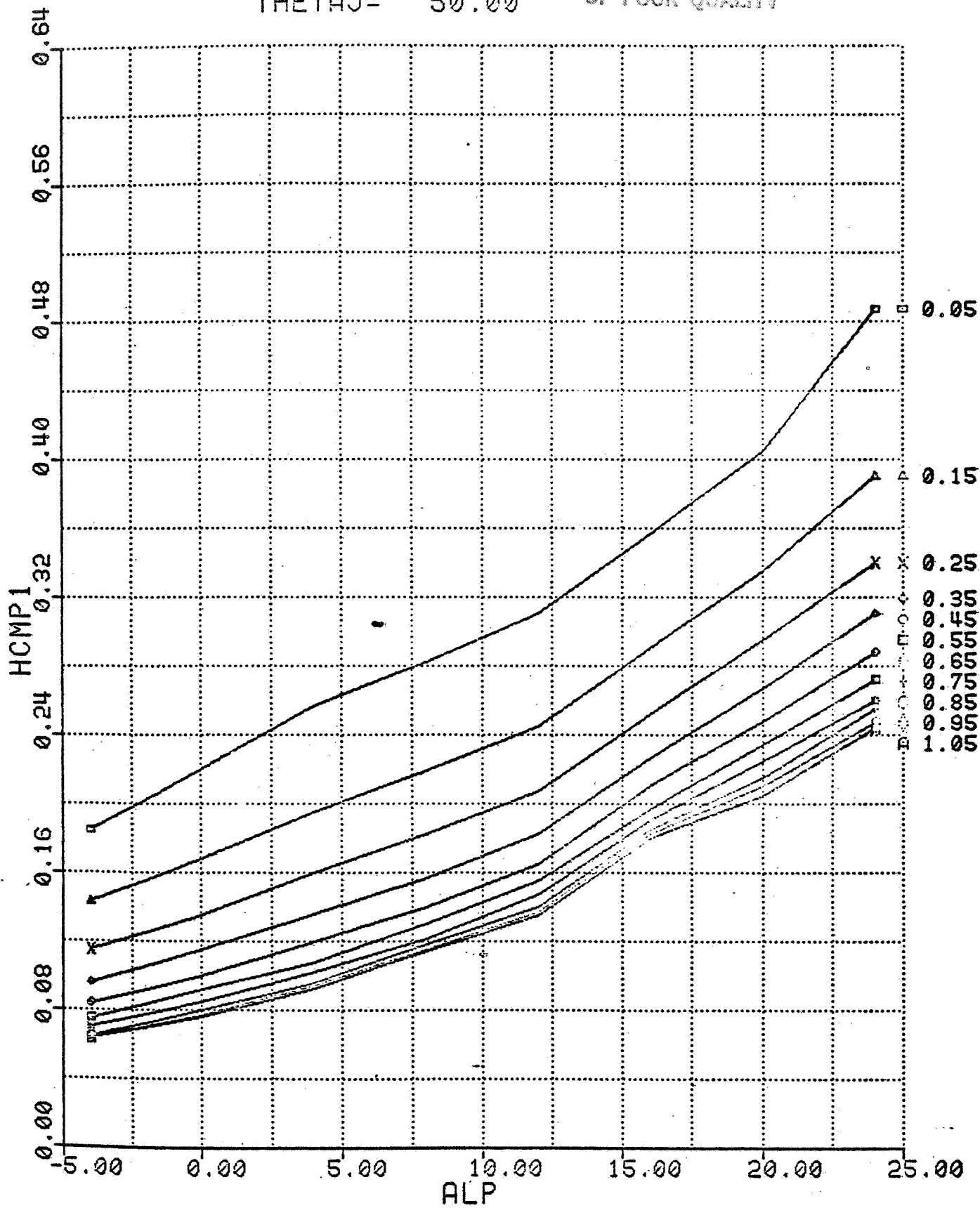
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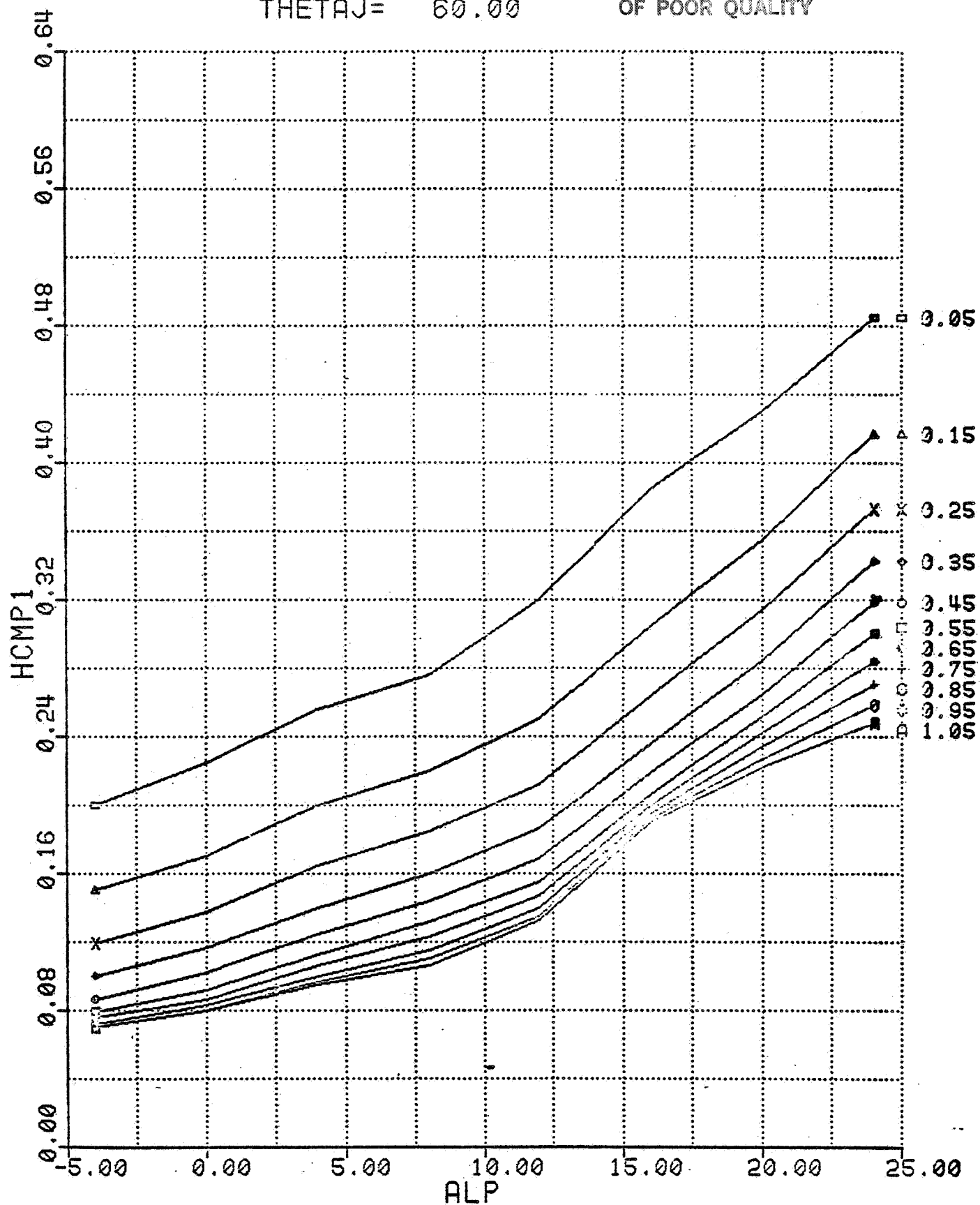
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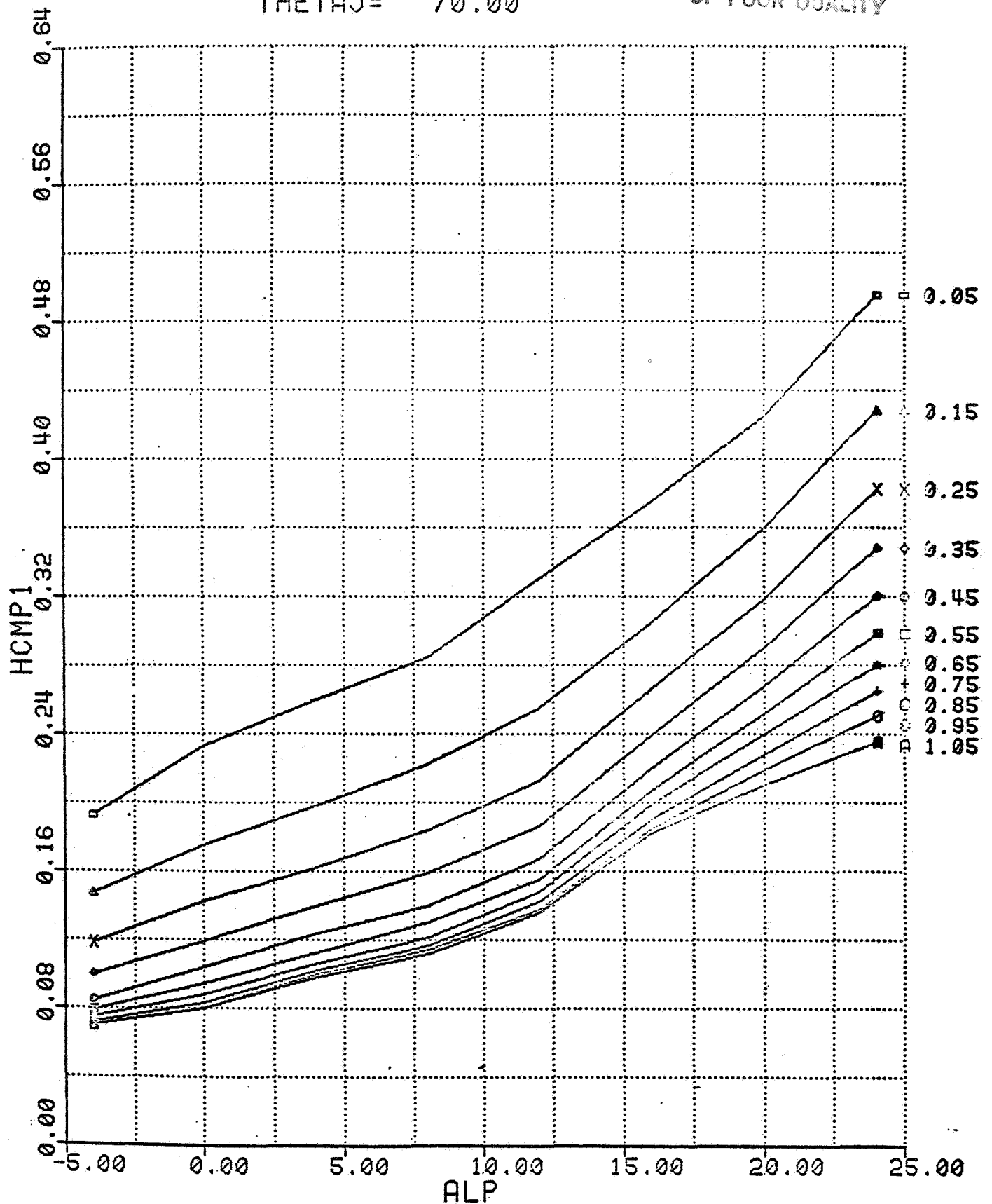
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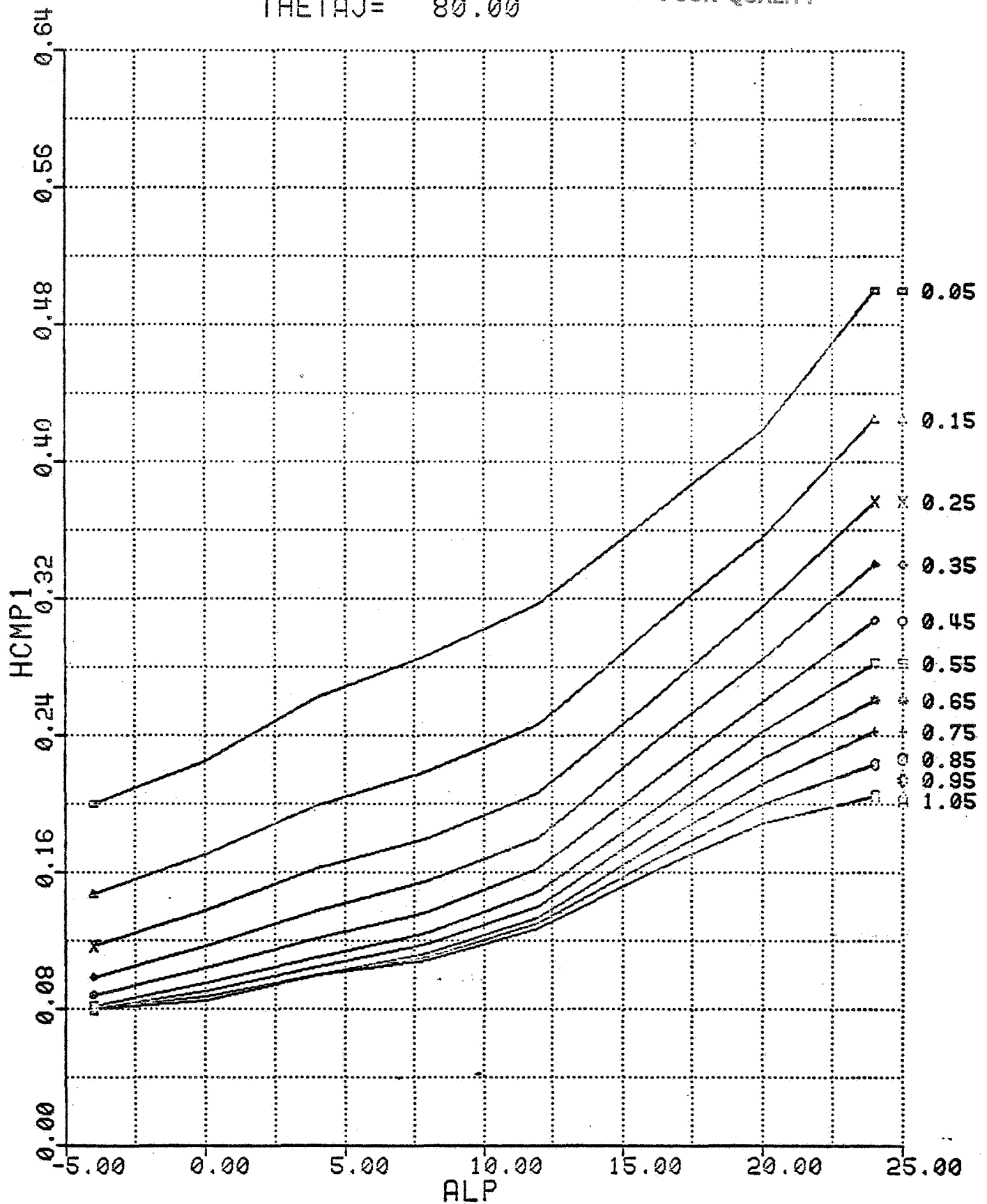
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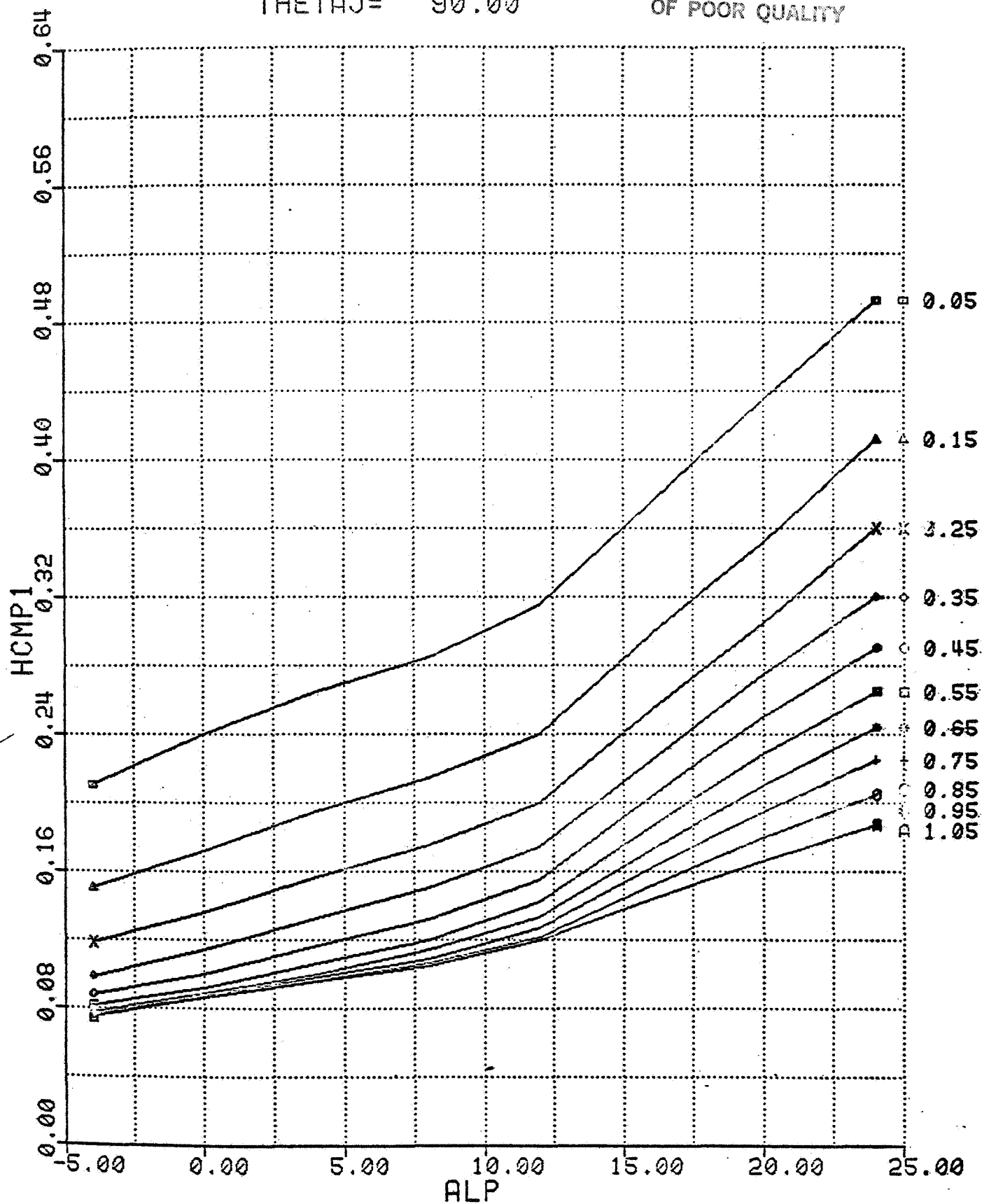
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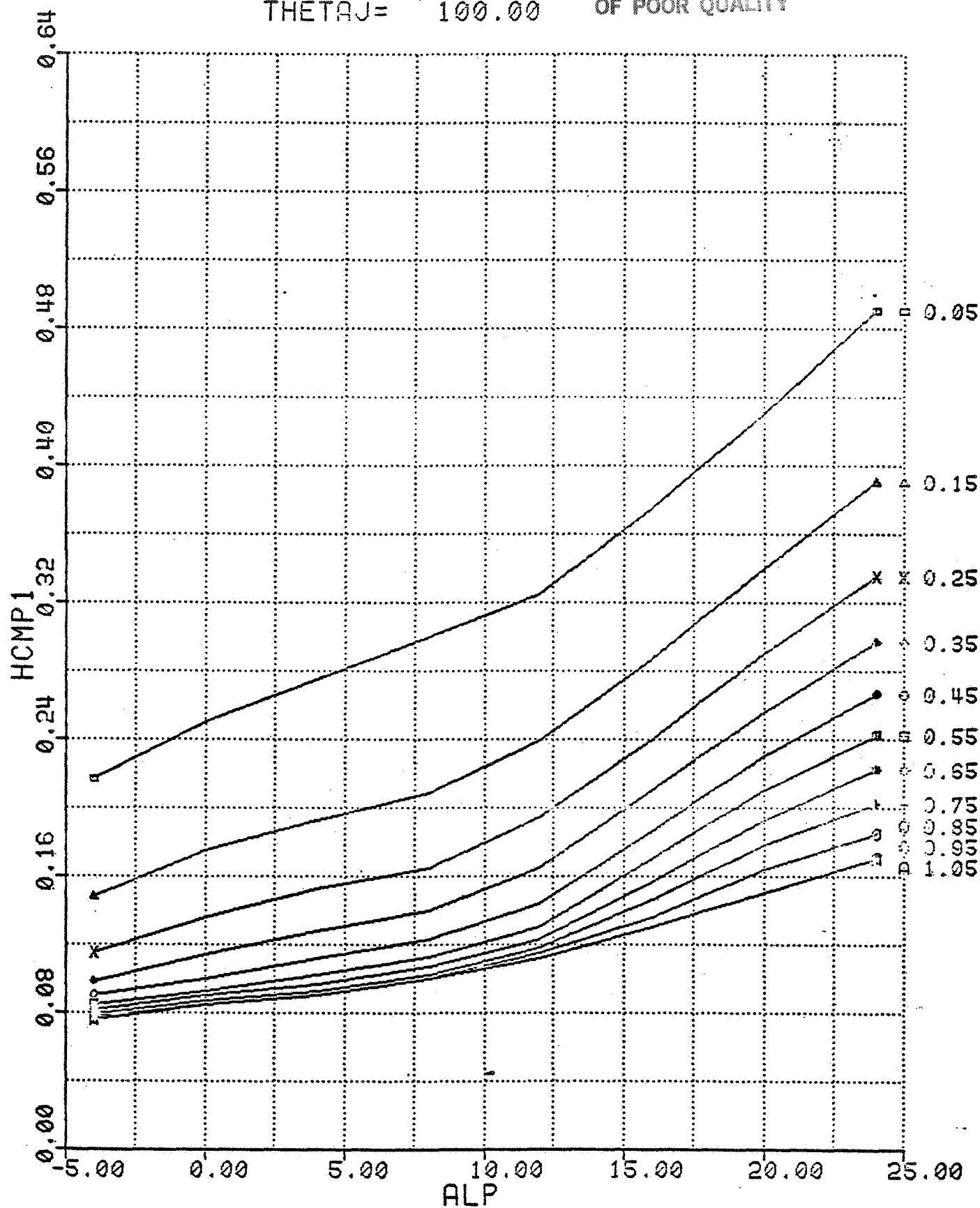
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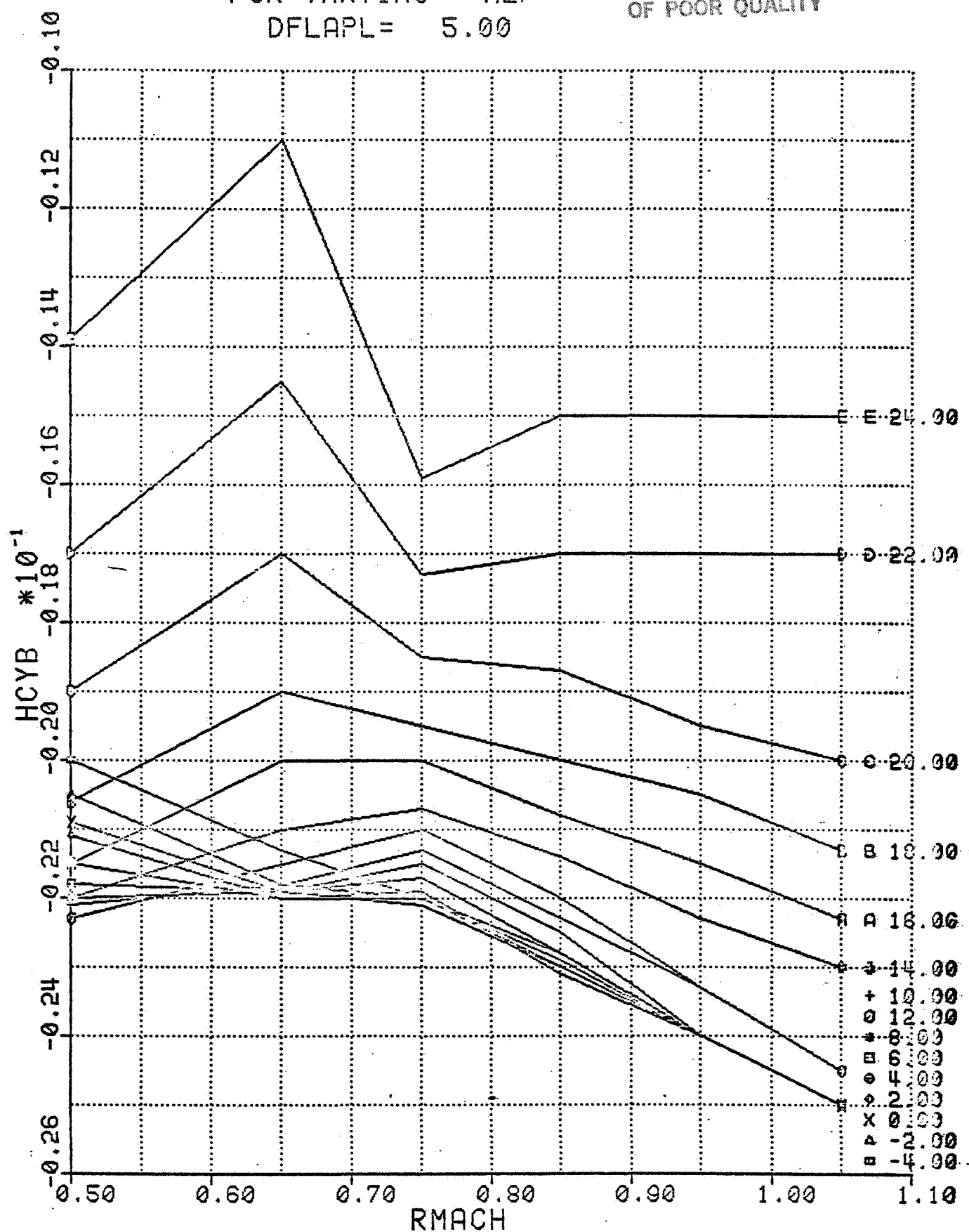
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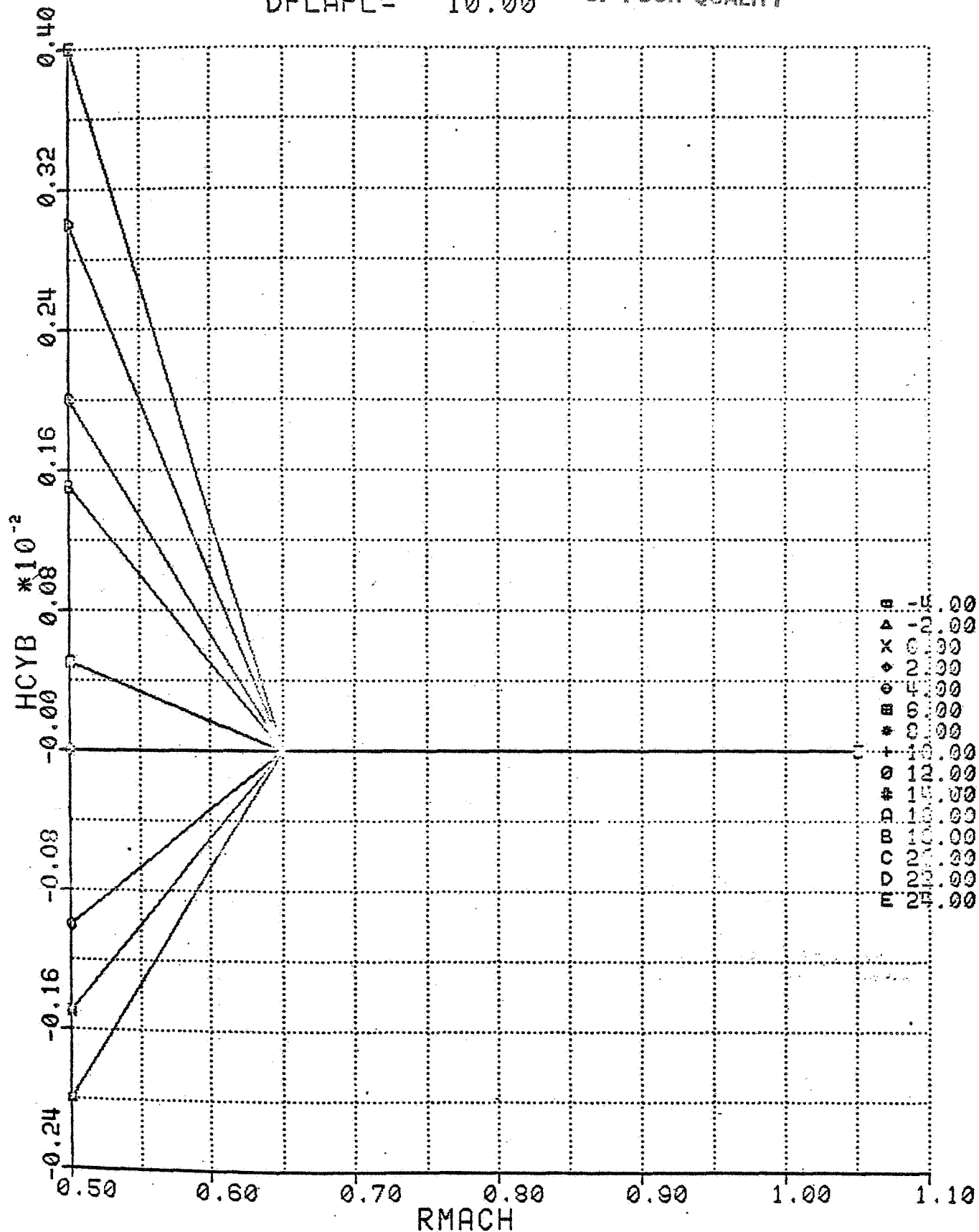


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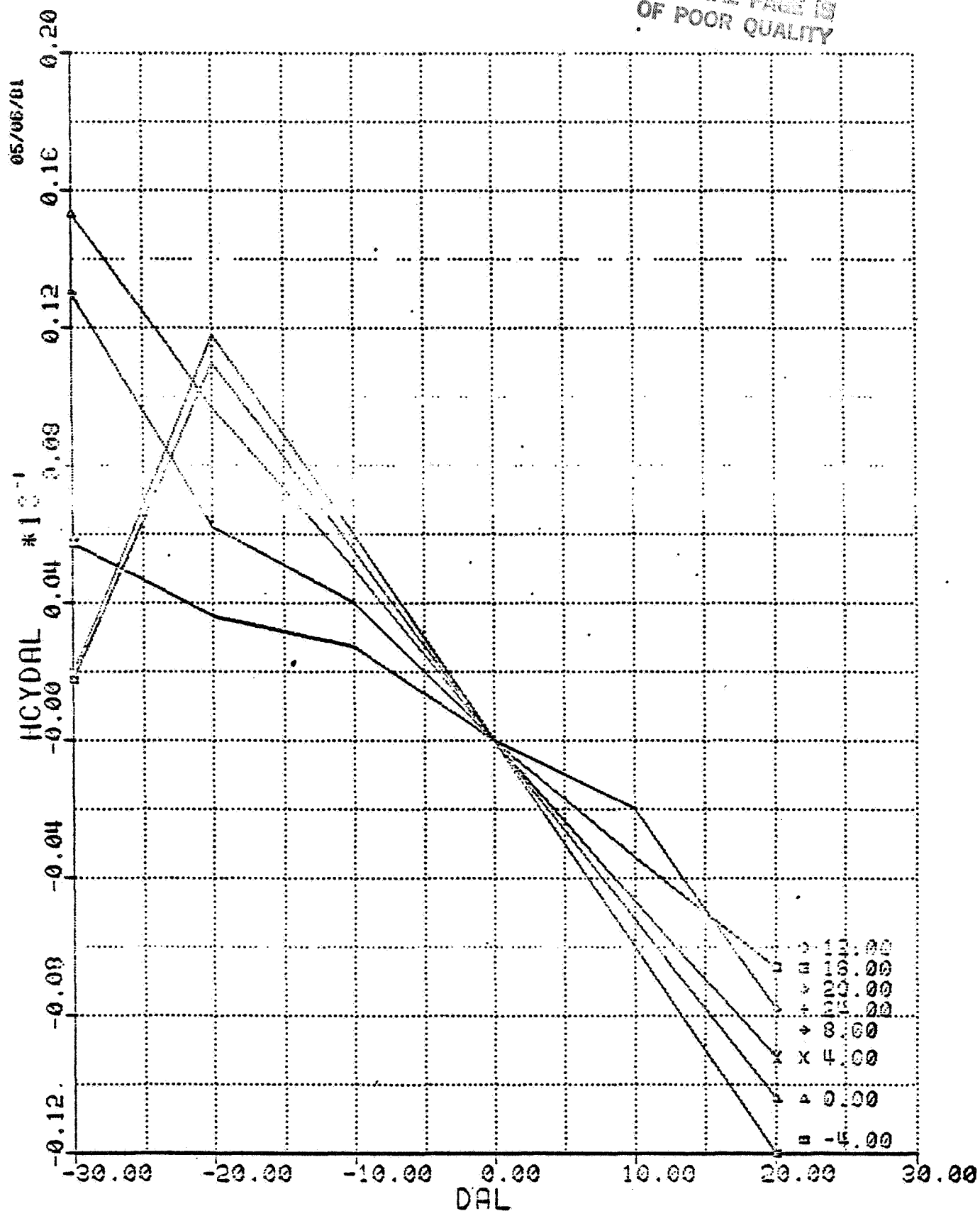


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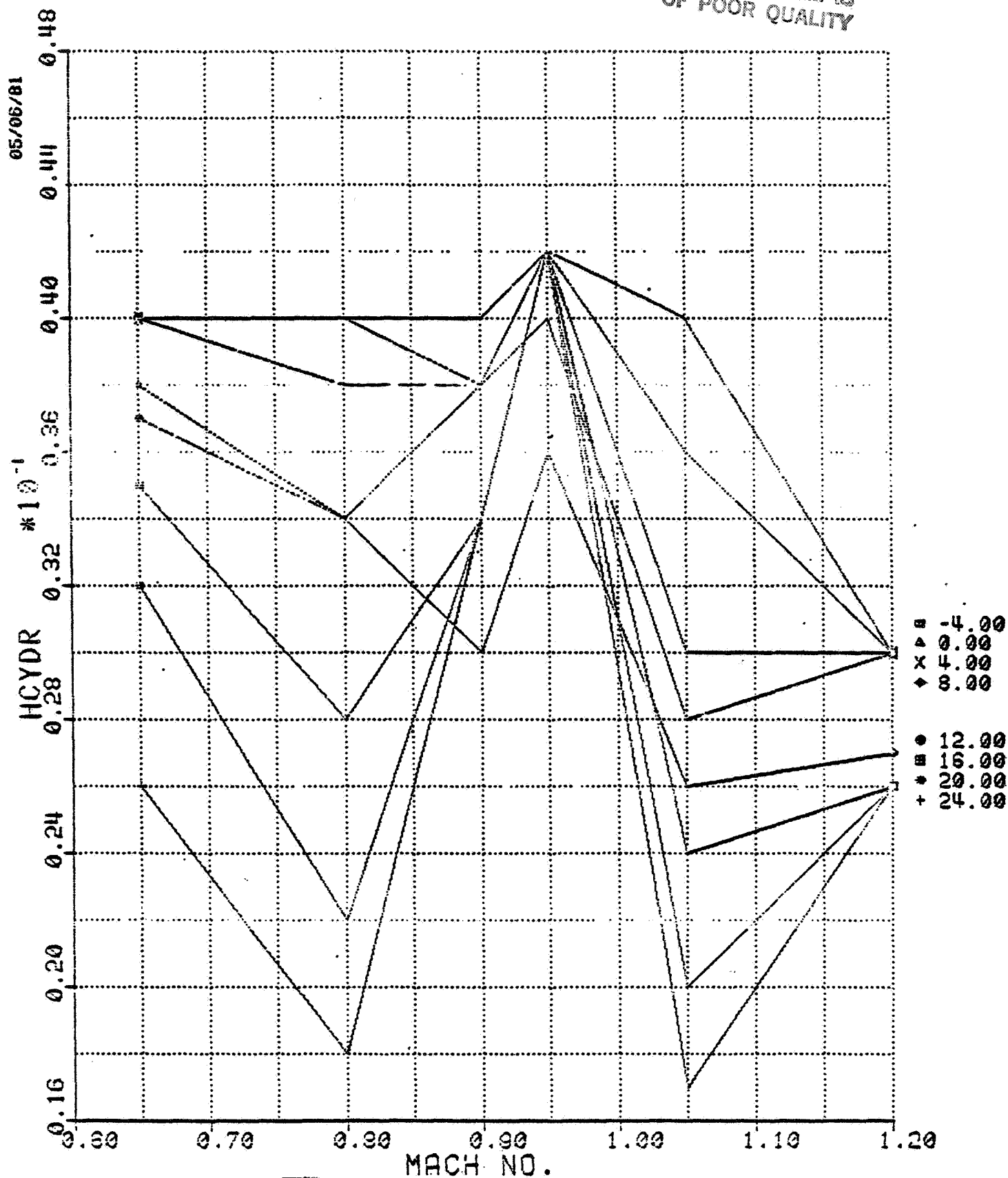
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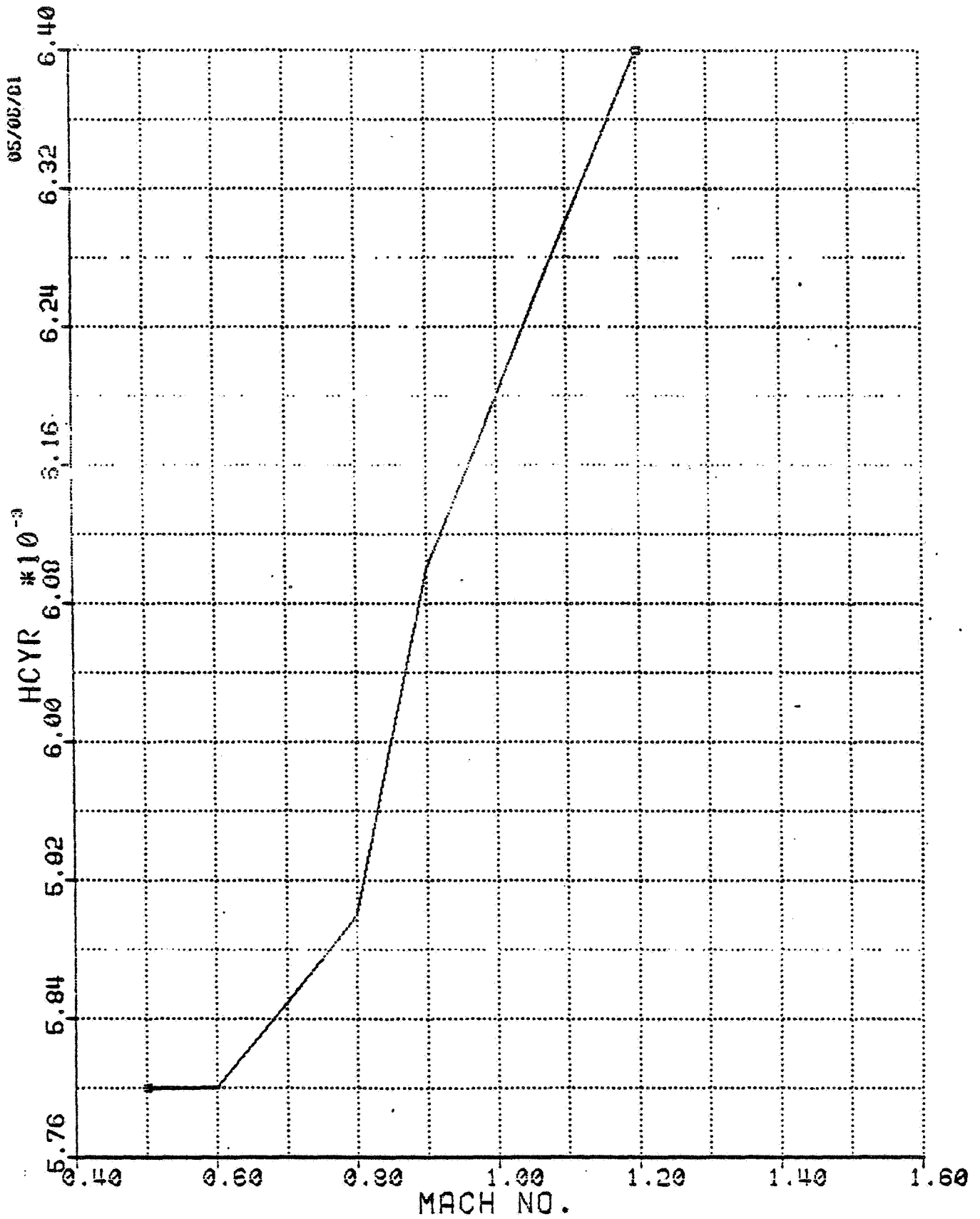


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HCYR VS MACH NO.



GLOSSARY OF TERMS

ABETAP	Absolute value of BETAP
AIL D	Aileron deflection in degrees
ALP	Angle of attack in degrees
ALPC	Corrected angle of attack in degrees used in longitudinal data
ALPHA	Angle of attack in degrees
ALPT	Tail angle of attack in degrees
ALT	Altitude in feet
BETAP	Angle of sideslip (angle in body-fixed x-y plane between the projection of the relative wind vector and the body x-axis)
DAL	Left aileron deflection in degrees
DELTT2	Ram recovery ratio
DFLAPL,DFLPL	Left flap deflection in degrees
DHTD	Stabilator deflection in degrees
FG/FGMAX	Percent maximum gross thrust
FLAP	Average flap deflection in degrees
H	Altitude in feet
HP	Height above ground (to the bottom of extended main gear with aircraft at nominal attitude $\theta = 7.5^\circ$)
MACH	Mach number
PNFRPM	Engine fan speed
PNOZPOS	Nozzle angle in degrees
PRESHPI	Atmospheric static pressure in pounds/inch ²
PSA	Power spindle angle in degrees
RWTOT	Total RCS bleed rate in pounds/sec
SUCAL	Calibrated airspeed x-component in knots
TAMB	$T_{AMB} (^{\circ}R)/518.6^{\circ}R$
TERM	Body-axis roll angle with sign of BETAP
THALP	Pitch attitude, angle of attack, or a blend of the two depending on the value of VEQ
THETAJ,THETJ	Nozzle angle in degrees
VEQ	Square root of the ratio of freestream dynamic pressure to jet dynamic pressure
VET	Bounded VEQ
YMPHIE	Lateral-directional bias term
YPHIE	Phi bias term

APPENDIX D
SIMULATION RUN
SAMPLE OUTPUT

82/11/15. 13.38.43.

D-3

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25	FMIRAN	REL	1120	2673	82/11/09.	SUBROUTINEOPT-2	
26	FMIRAN	REL	1362	5035	82/10/14.	SUBROUTINEOPT-2	
27	FMIRAN	REL	27	0715	82/10/14.		
28	MSGART	REL	24	3116	82/08/19.		
29	LOCBUF	REL	42	3743	82/08/19.		
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3

PAGE

82/11/15. 13-38-52.

COMMENTS

DATE

CRSUM

FILE
LENGTH

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CATALOG OF YLDFL
NAME

SUM =

* EDI *

REC

[illegible]

START OF RUN DATA
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IXZ
1509.6

MDC A7910
Volume II

D-9

MDC A7910
Volume II

D-10

D-11

D-12

D-13

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MDC A7910
Volume II

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D-15

D-16

D-17

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13:38:05: LP
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1. Report No. NASA CR-170397 -2		2. Government Accession No.		3. Recipient's Catalog No.	
4. Title and Subtitle YAV-8B SIMULATION AND MODELING VOLUME II: PROGRAM LISTING				5. Report Date March 1983	
				6. Performing Organization Code	
7. Author(s)				8. Performing Organization Report No. MDC A7910	
9. Performing Organization Name and Address McDonnell Douglas Corporation McDonnell Aircraft Company P.O. Box 516 St. Louis, Missouri 63166				10. Work Unit No.	
				11. Contract or Grant No. NAS4-2839	
12. Sponsoring Agency Name and Address National Aeronautics and Space Administration Washington, D.C. 20546				13. Type of Report and Period Covered Contractor Report -- Final	
				14. Sponsoring Agency Code RTOP 505-42-74	
15. Supplementary Notes NASA Technical Monitor: Donald H. Gatlin, Ames Research Center, Dryden Flight Research Facility, Edwards, CA 93523. Magnetic tapes of computer programs used in this report are available from technical monitor.					
16. Abstract This document consists of a FORTRAN batch simulation of the YAV-8B aircraft and supporting documentation. A complete description of the aircraft is included. Simulation outputs are compared with flight test data.					
17. Key Words (Suggested by Author(s)) VSTOL Simulation Harrier aircraft YAV-8B aircraft			18. Distribution Statement Unclassified-Unlimited STAR category 05		
19. Security Classif. (of this report) Unclassified		20. Security Classif. (of this page) Unclassified		21. No. of Pages	
				22. Price*	

*For sale by the National Technical Information Service, Springfield, Virginia 22161.